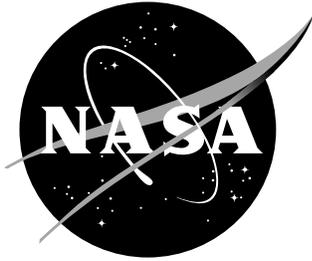


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# DSMC Simulations of Shock Interactions About Sharp Double Cones

*James N. Moss  
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August 2000

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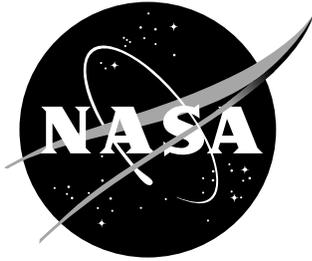
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# DSMC Simulations of Shock Interactions about Sharp Double Cones

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**Abstract.** This paper presents the results of a numerical study of shock interactions resulting from Mach 10 flow about sharp double cones. Computations are made by using the direct simulation Monte Carlo (DSMC) method of Bird. The sensitivity and characteristics of the interactions are examined by varying flow conditions, model size, and configuration. The range of conditions investigated includes those for which experiments have been or will be performed in the ONERA R5Ch low-density wind tunnel and the Calspan-University of Buffalo Research Center (CUBRC) Large Energy National Shock (LENS) tunnel.

## INTRODUCTION

Shock/shock and shock/boundary layer interactions continue to receive considerable attention because of their impact on the performance and design requirements of hypersonic vehicles. Augmented aerothermal loads and degraded control surface effectiveness are often unavoidable because of these interactions. Therefore, techniques that accurately predict these interactions and their consequences are required for vehicle design. Careful comparisons and analysis of computational and experimental results are essential in establishing confidence in the prediction tools. The current study provides numerical results for hypersonic low-density flows where the resulting database can be used for guidance and comparison with future experiments.

The current investigation focuses on Mach 10, low Reynolds number ( $Re_{\infty,d} < 45\,000$ ) flows. For the double-cone models investigated, the first cone half angle is  $25^\circ$ , while the second cone half angle is either  $55^\circ$  or  $65^\circ$ . These double cone geometries produce strong shock interactions because the attached shock from the first cone interacts with the detached bow shock from the second cone. Also, the outer shocks are modified by the separation and reattachment shocks where the extent of flow separation is significant for several combinations of model size and flow conditions. Two of the flow conditions investigated are for experiments that have been or will be performed. The calculations for the  $25^\circ/65^\circ$  model are for nominal flow conditions produced by the ONERA R5Ch wind tunnel. Calculations for a range of model diameters are made that encompass the diameter for which an experiment is scheduled. Calculations performed for the  $25^\circ/55^\circ$  model configuration include those for the model size and both actual and nominal low Reynolds number test conditions produced in the CUBRC LENS tunnel. Also, the flow about a smaller scaled model of the  $25^\circ/55^\circ$  cone is calculated for both R5Ch and LENS flow conditions. The calculations are performed by using the direct simulation Monte Carlo (DSMC) method of Bird [1]. Results presented emphasize the sensitivity of the surface quantities (heating, pressure, and skin friction) to model configuration, size, flow conditions, and grid resolution.

## RESULTS OF CALCULATIONS FOR SHARP DOUBLE CONES

Table 1 provides a summary of the free-stream and surface boundary conditions used in the current study. Information concerning model size, configuration, and locations and extent of separation are included in Table 2. Data for the extent of separation are presented in terms of two dimensions: (1) the distance measured along the x-axis of the model and (2) the wetted distance along the surface  $s$ . The selection of the grid and numerical parameters involved a series of calculations for each test condition. The grid refinement procedure was influenced by the experience of Refs. 2 and 3, which demonstrated a very sensitive dependence of separation

**TABLE 1.** Free-stream and surface<sup>a</sup> conditions.

Facility	$V_\infty$ , m/s	$\rho_\infty \times 10^4$ , kg/m <sup>3</sup>	$n_\infty \times 10^{-22}$ , m <sup>-3</sup>	$T_\infty$ , K	$p_\infty$ , N/m <sup>2</sup>	Gas	$M_\infty$	$T_W$ , K
ONERA R5Ch <sup>b</sup>	1 418.7	4.303	0.895	51.0	6.30	Air	9.91	293.0
CUBRC LENS-A <sup>c</sup>	2 713.6	6.808	1.463	194.1	39.21	N <sub>2</sub>	9.56	297.8
CUBRC LENS-B	2 657.9	7.782	1.673	198.9	45.93	N <sub>2</sub>	9.25	293.0
CUBRC LENS-C	2 713.6	8.647	1.858	194.1	49.80	N <sub>2</sub>	9.56	293.0

<sup>a</sup> Diffuse with full thermal accommodation.<sup>b</sup> Denotes nominal test conditions.<sup>c</sup> A denotes actual test conditions, B denotes nominal pretest conditions, and C denotes fictitious conditions (adjustment of density) to achieve a specific Reynolds number.**TABLE 2.** Results of DSMC calculations for sharp double cones.

Cone parameters <sup>a</sup>			Grid <sup>b</sup>	Test condition	Separation $Re_{\infty,d}$	Reattachment $x_S$ , mm	Reattachment $x_R$ , mm	$\Delta x/L_1$	$\Delta s/L_1$
Angles	$L_1$ , mm	d, mm							
25°/65°	25.0	66.4	F	R5Ch	12 360	13.86	25.95	0.484	0.700
25°/65°	25.0	66.4	I	R5Ch	12 360	13.86	25.87	0.480	0.692
25°/65°	25.0	66.4	C	R5Ch	12 360	14.34	25.45	0.444	0.631
25°/65°	25.0	66.4	VC	R5Ch	12 360	15.50	24.38	0.355	0.479
25°/65°	30.1	80.0	C	R5Ch	14 880	16.72	31.14	0.478	0.691
25°/65°	40.0	106.3	C	R5Ch	19 775	20.80	42.33	0.538	0.786
25°/65°	45.5	121.0	C	R5Ch	22 500	21.41	50.63	0.642	0.969
25°/65° <sup>c</sup>	50.0	132.9	I	R5Ch	24 719	21.31	59.43	1.109	1.198
25°/55°	25.8	66.4	I	R5Ch	12 360	21.17	25.36	0.162	0.229
25°/55°	25.8	66.4	I	LENS-A	9 730	21.75	24.61	0.111	0.154
25°/55°	25.8	66.4	I	LENS-C	12 360	21.45	24.74	0.127	0.179
25°/55° <sup>d</sup>	101.6	261.8	I	LENS-A	38 340	80.02	99.87	0.196	0.265
25°/55°	101.6	261.8	I	LENS-B	42 150	80.01	100.10	0.198	0.269
25°/55°	101.6	261.8	C	LENS-B	42 150	80.60	99.17	0.182	0.246
25°/55°	101.6	261.8	VC	LENS-B	42 150	84.00	97.81	0.136	0.186

<sup>a</sup>  $L_1$  is wetted length of first cone and d is maximum diameter.<sup>b</sup> Qualitative description of grid resolution: F-fine, I-intermediate, C-coarse, and VC-very coarse.<sup>c</sup> From Ref. 3.<sup>d</sup> Only case for which experimental measurements have been made—data to be released later.

extent to grid refinement. The Reynolds number is based on free-stream conditions with a characteristic length  $d$ , the maximum diameter of the model. For the R5Ch flow conditions, the Sutherland viscosity has been used in defining the Reynolds number to be consistent with experimentally reported values. For the LENS conditions, the variable hard sphere model for viscosity (temperature exponent of 0.75 and a reference temperature of 300 K) is used in specifying Reynolds number.

## 25°/65° Cones at Mach 9.9 Air Flow—R5Ch Conditions

Calculations presented in this section are an extension of those reported in Refs. 2 and 3, where the flow about a sharp double-cone model (25°/65°) with a maximum diameter of 132.893 mm was calculated with both DSMC and Navier Stokes codes for Reynolds numbers ranging from 24 719 to 247. This Reynolds number range was achieved by using the R5Ch nominal free-stream flow conditions (highest Reynolds number) and then parametrically reducing the free-stream density. The current results are those for smaller scale models with diameters between 66.4 and 121.0 mm. The maximum diameter of the current model configuration that can be tested in the R5Ch wind tunnel is near 70 mm, or about half of the model size used in the previous studies. The configuration is such that the length of the first and second cones are equal ( $L_1 = L_2$ , Fig. 1a).

Figures 1 and 2 present representative results of the calculations. The nature of the shock interactions is demonstrated in Fig. 1a by using the fine grid results for the 66.4-mm-diameter model, a model size that the ONERA R5Ch wind tunnel should be able to accommodate. Selected Mach contours are shown where a large subsonic region, indicated by the darker shading, is located in front of the second cone. Locations for

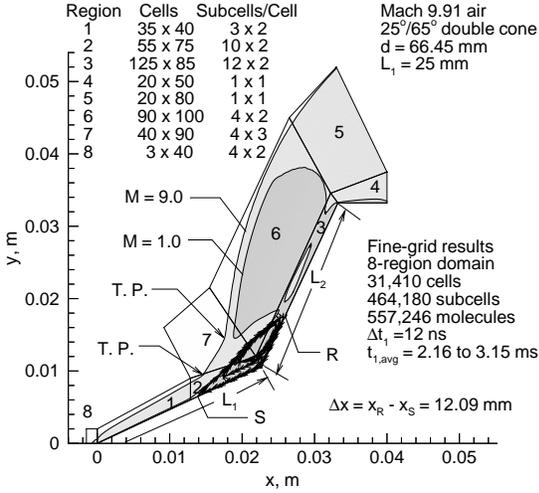


Fig. 1a. Flow structure.

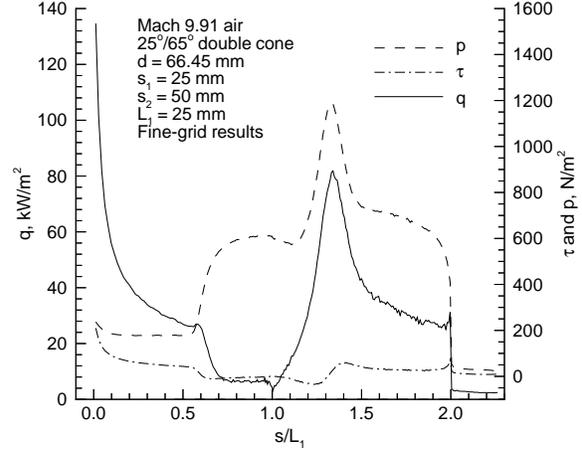


Fig. 1b. Surface results.

FIGURE 1. Fine-grid results for 25°/65° double cone at R5Ch flow conditions; d = 66.45 mm.

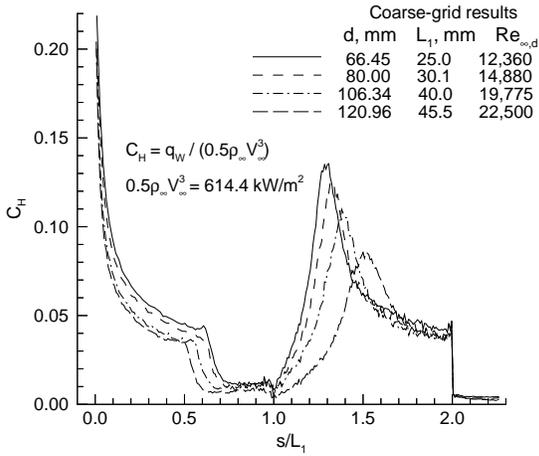


Fig. 2a. Heat-transfer coefficient.

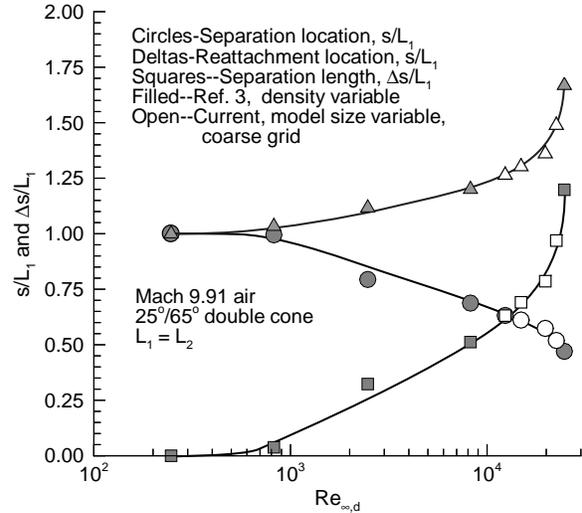


Fig. 2b. Separation data.

FIGURE 2. 25°/65° double-cone results at R5Ch flow conditions.

flow separation and reattachment along the surface are denoted by S and R, respectively. Also evident is the influence of the separation shock on the oblique shock that is produced by the first cone, resulting in a triple point (T. P.) followed by a stronger transmitted shock that interacts with the stronger bow shock of the second cone—creating a second triple point. These shock/shock and shock/boundary layer interactions are induced by the larger cone and produce a significant separation region characterized by a single vortex embedded within the subsonic region near the intersecting cones. The general flow structure evident for the 66.45-mm-diameter model is that found for the larger 25°/65° models. However, when the model diameter is increased to 132.9 mm (results from Ref. 3 and included in Table 2), secondary vortices were evident, and a Navier-Stokes computation indicated some unsteadiness (small oscillations of separation location). Undoubtedly, the flow would become

unsteady for larger models, as is demonstrated by the rapid growth of the extent of separation presented in Fig. 2.

Also included in Fig. 1a is information concerning the computational domain, which consisted of eight arbitrary regions. Each region is subdivided into cells, and the cells in selected regions are subdivided into subcells to enhance the spatial resolution used to select collision partners. Time step information for region one and the time interval for which the time-averaged results were obtained are included in Fig. 1a. Since the computational regions were not run with necessarily the same time step, it was essential that steady state conditions be established before generating the final time-averaged results. Steady state was assumed to occur when the total molecules used in the simulation, average molecules in each region, and locations and size of the separation region became constant when sampled over some significant time interval.

Figure 1b presents the corresponding surface results—heating rate, pressure, and skin friction—for the 66.45-mm-diameter model. Results are for the fine-grid solution, the only condition for which the surface results and extent of separation indicate grid independence (Table 2)—fine and intermediate grid results are the same for surface quantities. (Additional grid refinement is necessary to determine if the remaining intermediate grid results are grid independent.) The qualitative features are consistent with experimental measurements [4] for laminar separated flows. First, the separation position is in close agreement with the location of the first inflection point (maximum slope) of the initial pressure rise and the location where the heat transfer rate decreases significantly with respect to the single cone results. Second, the pressure reaches a plateau for a significantly large separation region, while the heat transfer is significantly reduced. Third, at or preceding the intersection of the two cones, the heat transfer experiences a minimum and then increases rapidly, as does the pressure, with increasing distance along the second cone.

Figure 2 presents results that highlight the effect of model size or Reynolds number on the calculation where the data presented are for coarse grids (comparable grid resolution for the four cases). Heat transfer coefficient results for the four model sizes investigated (Fig. 2a) show the expected trend of decreasing magnitude with increasing Reynolds number. Also, as expected for laminar flow, the extent of separation increases (earlier separation and delayed reattachment), as can be inferred from Fig. 2a, and is explicitly shown by the nondimensional separation data included in Table 2.

The sensitivity of the extent of separation to Reynolds number is presented in Fig. 2b, where the current data (coarse grid results) are those obtained by varying the model size. The data from Ref. 3 were obtained by varying the free-stream conditions (density) for a fixed model size ( $d = 132.89$  mm). The two data sets show a consistent trend: the extent of separation increasing with Reynolds number and a very rapid increase in separation near a Reynolds number of 25 000. For the conditions investigated, the calculations show that separation persists for Reynolds numbers as low as about 800.

## 25°/55° Cone With a Diameter of 66.45 mm—R5Ch and LENS Conditions

To clarify the effect of different experimental test conditions on surface and flow-field features, a common model is used for making calculations at both ONERA R5Ch and LENS nominal test conditions. The model configuration is one that has been used in the CUBRC tests, but the maximum model diameter is 66.45 mm rather than the 261.8-mm-diameter model tested. Figure 3 presents information concerning flow-field features and computational parameters, while Fig. 4 provides information concerning surface results for heating and pressure. Table 2 provides information concerning the location and extent of separation.

A 10° reduction in the second cone half angle has a very pronounced impact on the flow-field features for the R5Ch nominal test conditions, as is clearly evident when the results of Fig. 3a are compared with those of Fig. 1a. Marked differences are evident for the nature of the shock/shock and shock/boundary layer interactions, size and location of the subsonic region, and size of the separation zone. When the calculation is made for the LENS-A test conditions (Fig. 3b), the shock layer disturbance is slightly smaller, and the size of the subsonic region and the extent of separation are noticeably reduced when compared with the results for the R5Ch flow conditions. The corresponding surface results for heating and pressure coefficients are included in Fig. 4. Data are also included for a flow condition referred to as LENS-C, where an adjustment to the density of the LENS-A nominal test condition is made to produce a larger free-stream Reynolds number, a value equal to that of the R5Ch test condition. The nondimensional heating and pressure results presented in Fig. 4 show to what extent the distributions are consistent—very good agreement for pressure with the exception of the strong interaction region, while that for heating is more qualitative. For the surface region where separation occurs, the heating and pressure coefficient values are much larger for the LENS test conditions than those for

the R5Ch conditions. Of course, the dimensional heating and pressure values are much larger for the LENS conditions, about an order of magnitude difference in heating rates. The effect of increasing the free-stream density of the LENS-A condition, to produce the LENS-C conditions (same Reynolds number as the R5Ch case), is clearly evident in the  $C_H$  distributions and extent of separation (Table 2) but has a minor effect on the  $C_p'$  distribution. However, the present results for the surface coefficients (friction not shown) indicate that the Reynolds number is not the only controlling parameter.

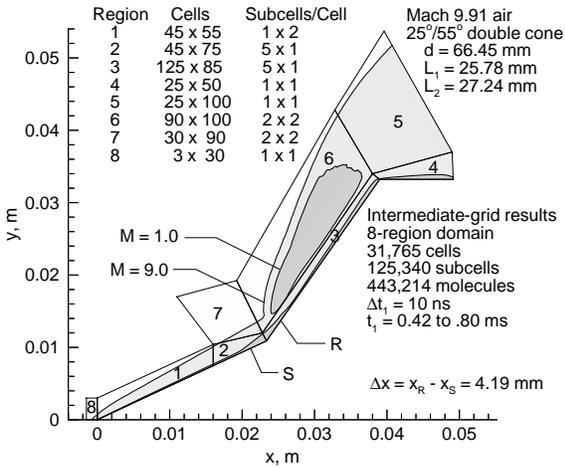


Fig. 3a. R5Ch conditions.

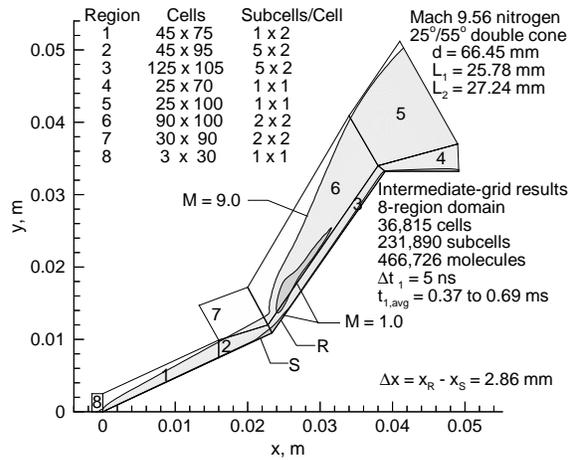


Fig. 3b. LENS-A conditions.

FIGURE 3. Flow structure for 25°/55° double cone; d = 66.45 mm.

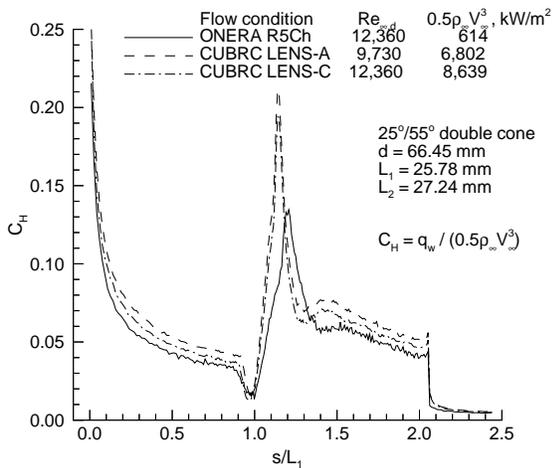


Fig. 4a. Heat-transfer coefficient.

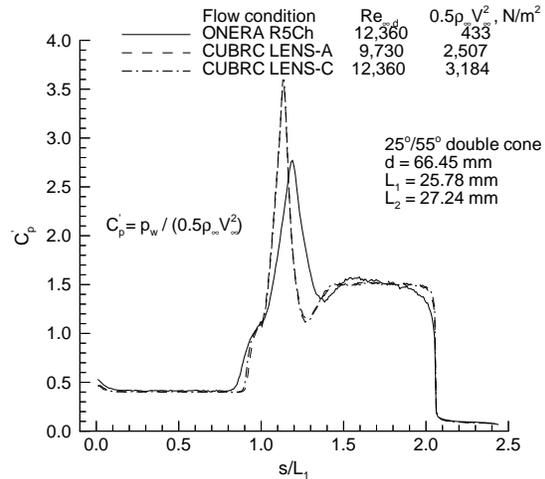


Fig. 4b. Pressure coefficient.

FIGURE 4. Surface results as a function of test conditions for 25°/55° double cone; d = 66.45 mm.

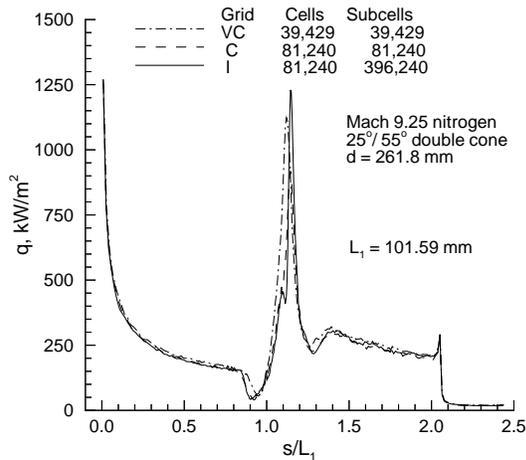


Fig. 5a. Heating-rate distributions.

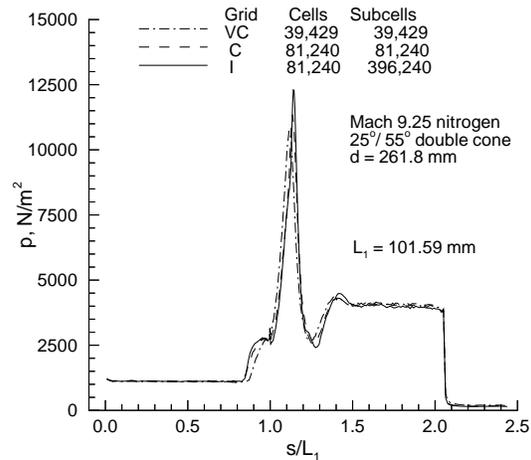


Fig. 5b. Pressure distributions.

**FIGURE 5.** Effect of grid on surface results for 25°/55° double cone; d = 261.8 mm and LENS-B flow conditions.

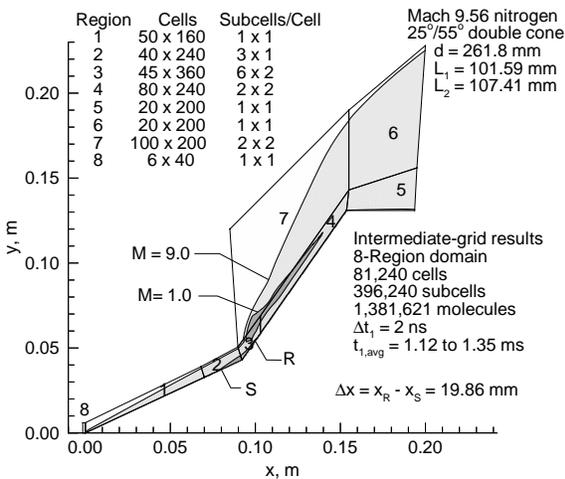


Fig. 6a. Flow structure.

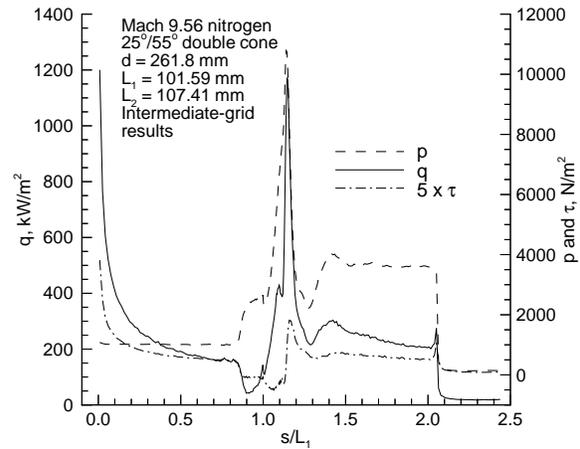


Fig. 6b. Surface quantities.

**FIGURE 6.** Intermediate-grid results for 25°/55° double cone; d = 261.8 mm and LENS-A flow conditions.

## 25°/55° Cone at Mach 9.6 Nitrogen Flow— LENS Conditions

This section focuses on results for the CUBRC LENS flow conditions where the maximum model diameter is 261.8 mm. The initial calculations were made for pretest nominal conditions—denoted as LENS-B test condition. A grid sensitivity study was conducted, and the results of this study, as it impacts separation and reattachment locations, are listed in Table 2. The sensitivity on heating and pressure distributions is presented in Fig. 5. The finest grid used in this exercise (described as intermediate I, since grid independence was not demonstrated) was then used to make a calculation for the actual test condition (LENS-A), and selected results are presented in Fig. 6. The general features of the shock layer structure are given in Fig. 6a where selected Mach contours are included, along with details of the numerical parameters used in the simulation. The impact

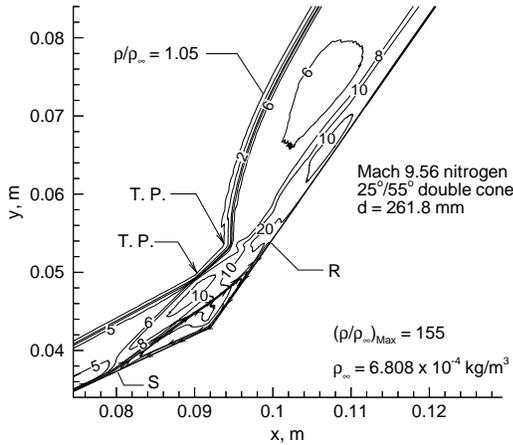


Fig. 7a. Density contours.

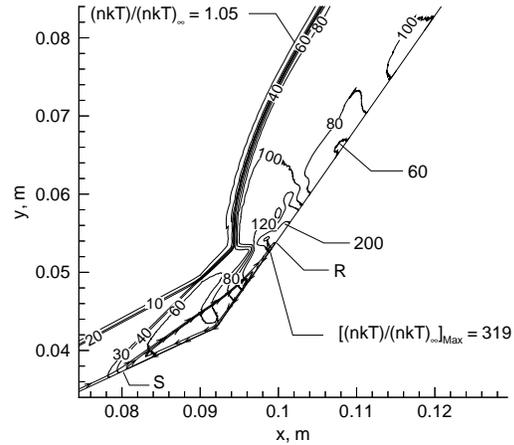


Fig. 7b. Scalar pressure contours.

**FIGURE 7.** Interaction region results for 25°/55° double cone;  $d = 261.8$  mm and LENS-A flow conditions.

of model size and flow conditions on shock layer features can be observed by comparing these results with those given in Fig. 3. Values for the surface quantities are shown in Fig. 6b. For the surface pressure distribution, the calculated values outside the region influenced by the shock/boundary layer interactions are in close agreement with the inviscid cone values (Ref. 5) of  $948 \text{ N/m}^2$  along the 25° cone and  $3710 \text{ N/m}^2$  along the 55° cone. Opportunities will exist for comparison with the experimental measurements that have been completed when the CUBRC data are released.

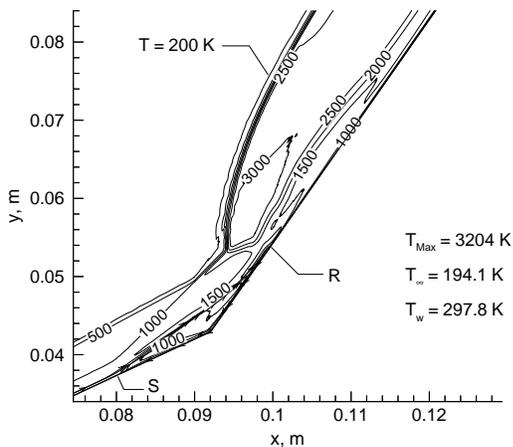


Fig. 8a. Overall kinetic temperature contours.

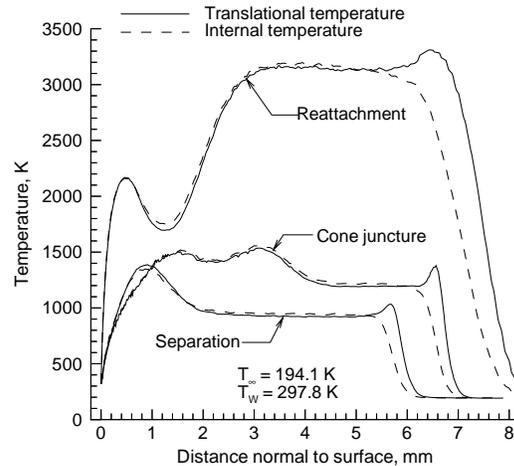


Fig. 8b. Temperature profiles.

**FIGURE 8.** Interaction region results for 25°/55° double cone;  $d = 261.8$  mm and LENS-A flow conditions.

Figures 7 and 8 present details concerning the flow-field structure for the CUBRC test case where the focus is on the interaction region. From the density and scalar pressure contours presented in Figs 7a and 7b, respectively, one gets an appreciation of the compression and large gradients that occur near reattachment—

maximum values for density equal 155 times free-stream and maximum scalar pressure (displaced a substantial distance from the surface) equal 319 times free stream. The overall kinetic temperature, denoted by  $T$  in Fig. 8a, experiences a maximum value of about 1000 K along most of the first cone, but values as large as 3200 K occur along the second cone. (For comparison, the corresponding maximum values for the calculation presented in Fig. 1 are 30, 190, and 974 K, respectively.) More details concerning the thermal structure of the flow are presented in Fig. 8b, where translational and internal temperature (rotational and vibrational contributions, see Ref. 1) profiles are shown. These temperature profiles are approximately normal to the surface, and results are included for three surface locations: separation, cone juncture (normal to the  $25^\circ$  cone), and reattachment. The current results show that the nonequilibrium effects are confined primarily to the outer bow shock crossings with close agreement between translational and internal temperatures for the remainder of the shock layer. Evident from the flow structure results are the existences of two triple points, a region of separated flow with a single vortex, two subsonic regions along the second cone that sandwich a supersonic region, and a flow that for the most part is in thermal equilibrium. Reattachment occurs subsonically.

## CONCLUDING REMARKS

Results of a computational study are presented for Mach 10 flow about sharp double cones where the combination of model configurations, size, and flow conditions produce a significant range of shock/shock and shock/boundary layer interactions. The computations are made with the direct simulation Monte Carlo (DSMC) method, hence, low Reynolds number flows. The results presented provide insight into the nature of the shock interactions, their impact on surface quantities, and the sensitivity of the results to computational parameters for flow conditions that can be produced in current ground-based facilities. Extent of separation as a function of free-stream Reynolds number is demonstrated, and the current results are shown to be consistent with previous calculations. Computations are made for a common model size and configuration at conditions that can be produced in a hypersonic cold flow wind tunnel and a much higher enthalpy impulse facility—contrasting computational results for substantially different flow conditions. Opportunities should exist for comparing the current results with experimental measurements for surface heating and pressure distributions.

## ACKNOWLEDGMENTS

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13. ABSTRACT (Maximum 200 words) This paper presents the results of a numerical study of shock interactions resulting from Mach 10 flow about sharp double cones. Computations are made by using the direct simulation Monte Carlo (DSMC) method of Bird. The sensitivity and characteristics of the interactions are examined by varying flow conditions, model size, and configuration. The range of conditions investigated includes those for which experiments have been or will be performed in the ONERA R5Ch low-density wind tunnel and the Calspan-University of Buffalo Research Center (CUBRC) Large Energy National Shock (LENS) tunnel.				
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