## Appendix D

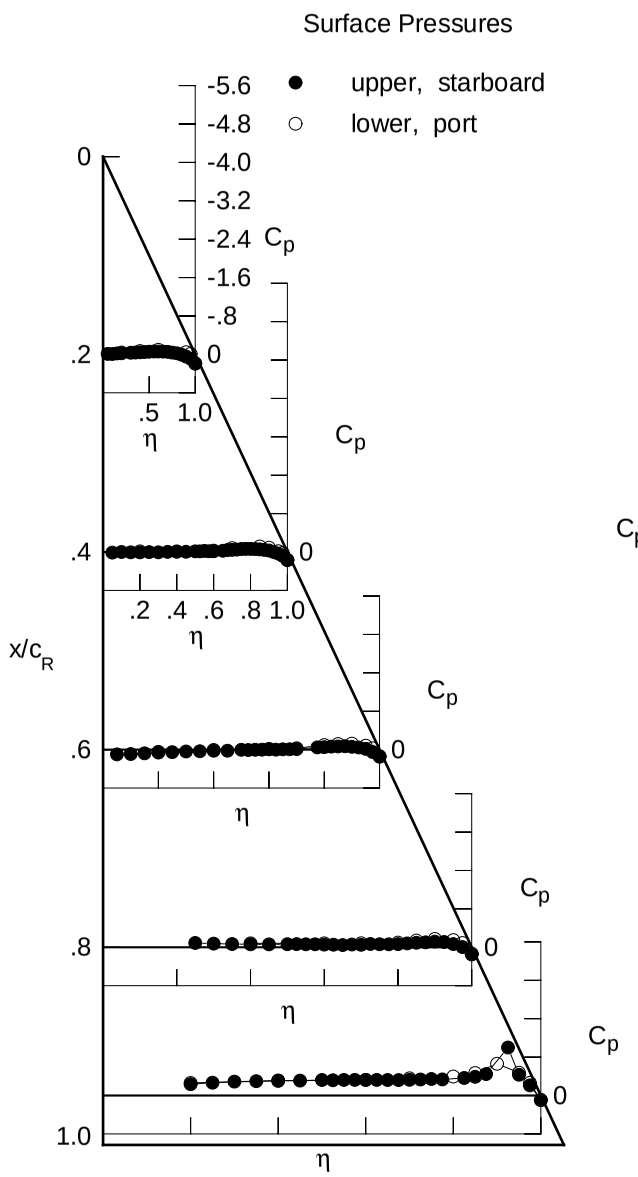
## Experimental Surface Pressure Data for 65° Delta Wing, $R_{mac} = 6 \times 10^6$

The experimental surface pressure data for the 65° delta wing at constant $R_{mac} = 6 \times 10^6$ are summarized in tables D1–D6. Because of the extensive data contained in these tables, they have not been included in the printed copy of the paper but are available electronically from the Langley Technical Report Server (LTRS). Open the files with the following Uniform Resource Locator (URL):

ftp://techreports.larc.nasa.gov/pub/techreports/larc/95/NASA-95-tm4645vol2appD.ps.Z

# Table D1. Tabulations and Plots of Surface Pressure Coefficients.

| | $x/c_R$ .2 | $x/c_R$ .4 | $x/c_R$ .6 | $x/c_R$ .8 | $x/c_R$ .95 |
|---|---|---|---|---|---|
| $\eta$ | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ |
| 0.050 | -0.0105 | 0.0117 | 0.0987 | ******* | ******* |
| 0.100 | -0.0081 | -0.0008 | 0.0911 | ******* | ******* |
| 0.150 | -0.0198 | 0.0055 | 0.0770 | ******* | ******* |
| 0.200 | -0.0229 | 0.0065 | 0.0608 | ******* | -0.2359 |
| 0.250 | ******* | 0.0020 | 0.0529 | -0.0901 | -0.2675 |
| 0.300 | -0.0347 | 0.0054 | 0.0387 | -0.0763 | -0.2893 |
| 0.350 | -0.0381 | -0.0028 | 0.0333 | -0.0679 | -0.2987 |
| 0.400 | -0.0432 | -0.0073 | 0.0222 | -0.0628 | -0.3140 |
| 0.450 | -0.0499 | -0.0054 | 0.0221 | -0.0610 | -0.3104 |
| 0.500 | -0.0557 | -0.0146 | 0.0030 | -0.0637 | -0.3230 |
| 0.525 | ******* | -0.0141 | 0.0077 | -0.0665 | -0.3177 |
| 0.550 | -0.0605 | -0.0232 | 0.0020 | -0.0624 | -0.3248 |
| 0.575 | ******* | -0.0161 | 0.0011 | -0.0625 | -0.3257 |
| 0.600 | -0.0596 | -0.0170 | -0.0064 | -0.0557 | -0.3239 |
| 0.625 | ******* | ******* | 0.0004 | -0.0534 | -0.3246 |
| 0.650 | -0.0584 | -0.0260 | -0.0067 | -0.0466 | -0.3231 |
| 0.675 | ******* | -0.0413 | -0.0071 | -0.0578 | -0.3219 |
| 0.700 | -0.0539 | -0.0452 | -0.0120 | -0.0520 | -0.3276 |
| 0.725 | ******* | -0.0504 | ******* | -0.0684 | -0.3338 |
| 0.750 | -0.0373 | -0.0634 | ******* | -0.0636 | -0.3439 |
| 0.775 | ******* | -0.0657 | -0.0467 | -0.0627 | -0.3348 |
| 0.800 | -0.0234 | -0.0654 | -0.0520 | -0.0654 | ******* |
| 0.825 | ******* | -0.0628 | -0.0634 | -0.0809 | -0.3653 |
| 0.850 | 0.0049 | -0.0549 | -0.0662 | -0.0940 | -0.3894 |
| 0.875 | ******* | -0.0445 | -0.0711 | -0.1031 | -0.4463 |
| 0.900 | 0.0450 | -0.0317 | -0.0594 | -0.1186 | ******* |
| 0.925 | ******* | -0.0012 | -0.0446 | -0.1106 | -1.0001 |
| 0.950 | 0.0895 | 0.0320 | -0.0162 | -0.0669 | -0.4327 |
| 0.975 | ******* | 0.0809 | 0.0499 | -0.0051 | -0.2115 |
| 1.000 | 0.1935 | 0.1704 | 0.1479 | 0.1495 | 0.0903 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0390 | -0.0141 | 0.0455 | ******* | -0.2616 |
| -0.400 | -0.0695 | -0.0117 | 0.0065 | -0.0821 | -0.3044 |
| -0.600 | -0.0961 | -0.0286 | -0.0153 | -0.0823 | -0.3264 |
| -0.700 | ******* | -0.0816 | -0.0289 | -0.0837 | -0.3582 |
| -0.800 | ******* | ******* | -0.0954 | -0.0973 | -0.3952 |
| -0.850 | ******* | -0.1162 | -0.1171 | -0.1401 | -0.4680 |
| -0.900 | -0.0456 | -0.0903 | -0.1250 | -0.1748 | -0.6617 |
| -0.950 | -0.0123 | -0.0179 | -0.0826 | -0.1501 | -0.4760 |
| -0.975 | ******* | 0.0170 | -0.0276 | -0.0885 | -0.2638 |
| -1.000 | 0.1831 | 0.1617 | 0.1350 | 0.1308 | 0.0972 |



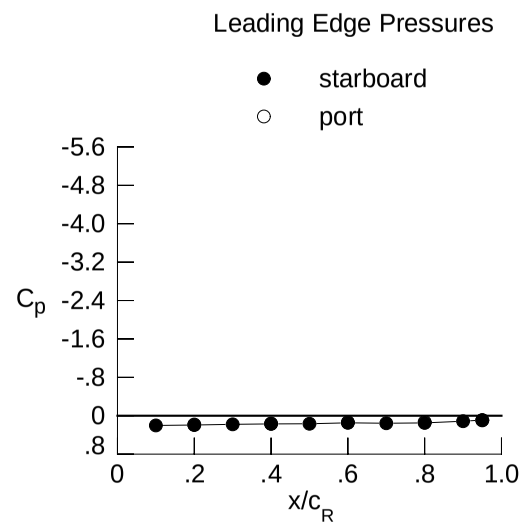

Small Radius L.E.

Run No. = 36 , Point No. = 713

$C_N$ = -0.054, $C_m$ = 0.0241

$\alpha$ = -0.4 °, $M_\infty$ = 0.399

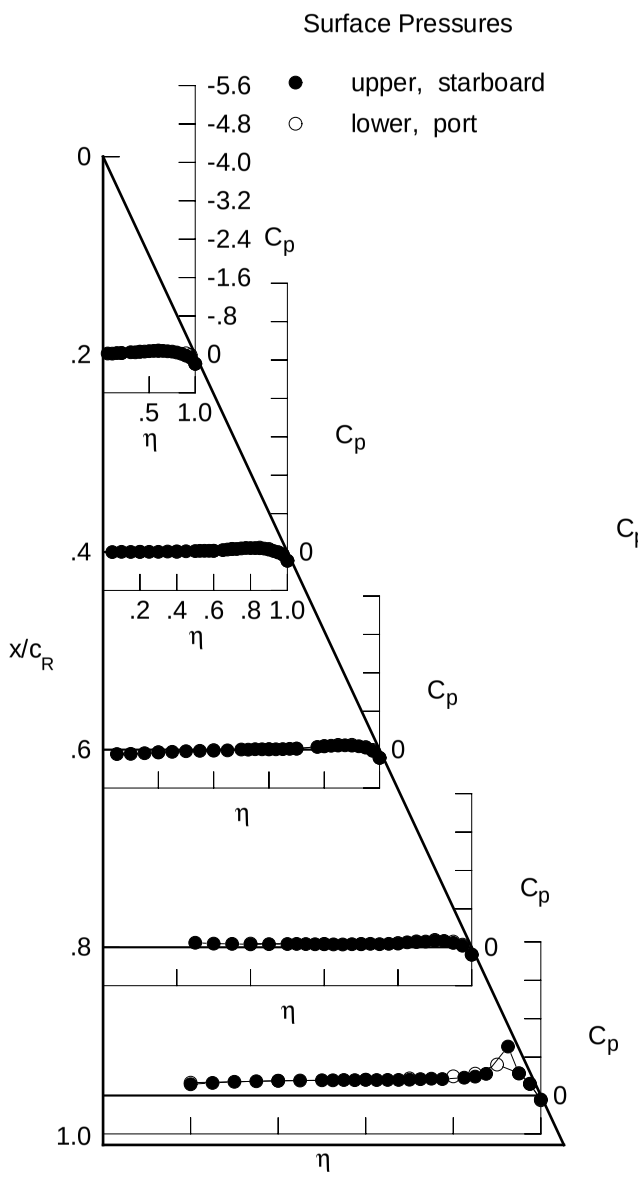
$R_{mac}$ = $5.8 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2026 | ******* |
| 0.20 | 0.1935 | 0.1831 |
| 0.30 | 0.1790 | ******* |
| 0.40 | 0.1704 | 0.1617 |
| 0.50 | 0.1673 | ******* |
| 0.60 | 0.1479 | 0.1350 |
| 0.70 | 0.1567 | ******* |
| 0.80 | 0.1495 | 0.1308 |
| 0.90 | 0.1142 | ******* |
| 0.95 | 0.0903 | 0.0972 |

# Table D1. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0180 | 0.0008 | 0.0919 | ******* | ******* |
| 0.100 | -0.0164 | -0.0043 | 0.0881 | ******* | ******* |
| 0.150 | -0.0284 | -0.0016 | 0.0742 | ******* | ******* |
| 0.200 | -0.0281 | -0.0059 | 0.0592 | ******* | -0.2345 |
| 0.250 | ******* | -0.0038 | 0.0458 | -0.0947 | -0.2623 |
| 0.300 | -0.0446 | -0.0039 | 0.0330 | -0.0764 | -0.2854 |
| 0.350 | -0.0430 | -0.0102 | 0.0250 | -0.0713 | -0.2967 |
| 0.400 | -0.0543 | -0.0142 | 0.0213 | -0.0613 | -0.3084 |
| 0.450 | -0.0585 | -0.0161 | 0.0152 | -0.0656 | -0.3122 |
| 0.500 | -0.0675 | -0.0196 | -0.0021 | -0.0679 | -0.3175 |
| 0.525 | ******* | -0.0252 | 0.0010 | -0.0704 | -0.3168 |
| 0.550 | -0.0726 | -0.0253 | -0.0091 | -0.0672 | -0.3230 |
| 0.575 | ******* | -0.0259 | -0.0069 | -0.0633 | -0.3197 |
| 0.600 | -0.0727 | -0.0256 | -0.0102 | -0.0633 | -0.3296 |
| 0.625 | ******* | ******* | -0.0069 | -0.0597 | -0.3222 |
| 0.650 | -0.0731 | -0.0404 | -0.0103 | -0.0587 | -0.3244 |
| 0.675 | ******* | -0.0520 | -0.0166 | -0.0636 | -0.3251 |
| 0.700 | -0.0651 | -0.0625 | -0.0209 | -0.0632 | -0.3298 |
| 0.725 | ******* | -0.0633 | ******* | -0.0720 | -0.3412 |
| 0.750 | -0.0579 | -0.0753 | ******* | -0.0651 | -0.3504 |
| 0.775 | ******* | -0.0846 | -0.0562 | -0.0717 | -0.3424 |
| 0.800 | -0.0395 | -0.0824 | -0.0676 | -0.0770 | ******* |
| 0.825 | ******* | -0.0820 | -0.0808 | -0.1033 | -0.3710 |
| 0.850 | -0.0129 | -0.0796 | -0.0857 | -0.1102 | -0.3938 |
| 0.875 | ******* | -0.0710 | -0.0901 | -0.1188 | -0.4513 |
| 0.900 | 0.0264 | -0.0506 | -0.0844 | -0.1387 | ******* |
| 0.925 | ******* | -0.0214 | -0.0708 | -0.1317 | -1.0203 |
| 0.950 | 0.0688 | 0.0097 | -0.0425 | -0.0912 | -0.4573 |
| 0.975 | ******* | 0.0492 | 0.0237 | -0.0331 | -0.2400 |
| 1.000 | 0.1966 | 0.1807 | 0.1723 | 0.1560 | 0.0829 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0281 | -0.0025 | 0.0531 | ******* | -0.2672 |
| -0.400 | -0.0571 | -0.0037 | 0.0101 | -0.0771 | -0.3054 |
| -0.600 | -0.0806 | -0.0264 | -0.0050 | -0.0716 | -0.3268 |
| -0.700 | ******* | -0.0663 | -0.0215 | -0.0707 | -0.3565 |
| -0.800 | ******* | ******* | -0.0759 | -0.0886 | -0.3995 |
| -0.850 | ******* | -0.0926 | -0.0991 | -0.1232 | -0.4555 |
| -0.900 | -0.0226 | -0.0633 | -0.1010 | -0.1538 | -0.6447 |
| -0.950 | 0.0105 | 0.0021 | -0.0526 | -0.1193 | -0.4648 |
| -0.975 | ******* | 0.0490 | 0.0046 | -0.0543 | -0.2454 |
| -1.000 | 0.1951 | 0.1808 | 0.1688 | 0.1501 | 0.0984 |



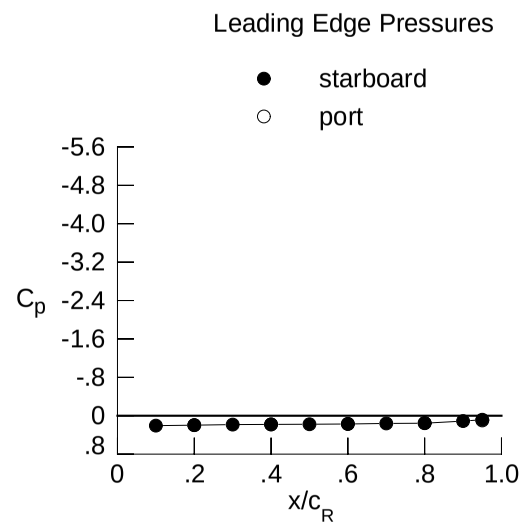

Small Radius L.E.

Run No. = 36 , Point No. = 714

$C_N$ = -0.030, $C_m$ = 0.0175

$\alpha$ = 0.0 °, $M_\infty$ = 0.398

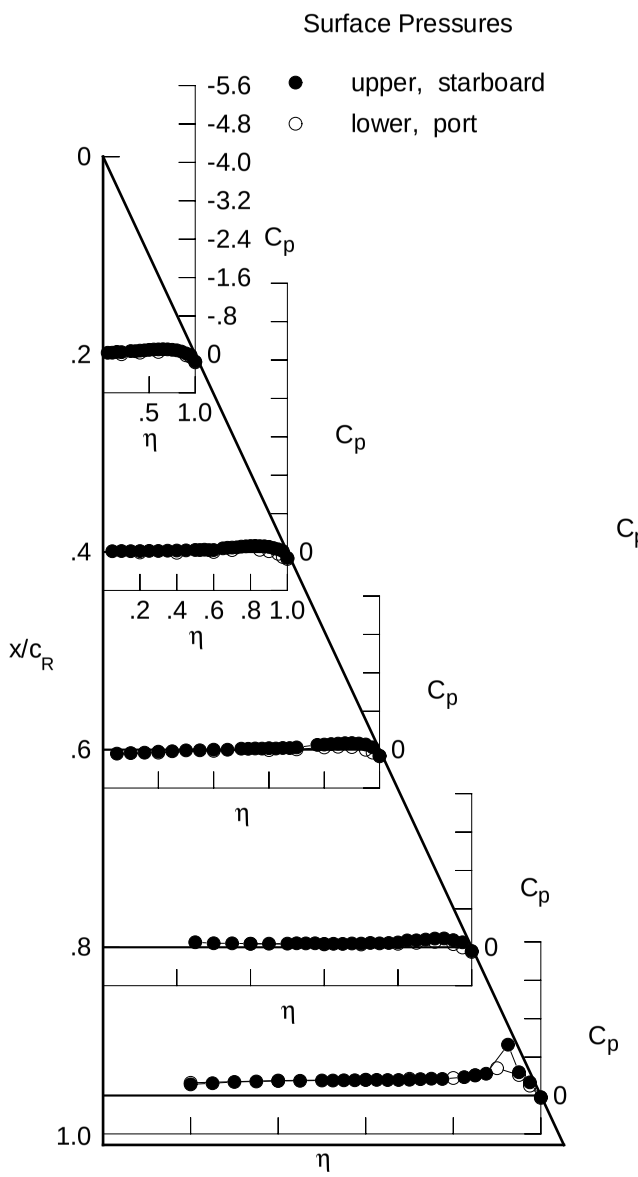
$R_{mac}$ = $5.8 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2066 | ******* |
| 0.20 | 0.1966 | 0.1951 |
| 0.30 | 0.1845 | ******* |
| 0.40 | 0.1807 | 0.1808 |
| 0.50 | 0.1772 | ******* |
| 0.60 | 0.1723 | 0.1688 |
| 0.70 | 0.1606 | ******* |
| 0.80 | 0.1560 | 0.1501 |
| 0.90 | 0.1116 | ******* |
| 0.95 | 0.0829 | 0.0984 |

# Table D1. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0334 | -0.0167 | 0.0829 | ******* | ******* |
| 0.100 | -0.0353 | -0.0208 | 0.0722 | ******* | ******* |
| 0.150 | -0.0520 | -0.0175 | 0.0636 | ******* | ******* |
| 0.200 | -0.0460 | -0.0203 | 0.0426 | ******* | -0.2318 |
| 0.250 | ******* | -0.0237 | 0.0340 | -0.1048 | -0.2558 |
| 0.300 | -0.0690 | -0.0227 | 0.0150 | -0.0839 | -0.2820 |
| 0.350 | -0.0667 | -0.0283 | 0.0137 | -0.0824 | -0.2923 |
| 0.400 | -0.0781 | -0.0316 | 0.0011 | -0.0745 | -0.3026 |
| 0.450 | -0.0841 | -0.0343 | 0.0018 | -0.0749 | -0.3068 |
| 0.500 | -0.0947 | -0.0431 | -0.0199 | -0.0758 | -0.3130 |
| 0.525 | ******* | -0.0412 | -0.0174 | -0.0828 | -0.3120 |
| 0.550 | -0.1014 | -0.0486 | -0.0240 | -0.0807 | -0.3165 |
| 0.575 | ******* | -0.0402 | -0.0219 | -0.0834 | -0.3176 |
| 0.600 | -0.1042 | -0.0413 | -0.0306 | -0.0705 | -0.3233 |
| 0.625 | ******* | ******* | -0.0232 | -0.0729 | -0.3258 |
| 0.650 | -0.1071 | -0.0766 | -0.0345 | -0.0702 | -0.3226 |
| 0.675 | ******* | -0.0884 | -0.0330 | -0.0792 | -0.3229 |
| 0.700 | -0.1048 | -0.0926 | -0.0466 | -0.0766 | -0.3286 |
| 0.725 | ******* | -0.0976 | ******* | -0.0902 | -0.3406 |
| 0.750 | -0.0962 | -0.1128 | ******* | -0.0817 | -0.3507 |
| 0.775 | ******* | -0.1195 | -0.0996 | -0.0893 | -0.3449 |
| 0.800 | -0.0845 | -0.1246 | -0.1055 | -0.1010 | ******* |
| 0.825 | ******* | -0.1281 | -0.1161 | -0.1435 | -0.3821 |
| 0.850 | -0.0589 | -0.1224 | -0.1257 | -0.1444 | -0.4172 |
| 0.875 | ******* | -0.1200 | -0.1346 | -0.1604 | -0.4536 |
| 0.900 | -0.0198 | -0.1078 | -0.1371 | -0.1816 | ******* |
| 0.925 | ******* | -0.0826 | -0.1270 | -0.1842 | -1.0591 |
| 0.950 | 0.0159 | -0.0564 | -0.1075 | -0.1489 | -0.4848 |
| 0.975 | ******* | -0.0195 | -0.0482 | -0.1038 | -0.2742 |
| 1.000 | 0.1498 | 0.1209 | 0.1265 | 0.0773 | 0.0339 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0032 | 0.0084 | 0.0623 | ******* | -0.2650 |
| -0.400 | -0.0361 | 0.0151 | 0.0256 | -0.0732 | -0.3117 |
| -0.600 | -0.0509 | -0.0016 | 0.0092 | -0.0604 | -0.3296 |
| -0.700 | ******* | -0.0405 | -0.0060 | -0.0581 | -0.3488 |
| -0.800 | ******* | ******* | -0.0467 | -0.0729 | -0.3649 |
| -0.850 | ******* | -0.0466 | -0.0611 | -0.0917 | -0.4250 |
| -0.900 | 0.0195 | -0.0174 | -0.0540 | -0.1134 | -0.5690 |
| -0.950 | 0.0516 | 0.0356 | 0.0028 | -0.0652 | -0.4270 |
| -0.975 | ******* | 0.1027 | 0.0619 | 0.0039 | -0.2053 |
| -1.000 | 0.1653 | 0.1447 | 0.1396 | 0.0965 | 0.0492 |



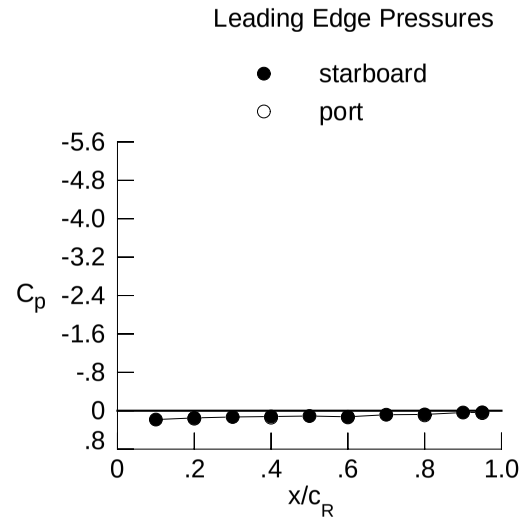

Small Radius L.E.

Run No. = 36 , Point No. = 715

$C_N$ = 0.004, $C_m$ = 0.0144

$\alpha$ = 1.1 °, $M_\infty$ = 0.399

$R_{mac}$ = $5.8 \times 10^6$

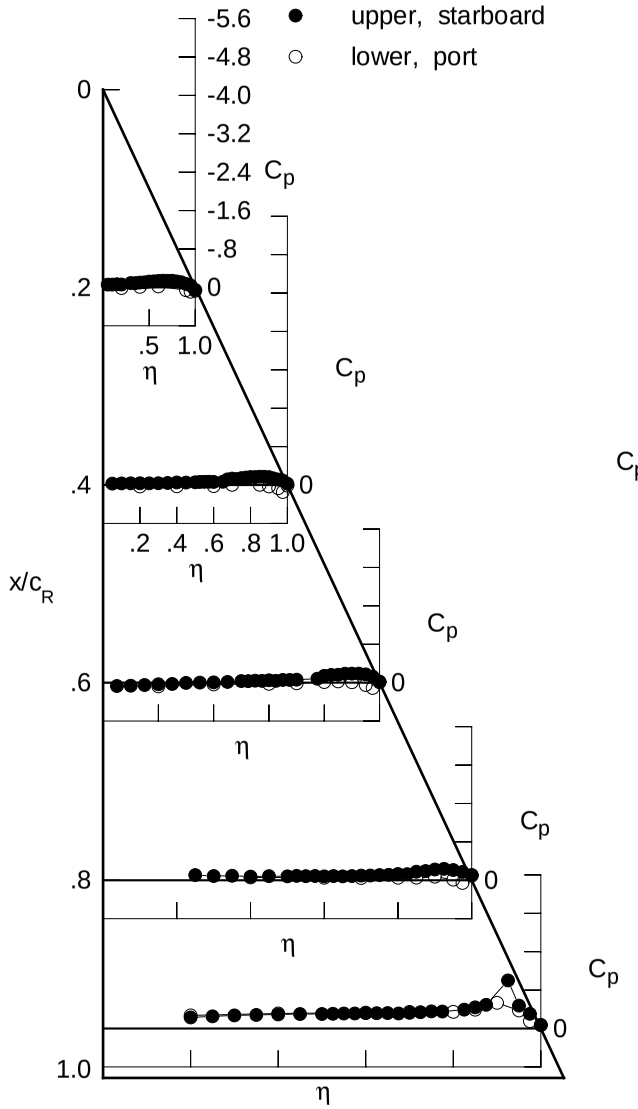



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.1840 | ******* |
| 0.20 | 0.1498 | 0.1653 |
| 0.30 | 0.1303 | ******* |
| 0.40 | 0.1209 | 0.1447 |
| 0.50 | 0.1102 | ******* |
| 0.60 | 0.1265 | 0.1396 |
| 0.70 | 0.0834 | ******* |
| 0.80 | 0.0773 | 0.0965 |
| 0.90 | 0.0375 | ******* |
| 0.95 | 0.0339 | 0.0492 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0577 | -0.0297 | 0.0700 | ******* | ******* |
| 0.100 | -0.0575 | -0.0336 | 0.0638 | ******* | ******* |
| 0.150 | -0.0653 | -0.0362 | 0.0493 | ******* | ******* |
| 0.200 | -0.0601 | -0.0371 | 0.0336 | ******* | -0.2302 |
| 0.250 | ******* | -0.0351 | 0.0270 | -0.1087 | -0.2540 |
| 0.300 | -0.0903 | -0.0378 | 0.0059 | -0.0887 | -0.2731 |
| 0.350 | -0.0887 | -0.0434 | -0.0010 | -0.0945 | -0.2825 |
| 0.400 | -0.1007 | -0.0535 | -0.0053 | -0.0771 | -0.2929 |
| 0.450 | -0.1051 | -0.0515 | -0.0143 | -0.0861 | -0.3016 |
| 0.500 | -0.1215 | -0.0579 | -0.0327 | -0.0822 | -0.3025 |
| 0.525 | ******* | -0.0645 | -0.0309 | -0.0922 | -0.3068 |
| 0.550 | -0.1268 | -0.0669 | -0.0405 | -0.0854 | -0.3123 |
| 0.575 | ******* | -0.0686 | -0.0372 | -0.0893 | -0.3128 |
| 0.600 | -0.1339 | -0.0652 | -0.0496 | -0.0813 | -0.3198 |
| 0.625 | ******* | ******* | -0.0380 | -0.0883 | -0.3194 |
| 0.650 | -0.1389 | -0.0681 | -0.0570 | -0.0815 | -0.3217 |
| 0.675 | ******* | -0.1178 | -0.0562 | -0.0876 | -0.3134 |
| 0.700 | -0.1374 | -0.1347 | -0.0613 | -0.0974 | -0.3263 |
| 0.725 | ******* | -0.1231 | ******* | -0.0993 | -0.3389 |
| 0.750 | -0.1386 | -0.1429 | ******* | -0.1090 | -0.3570 |
| 0.775 | ******* | -0.1559 | -0.0818 | -0.1141 | -0.3532 |
| 0.800 | -0.1242 | -0.1661 | -0.1421 | -0.1303 | ******* |
| 0.825 | ******* | -0.1658 | -0.1611 | -0.1276 | -0.3928 |
| 0.850 | -0.1063 | -0.1727 | -0.1639 | -0.1787 | -0.4409 |
| 0.875 | ******* | -0.1717 | -0.1868 | -0.1926 | -0.4935 |
| 0.900 | -0.0711 | -0.1650 | -0.1882 | -0.2238 | ******* |
| 0.925 | ******* | -0.1381 | -0.1883 | -0.2386 | -1.0012 |
| 0.950 | -0.0404 | -0.1140 | -0.1717 | -0.2137 | -0.4769 |
| 0.975 | ******* | -0.0928 | -0.1266 | -0.1747 | -0.3067 |
| 1.000 | 0.0516 | -0.0278 | -0.0221 | -0.1108 | -0.0742 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0133 | 0.0297 | 0.0778 | ******* | -0.2730 |
| -0.400 | -0.0114 | 0.0266 | 0.0378 | -0.0604 | -0.3134 |
| -0.600 | -0.0207 | 0.0226 | 0.0241 | -0.0529 | -0.3301 |
| -0.700 | ******* | -0.0047 | 0.0137 | -0.0471 | -0.3465 |
| -0.800 | ******* | ******* | -0.0120 | -0.0527 | -0.3475 |
| -0.850 | ******* | -0.0049 | -0.0263 | -0.0555 | -0.3926 |
| -0.900 | 0.0580 | 0.0296 | -0.0083 | -0.0745 | -0.5350 |
| -0.950 | 0.0910 | 0.0664 | 0.0496 | -0.0137 | -0.3758 |
| -0.975 | ******* | 0.1453 | 0.1112 | 0.0556 | -0.1521 |
| -1.000 | 0.0700 | 0.0120 | -0.0065 | -0.0953 | -0.0698 |

Surface Pressures




Small Radius L.E.

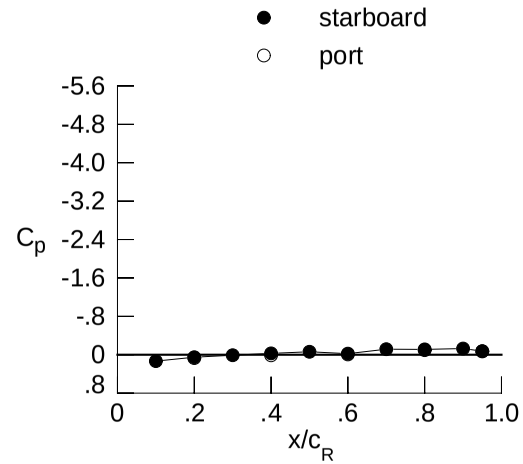
Run No. = 36 , Point No. = 716

$C_N$ = 0.039, $C_m$ = 0.0100

$\alpha$ = 2.1 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

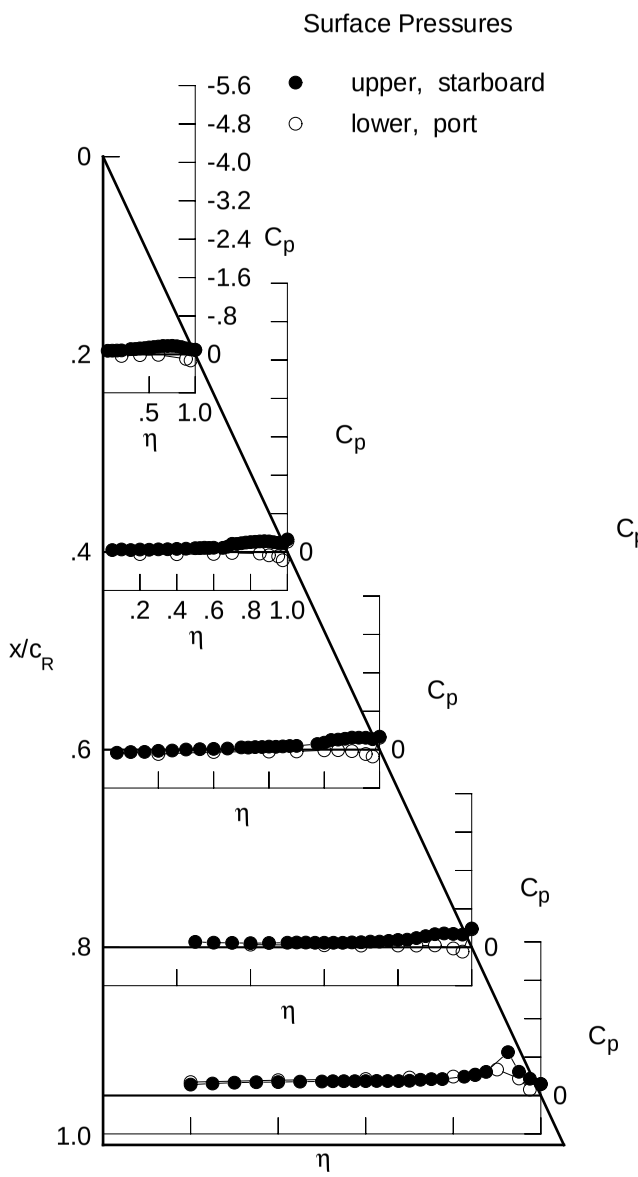
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.1332 | ******* |
| 0.20 | 0.0516 | 0.0700 |
| 0.30 | 0.0105 | ******* |
| 0.40 | -0.0278 | 0.0120 |
| 0.50 | -0.0618 | ******* |
| 0.60 | -0.0221 | -0.0065 |
| 0.70 | -0.1154 | ******* |
| 0.80 | -0.1108 | -0.0953 |
| 0.90 | -0.1290 | ******* |
| 0.95 | -0.0742 | -0.0698 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0748 | -0.0412 | 0.0650 | ******* | ******* |
| 0.100 | -0.0777 | -0.0537 | 0.0508 | ******* | ******* |
| 0.150 | -0.0803 | -0.0410 | 0.0474 | ******* | ******* |
| 0.200 | -0.0830 | -0.0520 | 0.0249 | ******* | -0.2269 |
| 0.250 | ******* | -0.0477 | 0.0182 | -0.1132 | -0.2497 |
| 0.300 | -0.1100 | -0.0558 | -0.0023 | -0.0961 | -0.2671 |
| 0.350 | -0.1123 | -0.0581 | -0.0097 | -0.0922 | -0.2767 |
| 0.400 | -0.1251 | -0.0653 | -0.0157 | -0.0859 | -0.2793 |
| 0.450 | -0.1304 | -0.0692 | -0.0233 | -0.0898 | -0.2886 |
| 0.500 | -0.1450 | -0.0798 | -0.0465 | -0.0953 | -0.2923 |
| 0.525 | ******* | -0.0823 | -0.0421 | -0.0990 | -0.2978 |
| 0.550 | -0.1532 | -0.0898 | -0.0528 | -0.0987 | -0.2980 |
| 0.575 | ******* | -0.0855 | -0.0545 | -0.0943 | -0.2982 |
| 0.600 | -0.1634 | -0.0900 | -0.0635 | -0.0947 | -0.2998 |
| 0.625 | ******* | ******* | -0.0590 | -0.0946 | -0.3032 |
| 0.650 | -0.1749 | -0.0872 | -0.0675 | -0.0937 | -0.3014 |
| 0.675 | ******* | -0.1109 | -0.0755 | -0.1019 | -0.3006 |
| 0.700 | -0.1736 | -0.1716 | -0.0786 | -0.1054 | -0.3076 |
| 0.725 | ******* | -0.1679 | ******* | -0.1187 | -0.3280 |
| 0.750 | -0.1782 | -0.1834 | ******* | -0.1188 | -0.3411 |
| 0.775 | ******* | -0.1977 | -0.1170 | -0.1333 | -0.3426 |
| 0.800 | -0.1697 | -0.2064 | -0.1449 | -0.1531 | ******* |
| 0.825 | ******* | -0.2126 | -0.2008 | -0.1584 | -0.3922 |
| 0.850 | -0.1521 | -0.2207 | -0.2092 | -0.1916 | -0.4349 |
| 0.875 | ******* | -0.2258 | -0.2261 | -0.2322 | -0.4920 |
| 0.900 | -0.1253 | -0.2219 | -0.2501 | -0.2730 | ******* |
| 0.925 | ******* | -0.2046 | -0.2488 | -0.2881 | -0.9035 |
| 0.950 | -0.1041 | -0.1898 | -0.2478 | -0.2783 | -0.4944 |
| 0.975 | ******* | -0.1801 | -0.2178 | -0.2637 | -0.3497 |
| 1.000 | -0.0978 | -0.2622 | -0.2703 | -0.3914 | -0.2408 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0323 | 0.0420 | 0.0905 | ******* | -0.2796 |
| -0.400 | 0.0151 | 0.0450 | 0.0490 | -0.0551 | -0.3191 |
| -0.600 | 0.0088 | 0.0394 | 0.0402 | -0.0423 | -0.3433 |
| -0.700 | ******* | 0.0194 | 0.0366 | -0.0360 | -0.3735 |
| -0.800 | ******* | ******* | 0.0138 | -0.0378 | -0.3943 |
| -0.850 | ******* | 0.0302 | 0.0104 | -0.0362 | -0.4268 |
| -0.900 | 0.0935 | 0.0676 | 0.0301 | -0.0397 | -0.5414 |
| -0.950 | 0.1259 | 0.0898 | 0.0908 | 0.0245 | -0.3552 |
| -0.975 | ******* | 0.1715 | 0.1422 | 0.0902 | -0.1248 |
| -1.000 | -0.0885 | -0.2169 | -0.2484 | -0.3753 | -0.2371 |



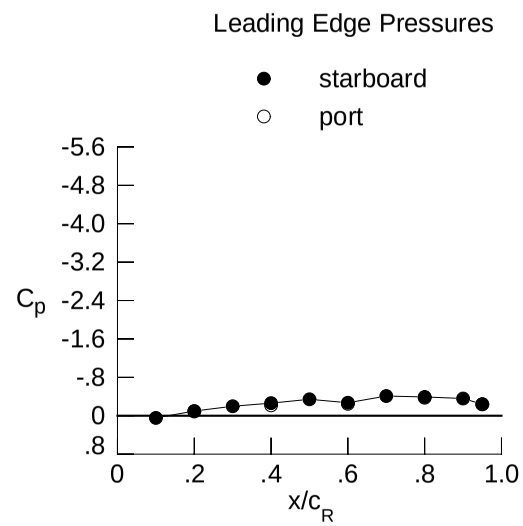

Small Radius L.E.

Run No. = 36 , Point No. = 717

$C_N$ = 0.070, $C_m$ = 0.0089

$\alpha$ = 3.1 °, $M_\infty$ = 0.398

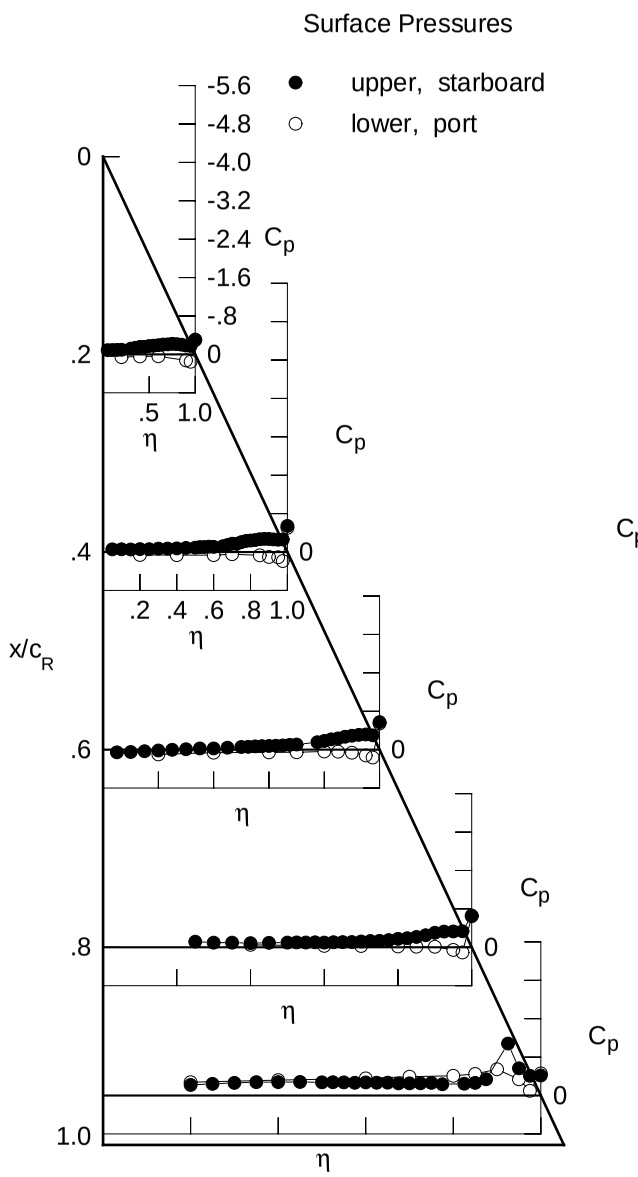
$R_{mac}$ = $5.8 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.0454 | ******* |
| 0.20 | -0.0978 | -0.0885 |
| 0.30 | -0.1973 | ******* |
| 0.40 | -0.2622 | -0.2169 |
| 0.50 | -0.3424 | ******* |
| 0.60 | -0.2703 | -0.2484 |
| 0.70 | -0.4101 | ******* |
| 0.80 | -0.3914 | -0.3753 |
| 0.90 | -0.3587 | ******* |
| 0.95 | -0.2408 | -0.2371 |

# Table D1. Continued.

| η | x/c_R .2 C_p,u | x/c_R .4 C_p,u | x/c_R .6 C_p,u | x/c_R .8 C_p,u | x/c_R .95 C_p,u |
|---|---|---|---|---|---|
| 0.050 | -0.0881 | -0.0562 | 0.0557 | ******* | ******* |
| 0.100 | -0.0908 | -0.0573 | 0.0487 | ******* | ******* |
| 0.150 | -0.0928 | -0.0526 | 0.0324 | ******* | ******* |
| 0.200 | -0.0964 | -0.0605 | 0.0173 | ******* | -0.2197 |
| 0.250 | ******* | -0.0594 | 0.0034 | -0.1168 | -0.2436 |
| 0.300 | -0.1189 | -0.0715 | -0.0077 | -0.0960 | -0.2633 |
| 0.350 | -0.1376 | -0.0716 | -0.0246 | -0.0967 | -0.2784 |
| 0.400 | -0.1560 | -0.0758 | -0.0252 | -0.0861 | -0.2793 |
| 0.450 | -0.1579 | -0.0858 | -0.0406 | -0.0939 | -0.2822 |
| 0.500 | -0.1744 | -0.0909 | -0.0554 | -0.0973 | -0.2741 |
| 0.525 | ******* | -0.1030 | -0.0595 | -0.1019 | -0.2766 |
| 0.550 | -0.1817 | -0.1040 | -0.0683 | -0.0989 | -0.2733 |
| 0.575 | ******* | -0.1116 | -0.0717 | -0.1040 | -0.2658 |
| 0.600 | -0.1914 | -0.1080 | -0.0768 | -0.0976 | -0.2727 |
| 0.625 | ******* | ******* | -0.0818 | -0.1058 | -0.2663 |
| 0.650 | -0.2050 | -0.1210 | -0.0871 | -0.1081 | -0.2684 |
| 0.675 | ******* | -0.1467 | -0.0991 | -0.1099 | -0.2524 |
| 0.700 | -0.2085 | -0.1735 | -0.1061 | -0.1210 | -0.2536 |
| 0.725 | ******* | -0.1716 | ******* | -0.1308 | -0.2547 |
| 0.750 | -0.2198 | -0.2064 | ******* | -0.1345 | -0.2631 |
| 0.775 | ******* | -0.2301 | -0.1547 | -0.1502 | -0.2346 |
| 0.800 | -0.2131 | -0.2402 | -0.1811 | -0.1763 | ******* |
| 0.825 | ******* | -0.2493 | -0.2147 | -0.1890 | -0.2456 |
| 0.850 | -0.2024 | -0.2661 | -0.2346 | -0.2153 | -0.2636 |
| 0.875 | ******* | -0.2748 | -0.2691 | -0.2510 | -0.3381 |
| 0.900 | -0.1851 | -0.2721 | -0.2897 | -0.3025 | ******* |
| 0.925 | ******* | -0.2632 | -0.3078 | -0.3273 | -1.0821 |
| 0.950 | -0.1759 | -0.2571 | -0.3159 | -0.3292 | -0.5672 |
| 0.975 | ******* | -0.2612 | -0.2987 | -0.3334 | -0.4113 |
| 1.000 | -0.2979 | -0.5434 | -0.5737 | -0.6609 | -0.4166 |
| | C_p,l | C_p,l | C_p,l | C_p,l | C_p,l |
| -0.200 | 0.0566 | 0.0606 | 0.0991 | ******* | -0.2772 |
| -0.400 | 0.0416 | 0.0650 | 0.0633 | -0.0509 | -0.3207 |
| -0.600 | 0.0393 | 0.0639 | 0.0571 | -0.0297 | -0.3567 |
| -0.700 | ******* | 0.0454 | 0.0546 | -0.0271 | -0.3920 |
| -0.800 | ******* | ******* | 0.0383 | -0.0179 | -0.4105 |
| -0.850 | ******* | 0.0684 | 0.0415 | -0.0130 | -0.4491 |
| -0.900 | 0.1253 | 0.1022 | 0.0642 | -0.0111 | -0.5465 |
| -0.950 | 0.1527 | 0.1091 | 0.1206 | 0.0554 | -0.3379 |
| -0.975 | ******* | 0.1881 | 0.1628 | 0.1078 | -0.0983 |
| -1.000 | -0.3086 | -0.5030 | -0.5455 | -0.6472 | -0.4602 |



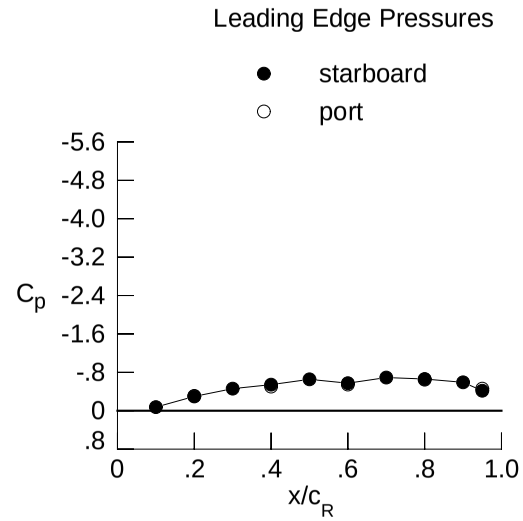

Small Radius L.E.

Run No. = 36 , Point No. = 718

$C_N$ = 0.099, $C_m$ = 0.0063

$\alpha$ = 4.2 °, $M_\infty$ = 0.399

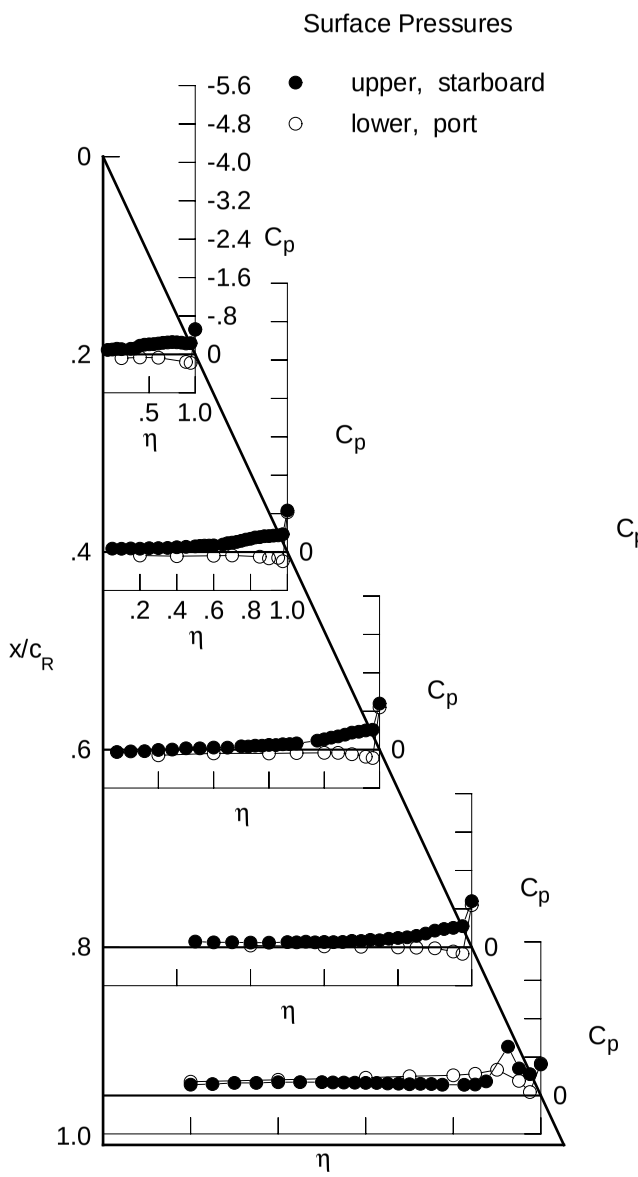
$R_{mac}$ = $5.8 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.0754 | ******* |
| 0.20 | -0.2979 | -0.3086 |
| 0.30 | -0.4599 | ******* |
| 0.40 | -0.5434 | -0.5030 |
| 0.50 | -0.6541 | ******* |
| 0.60 | -0.5737 | -0.5455 |
| 0.70 | -0.6912 | ******* |
| 0.80 | -0.6609 | -0.6472 |
| 0.90 | -0.5917 | ******* |
| 0.95 | -0.4166 | -0.4602 |

# Table D1. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0930 | -0.0704 | 0.0500 | ******* | ******* |
| 0.100 | -0.1005 | -0.0682 | 0.0368 | ******* | ******* |
| 0.150 | -0.1173 | -0.0747 | 0.0317 | ******* | ******* |
| 0.200 | -0.1088 | -0.0697 | 0.0064 | ******* | -0.2258 |
| 0.250 | ******* | -0.0802 | -0.0014 | -0.1193 | -0.2383 |
| 0.300 | -0.1170 | -0.0812 | -0.0280 | -0.1028 | -0.2624 |
| 0.350 | -0.1247 | -0.0856 | -0.0270 | -0.1038 | -0.2624 |
| 0.400 | -0.1809 | -0.0999 | -0.0433 | -0.0973 | -0.2771 |
| 0.450 | -0.2015 | -0.1091 | -0.0419 | -0.0956 | -0.2782 |
| 0.500 | -0.2094 | -0.1182 | -0.0691 | -0.1083 | -0.2780 |
| 0.525 | ******* | -0.1272 | -0.0649 | -0.1029 | -0.2722 |
| 0.550 | -0.2144 | -0.1333 | -0.0821 | -0.1165 | -0.2696 |
| 0.575 | ******* | -0.1340 | -0.0816 | -0.1033 | -0.2671 |
| 0.600 | -0.2262 | -0.1385 | -0.0986 | -0.1113 | -0.2632 |
| 0.625 | ******* | ******* | -0.0954 | -0.1070 | -0.2614 |
| 0.650 | -0.2407 | -0.1555 | -0.1121 | -0.1109 | -0.2506 |
| 0.675 | ******* | -0.1842 | -0.1154 | -0.1338 | -0.2465 |
| 0.700 | -0.2484 | -0.1959 | -0.1301 | -0.1309 | -0.2350 |
| 0.725 | ******* | -0.2103 | ******* | -0.1542 | -0.2433 |
| 0.750 | -0.2569 | -0.2337 | ******* | -0.1467 | -0.2391 |
| 0.775 | ******* | -0.2593 | -0.1872 | -0.1779 | -0.2246 |
| 0.800 | -0.2520 | -0.2763 | -0.2148 | -0.1944 | ******* |
| 0.825 | ******* | -0.3033 | -0.2496 | -0.2080 | -0.2230 |
| 0.850 | -0.2442 | -0.3102 | -0.2764 | -0.2374 | -0.2292 |
| 0.875 | ******* | -0.3293 | -0.3117 | -0.2854 | -0.2947 |
| 0.900 | -0.2275 | -0.3322 | -0.3548 | -0.3475 | ******* |
| 0.925 | ******* | -0.3416 | -0.3727 | -0.3810 | -1.0179 |
| 0.950 | -0.2337 | -0.3474 | -0.4001 | -0.4051 | -0.5642 |
| 0.975 | ******* | -0.3711 | -0.4145 | -0.4400 | -0.4448 |
| 1.000 | -0.5139 | -0.8646 | -0.9602 | -0.9612 | -0.6474 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0785 | 0.0722 | 0.1180 | ******* | -0.2868 |
| -0.400 | 0.0632 | 0.0866 | 0.0776 | -0.0367 | -0.3271 |
| -0.600 | 0.0688 | 0.0780 | 0.0794 | -0.0190 | -0.3699 |
| -0.700 | ******* | 0.0710 | 0.0712 | -0.0108 | -0.4014 |
| -0.800 | ******* | ******* | 0.0668 | 0.0021 | -0.4205 |
| -0.850 | ******* | 0.0977 | 0.0676 | 0.0080 | -0.4523 |
| -0.900 | 0.1567 | 0.1311 | 0.0953 | 0.0210 | -0.5368 |
| -0.950 | 0.1771 | 0.1210 | 0.1473 | 0.0880 | -0.3045 |
| -0.975 | ******* | 0.1922 | 0.1737 | 0.1364 | -0.0718 |
| -1.000 | -0.5268 | -0.8288 | -0.8801 | -0.8784 | -0.6666 |



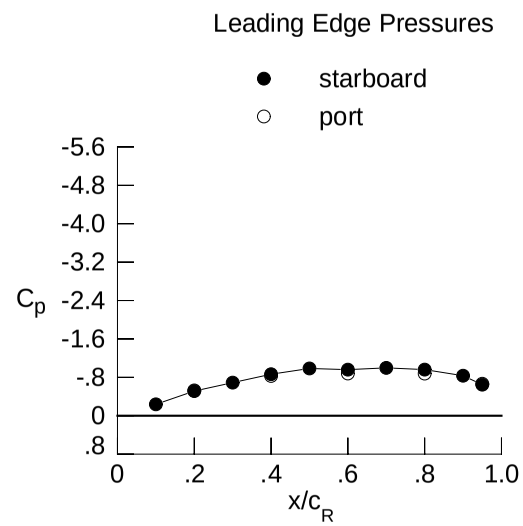

Small Radius L.E.

Run No. = 36 , Point No. = 719

$C_N$ = 0.143, $C_m$ = -0.0056

$\alpha$ = 5.2 °, $M_\infty$ = 0.398

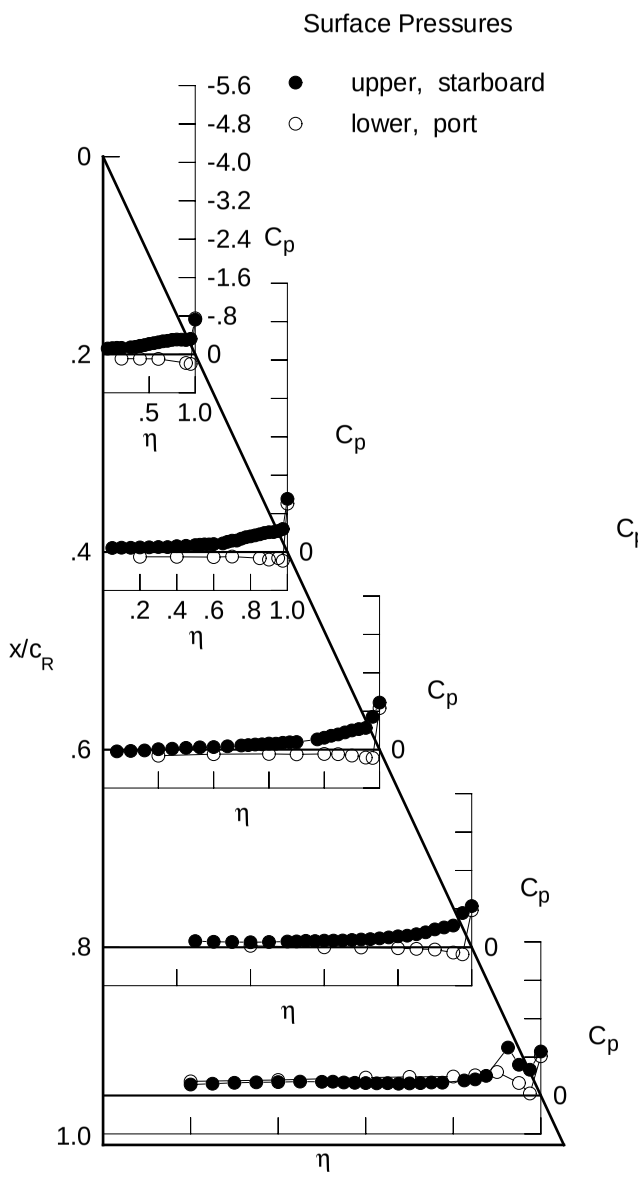
$R_{mac}$ = $5.8 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.2378 | ******* |
| 0.20 | -0.5139 | -0.5268 |
| 0.30 | -0.6893 | ******* |
| 0.40 | -0.8646 | -0.8288 |
| 0.50 | -0.9846 | ******* |
| 0.60 | -0.9602 | -0.8801 |
| 0.70 | -0.9972 | ******* |
| 0.80 | -0.9612 | -0.8784 |
| 0.90 | -0.8335 | ******* |
| 0.95 | -0.6474 | -0.6666 |

# Table D1. Continued.

| η | x/c_R .2 C_p,u | x/c_R .4 C_p,u | x/c_R .6 C_p,u | x/c_R .8 C_p,u | x/c_R .95 C_p,u |
|---|---|---|---|---|---|
| 0.050 | -0.1225 | -0.0847 | 0.0359 | ******* | ******* |
| 0.100 | -0.1300 | -0.0903 | 0.0271 | ******* | ******* |
| 0.150 | -0.1368 | -0.0891 | 0.0167 | ******* | ******* |
| 0.200 | -0.1359 | -0.0957 | -0.0085 | ******* | -0.2286 |
| 0.250 | ******* | -0.0982 | -0.0192 | -0.1285 | -0.2455 |
| 0.300 | -0.1476 | -0.1049 | -0.0371 | -0.1144 | -0.2651 |
| 0.350 | -0.1563 | -0.1034 | -0.0481 | -0.1102 | -0.2743 |
| 0.400 | -0.1788 | -0.1224 | -0.0535 | -0.1051 | -0.2792 |
| 0.450 | -0.1932 | -0.1298 | -0.0697 | -0.1102 | -0.2897 |
| 0.500 | -0.2180 | -0.1438 | -0.0866 | -0.1197 | -0.2853 |
| 0.525 | ******* | -0.1522 | -0.0945 | -0.1227 | -0.2877 |
| 0.550 | -0.2335 | -0.1592 | -0.1065 | -0.1344 | -0.2715 |
| 0.575 | ******* | -0.1587 | -0.1113 | -0.1296 | -0.2647 |
| 0.600 | -0.2517 | -0.1658 | -0.1264 | -0.1384 | -0.2595 |
| 0.625 | ******* | ******* | -0.1237 | -0.1394 | -0.2539 |
| 0.650 | -0.2725 | -0.1795 | -0.1424 | -0.1414 | -0.2567 |
| 0.675 | ******* | -0.2116 | -0.1529 | -0.1520 | -0.2460 |
| 0.700 | -0.2821 | -0.2369 | -0.1581 | -0.1619 | -0.2521 |
| 0.725 | ******* | -0.2387 | ******* | -0.1700 | -0.2587 |
| 0.750 | -0.3023 | -0.2773 | ******* | -0.1857 | -0.2704 |
| 0.775 | ******* | -0.3089 | -0.2133 | -0.2054 | -0.2672 |
| 0.800 | -0.3096 | -0.3266 | -0.2478 | -0.2291 | ******* |
| 0.825 | ******* | -0.3475 | -0.2887 | -0.2415 | -0.3136 |
| 0.850 | -0.3063 | -0.3693 | -0.3167 | -0.2719 | -0.3356 |
| 0.875 | ******* | -0.3957 | -0.3592 | -0.3120 | -0.4094 |
| 0.900 | -0.3004 | -0.4131 | -0.4000 | -0.3729 | ******* |
| 0.925 | ******* | -0.4158 | -0.4277 | -0.4127 | -0.9995 |
| 0.950 | -0.3241 | -0.4373 | -0.4530 | -0.4531 | -0.6408 |
| 0.975 | ******* | -0.4801 | -0.6838 | -0.7132 | -0.5366 |
| 1.000 | -0.7237 | -1.1068 | -0.9798 | -0.8585 | -0.9171 |
| | C_p,l | C_p,l | C_p,l | C_p,l | C_p,l |
| -0.200 | 0.0898 | 0.0993 | 0.1265 | ******* | -0.2943 |
| -0.400 | 0.0895 | 0.1002 | 0.0943 | -0.0301 | -0.3234 |
| -0.600 | 0.0945 | 0.1055 | 0.0895 | -0.0001 | -0.3725 |
| -0.700 | ******* | 0.0945 | 0.0979 | 0.0037 | -0.3879 |
| -0.800 | ******* | ******* | 0.0901 | 0.0193 | -0.3950 |
| -0.850 | ******* | 0.1290 | 0.0947 | 0.0325 | -0.4212 |
| -0.900 | 0.1792 | 0.1578 | 0.1232 | 0.0470 | -0.4899 |
| -0.950 | 0.1986 | 0.1270 | 0.1656 | 0.1097 | -0.2609 |
| -0.975 | ******* | 0.1827 | 0.1732 | 0.1468 | -0.0424 |
| -1.000 | -0.7514 | -1.0089 | -0.8655 | -0.7714 | -0.8173 |



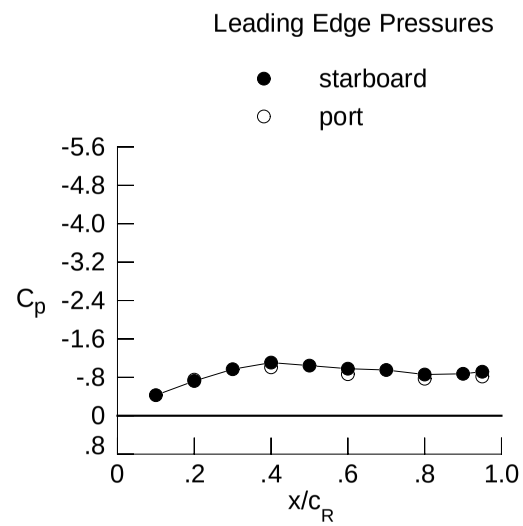

Small Radius L.E.

Run No. = 36 , Point No. = 720

$C_N$ = 0.188, $C_m$ = -0.0139

$\alpha$ = 6.2 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

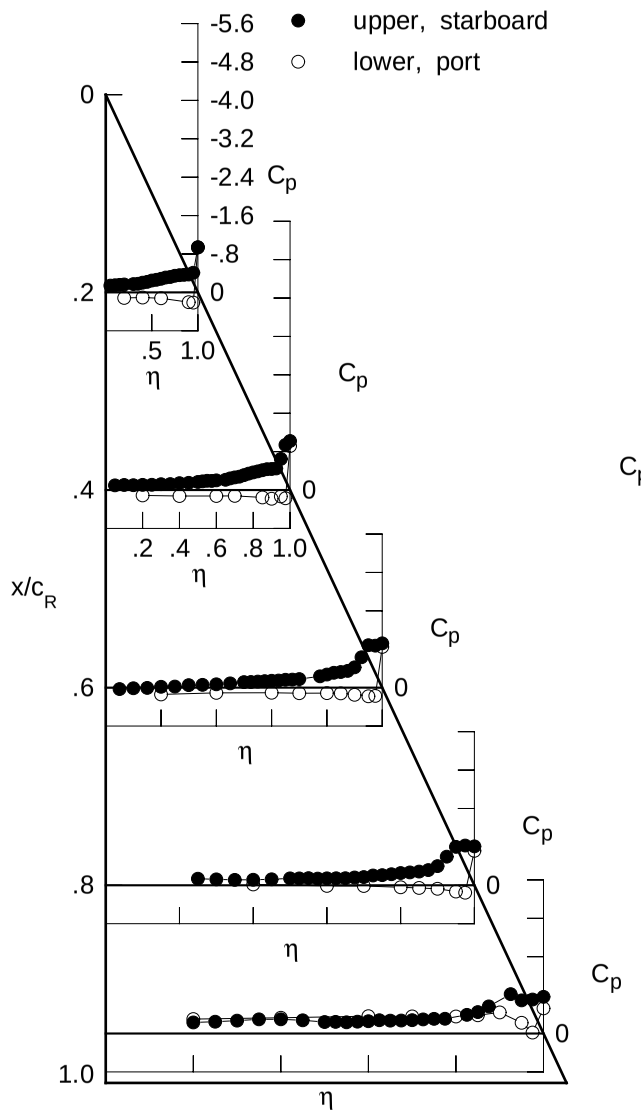



| x/c_R | starb'd C_p | port C_p |
|---|---|---|
| 0.10 | -0.4280 | ******* |
| 0.20 | -0.7237 | -0.7514 |
| 0.30 | -0.9686 | ******* |
| 0.40 | -1.1068 | -1.0089 |
| 0.50 | -1.0444 | ******* |
| 0.60 | -0.9798 | -0.8655 |
| 0.70 | -0.9526 | ******* |
| 0.80 | -0.8585 | -0.7714 |
| 0.90 | -0.8737 | ******* |
| 0.95 | -0.9171 | -0.8173 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1420 | -0.0976 | 0.0296 | ******* | ******* |
| 0.100 | -0.1488 | -0.1053 | 0.0131 | ******* | ******* |
| 0.150 | -0.1565 | -0.1010 | 0.0055 | ******* | ******* |
| 0.200 | -0.1648 | -0.1079 | -0.0173 | ******* | -0.2303 |
| 0.250 | ******* | -0.1099 | -0.0222 | -0.1371 | -0.2456 |
| 0.300 | -0.1730 | -0.1215 | -0.0521 | -0.1234 | -0.2682 |
| 0.350 | -0.1793 | -0.1243 | -0.0586 | -0.1131 | -0.2953 |
| 0.400 | -0.2024 | -0.1433 | -0.0698 | -0.1151 | -0.2960 |
| 0.450 | -0.2190 | -0.1501 | -0.0890 | -0.1251 | -0.2753 |
| 0.500 | -0.2475 | -0.1683 | -0.1149 | -0.1441 | -0.2392 |
| 0.525 | ******* | -0.1807 | -0.1175 | -0.1431 | -0.2424 |
| 0.550 | -0.2624 | -0.1931 | -0.1266 | -0.1487 | -0.2334 |
| 0.575 | ******* | -0.1892 | -0.1354 | -0.1389 | -0.2465 |
| 0.600 | -0.2831 | -0.2016 | -0.1434 | -0.1447 | -0.2557 |
| 0.625 | ******* | ******* | -0.1477 | -0.1460 | -0.2766 |
| 0.650 | -0.3095 | -0.2134 | -0.1640 | -0.1469 | -0.2683 |
| 0.675 | ******* | -0.2427 | -0.1670 | -0.1622 | -0.2701 |
| 0.700 | -0.3211 | -0.2634 | -0.1781 | -0.1715 | -0.2774 |
| 0.725 | ******* | -0.2782 | ******* | -0.2043 | -0.2935 |
| 0.750 | -0.3463 | -0.3105 | ******* | -0.2113 | -0.3059 |
| 0.775 | ******* | -0.3417 | -0.2362 | -0.2305 | -0.3075 |
| 0.800 | -0.3586 | -0.3673 | -0.2730 | -0.2555 | ******* |
| 0.825 | ******* | -0.3889 | -0.3098 | -0.2677 | -0.3889 |
| 0.850 | -0.3659 | -0.4125 | -0.3254 | -0.2856 | -0.4468 |
| 0.875 | ******* | -0.4343 | -0.3490 | -0.3170 | -0.5646 |
| 0.900 | -0.3719 | -0.4386 | -0.4229 | -0.3990 | ******* |
| 0.925 | ******* | -0.4497 | -0.6330 | -0.5963 | -0.8200 |
| 0.950 | -0.4096 | -0.6477 | -0.8843 | -0.8009 | -0.6903 |
| 0.975 | ******* | -0.9403 | -0.8745 | -0.8277 | -0.7083 |
| 1.000 | -0.9415 | -1.0215 | -0.9228 | -0.8115 | -0.7642 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1154 | 0.1123 | 0.1412 | ******* | -0.3005 |
| -0.400 | 0.1071 | 0.1245 | 0.1089 | -0.0176 | -0.3280 |
| -0.600 | 0.1226 | 0.1243 | 0.1066 | 0.0126 | -0.3611 |
| -0.700 | ******* | 0.1217 | 0.1162 | 0.0148 | -0.3564 |
| -0.800 | ******* | ******* | 0.1143 | 0.0416 | -0.3542 |
| -0.850 | ******* | 0.1542 | 0.1195 | 0.0553 | -0.3801 |
| -0.900 | 0.2039 | 0.1820 | 0.1488 | 0.0731 | -0.4395 |
| -0.950 | 0.2127 | 0.1328 | 0.1798 | 0.1302 | -0.2231 |
| -0.975 | ******* | 0.1709 | 0.1721 | 0.1542 | -0.0198 |
| -1.000 | -0.9356 | -0.9170 | -0.8479 | -0.7173 | -0.5239 |

Surface Pressures




Small Radius L.E.

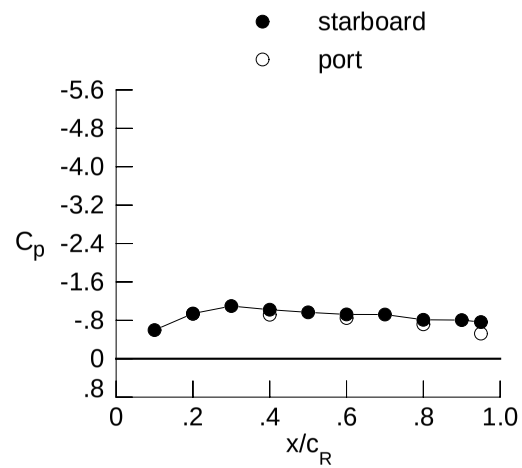
Run No. = 36 , Point No. = 721

$C_N$ = 0.237, $C_m$ = -0.0255

$\alpha$ = 7.2 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

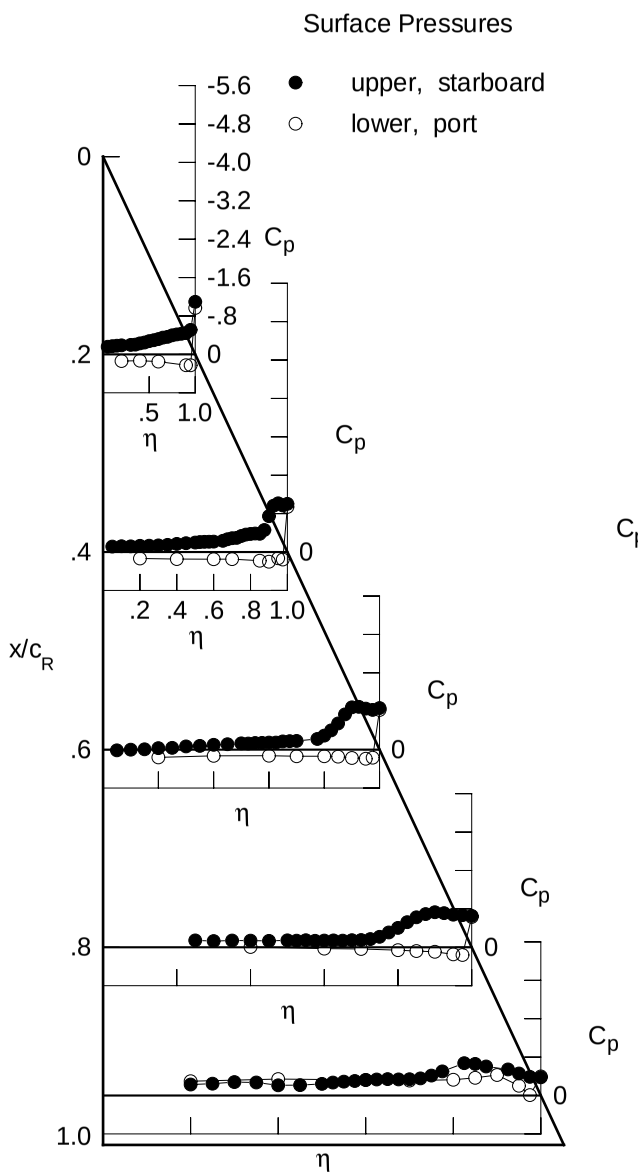
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.5971 | ******* |
| 0.20 | -0.9415 | -0.9356 |
| 0.30 | -1.0973 | ******* |
| 0.40 | -1.0215 | -0.9170 |
| 0.50 | -0.9661 | ******* |
| 0.60 | -0.9228 | -0.8479 |
| 0.70 | -0.9210 | ******* |
| 0.80 | -0.8115 | -0.7173 |
| 0.90 | -0.8050 | ******* |
| 0.95 | -0.7642 | -0.5239 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1596 | -0.1132 | 0.0145 | ******* | ******* |
| 0.100 | -0.1714 | -0.1206 | 0.0005 | ******* | ******* |
| 0.150 | -0.1811 | -0.1188 | -0.0071 | ******* | ******* |
| 0.200 | -0.1888 | -0.1298 | -0.0309 | ******* | -0.2284 |
| 0.250 | ******* | -0.1319 | -0.0377 | -0.1436 | -0.2466 |
| 0.300 | -0.1979 | -0.1384 | -0.0669 | -0.1293 | -0.2796 |
| 0.350 | -0.2030 | -0.1494 | -0.0782 | -0.1411 | -0.2711 |
| 0.400 | -0.2300 | -0.1695 | -0.1009 | -0.1383 | -0.2131 |
| 0.450 | -0.2473 | -0.1838 | -0.1125 | -0.1339 | -0.2160 |
| 0.500 | -0.2761 | -0.1977 | -0.1310 | -0.1444 | -0.2426 |
| 0.525 | ******* | -0.2082 | -0.1274 | -0.1379 | -0.2695 |
| 0.550 | -0.2954 | -0.2125 | -0.1385 | -0.1476 | -0.2889 |
| 0.575 | ******* | -0.2141 | -0.1404 | -0.1350 | -0.3024 |
| 0.600 | -0.3196 | -0.2164 | -0.1475 | -0.1401 | -0.3223 |
| 0.625 | ******* | ******* | -0.1473 | -0.1431 | -0.3338 |
| 0.650 | -0.3492 | -0.2337 | -0.1708 | -0.1384 | -0.3414 |
| 0.675 | ******* | -0.2665 | -0.1769 | -0.1482 | -0.3355 |
| 0.700 | -0.3658 | -0.2880 | -0.1816 | -0.1511 | -0.3392 |
| 0.725 | ******* | -0.2953 | ******* | -0.1709 | -0.3567 |
| 0.750 | -0.3976 | -0.3344 | ******* | -0.2182 | -0.4154 |
| 0.775 | ******* | -0.3637 | -0.2221 | -0.3089 | -0.5021 |
| 0.800 | -0.4159 | -0.3771 | -0.2921 | -0.4037 | ******* |
| 0.825 | ******* | -0.3852 | -0.4016 | -0.5233 | -0.6734 |
| 0.850 | -0.4293 | -0.3801 | -0.5454 | -0.6249 | -0.6583 |
| 0.875 | ******* | -0.4591 | -0.7342 | -0.6918 | -0.6050 |
| 0.900 | -0.4442 | -0.7469 | -0.8820 | -0.7304 | ******* |
| 0.925 | ******* | -0.9649 | -0.8923 | -0.7115 | -0.5434 |
| 0.950 | -0.5109 | -1.0156 | -0.8545 | -0.6788 | -0.4581 |
| 0.975 | ******* | -0.9704 | -0.8283 | -0.6697 | -0.3886 |
| 1.000 | -1.0949 | -1.0041 | -0.8661 | -0.6543 | -0.3792 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1385 | 0.1341 | 0.1614 | ******* | -0.2976 |
| -0.400 | 0.1314 | 0.1464 | 0.1289 | -0.0065 | -0.3427 |
| -0.600 | 0.1499 | 0.1493 | 0.1265 | 0.0278 | -0.3248 |
| -0.700 | ******* | 0.1477 | 0.1373 | 0.0352 | -0.3110 |
| -0.800 | ******* | ******* | 0.1373 | 0.0602 | -0.3278 |
| -0.850 | ******* | 0.1806 | 0.1454 | 0.0786 | -0.3689 |
| -0.900 | 0.2254 | 0.2015 | 0.1734 | 0.0936 | -0.4272 |
| -0.950 | 0.2261 | 0.1294 | 0.1896 | 0.1472 | -0.2033 |
| -0.975 | ******* | 0.1558 | 0.1668 | 0.1600 | -0.0089 |
| -1.000 | -0.9678 | -0.9396 | -0.8266 | -0.6316 | -0.3975 |



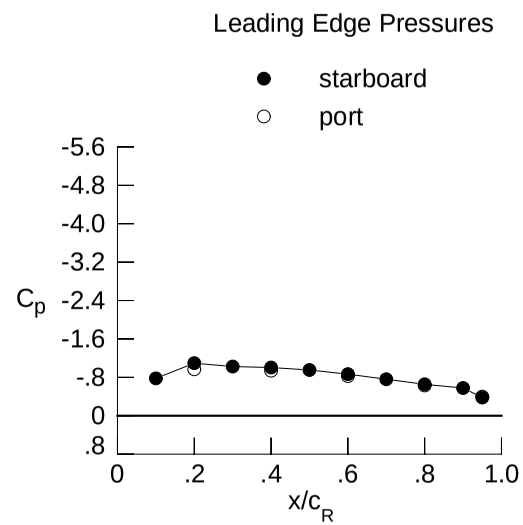

Small Radius L.E.

Run No. = 36 , Point No. = 722

$C_N$ = 0.292, $C_m$ = -0.0364

$\alpha$ = 8.3 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

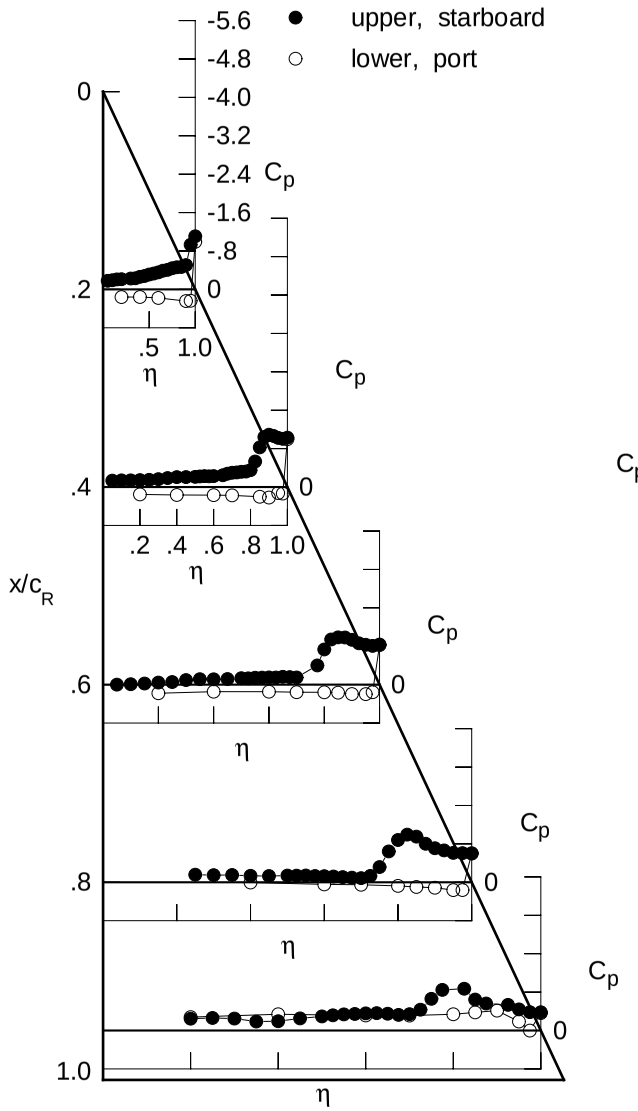



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.7781 | ******* |
| 0.20 | -1.0949 | -0.9678 |
| 0.30 | -1.0245 | ******* |
| 0.40 | -1.0041 | -0.9396 |
| 0.50 | -0.9526 | ******* |
| 0.60 | -0.8661 | -0.8266 |
| 0.70 | -0.7603 | ******* |
| 0.80 | -0.6543 | -0.6316 |
| 0.90 | -0.5775 | ******* |
| 0.95 | -0.3792 | -0.3975 |

# Table D1. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1796 | -0.1337 | -0.0004 | ******* | ******* |
| 0.100 | -0.1906 | -0.1388 | -0.0088 | ******* | ******* |
| 0.150 | -0.2080 | -0.1389 | -0.0234 | ******* | ******* |
| 0.200 | -0.2118 | -0.1449 | -0.0428 | ******* | -0.2466 |
| 0.250 | ******* | -0.1506 | -0.0546 | -0.1585 | -0.2612 |
| 0.300 | -0.2263 | -0.1637 | -0.0953 | -0.1486 | -0.2489 |
| 0.350 | -0.2313 | -0.1870 | -0.1135 | -0.1519 | -0.1875 |
| 0.400 | -0.2616 | -0.2060 | -0.1110 | -0.1349 | -0.1936 |
| 0.450 | -0.2791 | -0.2074 | -0.1170 | -0.1302 | -0.2524 |
| 0.500 | -0.3099 | -0.2121 | -0.1340 | -0.1397 | -0.2934 |
| 0.525 | ******* | -0.2209 | -0.1312 | -0.1386 | -0.3169 |
| 0.550 | -0.3306 | -0.2271 | -0.1441 | -0.1414 | -0.3360 |
| 0.575 | ******* | -0.2233 | -0.1467 | -0.1307 | -0.3444 |
| 0.600 | -0.3550 | -0.2280 | -0.1503 | -0.1272 | -0.3566 |
| 0.625 | ******* | ******* | -0.1492 | -0.1201 | -0.3612 |
| 0.650 | -0.3898 | -0.2456 | -0.1628 | -0.1082 | -0.3498 |
| 0.675 | ******* | -0.2776 | -0.1567 | -0.0970 | -0.3256 |
| 0.700 | -0.4068 | -0.2978 | -0.1499 | -0.0868 | -0.3399 |
| 0.725 | ******* | -0.3037 | ******* | -0.1331 | -0.4340 |
| 0.750 | -0.4409 | -0.3172 | ******* | -0.3173 | -0.6601 |
| 0.775 | ******* | -0.3221 | -0.4001 | -0.6433 | -0.8466 |
| 0.800 | -0.4612 | -0.3523 | -0.7330 | -0.8808 | ******* |
| 0.825 | ******* | -0.5317 | -0.9410 | -0.9929 | -0.8706 |
| 0.850 | -0.4671 | -0.8261 | -0.9845 | -0.9509 | -0.6452 |
| 0.875 | ******* | -1.0414 | -0.9825 | -0.8027 | -0.5627 |
| 0.900 | -0.5074 | -1.0901 | -0.9340 | -0.7096 | ******* |
| 0.925 | ******* | -1.0639 | -0.8613 | -0.6637 | -0.5343 |
| 0.950 | -0.9308 | -1.0244 | -0.8302 | -0.6130 | -0.4397 |
| 0.975 | ******* | -1.0042 | -0.8073 | -0.6071 | -0.3827 |
| 1.000 | -1.1067 | -1.0290 | -0.8349 | -0.5990 | -0.3807 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1597 | 0.1537 | 0.1793 | ******* | -0.2793 |
| -0.400 | 0.1584 | 0.1655 | 0.1464 | 0.0052 | -0.3386 |
| -0.600 | 0.1781 | 0.1688 | 0.1468 | 0.0436 | -0.3134 |
| -0.700 | ******* | 0.1737 | 0.1580 | 0.0516 | -0.3113 |
| -0.800 | ******* | ******* | 0.1595 | 0.0754 | -0.3386 |
| -0.850 | ******* | 0.2023 | 0.1674 | 0.0978 | -0.3776 |
| -0.900 | 0.2435 | 0.2190 | 0.1963 | 0.1137 | -0.4147 |
| -0.950 | 0.2365 | 0.1247 | 0.1979 | 0.1622 | -0.1869 |
| -0.975 | ******* | 0.1358 | 0.1578 | 0.1615 | 0.0016 |
| -1.000 | -0.9914 | -0.9964 | -0.8237 | -0.6050 | -0.3629 |

Surface Pressures




Small Radius L.E.

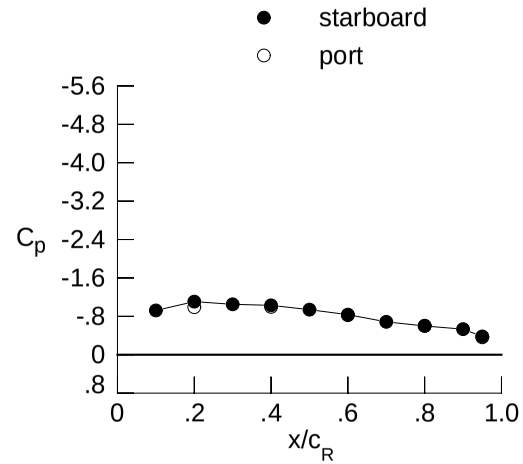
Run No. = 36 , Point No. = 723

$C_N$ = 0.344, $C_m$ = -0.0428

$\alpha$ = 9.3 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

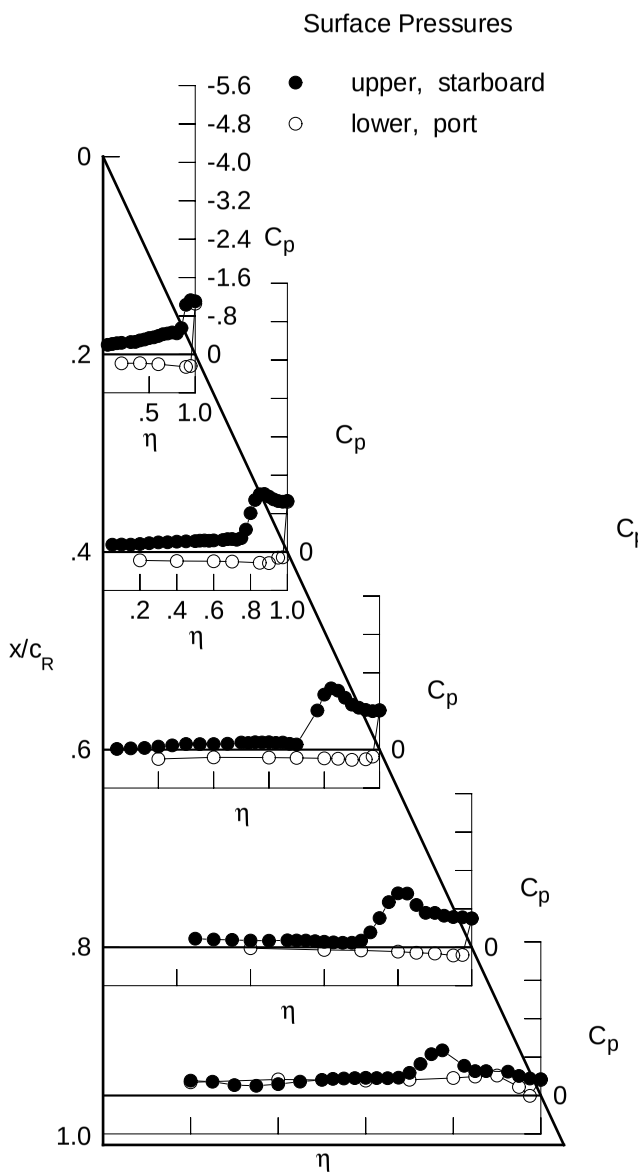
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.9222 | ******* |
| 0.20 | -1.1067 | -0.9914 |
| 0.30 | -1.0502 | ******* |
| 0.40 | -1.0290 | -0.9964 |
| 0.50 | -0.9388 | ******* |
| 0.60 | -0.8349 | -0.8237 |
| 0.70 | -0.6853 | ******* |
| 0.80 | -0.5990 | -0.6050 |
| 0.90 | -0.5326 | ******* |
| 0.95 | -0.3807 | -0.3629 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1992 | -0.1530 | -0.0142 | ******* | ******* |
| 0.100 | -0.2165 | -0.1559 | -0.0265 | ******* | ******* |
| 0.150 | -0.2330 | -0.1535 | -0.0356 | ******* | ******* |
| 0.200 | -0.2410 | -0.1671 | -0.0630 | ******* | -0.3097 |
| 0.250 | ******* | -0.1840 | -0.0887 | -0.1793 | -0.2872 |
| 0.300 | -0.2566 | -0.2006 | -0.1180 | -0.1621 | -0.2170 |
| 0.350 | -0.2599 | -0.2036 | -0.1152 | -0.1543 | -0.2026 |
| 0.400 | -0.2910 | -0.2160 | -0.1160 | -0.1399 | -0.2370 |
| 0.450 | -0.3108 | -0.2222 | -0.1233 | -0.1370 | -0.2886 |
| 0.500 | -0.3399 | -0.2275 | -0.1480 | -0.1453 | -0.3254 |
| 0.525 | ******* | -0.2370 | -0.1381 | -0.1413 | -0.3464 |
| 0.550 | -0.3554 | -0.2409 | -0.1544 | -0.1401 | -0.3548 |
| 0.575 | ******* | -0.2347 | -0.1493 | -0.1271 | -0.3623 |
| 0.600 | -0.3844 | -0.2426 | -0.1547 | -0.1153 | -0.3686 |
| 0.625 | ******* | ******* | -0.1402 | -0.1021 | -0.3636 |
| 0.650 | -0.4201 | -0.2495 | -0.1470 | -0.0938 | -0.3608 |
| 0.675 | ******* | -0.2690 | -0.1209 | -0.0942 | -0.3712 |
| 0.700 | -0.4348 | -0.2708 | -0.1074 | -0.1393 | -0.4723 |
| 0.725 | ******* | -0.2560 | ******* | -0.3103 | -0.6565 |
| 0.750 | -0.4571 | -0.2908 | ******* | -0.6091 | -0.8609 |
| 0.775 | ******* | -0.4682 | -0.8158 | -0.9404 | -0.9405 |
| 0.800 | -0.4387 | -0.8099 | -1.1463 | -1.1242 | ******* |
| 0.825 | ******* | -1.0852 | -1.2770 | -1.1192 | -0.6195 |
| 0.850 | -0.5489 | -1.2034 | -1.2281 | -0.8819 | -0.5080 |
| 0.875 | ******* | -1.2097 | -1.0819 | -0.7174 | -0.5080 |
| 0.900 | -1.0327 | -1.1537 | -0.9378 | -0.7162 | ******* |
| 0.925 | ******* | -1.0974 | -0.8737 | -0.6575 | -0.4967 |
| 0.950 | -1.1288 | -1.0628 | -0.8268 | -0.6298 | -0.4072 |
| 0.975 | ******* | -1.0479 | -0.8014 | -0.6241 | -0.3539 |
| 1.000 | -1.1052 | -1.0653 | -0.8130 | -0.6024 | -0.3398 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1866 | 0.1740 | 0.1942 | ******* | -0.2749 |
| -0.400 | 0.1832 | 0.1873 | 0.1609 | 0.0195 | -0.3348 |
| -0.600 | 0.2036 | 0.1917 | 0.1653 | 0.0553 | -0.3107 |
| -0.700 | ******* | 0.1989 | 0.1718 | 0.0647 | -0.3277 |
| -0.800 | ******* | ******* | 0.1813 | 0.0906 | -0.3646 |
| -0.850 | ******* | 0.2238 | 0.1894 | 0.1145 | -0.3949 |
| -0.900 | 0.2606 | 0.2314 | 0.2125 | 0.1293 | -0.4160 |
| -0.950 | 0.2416 | 0.1178 | 0.2006 | 0.1707 | -0.1782 |
| -0.975 | ******* | 0.1105 | 0.1443 | 0.1593 | 0.0071 |
| -1.000 | -1.0568 | -1.0459 | -0.8229 | -0.5975 | -0.3242 |



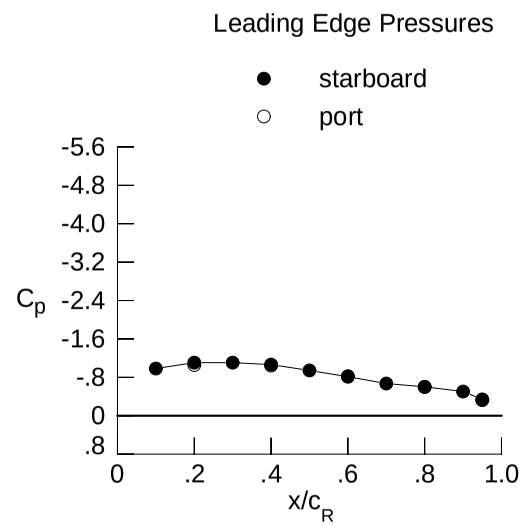

Small Radius L.E.

Run No. = 36 , Point No. = 724

$C_N$ = 0.404, $C_m$ = -0.0568

$\alpha$ = 10.3 °, $M_\infty$ = 0.398

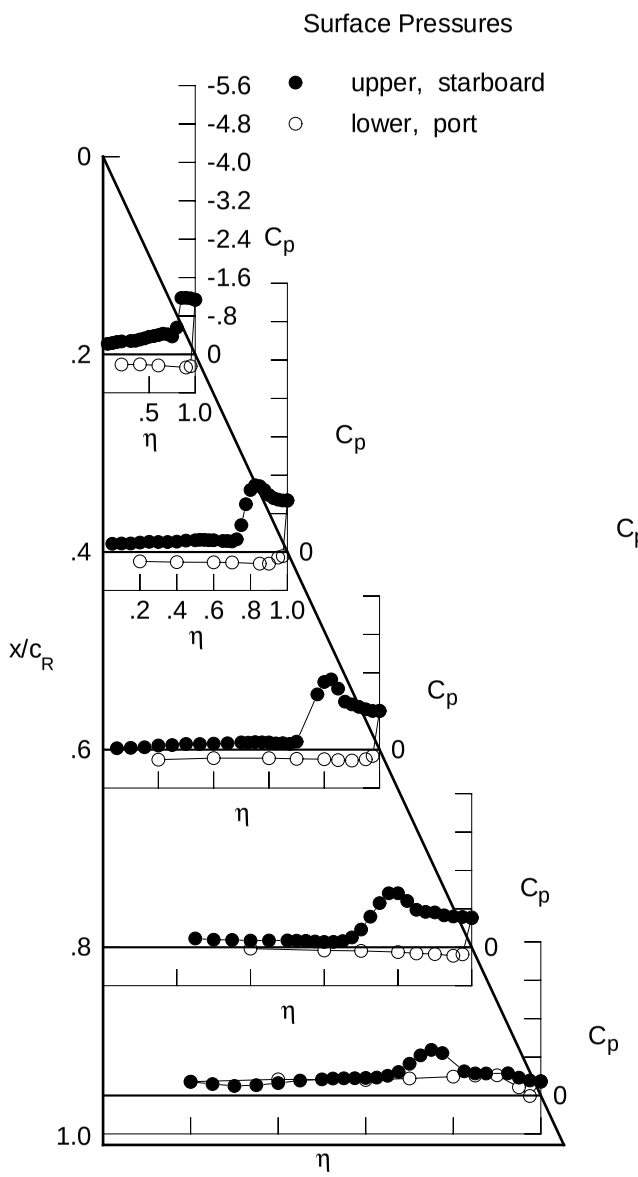
$R_{mac}$ = $5.8 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.9834 | ******* |
| 0.20 | -1.1052 | -1.0568 |
| 0.30 | -1.1056 | ******* |
| 0.40 | -1.0653 | -1.0459 |
| 0.50 | -0.9432 | ******* |
| 0.60 | -0.8130 | -0.8229 |
| 0.70 | -0.6708 | ******* |
| 0.80 | -0.6024 | -0.5975 |
| 0.90 | -0.5043 | ******* |
| 0.95 | -0.3398 | -0.3242 |

# Table D1. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2188 | -0.1723 | -0.0285 | ******* | ******* |
| 0.100 | -0.2358 | -0.1776 | -0.0380 | ******* | ******* |
| 0.150 | -0.2588 | -0.1783 | -0.0494 | ******* | ******* |
| 0.200 | -0.2700 | -0.1971 | -0.0863 | ******* | -0.2854 |
| 0.250 | ******* | -0.2127 | -0.0954 | -0.1833 | -0.2384 |
| 0.300 | -0.2788 | -0.2085 | -0.1182 | -0.1577 | -0.1992 |
| 0.350 | -0.2843 | -0.2086 | -0.1169 | -0.1535 | -0.2154 |
| 0.400 | -0.3104 | -0.2171 | -0.1248 | -0.1393 | -0.2587 |
| 0.450 | -0.3337 | -0.2380 | -0.1329 | -0.1417 | -0.3116 |
| 0.500 | -0.3668 | -0.2449 | -0.1513 | -0.1429 | -0.3360 |
| 0.525 | ******* | -0.2549 | -0.1458 | -0.1379 | -0.3539 |
| 0.550 | -0.3813 | -0.2530 | -0.1565 | -0.1342 | -0.3584 |
| 0.575 | ******* | -0.2460 | -0.1518 | -0.1205 | -0.3601 |
| 0.600 | -0.4026 | -0.2456 | -0.1505 | -0.1115 | -0.3666 |
| 0.625 | ******* | ******* | -0.1296 | -0.1126 | -0.3739 |
| 0.650 | -0.4310 | -0.2296 | -0.1345 | -0.1286 | -0.4108 |
| 0.675 | ******* | -0.2294 | -0.1195 | -0.2048 | -0.4905 |
| 0.700 | -0.4184 | -0.2210 | -0.1661 | -0.3694 | -0.6620 |
| 0.725 | ******* | -0.2653 | ******* | -0.6378 | -0.8363 |
| 0.750 | -0.3733 | -0.5604 | ******* | -0.9200 | -0.9507 |
| 0.775 | ******* | -0.9957 | -1.1511 | -1.1249 | -0.8840 |
| 0.800 | -0.5583 | -1.2928 | -1.4098 | -1.1253 | ******* |
| 0.825 | ******* | -1.3916 | -1.4628 | -0.9646 | -0.5039 |
| 0.850 | -1.1757 | -1.3714 | -1.2711 | -0.7819 | -0.4602 |
| 0.875 | ******* | -1.2917 | -1.0003 | -0.7377 | -0.4585 |
| 0.900 | -1.1795 | -1.1869 | -0.9424 | -0.7261 | ******* |
| 0.925 | ******* | -1.1234 | -0.8921 | -0.6657 | -0.4634 |
| 0.950 | -1.1683 | -1.0915 | -0.8406 | -0.6416 | -0.3722 |
| 0.975 | ******* | -1.0734 | -0.8056 | -0.6316 | -0.3132 |
| 1.000 | -1.1406 | -1.0790 | -0.8102 | -0.6055 | -0.3003 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2111 | 0.1952 | 0.2086 | ******* | -0.2881 |
| -0.400 | 0.2084 | 0.2107 | 0.1765 | 0.0280 | -0.3361 |
| -0.600 | 0.2305 | 0.2145 | 0.1781 | 0.0661 | -0.3229 |
| -0.700 | ******* | 0.2174 | 0.1918 | 0.0751 | -0.3549 |
| -0.800 | ******* | ******* | 0.1989 | 0.0997 | -0.3928 |
| -0.850 | ******* | 0.2420 | 0.2183 | 0.1279 | -0.4159 |
| -0.900 | 0.2727 | 0.2421 | 0.2273 | 0.1415 | -0.4215 |
| -0.950 | 0.2464 | 0.1150 | 0.2009 | 0.1769 | -0.1713 |
| -0.975 | ******* | 0.0844 | 0.1310 | 0.1465 | 0.0107 |
| -1.000 | -1.1348 | -1.0685 | -0.8035 | -0.6241 | -0.2846 |



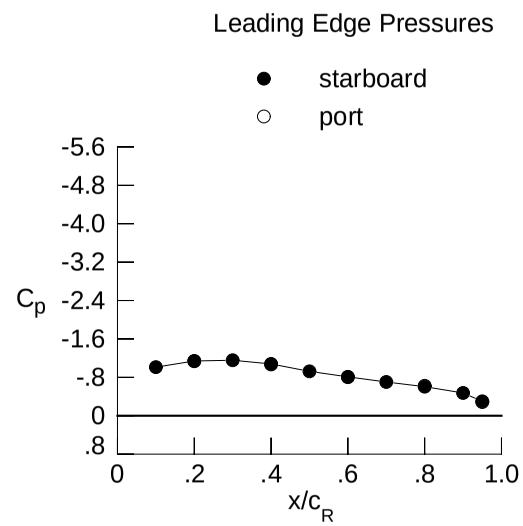

Small Radius L.E.

Run No. = 36 , Point No. = 725

$C_N$ = 0.438, $C_m$ = -0.0532

$\alpha$ = 11.3 °, $M_\infty$ = 0.399

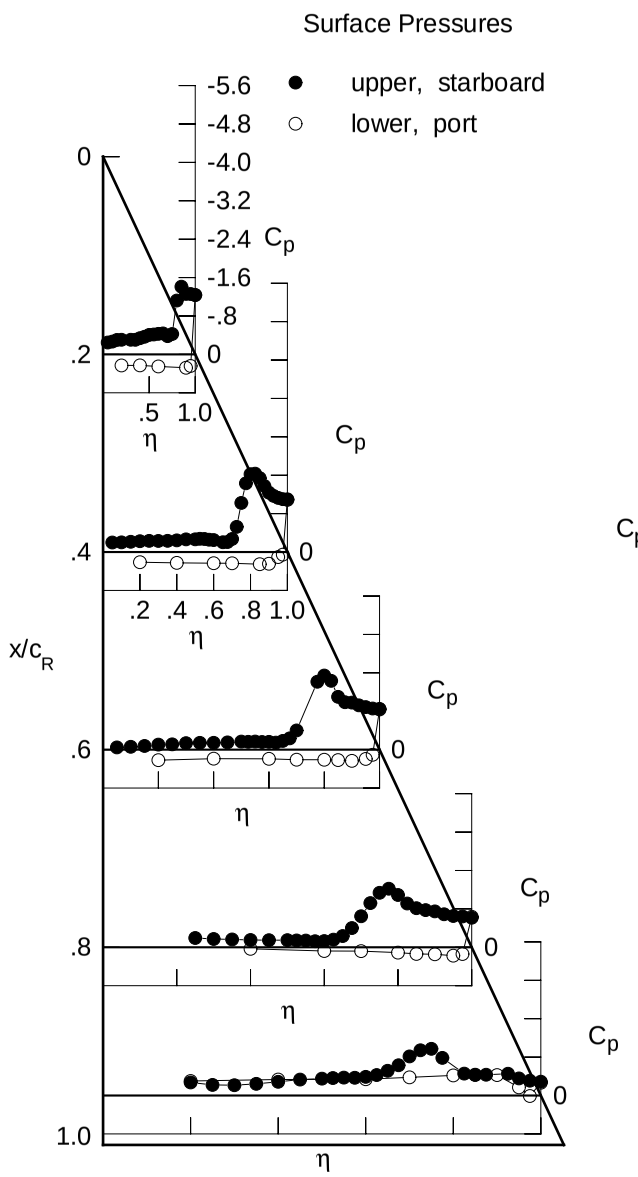
$R_{mac}$ = $5.8 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0119 | ******* |
| 0.20 | -1.1406 | -1.1348 |
| 0.30 | -1.1559 | ******* |
| 0.40 | -1.0790 | -1.0685 |
| 0.50 | -0.9247 | ******* |
| 0.60 | -0.8102 | -0.8035 |
| 0.70 | -0.7028 | ******* |
| 0.80 | -0.6055 | -0.6241 |
| 0.90 | -0.4741 | ******* |
| 0.95 | -0.3003 | -0.2846 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2472 | -0.1988 | -0.0461 | ******* | ******* |
| 0.100 | -0.2660 | -0.2013 | -0.0592 | ******* | ******* |
| 0.150 | -0.3011 | -0.2137 | -0.0769 | ******* | ******* |
| 0.200 | -0.3051 | -0.2258 | -0.1049 | ******* | -0.2722 |
| 0.250 | ******* | -0.2325 | -0.1106 | -0.1939 | -0.2209 |
| 0.300 | -0.3050 | -0.2310 | -0.1353 | -0.1731 | -0.2145 |
| 0.350 | -0.3040 | -0.2336 | -0.1415 | -0.1635 | -0.2434 |
| 0.400 | -0.3379 | -0.2431 | -0.1427 | -0.1524 | -0.2855 |
| 0.450 | -0.3672 | -0.2642 | -0.1511 | -0.1479 | -0.3320 |
| 0.500 | -0.4053 | -0.2648 | -0.1684 | -0.1491 | -0.3511 |
| 0.525 | ******* | -0.2757 | -0.1633 | -0.1424 | -0.3640 |
| 0.550 | -0.4140 | -0.2717 | -0.1689 | -0.1398 | -0.3727 |
| 0.575 | ******* | -0.2566 | -0.1595 | -0.1261 | -0.3698 |
| 0.600 | -0.4278 | -0.2495 | -0.1622 | -0.1293 | -0.3887 |
| 0.625 | ******* | ******* | -0.1467 | -0.1596 | -0.4262 |
| 0.650 | -0.4366 | -0.2040 | -0.1817 | -0.2348 | -0.5154 |
| 0.675 | ******* | -0.2085 | -0.2354 | -0.4008 | -0.6305 |
| 0.700 | -0.3798 | -0.2720 | -0.4004 | -0.6466 | -0.8141 |
| 0.725 | ******* | -0.5251 | ******* | -0.9209 | -0.9426 |
| 0.750 | -0.4248 | -1.0232 | ******* | -1.1352 | -0.9725 |
| 0.775 | ******* | -1.4321 | -1.4141 | -1.2198 | -0.7838 |
| 0.800 | -1.1214 | -1.6215 | -1.5439 | -1.0893 | ******* |
| 0.825 | ******* | -1.6332 | -1.4333 | -0.9123 | -0.4562 |
| 0.850 | -1.4101 | -1.5399 | -1.0996 | -0.8147 | -0.4277 |
| 0.875 | ******* | -1.3757 | -0.9877 | -0.7746 | -0.4324 |
| 0.900 | -1.2604 | -1.2370 | -0.9801 | -0.7483 | ******* |
| 0.925 | ******* | -1.1705 | -0.9234 | -0.6879 | -0.4534 |
| 0.950 | -1.2581 | -1.1283 | -0.8866 | -0.6520 | -0.3562 |
| 0.975 | ******* | -1.1018 | -0.8570 | -0.6425 | -0.3089 |
| 1.000 | -1.2370 | -1.0980 | -0.8486 | -0.6160 | -0.2881 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2300 | 0.2124 | 0.2195 | ******* | -0.3023 |
| -0.400 | 0.2291 | 0.2258 | 0.1883 | 0.0323 | -0.3331 |
| -0.600 | 0.2515 | 0.2326 | 0.1915 | 0.0773 | -0.3388 |
| -0.700 | ******* | 0.2341 | 0.2099 | 0.0797 | -0.3785 |
| -0.800 | ******* | ******* | 0.2101 | 0.1109 | -0.4187 |
| -0.850 | ******* | 0.2535 | 0.2180 | 0.1381 | -0.4338 |
| -0.900 | 0.2781 | 0.2444 | 0.2333 | 0.1458 | -0.4256 |
| -0.950 | 0.2411 | 0.1047 | 0.1938 | 0.1745 | -0.1698 |
| -0.975 | ******* | 0.0541 | 0.1069 | 0.1403 | 0.0102 |
| -1.000 | -1.2364 | -1.0865 | -0.8369 | -0.6362 | -0.2664 |



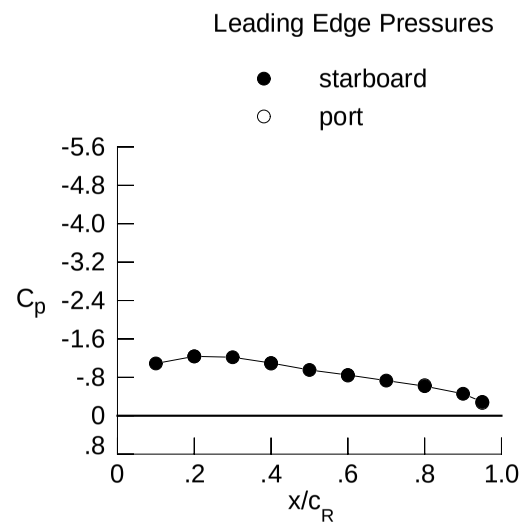

Small Radius L.E.

Run No. = 36 , Point No. = 726

$C_N$ = 0.480, $C_m$ = -0.0520

$\alpha$ = 12.3 °, $M_\infty$ = 0.398

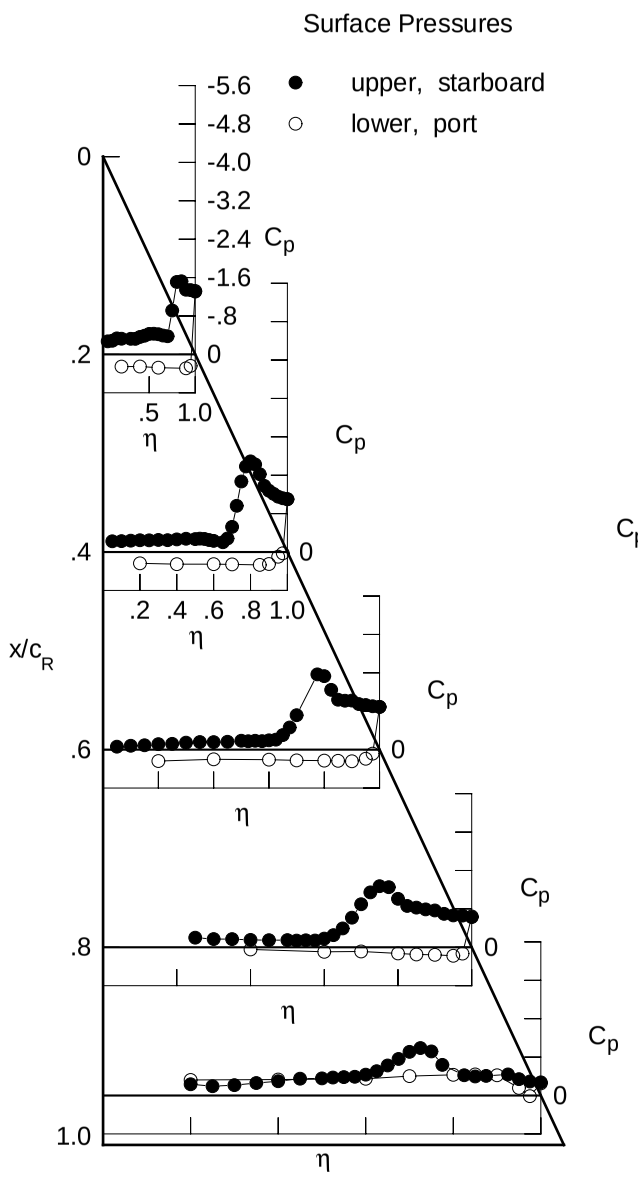
$R_{mac}$ = $5.8 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0885 | ******* |
| 0.20 | -1.2370 | -1.2364 |
| 0.30 | -1.2187 | ******* |
| 0.40 | -1.0980 | -1.0865 |
| 0.50 | -0.9536 | ******* |
| 0.60 | -0.8486 | -0.8369 |
| 0.70 | -0.7324 | ******* |
| 0.80 | -0.6160 | -0.6362 |
| 0.90 | -0.4577 | ******* |
| 0.95 | -0.2881 | -0.2664 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2723 | -0.2241 | -0.0614 | ******* | ******* |
| 0.100 | -0.2844 | -0.2274 | -0.0807 | ******* | ******* |
| 0.150 | -0.3338 | -0.2365 | -0.0916 | ******* | ******* |
| 0.200 | -0.3266 | -0.2460 | -0.1147 | ******* | -0.2347 |
| 0.250 | ******* | -0.2443 | -0.1211 | -0.1998 | -0.1939 |
| 0.300 | -0.3244 | -0.2521 | -0.1459 | -0.1714 | -0.2158 |
| 0.350 | -0.3239 | -0.2472 | -0.1584 | -0.1703 | -0.2598 |
| 0.400 | -0.3634 | -0.2635 | -0.1568 | -0.1537 | -0.2972 |
| 0.450 | -0.3888 | -0.2767 | -0.1641 | -0.1481 | -0.3506 |
| 0.500 | -0.4262 | -0.2697 | -0.1852 | -0.1496 | -0.3571 |
| 0.525 | ******* | -0.2792 | -0.1751 | -0.1391 | -0.3742 |
| 0.550 | -0.4306 | -0.2729 | -0.1850 | -0.1455 | -0.3835 |
| 0.575 | ******* | -0.2505 | -0.1767 | -0.1408 | -0.3905 |
| 0.600 | -0.4203 | -0.2326 | -0.1941 | -0.1807 | -0.4347 |
| 0.625 | ******* | ******* | -0.2080 | -0.2530 | -0.5063 |
| 0.650 | -0.3930 | -0.2039 | -0.3032 | -0.3924 | -0.6257 |
| 0.675 | ******* | -0.2821 | -0.4615 | -0.6165 | -0.7613 |
| 0.700 | -0.3783 | -0.5246 | -0.7177 | -0.8969 | -0.9097 |
| 0.725 | ******* | -0.9634 | ******* | -1.1438 | -0.9891 |
| 0.750 | -0.9147 | -1.4699 | ******* | -1.2731 | -0.9185 |
| 0.775 | ******* | -1.7833 | -1.5680 | -1.2518 | -0.6384 |
| 0.800 | -1.5090 | -1.8885 | -1.5311 | -1.0098 | ******* |
| 0.825 | ******* | -1.8247 | -1.2454 | -0.8620 | -0.4225 |
| 0.850 | -1.5235 | -1.6216 | -1.0400 | -0.8261 | -0.3964 |
| 0.875 | ******* | -1.3782 | -1.0192 | -0.7895 | -0.4086 |
| 0.900 | -1.3472 | -1.2775 | -1.0228 | -0.7676 | ******* |
| 0.925 | ******* | -1.2130 | -0.9499 | -0.6969 | -0.4394 |
| 0.950 | -1.3389 | -1.1529 | -0.9293 | -0.6639 | -0.3406 |
| 0.975 | ******* | -1.1206 | -0.9039 | -0.6599 | -0.2920 |
| 1.000 | -1.3081 | -1.1016 | -0.8911 | -0.6288 | -0.2746 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2541 | 0.2349 | 0.2377 | ******* | -0.3238 |
| -0.400 | 0.2527 | 0.2528 | 0.2014 | 0.0447 | -0.3324 |
| -0.600 | 0.2772 | 0.2528 | 0.2091 | 0.0942 | -0.3485 |
| -0.700 | ******* | 0.2574 | 0.2238 | 0.0873 | -0.4043 |
| -0.800 | ******* | ******* | 0.2285 | 0.1278 | -0.4310 |
| -0.850 | ******* | 0.2684 | 0.2326 | 0.1499 | -0.4392 |
| -0.900 | 0.2899 | 0.2495 | 0.2425 | 0.1567 | -0.4220 |
| -0.950 | 0.2388 | 0.0976 | 0.1892 | 0.1770 | -0.1574 |
| -0.975 | ******* | 0.0268 | 0.0831 | 0.1313 | 0.0138 |
| -1.000 | -1.3217 | -1.0993 | -0.8889 | -0.6436 | -0.2528 |



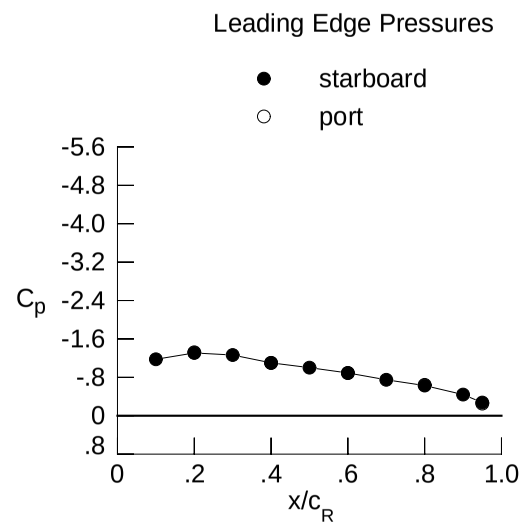

Small Radius L.E.

Run No. = 36 , Point No. = 727

$C_N$ = 0.530, $C_m$ = -0.0591

$\alpha$ = 13.3 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

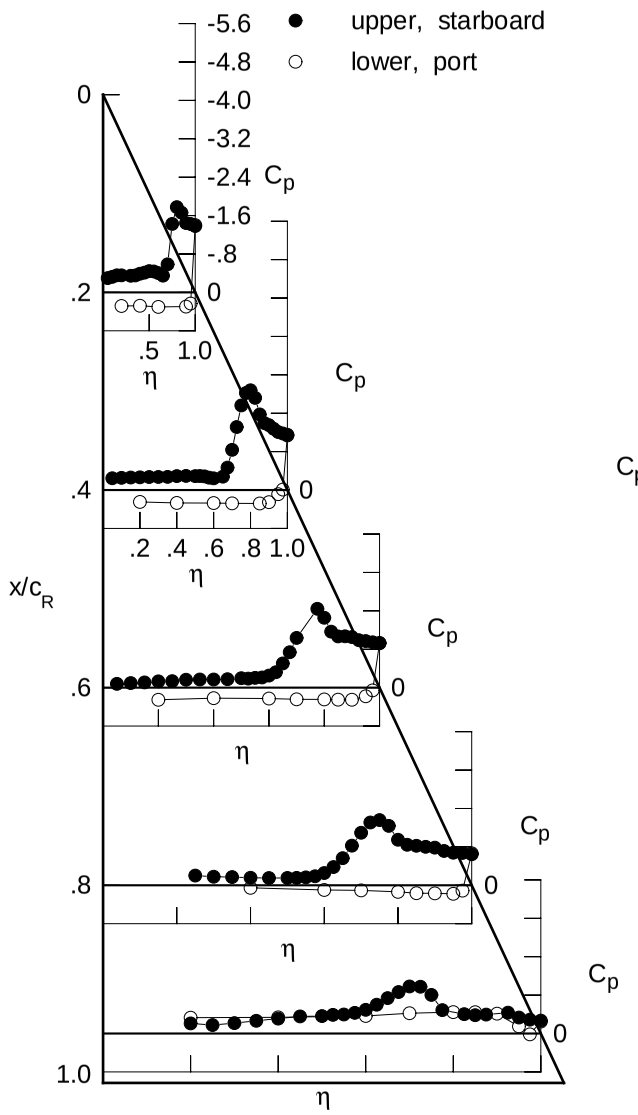



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1758 | ******* |
| 0.20 | -1.3081 | -1.3217 |
| 0.30 | -1.2648 | ******* |
| 0.40 | -1.1016 | -1.0993 |
| 0.50 | -1.0015 | ******* |
| 0.60 | -0.8911 | -0.8889 |
| 0.70 | -0.7488 | ******* |
| 0.80 | -0.6288 | -0.6436 |
| 0.90 | -0.4407 | ******* |
| 0.95 | -0.2746 | -0.2528 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2973 | -0.2453 | -0.0789 | ******* | ******* |
| 0.100 | -0.3242 | -0.2542 | -0.0949 | ******* | ******* |
| 0.150 | -0.3556 | -0.2606 | -0.1090 | ******* | ******* |
| 0.200 | -0.3549 | -0.2647 | -0.1312 | ******* | -0.2104 |
| 0.250 | ******* | -0.2710 | -0.1355 | -0.2025 | -0.1763 |
| 0.300 | -0.3467 | -0.2726 | -0.1647 | -0.1780 | -0.2165 |
| 0.350 | -0.3529 | -0.2747 | -0.1692 | -0.1715 | -0.2649 |
| 0.400 | -0.3885 | -0.2900 | -0.1698 | -0.1565 | -0.3107 |
| 0.450 | -0.4112 | -0.2948 | -0.1761 | -0.1513 | -0.3562 |
| 0.500 | -0.4433 | -0.2898 | -0.1971 | -0.1525 | -0.3629 |
| 0.525 | ******* | -0.2917 | -0.1880 | -0.1547 | -0.3887 |
| 0.550 | -0.4362 | -0.2848 | -0.2044 | -0.1648 | -0.3961 |
| 0.575 | ******* | -0.2576 | -0.2123 | -0.1877 | -0.4308 |
| 0.600 | -0.4016 | -0.2437 | -0.2513 | -0.2555 | -0.4939 |
| 0.625 | ******* | ******* | -0.3207 | -0.3802 | -0.6004 |
| 0.650 | -0.3484 | -0.2788 | -0.5044 | -0.5645 | -0.7379 |
| 0.675 | ******* | -0.4668 | -0.7375 | -0.8256 | -0.8638 |
| 0.700 | -0.5845 | -0.8377 | -1.0356 | -1.0947 | -0.9803 |
| 0.725 | ******* | -1.3126 | ******* | -1.3080 | -0.9741 |
| 0.750 | -1.4261 | -1.7624 | ******* | -1.3588 | -0.8038 |
| 0.775 | ******* | -2.0215 | -1.6424 | -1.2374 | -0.4874 |
| 0.800 | -1.7762 | -2.0782 | -1.4562 | -0.9488 | ******* |
| 0.825 | ******* | -1.9196 | -1.1665 | -0.8436 | -0.4035 |
| 0.850 | -1.6616 | -1.5751 | -1.0674 | -0.8231 | -0.3813 |
| 0.875 | ******* | -1.3950 | -1.0696 | -0.8017 | -0.3944 |
| 0.900 | -1.4446 | -1.3510 | -1.0539 | -0.7838 | ******* |
| 0.925 | ******* | -1.2772 | -0.9888 | -0.7156 | -0.4344 |
| 0.950 | -1.4246 | -1.2087 | -0.9703 | -0.6781 | -0.3326 |
| 0.975 | ******* | -1.1784 | -0.9448 | -0.6737 | -0.2884 |
| 1.000 | -1.3825 | -1.1513 | -0.9250 | -0.6464 | -0.2687 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2836 | 0.2482 | 0.2524 | ******* | -0.3299 |
| -0.400 | 0.2783 | 0.2691 | 0.2193 | 0.0530 | -0.3370 |
| -0.600 | 0.3023 | 0.2714 | 0.2268 | 0.0976 | -0.3654 |
| -0.700 | ******* | 0.2777 | 0.2428 | 0.1063 | -0.4225 |
| -0.800 | ******* | ******* | 0.2455 | 0.1366 | -0.4455 |
| -0.850 | ******* | 0.2797 | 0.2508 | 0.1648 | -0.4443 |
| -0.900 | 0.2957 | 0.2530 | 0.2518 | 0.1677 | -0.4136 |
| -0.950 | 0.2324 | 0.0868 | 0.1802 | 0.1779 | -0.1478 |
| -0.975 | ******* | -0.0094 | 0.0572 | 0.1113 | 0.0177 |
| -1.000 | -1.4023 | -1.1371 | -0.9313 | -0.6667 | -0.2485 |

Surface Pressures




Small Radius L.E.

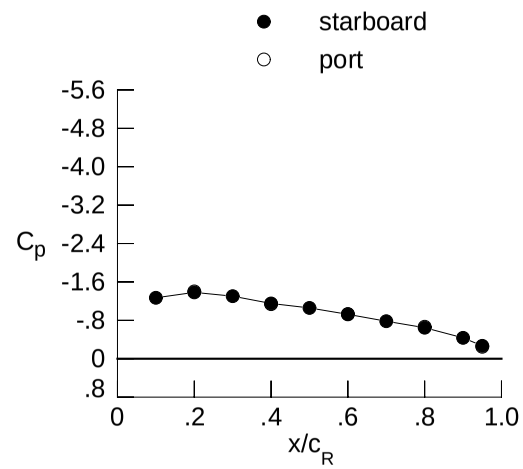
Run No. = 36 , Point No. = 728

$C_N$ = 0.580, $C_m$ = -0.0651

$\alpha$ = 14.3 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

Leading Edge Pressures

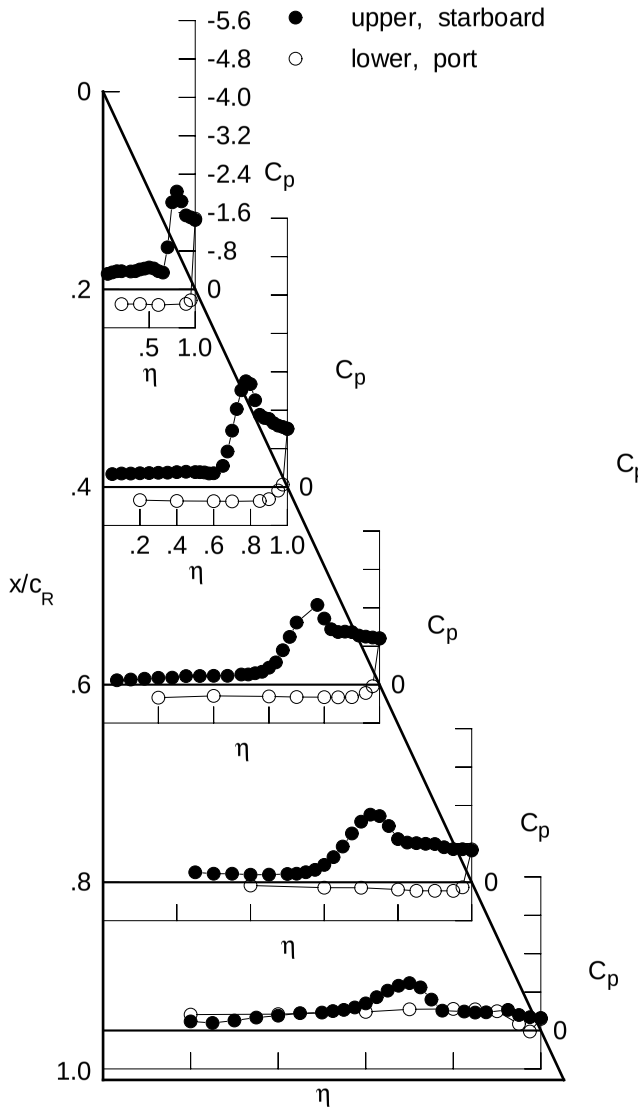



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.2695 | ******* |
| 0.20 | -1.3825 | -1.4023 |
| 0.30 | -1.3033 | ******* |
| 0.40 | -1.1513 | -1.1371 |
| 0.50 | -1.0584 | ******* |
| 0.60 | -0.9250 | -0.9313 |
| 0.70 | -0.7812 | ******* |
| 0.80 | -0.6464 | -0.6667 |
| 0.90 | -0.4351 | ******* |
| 0.95 | -0.2687 | -0.2485 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3235 | -0.2696 | -0.0909 | ******* | ******* |
| 0.100 | -0.3539 | -0.2818 | -0.1063 | ******* | ******* |
| 0.150 | -0.3786 | -0.2806 | -0.1233 | ******* | ******* |
| 0.200 | -0.3782 | -0.2874 | -0.1428 | ******* | -0.1893 |
| 0.250 | ******* | -0.2911 | -0.1456 | -0.2078 | -0.1572 |
| 0.300 | -0.3724 | -0.2968 | -0.1788 | -0.1783 | -0.2079 |
| 0.350 | -0.3793 | -0.2991 | -0.1797 | -0.1783 | -0.2697 |
| 0.400 | -0.4147 | -0.3106 | -0.1839 | -0.1577 | -0.3088 |
| 0.450 | -0.4325 | -0.3183 | -0.1842 | -0.1589 | -0.3613 |
| 0.500 | -0.4562 | -0.3108 | -0.2115 | -0.1730 | -0.3733 |
| 0.525 | ******* | -0.3098 | -0.2121 | -0.1781 | -0.4046 |
| 0.550 | -0.4362 | -0.3037 | -0.2376 | -0.2093 | -0.4297 |
| 0.575 | ******* | -0.2823 | -0.2677 | -0.2591 | -0.4802 |
| 0.600 | -0.3798 | -0.2873 | -0.3526 | -0.3621 | -0.5648 |
| 0.625 | ******* | ******* | -0.4640 | -0.5241 | -0.6946 |
| 0.650 | -0.3504 | -0.4405 | -0.7167 | -0.7446 | -0.8303 |
| 0.675 | ******* | -0.7398 | -0.9942 | -1.0169 | -0.9326 |
| 0.700 | -0.8764 | -1.1745 | -1.2933 | -1.2626 | -0.9870 |
| 0.725 | ******* | -1.6249 | ******* | -1.4088 | -0.8987 |
| 0.750 | -1.8140 | -2.0161 | ******* | -1.3789 | -0.6443 |
| 0.775 | ******* | -2.2037 | -1.6608 | -1.1724 | -0.4139 |
| 0.800 | -2.0382 | -2.1445 | -1.3766 | -0.8999 | ******* |
| 0.825 | ******* | -1.8080 | -1.1540 | -0.8272 | -0.3950 |
| 0.850 | -1.8340 | -1.5044 | -1.0959 | -0.8151 | -0.3737 |
| 0.875 | ******* | -1.4403 | -1.1041 | -0.8019 | -0.3790 |
| 0.900 | -1.5418 | -1.4187 | -1.0942 | -0.7968 | ******* |
| 0.925 | ******* | -1.3316 | -1.0221 | -0.7307 | -0.4296 |
| 0.950 | -1.5005 | -1.2795 | -1.0003 | -0.6906 | -0.3234 |
| 0.975 | ******* | -1.2508 | -0.9819 | -0.6888 | -0.2777 |
| 1.000 | -1.4464 | -1.2182 | -0.9583 | -0.6625 | -0.2620 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3069 | 0.2729 | 0.2714 | ******* | -0.3313 |
| -0.400 | 0.3047 | 0.2902 | 0.2346 | 0.0672 | -0.3410 |
| -0.600 | 0.3243 | 0.2942 | 0.2455 | 0.1124 | -0.3883 |
| -0.700 | ******* | 0.2988 | 0.2586 | 0.1139 | -0.4418 |
| -0.800 | ******* | ******* | 0.2610 | 0.1515 | -0.4500 |
| -0.850 | ******* | 0.2903 | 0.2643 | 0.1777 | -0.4407 |
| -0.900 | 0.3028 | 0.2526 | 0.2603 | 0.1778 | -0.4012 |
| -0.950 | 0.2272 | 0.0738 | 0.1738 | 0.1788 | -0.1359 |
| -0.975 | ******* | -0.0513 | 0.0324 | 0.1047 | 0.0211 |
| -1.000 | -1.4738 | -1.2080 | -0.9677 | -0.6846 | -0.2406 |

Surface Pressures




Small Radius L.E.

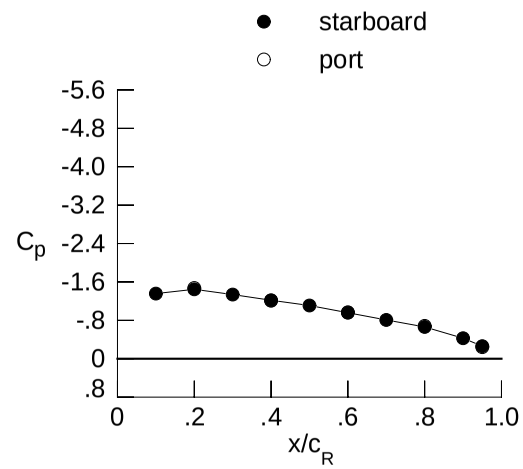
Run No. = 36 , Point No. = 729

$C_N$ = 0.631, $C_m$ = -0.0711

$\alpha$ = 15.4 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

Leading Edge Pressures

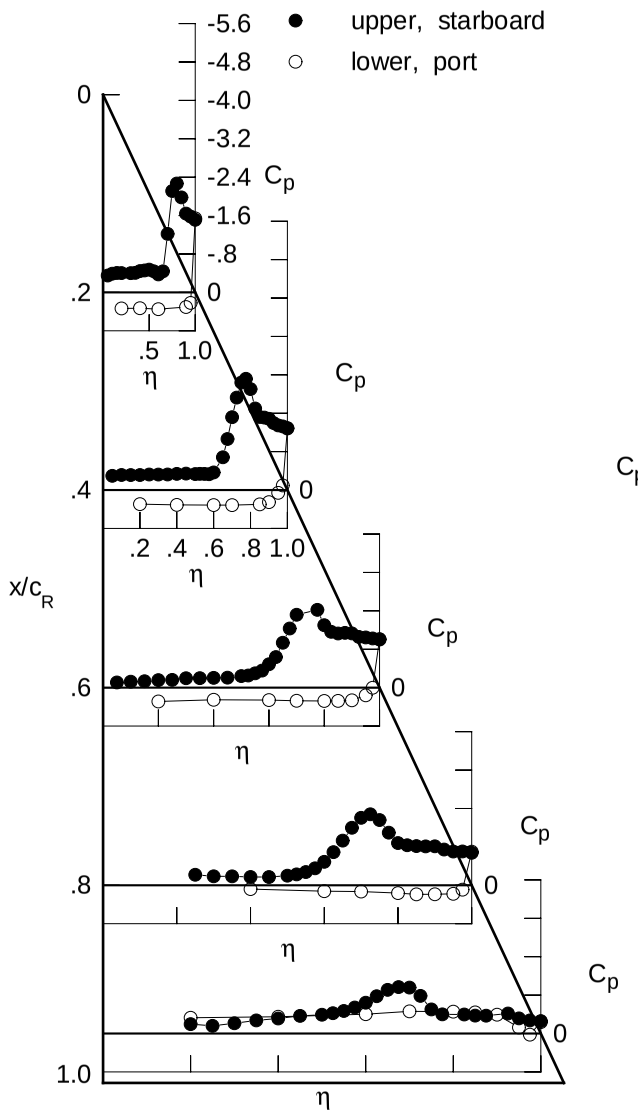



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.3571 | ******* |
| 0.20 | -1.4464 | -1.4738 |
| 0.30 | -1.3369 | ******* |
| 0.40 | -1.2182 | -1.2080 |
| 0.50 | -1.1090 | ******* |
| 0.60 | -0.9583 | -0.9677 |
| 0.70 | -0.8079 | ******* |
| 0.80 | -0.6625 | -0.6846 |
| 0.90 | -0.4274 | ******* |
| 0.95 | -0.2620 | -0.2406 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3509 | -0.2962 | -0.1082 | ******* | ******* |
| 0.100 | -0.3896 | -0.3135 | -0.1238 | ******* | ******* |
| 0.150 | -0.4049 | -0.3116 | -0.1333 | ******* | ******* |
| 0.200 | -0.4027 | -0.3128 | -0.1571 | ******* | -0.1955 |
| 0.250 | ******* | -0.3231 | -0.1616 | -0.2189 | -0.1600 |
| 0.300 | -0.4011 | -0.3224 | -0.1960 | -0.1872 | -0.2133 |
| 0.350 | -0.4073 | -0.3243 | -0.1980 | -0.1863 | -0.2731 |
| 0.400 | -0.4442 | -0.3367 | -0.2039 | -0.1731 | -0.3130 |
| 0.450 | -0.4570 | -0.3423 | -0.2083 | -0.1721 | -0.3669 |
| 0.500 | -0.4742 | -0.3326 | -0.2406 | -0.1999 | -0.3909 |
| 0.525 | ******* | -0.3373 | -0.2528 | -0.2272 | -0.4235 |
| 0.550 | -0.4396 | -0.3357 | -0.2984 | -0.2760 | -0.4698 |
| 0.575 | ******* | -0.3299 | -0.3556 | -0.3536 | -0.5417 |
| 0.600 | -0.3747 | -0.3662 | -0.4873 | -0.4890 | -0.6419 |
| 0.625 | ******* | ******* | -0.6368 | -0.6903 | -0.7766 |
| 0.650 | -0.4392 | -0.6821 | -0.9353 | -0.9304 | -0.9093 |
| 0.675 | ******* | -1.0630 | -1.2318 | -1.1987 | -0.9669 |
| 0.700 | -1.2190 | -1.5175 | -1.5183 | -1.4053 | -0.9571 |
| 0.725 | ******* | -1.9253 | ******* | -1.4794 | -0.7839 |
| 0.750 | -2.1120 | -2.2392 | ******* | -1.3589 | -0.5019 |
| 0.775 | ******* | -2.3175 | -1.6206 | -1.0962 | -0.3992 |
| 0.800 | -2.2682 | -2.1031 | -1.3005 | -0.8799 | ******* |
| 0.825 | ******* | -1.6993 | -1.1633 | -0.8345 | -0.3963 |
| 0.850 | -1.9794 | -1.5227 | -1.1282 | -0.8172 | -0.3730 |
| 0.875 | ******* | -1.5096 | -1.1415 | -0.8103 | -0.3714 |
| 0.900 | -1.6417 | -1.4837 | -1.1293 | -0.8120 | ******* |
| 0.925 | ******* | -1.3961 | -1.0569 | -0.7444 | -0.4167 |
| 0.950 | -1.5800 | -1.3461 | -1.0459 | -0.7032 | -0.3155 |
| 0.975 | ******* | -1.3253 | -1.0249 | -0.7044 | -0.2727 |
| 1.000 | -1.5123 | -1.2901 | -1.0027 | -0.6772 | -0.2596 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3347 | 0.2939 | 0.2881 | ******* | -0.3282 |
| -0.400 | 0.3298 | 0.3093 | 0.2530 | 0.0791 | -0.3492 |
| -0.600 | 0.3494 | 0.3136 | 0.2589 | 0.1233 | -0.4022 |
| -0.700 | ******* | 0.3144 | 0.2739 | 0.1308 | -0.4619 |
| -0.800 | ******* | ******* | 0.2780 | 0.1625 | -0.4552 |
| -0.850 | ******* | 0.2984 | 0.2760 | 0.1890 | -0.4401 |
| -0.900 | 0.3050 | 0.2521 | 0.2643 | 0.1873 | -0.3922 |
| -0.950 | 0.2194 | 0.0584 | 0.1603 | 0.1775 | -0.1259 |
| -0.975 | ******* | -0.0961 | 0.0024 | 0.0914 | 0.0238 |
| -1.000 | -1.5422 | -1.2828 | -1.0105 | -0.7002 | -0.2377 |

Surface Pressures




Small Radius L.E.

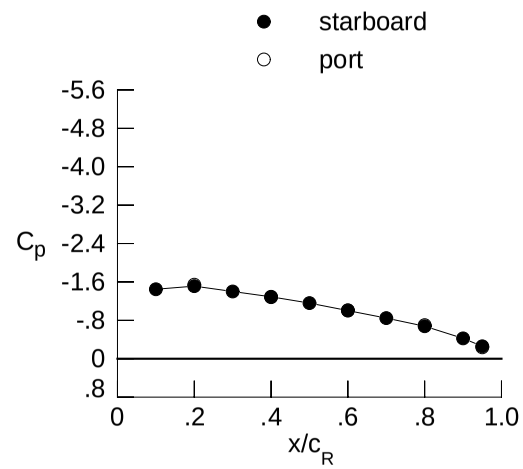
Run No. = 36 , Point No. = 730

$C_N$ = 0.682, $C_m$ = -0.0763

$\alpha$ = 16.3 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

Leading Edge Pressures

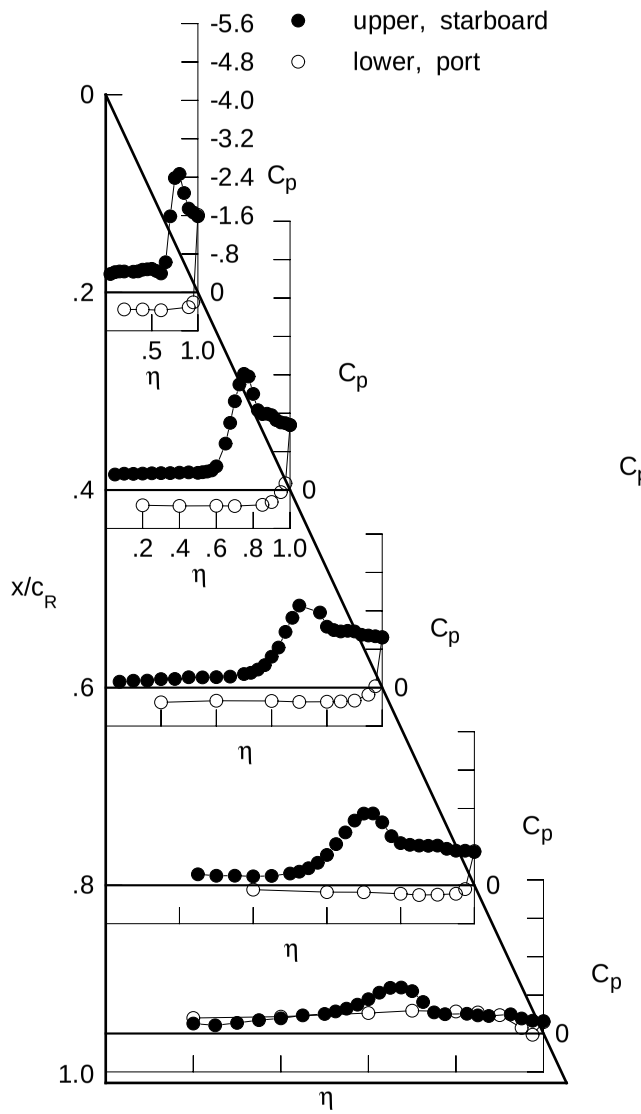



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.4475 | ******* |
| 0.20 | -1.5123 | -1.5422 |
| 0.30 | -1.4008 | ******* |
| 0.40 | -1.2901 | -1.2828 |
| 0.50 | -1.1590 | ******* |
| 0.60 | -1.0027 | -1.0105 |
| 0.70 | -0.8466 | ******* |
| 0.80 | -0.6772 | -0.7002 |
| 0.90 | -0.4240 | ******* |
| 0.95 | -0.2596 | -0.2377 |

# Table D1. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3831 | -0.3231 | -0.1242 | ******* | ******* |
| 0.100 | -0.4219 | -0.3398 | -0.1439 | ******* | ******* |
| 0.150 | -0.4361 | -0.3367 | -0.1468 | ******* | ******* |
| 0.200 | -0.4349 | -0.3421 | -0.1775 | ******* | -0.2076 |
| 0.250 | ******* | -0.3490 | -0.1807 | -0.2291 | -0.1702 |
| 0.300 | -0.4304 | -0.3520 | -0.2169 | -0.1987 | -0.2208 |
| 0.350 | -0.4388 | -0.3531 | -0.2138 | -0.1994 | -0.2784 |
| 0.400 | -0.4730 | -0.3619 | -0.2181 | -0.1863 | -0.3159 |
| 0.450 | -0.4810 | -0.3676 | -0.2299 | -0.1953 | -0.3776 |
| 0.500 | -0.4902 | -0.3584 | -0.2834 | -0.2449 | -0.4068 |
| 0.525 | ******* | -0.3715 | -0.3091 | -0.2833 | -0.4602 |
| 0.550 | -0.4454 | -0.3845 | -0.3764 | -0.3550 | -0.5175 |
| 0.575 | ******* | -0.4085 | -0.4689 | -0.4687 | -0.6011 |
| 0.600 | -0.3947 | -0.4939 | -0.6449 | -0.6324 | -0.7147 |
| 0.625 | ******* | ******* | -0.8348 | -0.8575 | -0.8501 |
| 0.650 | -0.6290 | -0.9668 | -1.1618 | -1.1017 | -0.9512 |
| 0.675 | ******* | -1.3995 | -1.4549 | -1.3477 | -0.9573 |
| 0.700 | -1.5852 | -1.8494 | -1.7097 | -1.4939 | -0.8828 |
| 0.725 | ******* | -2.1994 | ******* | -1.4964 | -0.6558 |
| 0.750 | -2.3835 | -2.4202 | ******* | -1.3116 | -0.4402 |
| 0.775 | ******* | -2.3654 | -1.5649 | -1.0236 | -0.4022 |
| 0.800 | -2.4678 | -2.0026 | -1.2700 | -0.8784 | ******* |
| 0.825 | ******* | -1.6643 | -1.1995 | -0.8432 | -0.4112 |
| 0.850 | -2.0707 | -1.5827 | -1.1704 | -0.8265 | -0.3779 |
| 0.875 | ******* | -1.5895 | -1.1837 | -0.8223 | -0.3647 |
| 0.900 | -1.7453 | -1.5596 | -1.1704 | -0.8261 | ******* |
| 0.925 | ******* | -1.4571 | -1.1008 | -0.7597 | -0.3997 |
| 0.950 | -1.6656 | -1.4085 | -1.0853 | -0.7196 | -0.3129 |
| 0.975 | ******* | -1.3924 | -1.0701 | -0.7199 | -0.2667 |
| 1.000 | -1.5863 | -1.3530 | -1.0421 | -0.6932 | -0.2587 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3553 | 0.3172 | 0.3061 | ******* | -0.3232 |
| -0.400 | 0.3559 | 0.3313 | 0.2731 | 0.0912 | -0.3512 |
| -0.600 | 0.3721 | 0.3282 | 0.2778 | 0.1424 | -0.4263 |
| -0.700 | ******* | 0.3334 | 0.2974 | 0.1443 | -0.4750 |
| -0.800 | ******* | ******* | 0.2937 | 0.1765 | -0.4589 |
| -0.850 | ******* | 0.3087 | 0.2880 | 0.2033 | -0.4381 |
| -0.900 | 0.3080 | 0.2500 | 0.2705 | 0.1956 | -0.3828 |
| -0.950 | 0.2071 | 0.0428 | 0.1467 | 0.1771 | -0.1167 |
| -0.975 | ******* | -0.1402 | -0.0286 | 0.0794 | 0.0257 |
| -1.000 | -1.6149 | -1.3554 | -1.0524 | -0.7129 | -0.2365 |

Surface Pressures




Small Radius L.E.

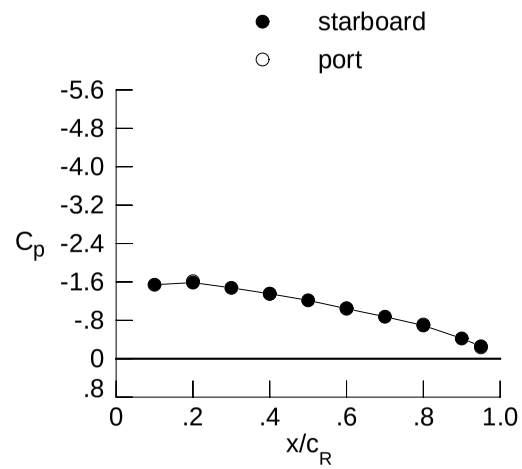
Run No. = 36 , Point No. = 731

$C_N$ = 0.732, $C_m$ = -0.0805

$\alpha$ = 17.3 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

Leading Edge Pressures

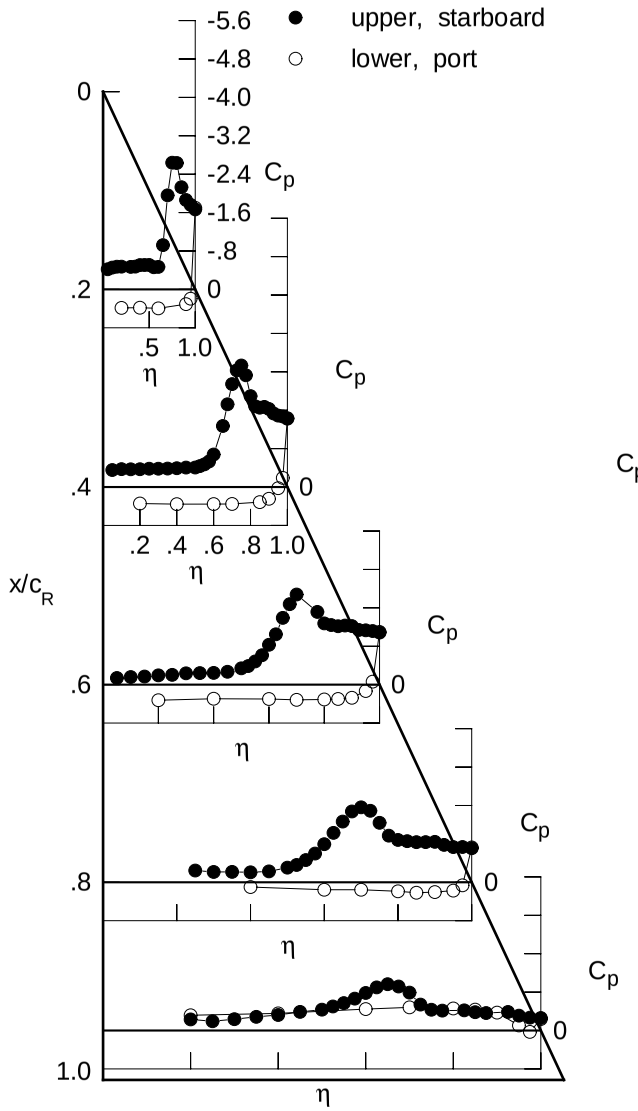



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.5419 | ******* |
| 0.20 | -1.5863 | -1.6149 |
| 0.30 | -1.4768 | ******* |
| 0.40 | -1.3530 | -1.3554 |
| 0.50 | -1.2170 | ******* |
| 0.60 | -1.0421 | -1.0524 |
| 0.70 | -0.8754 | ******* |
| 0.80 | -0.6932 | -0.7129 |
| 0.90 | -0.4225 | ******* |
| 0.95 | -0.2587 | -0.2365 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4195 | -0.3547 | -0.1383 | ******* | ******* |
| 0.100 | -0.4544 | -0.3731 | -0.1581 | ******* | ******* |
| 0.150 | -0.4726 | -0.3692 | -0.1689 | ******* | ******* |
| 0.200 | -0.4736 | -0.3710 | -0.1938 | ******* | -0.2311 |
| 0.250 | ******* | -0.3817 | -0.2039 | -0.2446 | -0.1928 |
| 0.300 | -0.4685 | -0.3814 | -0.2357 | -0.2153 | -0.2357 |
| 0.350 | -0.4747 | -0.3851 | -0.2406 | -0.2165 | -0.2846 |
| 0.400 | -0.5067 | -0.3917 | -0.2450 | -0.2083 | -0.3230 |
| 0.450 | -0.5077 | -0.4057 | -0.2678 | -0.2270 | -0.3878 |
| 0.500 | -0.5091 | -0.4060 | -0.3396 | -0.3044 | -0.4346 |
| 0.525 | ******* | -0.4362 | -0.3869 | -0.3609 | -0.5010 |
| 0.550 | -0.4616 | -0.4725 | -0.4832 | -0.4634 | -0.5716 |
| 0.575 | ******* | -0.5327 | -0.6127 | -0.5984 | -0.6640 |
| 0.600 | -0.4687 | -0.6778 | -0.8302 | -0.7936 | -0.7820 |
| 0.625 | ******* | ******* | -1.0491 | -1.0298 | -0.8987 |
| 0.650 | -0.9227 | -1.2724 | -1.3908 | -1.2650 | -0.9651 |
| 0.675 | ******* | -1.7236 | -1.6767 | -1.4753 | -0.9171 |
| 0.700 | -1.9598 | -2.1449 | -1.8774 | -1.5618 | -0.7896 |
| 0.725 | ******* | -2.4304 | ******* | -1.4895 | -0.5401 |
| 0.750 | -2.6395 | -2.5316 | ******* | -1.2394 | -0.4326 |
| 0.775 | ******* | -2.3281 | -1.5150 | -0.9711 | -0.4144 |
| 0.800 | -2.6326 | -1.8944 | -1.2758 | -0.8826 | ******* |
| 0.825 | ******* | -1.6836 | -1.2413 | -0.8572 | -0.4199 |
| 0.850 | -2.1284 | -1.6531 | -1.2171 | -0.8359 | -0.3814 |
| 0.875 | ******* | -1.6695 | -1.2312 | -0.8372 | -0.3636 |
| 0.900 | -1.8626 | -1.6268 | -1.2202 | -0.8423 | ******* |
| 0.925 | ******* | -1.5329 | -1.1393 | -0.7791 | -0.3863 |
| 0.950 | -1.7612 | -1.4881 | -1.1321 | -0.7335 | -0.3095 |
| 0.975 | ******* | -1.4707 | -1.1166 | -0.7348 | -0.2677 |
| 1.000 | -1.6660 | -1.4242 | -1.0844 | -0.7096 | -0.2609 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3854 | 0.3435 | 0.3247 | ******* | -0.3177 |
| -0.400 | 0.3813 | 0.3564 | 0.2940 | 0.0991 | -0.3567 |
| -0.600 | 0.3949 | 0.3556 | 0.2995 | 0.1553 | -0.4464 |
| -0.700 | ******* | 0.3528 | 0.3167 | 0.1552 | -0.4821 |
| -0.800 | ******* | ******* | 0.3092 | 0.1876 | -0.4591 |
| -0.850 | ******* | 0.3141 | 0.2982 | 0.2179 | -0.4348 |
| -0.900 | 0.3074 | 0.2445 | 0.2733 | 0.2041 | -0.3726 |
| -0.950 | 0.1933 | 0.0238 | 0.1325 | 0.1733 | -0.1056 |
| -0.975 | ******* | -0.1908 | -0.0622 | 0.0630 | 0.0288 |
| -1.000 | -1.6996 | -1.4337 | -1.0973 | -0.7264 | -0.2382 |

Surface Pressures




Small Radius L.E.

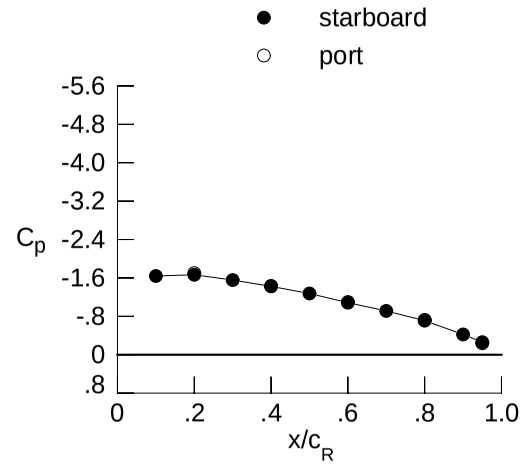
Run No. = 36 , Point No. = 732

$C_N$ = 0.790, $C_m$ = -0.0875

$\alpha$ = 18.4 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

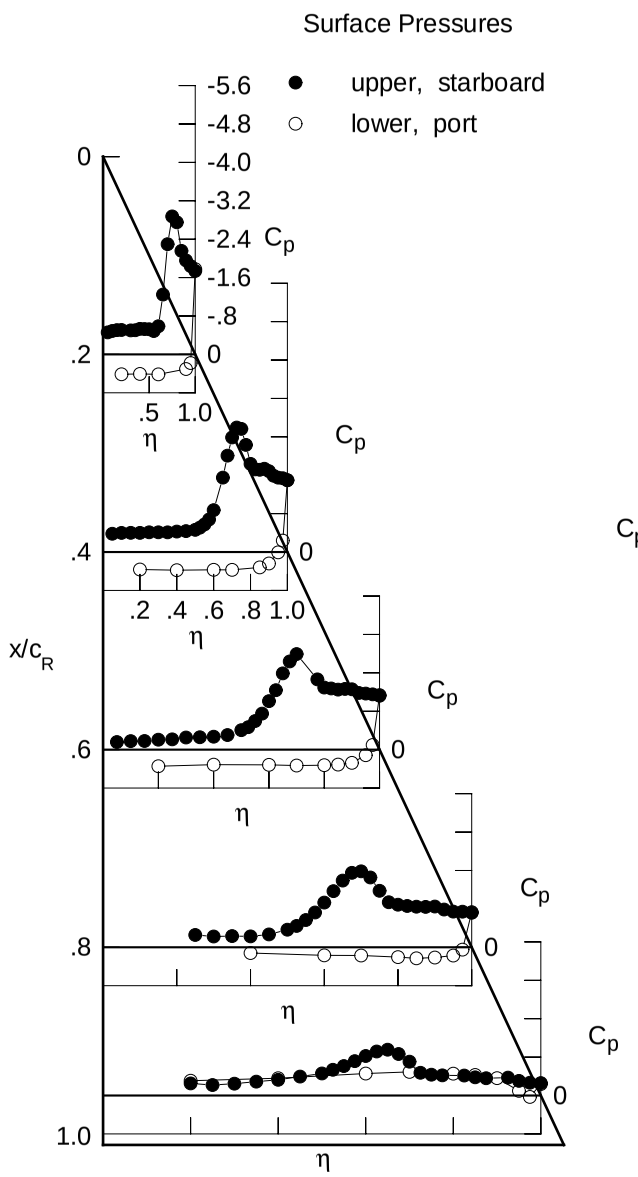
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.6402 | ******* |
| 0.20 | -1.6660 | -1.6996 |
| 0.30 | -1.5559 | ******* |
| 0.40 | -1.4242 | -1.4337 |
| 0.50 | -1.2759 | ******* |
| 0.60 | -1.0844 | -1.0973 |
| 0.70 | -0.9128 | ******* |
| 0.80 | -0.7096 | -0.7264 |
| 0.90 | -0.4221 | ******* |
| 0.95 | -0.2609 | -0.2382 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4587 | -0.3804 | -0.1585 | ******* | ******* |
| 0.100 | -0.4879 | -0.3985 | -0.1773 | ******* | ******* |
| 0.150 | -0.5053 | -0.4004 | -0.1798 | ******* | ******* |
| 0.200 | -0.5089 | -0.3994 | -0.2069 | ******* | -0.2520 |
| 0.250 | ******* | -0.4114 | -0.2141 | -0.2568 | -0.2184 |
| 0.300 | -0.4997 | -0.4116 | -0.2531 | -0.2250 | -0.2468 |
| 0.350 | -0.5033 | -0.4103 | -0.2583 | -0.2336 | -0.2887 |
| 0.400 | -0.5323 | -0.4261 | -0.2700 | -0.2273 | -0.3271 |
| 0.450 | -0.5280 | -0.4356 | -0.3037 | -0.2676 | -0.3948 |
| 0.500 | -0.5244 | -0.4622 | -0.4058 | -0.3664 | -0.4590 |
| 0.525 | ******* | -0.5077 | -0.4683 | -0.4451 | -0.5359 |
| 0.550 | -0.4862 | -0.5745 | -0.5962 | -0.5678 | -0.6138 |
| 0.575 | ******* | -0.6787 | -0.7503 | -0.7245 | -0.7160 |
| 0.600 | -0.5868 | -0.8732 | -1.0107 | -0.9311 | -0.8233 |
| 0.625 | ******* | ******* | -1.2382 | -1.1698 | -0.9172 |
| 0.650 | -1.2466 | -1.5507 | -1.5886 | -1.3896 | -0.9542 |
| 0.675 | ******* | -2.0078 | -1.8380 | -1.5514 | -0.8648 |
| 0.700 | -2.2958 | -2.3873 | -1.9913 | -1.5827 | -0.7049 |
| 0.725 | ******* | -2.5936 | ******* | -1.4541 | -0.4734 |
| 0.750 | -2.8748 | -2.5656 | ******* | -1.1766 | -0.4335 |
| 0.775 | ******* | -2.2322 | -1.4638 | -0.9382 | -0.4203 |
| 0.800 | -2.7522 | -1.8368 | -1.2933 | -0.8875 | ******* |
| 0.825 | ******* | -1.7217 | -1.2747 | -0.8610 | -0.4162 |
| 0.850 | -2.1569 | -1.7135 | -1.2507 | -0.8455 | -0.3793 |
| 0.875 | ******* | -1.7349 | -1.2648 | -0.8414 | -0.3598 |
| 0.900 | -1.9580 | -1.6848 | -1.2575 | -0.8484 | ******* |
| 0.925 | ******* | -1.5897 | -1.1811 | -0.7862 | -0.3727 |
| 0.950 | -1.8400 | -1.5495 | -1.1680 | -0.7431 | -0.3050 |
| 0.975 | ******* | -1.5376 | -1.1524 | -0.7412 | -0.2660 |
| 1.000 | -1.7377 | -1.4956 | -1.1227 | -0.7189 | -0.2590 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4146 | 0.3639 | 0.3455 | ******* | -0.3076 |
| -0.400 | 0.4069 | 0.3783 | 0.3128 | 0.1197 | -0.3603 |
| -0.600 | 0.4163 | 0.3702 | 0.3169 | 0.1680 | -0.4580 |
| -0.700 | ******* | 0.3716 | 0.3314 | 0.1708 | -0.4920 |
| -0.800 | ******* | ******* | 0.3242 | 0.2047 | -0.4548 |
| -0.850 | ******* | 0.3203 | 0.3115 | 0.2298 | -0.4283 |
| -0.900 | 0.3050 | 0.2385 | 0.2754 | 0.2134 | -0.3613 |
| -0.950 | 0.1797 | 0.0062 | 0.1164 | 0.1721 | -0.0966 |
| -0.975 | ******* | -0.2393 | -0.0968 | 0.0485 | 0.0294 |
| -1.000 | -1.7764 | -1.4978 | -1.1358 | -0.7319 | -0.2386 |



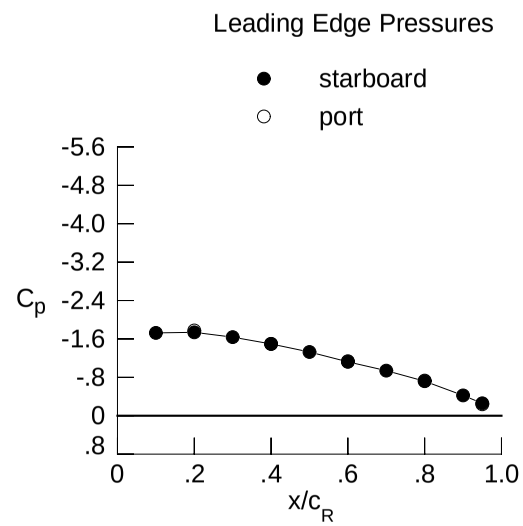

Small Radius L.E.

Run No. = 36 , Point No. = 733

$C_N$ = 0.845, $C_m$ = -0.0942

$\alpha$ = 19.4 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

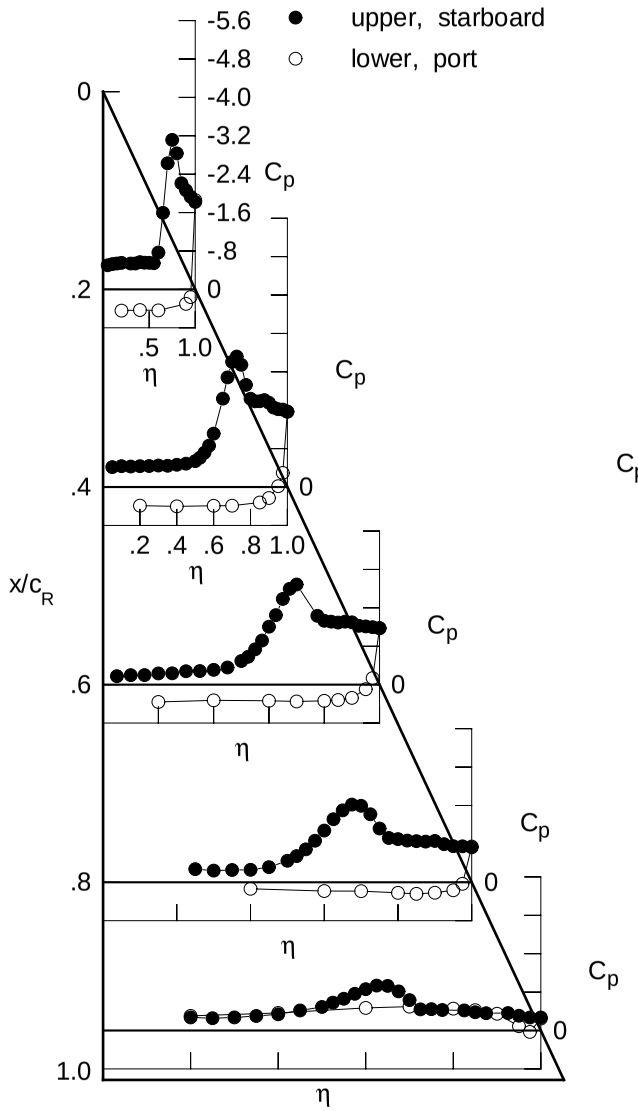



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.7255 | ******* |
| 0.20 | -1.7377 | -1.7764 |
| 0.30 | -1.6372 | ******* |
| 0.40 | -1.4956 | -1.4978 |
| 0.50 | -1.3279 | ******* |
| 0.60 | -1.1227 | -1.1358 |
| 0.70 | -0.9393 | ******* |
| 0.80 | -0.7189 | -0.7319 |
| 0.90 | -0.4229 | ******* |
| 0.95 | -0.2590 | -0.2386 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5021 | -0.4150 | -0.1756 | ******* | ******* |
| 0.100 | -0.5263 | -0.4345 | -0.1974 | ******* | ******* |
| 0.150 | -0.5392 | -0.4268 | -0.1995 | ******* | ******* |
| 0.200 | -0.5528 | -0.4348 | -0.2340 | ******* | -0.2730 |
| 0.250 | ******* | -0.4376 | -0.2358 | -0.2734 | -0.2558 |
| 0.300 | -0.5383 | -0.4481 | -0.2790 | -0.2428 | -0.2724 |
| 0.350 | -0.5388 | -0.4435 | -0.2833 | -0.2562 | -0.3023 |
| 0.400 | -0.5679 | -0.4641 | -0.3084 | -0.2598 | -0.3376 |
| 0.450 | -0.5562 | -0.4875 | -0.3566 | -0.3150 | -0.4172 |
| 0.500 | -0.5548 | -0.5401 | -0.4917 | -0.4481 | -0.4905 |
| 0.525 | ******* | -0.6087 | -0.5807 | -0.5456 | -0.5811 |
| 0.550 | -0.5458 | -0.7153 | -0.7361 | -0.6864 | -0.6613 |
| 0.575 | ******* | -0.8624 | -0.9193 | -0.8655 | -0.7646 |
| 0.600 | -0.7677 | -1.1131 | -1.2070 | -1.0777 | -0.8611 |
| 0.625 | ******* | ******* | -1.4483 | -1.3136 | -0.9364 |
| 0.650 | -1.5950 | -1.8416 | -1.7855 | -1.4985 | -0.9297 |
| 0.675 | ******* | -2.2838 | -1.9963 | -1.6196 | -0.8152 |
| 0.700 | -2.6270 | -2.6092 | -2.0866 | -1.5939 | -0.6333 |
| 0.725 | ******* | -2.7183 | ******* | -1.4169 | -0.4412 |
| 0.750 | -3.1141 | -2.5468 | ******* | -1.1204 | -0.4452 |
| 0.775 | ******* | -2.1278 | -1.4341 | -0.9233 | -0.4272 |
| 0.800 | -2.8342 | -1.8397 | -1.3302 | -0.8991 | ******* |
| 0.825 | ******* | -1.7859 | -1.3119 | -0.8692 | -0.4185 |
| 0.850 | -2.2113 | -1.7868 | -1.2940 | -0.8569 | -0.3809 |
| 0.875 | ******* | -1.8111 | -1.3122 | -0.8471 | -0.3603 |
| 0.900 | -2.0651 | -1.7563 | -1.2981 | -0.8614 | ******* |
| 0.925 | ******* | -1.6565 | -1.2256 | -0.7943 | -0.3637 |
| 0.950 | -1.9314 | -1.6213 | -1.2130 | -0.7523 | -0.3077 |
| 0.975 | ******* | -1.6139 | -1.1970 | -0.7494 | -0.2716 |
| 1.000 | -1.8224 | -1.5699 | -1.1725 | -0.7285 | -0.2708 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4421 | 0.3879 | 0.3608 | ******* | -0.3047 |
| -0.400 | 0.4302 | 0.4026 | 0.3270 | 0.1356 | -0.3658 |
| -0.600 | 0.4376 | 0.3900 | 0.3358 | 0.1824 | -0.4706 |
| -0.700 | ******* | 0.3888 | 0.3503 | 0.1844 | -0.4978 |
| -0.800 | ******* | ******* | 0.3378 | 0.2197 | -0.4556 |
| -0.850 | ******* | 0.3226 | 0.3199 | 0.2411 | -0.4233 |
| -0.900 | 0.3013 | 0.2289 | 0.2757 | 0.2176 | -0.3489 |
| -0.950 | 0.1602 | -0.0176 | 0.0955 | 0.1664 | -0.0893 |
| -0.975 | ******* | -0.2941 | -0.1359 | 0.0314 | 0.0297 |
| -1.000 | -1.8592 | -1.5719 | -1.1791 | -0.7446 | -0.2485 |

Surface Pressures




Small Radius L.E.

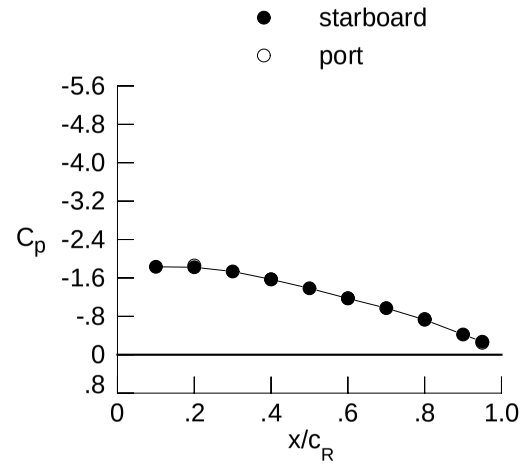
Run No. = 36 , Point No. = 734

$C_N$ = 0.902, $C_m$ = -0.1012

$\alpha$ = 20.4 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

Leading Edge Pressures

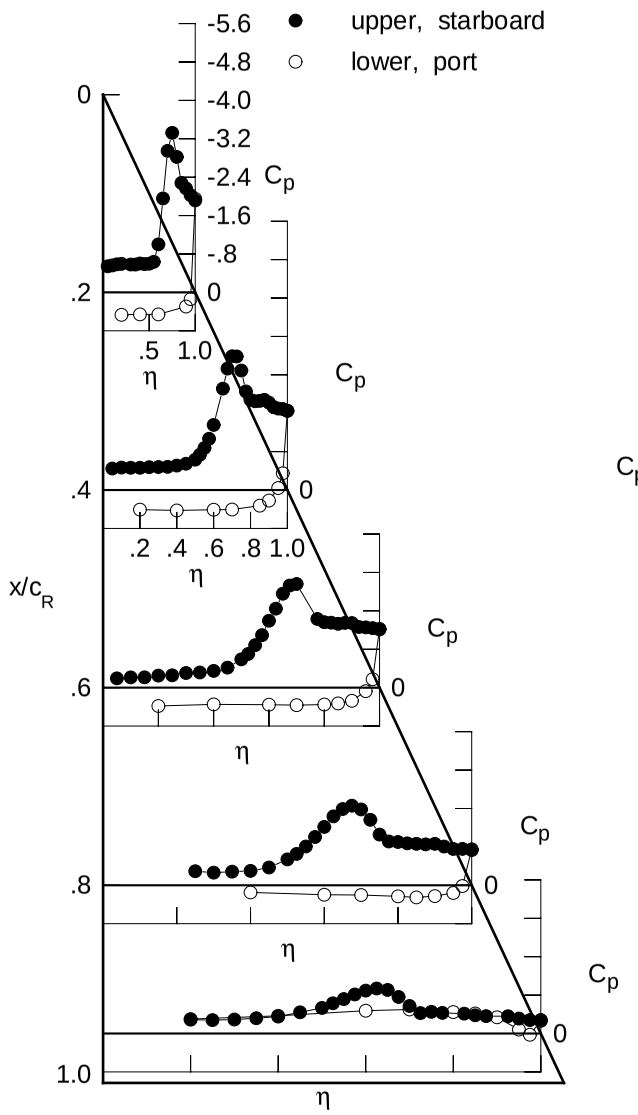



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.8321 | ******* |
| 0.20 | -1.8224 | -1.8592 |
| 0.30 | -1.7345 | ******* |
| 0.40 | -1.5699 | -1.5719 |
| 0.50 | -1.3839 | ******* |
| 0.60 | -1.1725 | -1.1791 |
| 0.70 | -0.9708 | ******* |
| 0.80 | -0.7285 | -0.7446 |
| 0.90 | -0.4217 | ******* |
| 0.95 | -0.2708 | -0.2485 |

# Table D1. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5430 | -0.4476 | -0.1940 | ******* | ******* |
| 0.100 | -0.5617 | -0.4682 | -0.2132 | ******* | ******* |
| 0.150 | -0.5850 | -0.4641 | -0.2150 | ******* | ******* |
| 0.200 | -0.5946 | -0.4637 | -0.2507 | ******* | -0.2884 |
| 0.250 | ******* | -0.4758 | -0.2569 | -0.2925 | -0.2795 |
| 0.300 | -0.5810 | -0.4797 | -0.3049 | -0.2635 | -0.2912 |
| 0.350 | -0.5791 | -0.4831 | -0.3160 | -0.2837 | -0.3187 |
| 0.400 | -0.6021 | -0.5093 | -0.3492 | -0.2997 | -0.3531 |
| 0.450 | -0.5898 | -0.5481 | -0.4167 | -0.3700 | -0.4419 |
| 0.500 | -0.5974 | -0.6329 | -0.5891 | -0.5394 | -0.5325 |
| 0.525 | ******* | -0.7350 | -0.7027 | -0.6537 | -0.6296 |
| 0.550 | -0.6365 | -0.8762 | -0.8847 | -0.8083 | -0.7175 |
| 0.575 | ******* | -1.0679 | -1.0935 | -1.0061 | -0.8134 |
| 0.600 | -1.0006 | -1.3570 | -1.3937 | -1.2161 | -0.8936 |
| 0.625 | ******* | ******* | -1.6454 | -1.4364 | -0.9379 |
| 0.650 | -1.9573 | -2.1130 | -1.9569 | -1.5887 | -0.9077 |
| 0.675 | ******* | -2.5303 | -2.1274 | -1.6582 | -0.7613 |
| 0.700 | -2.9489 | -2.7868 | -2.1589 | -1.5801 | -0.5737 |
| 0.725 | ******* | -2.7836 | ******* | -1.3638 | -0.4256 |
| 0.750 | -3.3238 | -2.4893 | ******* | -1.0565 | -0.4513 |
| 0.775 | ******* | -2.0544 | -1.4312 | -0.9127 | -0.4296 |
| 0.800 | -2.8219 | -1.8786 | -1.3635 | -0.9024 | ******* |
| 0.825 | ******* | -1.8489 | -1.3524 | -0.8735 | -0.4136 |
| 0.850 | -2.2793 | -1.8580 | -1.3295 | -0.8638 | -0.3795 |
| 0.875 | ******* | -1.8790 | -1.3497 | -0.8522 | -0.3617 |
| 0.900 | -2.1670 | -1.8209 | -1.3456 | -0.8644 | ******* |
| 0.925 | ******* | -1.7297 | -1.2639 | -0.8076 | -0.3599 |
| 0.950 | -2.0248 | -1.6969 | -1.2553 | -0.7570 | -0.3115 |
| 0.975 | ******* | -1.6879 | -1.2401 | -0.7580 | -0.2799 |
| 1.000 | -1.9164 | -1.6524 | -1.2132 | -0.7339 | -0.2821 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4668 | 0.4083 | 0.3820 | ******* | -0.3002 |
| -0.400 | 0.4581 | 0.4252 | 0.3485 | 0.1488 | -0.3685 |
| -0.600 | 0.4585 | 0.4106 | 0.3555 | 0.1969 | -0.4755 |
| -0.700 | ******* | 0.4068 | 0.3649 | 0.2029 | -0.5007 |
| -0.800 | ******* | ******* | 0.3520 | 0.2301 | -0.4464 |
| -0.850 | ******* | 0.3259 | 0.3289 | 0.2519 | -0.4170 |
| -0.900 | 0.2948 | 0.2189 | 0.2742 | 0.2254 | -0.3379 |
| -0.950 | 0.1412 | -0.0413 | 0.0735 | 0.1599 | -0.0818 |
| -0.975 | ******* | -0.3500 | -0.1753 | 0.0150 | 0.0256 |
| -1.000 | -1.9502 | -1.6476 | -1.2239 | -0.7505 | -0.2634 |

Surface Pressures




Small Radius L.E.

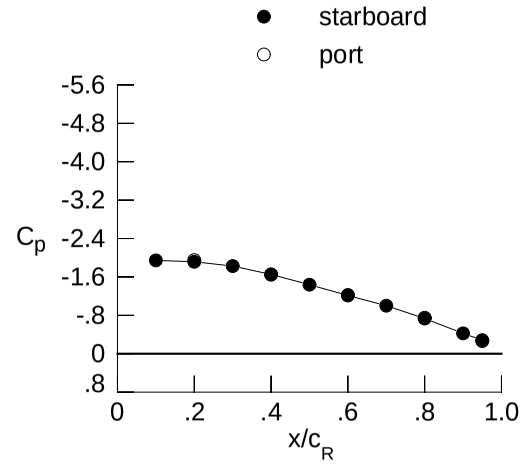
Run No. = 36 , Point No. = 735

$C_N$ = 0.967, $C_m$ = -0.1114

$\alpha$ = 21.4 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.8 \times 10^6$

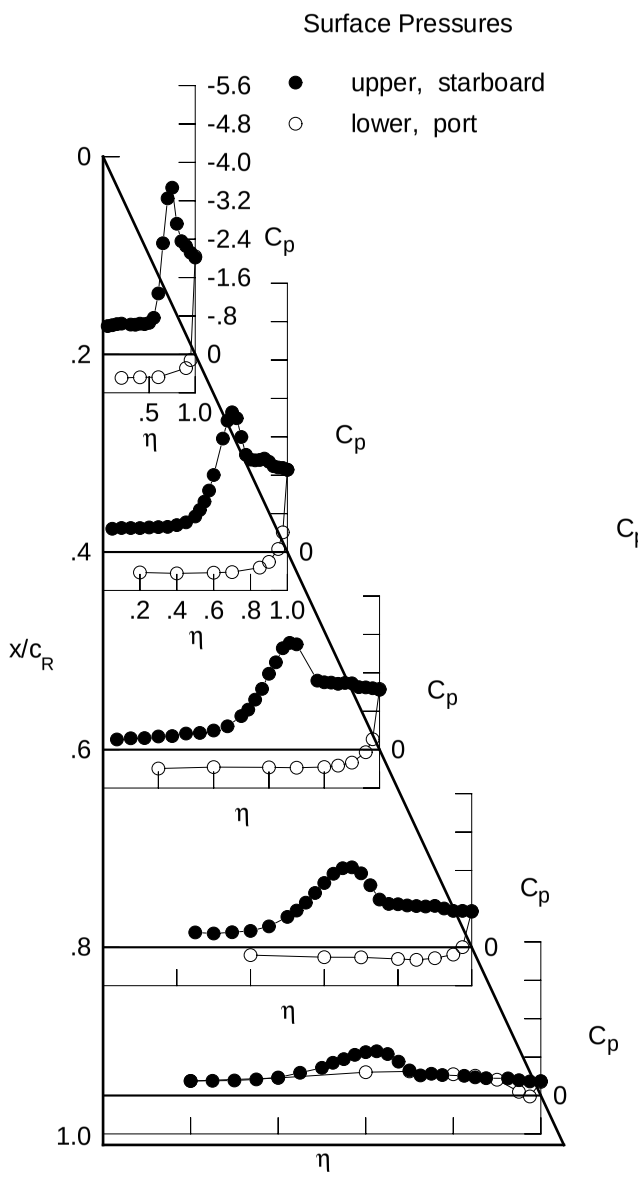
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.9448 | ******* |
| 0.20 | -1.9164 | -1.9502 |
| 0.30 | -1.8261 | ******* |
| 0.40 | -1.6524 | -1.6476 |
| 0.50 | -1.4384 | ******* |
| 0.60 | -1.2132 | -1.2239 |
| 0.70 | -1.0012 | ******* |
| 0.80 | -0.7339 | -0.7505 |
| 0.90 | -0.4238 | ******* |
| 0.95 | -0.2821 | -0.2634 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5896 | -0.4847 | -0.2123 | ******* | ******* |
| 0.100 | -0.6082 | -0.5008 | -0.2368 | ******* | ******* |
| 0.150 | -0.6303 | -0.5001 | -0.2410 | ******* | ******* |
| 0.200 | -0.6404 | -0.4990 | -0.2742 | ******* | -0.3040 |
| 0.250 | ******* | -0.5120 | -0.2827 | -0.3094 | -0.3061 |
| 0.300 | -0.6211 | -0.5196 | -0.3349 | -0.2873 | -0.3130 |
| 0.350 | -0.6172 | -0.5238 | -0.3476 | -0.3132 | -0.3352 |
| 0.400 | -0.6401 | -0.5608 | -0.3982 | -0.3412 | -0.3748 |
| 0.450 | -0.6308 | -0.6187 | -0.4863 | -0.4348 | -0.4739 |
| 0.500 | -0.6566 | -0.7408 | -0.6990 | -0.6330 | -0.5770 |
| 0.525 | ******* | -0.8774 | -0.8339 | -0.7646 | -0.6815 |
| 0.550 | -0.7618 | -1.0507 | -1.0412 | -0.9293 | -0.7579 |
| 0.575 | ******* | -1.2806 | -1.2657 | -1.1310 | -0.8470 |
| 0.600 | -1.2698 | -1.6045 | -1.5805 | -1.3395 | -0.9034 |
| 0.625 | ******* | ******* | -1.8194 | -1.5323 | -0.9218 |
| 0.650 | -2.3161 | -2.3629 | -2.1130 | -1.6470 | -0.8638 |
| 0.675 | ******* | -2.7371 | -2.2242 | -1.6656 | -0.7045 |
| 0.700 | -3.2503 | -2.9110 | -2.1940 | -1.5409 | -0.5227 |
| 0.725 | ******* | -2.7872 | ******* | -1.2930 | -0.4186 |
| 0.750 | -3.4726 | -2.3969 | ******* | -0.9947 | -0.4532 |
| 0.775 | ******* | -2.0258 | -1.4379 | -0.9035 | -0.4266 |
| 0.800 | -2.7219 | -1.9257 | -1.4032 | -0.8966 | ******* |
| 0.825 | ******* | -1.9104 | -1.3964 | -0.8711 | -0.4101 |
| 0.850 | -2.3581 | -1.9188 | -1.3711 | -0.8589 | -0.3781 |
| 0.875 | ******* | -1.9462 | -1.3894 | -0.8498 | -0.3610 |
| 0.900 | -2.2578 | -1.8811 | -1.3813 | -0.8627 | ******* |
| 0.925 | ******* | -1.7882 | -1.3013 | -0.8078 | -0.3568 |
| 0.950 | -2.1181 | -1.7618 | -1.2970 | -0.7581 | -0.3189 |
| 0.975 | ******* | -1.7514 | -1.2791 | -0.7583 | -0.2937 |
| 1.000 | -2.0174 | -1.7148 | -1.2465 | -0.7420 | -0.3011 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4899 | 0.4254 | 0.3933 | ******* | -0.3026 |
| -0.400 | 0.4778 | 0.4450 | 0.3639 | 0.1631 | -0.3660 |
| -0.600 | 0.4748 | 0.4307 | 0.3692 | 0.2066 | -0.4853 |
| -0.700 | ******* | 0.4185 | 0.3771 | 0.2092 | -0.5022 |
| -0.800 | ******* | ******* | 0.3623 | 0.2433 | -0.4433 |
| -0.850 | ******* | 0.3249 | 0.3331 | 0.2619 | -0.4116 |
| -0.900 | 0.2854 | 0.2054 | 0.2703 | 0.2275 | -0.3288 |
| -0.950 | 0.1180 | -0.0631 | 0.0534 | 0.1520 | -0.0770 |
| -0.975 | ******* | -0.4101 | -0.2166 | -0.0030 | 0.0200 |
| -1.000 | -2.0421 | -1.7136 | -1.2649 | -0.7556 | -0.2833 |



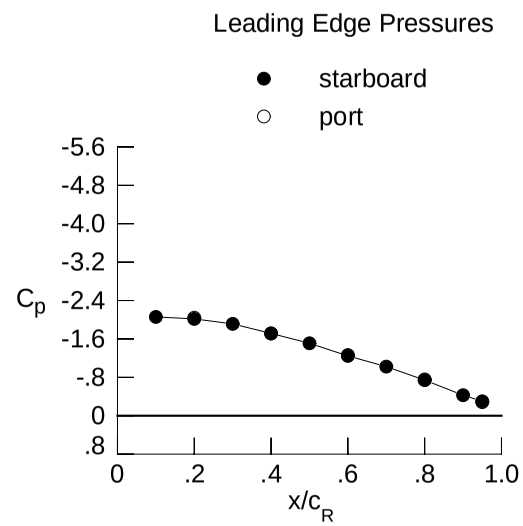

Small Radius L.E.

Run No. = 36 , Point No. = 736

$C_N$ = 1.036, $C_m$ = -0.1296

$\alpha$ = 22.4 °, $M_\infty$ = 0.399

$R_{mac}$ = $5.7 \times 10^6$

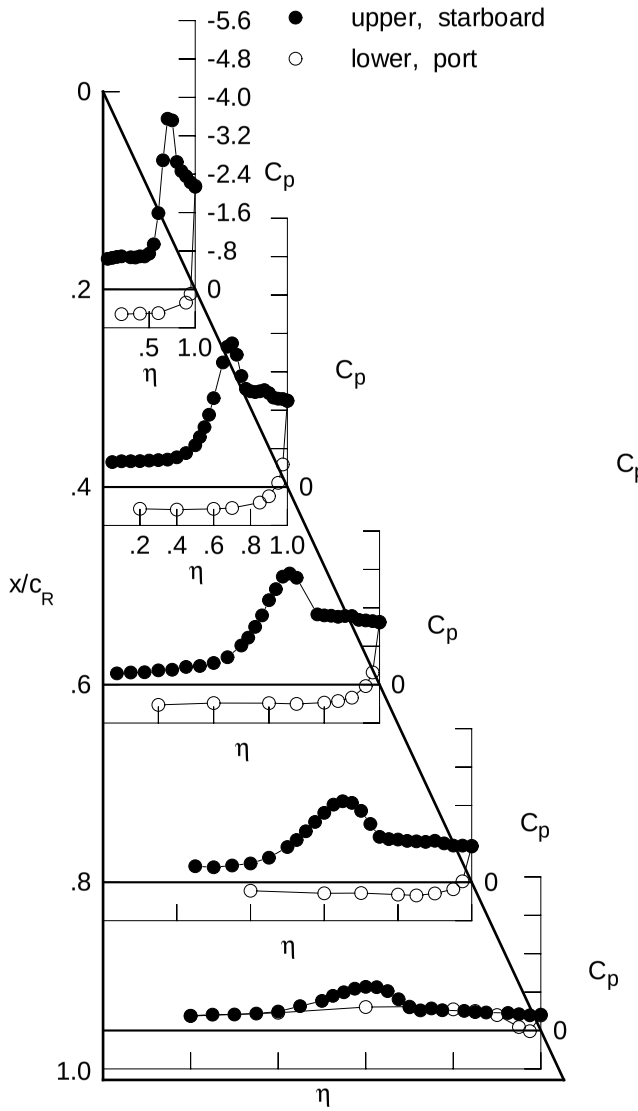



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -2.0586 | ******* |
| 0.20 | -2.0174 | -2.0421 |
| 0.30 | -1.9134 | ******* |
| 0.40 | -1.7148 | -1.7136 |
| 0.50 | -1.5094 | ******* |
| 0.60 | -1.2465 | -1.2649 |
| 0.70 | -1.0230 | ******* |
| 0.80 | -0.7420 | -0.7556 |
| 0.90 | -0.4271 | ******* |
| 0.95 | -0.3011 | -0.2833 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6368 | -0.5198 | -0.2345 | ******* | ******* |
| 0.100 | -0.6570 | -0.5365 | -0.2530 | ******* | ******* |
| 0.150 | -0.6759 | -0.5374 | -0.2584 | ******* | ******* |
| 0.200 | -0.6888 | -0.5398 | -0.2979 | ******* | -0.3078 |
| 0.250 | ******* | -0.5511 | -0.3101 | -0.3342 | -0.3306 |
| 0.300 | -0.6691 | -0.5609 | -0.3688 | -0.3130 | -0.3334 |
| 0.350 | -0.6636 | -0.5716 | -0.3892 | -0.3494 | -0.3524 |
| 0.400 | -0.6885 | -0.6193 | -0.4514 | -0.3919 | -0.3954 |
| 0.450 | -0.6864 | -0.7068 | -0.5713 | -0.5119 | -0.5068 |
| 0.500 | -0.7449 | -0.8704 | -0.8155 | -0.7343 | -0.6171 |
| 0.525 | ******* | -1.0413 | -0.9787 | -0.8811 | -0.7224 |
| 0.550 | -0.9400 | -1.2475 | -1.2038 | -1.0626 | -0.7965 |
| 0.575 | ******* | -1.5060 | -1.4426 | -1.2569 | -0.8713 |
| 0.600 | -1.5896 | -1.8516 | -1.7588 | -1.4466 | -0.9099 |
| 0.625 | ******* | ******* | -1.9896 | -1.6178 | -0.9027 |
| 0.650 | -2.6895 | -2.5951 | -2.2492 | -1.6878 | -0.8210 |
| 0.675 | ******* | -2.9240 | -2.3153 | -1.6544 | -0.6515 |
| 0.700 | -3.5555 | -2.9935 | -2.2273 | -1.4879 | -0.4842 |
| 0.725 | ******* | -2.7564 | ******* | -1.2155 | -0.4192 |
| 0.750 | -3.5209 | -2.3137 | ******* | -0.9467 | -0.4601 |
| 0.775 | ******* | -2.0459 | -1.4628 | -0.9000 | -0.4225 |
| 0.800 | -2.6545 | -1.9953 | -1.4425 | -0.8905 | ******* |
| 0.825 | ******* | -1.9785 | -1.4354 | -0.8627 | -0.4092 |
| 0.850 | -2.4650 | -1.9948 | -1.4135 | -0.8531 | -0.3838 |
| 0.875 | ******* | -2.0190 | -1.4302 | -0.8413 | -0.3751 |
| 0.900 | -2.3595 | -1.9568 | -1.4293 | -0.8644 | ******* |
| 0.925 | ******* | -1.8635 | -1.3495 | -0.8106 | -0.3655 |
| 0.950 | -2.2294 | -1.8400 | -1.3380 | -0.7651 | -0.3395 |
| 0.975 | ******* | -1.8335 | -1.3235 | -0.7644 | -0.3168 |
| 1.000 | -2.1372 | -1.8023 | -1.2935 | -0.7452 | -0.3304 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5162 | 0.4534 | 0.4220 | ******* | -0.3016 |
| -0.400 | 0.5046 | 0.4707 | 0.3837 | 0.1764 | -0.3695 |
| -0.600 | 0.4942 | 0.4551 | 0.3858 | 0.2298 | -0.4885 |
| -0.700 | ******* | 0.4371 | 0.4018 | 0.2251 | -0.4967 |
| -0.800 | ******* | ******* | 0.3751 | 0.2570 | -0.4409 |
| -0.850 | ******* | 0.3243 | 0.3415 | 0.2740 | -0.4074 |
| -0.900 | 0.2758 | 0.1916 | 0.2709 | 0.2327 | -0.3218 |
| -0.950 | 0.0918 | -0.0872 | 0.0304 | 0.1448 | -0.0730 |
| -0.975 | ******* | -0.4701 | -0.2545 | -0.0197 | 0.0148 |
| -1.000 | -2.1557 | -1.7922 | -1.3089 | -0.7592 | -0.3135 |

Surface Pressures




Small Radius L.E.

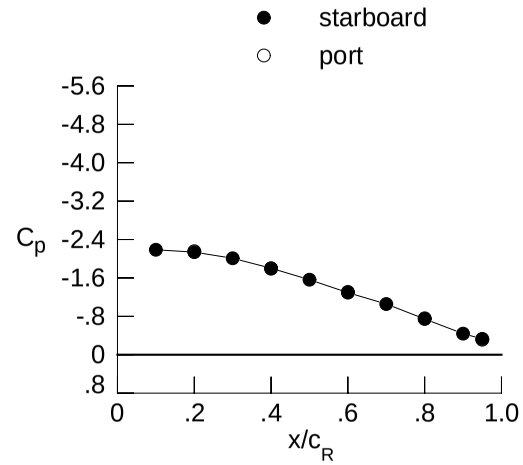
Run No. = 36 , Point No. = 737

$C_N$ = 1.084, $C_m$ = -0.1287

$\alpha$ = 23.4 °, $M_\infty$ = 0.398

$R_{mac}$ = $5.7 \times 10^6$

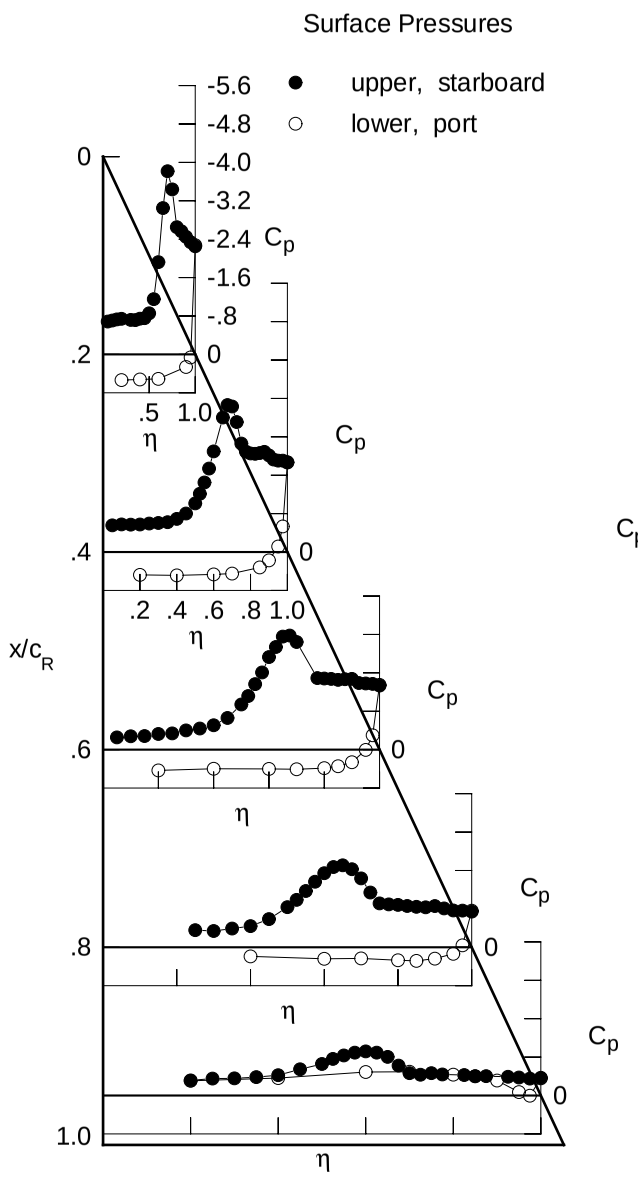
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -2.1868 | ******* |
| 0.20 | -2.1372 | -2.1557 |
| 0.30 | -2.0097 | ******* |
| 0.40 | -1.8023 | -1.7922 |
| 0.50 | -1.5630 | ******* |
| 0.60 | -1.2935 | -1.3089 |
| 0.70 | -1.0564 | ******* |
| 0.80 | -0.7452 | -0.7592 |
| 0.90 | -0.4391 | ******* |
| 0.95 | -0.3304 | -0.3135 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6839 | -0.5556 | -0.2554 | ******* | ******* |
| 0.100 | -0.7058 | -0.5753 | -0.2783 | ******* | ******* |
| 0.150 | -0.7288 | -0.5703 | -0.2828 | ******* | ******* |
| 0.200 | -0.7418 | -0.5738 | -0.3267 | ******* | -0.3145 |
| 0.250 | ******* | -0.5935 | -0.3385 | -0.3570 | -0.3531 |
| 0.300 | -0.7186 | -0.6056 | -0.4007 | -0.3392 | -0.3573 |
| 0.350 | -0.7140 | -0.6217 | -0.4397 | -0.3901 | -0.3832 |
| 0.400 | -0.7438 | -0.6905 | -0.5084 | -0.4406 | -0.4229 |
| 0.450 | -0.7546 | -0.8022 | -0.6603 | -0.5869 | -0.5463 |
| 0.500 | -0.8560 | -1.0139 | -0.9406 | -0.8358 | -0.6565 |
| 0.525 | ******* | -1.2137 | -1.1168 | -0.9883 | -0.7620 |
| 0.550 | -1.1511 | -1.4490 | -1.3650 | -1.1731 | -0.8348 |
| 0.575 | ******* | -1.7392 | -1.6080 | -1.3654 | -0.8929 |
| 0.600 | -1.9220 | -2.0966 | -1.9285 | -1.5431 | -0.9190 |
| 0.625 | ******* | ******* | -2.1381 | -1.6720 | -0.8926 |
| 0.650 | -3.0485 | -2.8025 | -2.3548 | -1.7081 | -0.8047 |
| 0.675 | ******* | -3.0624 | -2.3765 | -1.6267 | -0.6231 |
| 0.700 | -3.8157 | -3.0322 | -2.2421 | -1.4354 | -0.4656 |
| 0.725 | ******* | -2.7078 | ******* | -1.1408 | -0.4329 |
| 0.750 | -3.4376 | -2.2598 | ******* | -0.9145 | -0.4657 |
| 0.775 | ******* | -2.0909 | -1.4910 | -0.8935 | -0.4386 |
| 0.800 | -2.6505 | -2.0536 | -1.4816 | -0.8830 | ******* |
| 0.825 | ******* | -2.0461 | -1.4738 | -0.8606 | -0.4267 |
| 0.850 | -2.5651 | -2.0623 | -1.4536 | -0.8435 | -0.4012 |
| 0.875 | ******* | -2.0868 | -1.4671 | -0.8326 | -0.4031 |
| 0.900 | -2.4495 | -2.0125 | -1.4747 | -0.8589 | ******* |
| 0.925 | ******* | -1.9273 | -1.3883 | -0.8094 | -0.3901 |
| 0.950 | -2.3367 | -1.9043 | -1.3787 | -0.7668 | -0.3749 |
| 0.975 | ******* | -1.9039 | -1.3693 | -0.7643 | -0.3520 |
| 1.000 | -2.2523 | -1.8713 | -1.3348 | -0.7432 | -0.3699 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5351 | 0.4759 | 0.4326 | ******* | -0.3061 |
| -0.400 | 0.5225 | 0.4863 | 0.3982 | 0.1893 | -0.3633 |
| -0.600 | 0.5104 | 0.4662 | 0.4016 | 0.2397 | -0.4893 |
| -0.700 | ******* | 0.4487 | 0.4086 | 0.2322 | -0.4951 |
| -0.800 | ******* | ******* | 0.3859 | 0.2705 | -0.4346 |
| -0.850 | ******* | 0.3210 | 0.3459 | 0.2831 | -0.4006 |
| -0.900 | 0.2621 | 0.1737 | 0.2627 | 0.2365 | -0.3122 |
| -0.950 | 0.0630 | -0.1153 | 0.0056 | 0.1358 | -0.0709 |
| -0.975 | ******* | -0.5335 | -0.2992 | -0.0409 | 0.0042 |
| -1.000 | -2.2748 | -1.8654 | -1.3496 | -0.7624 | -0.3572 |



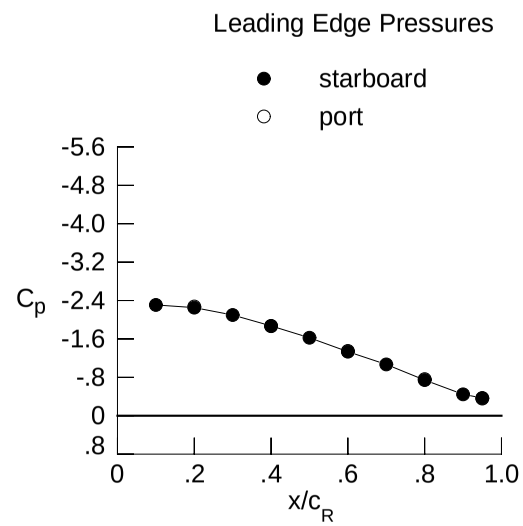

Small Radius L.E.

Run No. = 36 , Point No. = 738

$C_N$ = 1.147, $C_m$ = -0.1387

$\alpha$ = 24.5 °, $M_\infty$ = 0.398

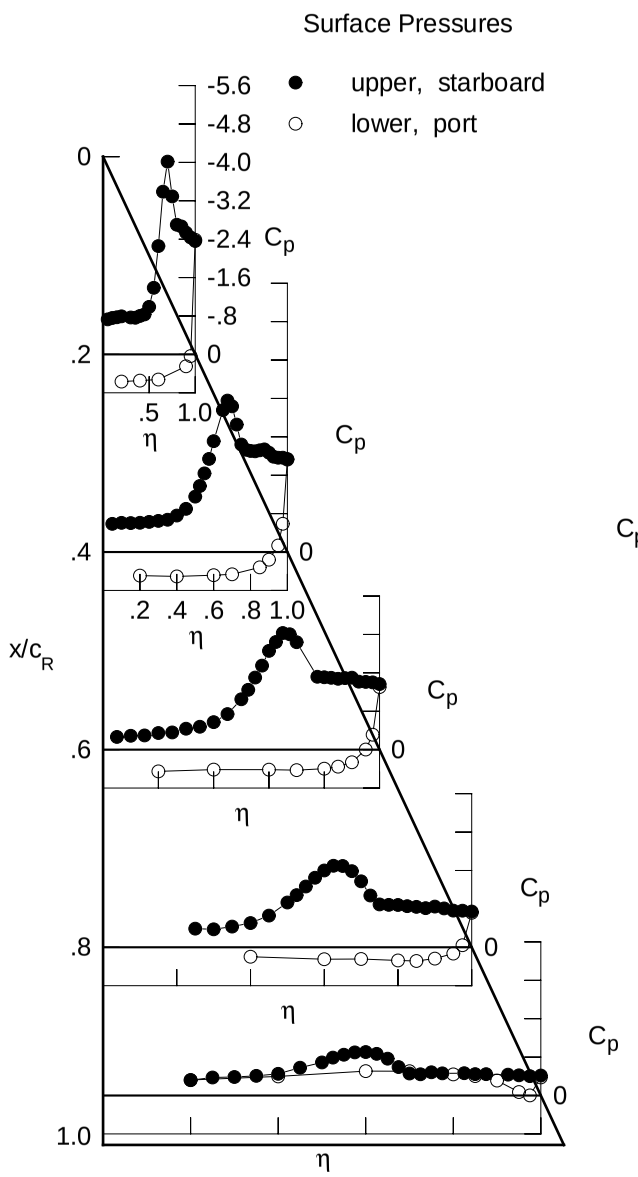
$R_{mac}$ = $5.7 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -2.3082 | ******* |
| 0.20 | -2.2523 | -2.2748 |
| 0.30 | -2.0985 | ******* |
| 0.40 | -1.8713 | -1.8654 |
| 0.50 | -1.6244 | ******* |
| 0.60 | -1.3348 | -1.3496 |
| 0.70 | -1.0686 | ******* |
| 0.80 | -0.7432 | -0.7624 |
| 0.90 | -0.4458 | ******* |
| 0.95 | -0.3699 | -0.3572 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.7299 | -0.5871 | -0.2647 | ******* | ******* |
| 0.100 | -0.7583 | -0.6077 | -0.2889 | ******* | ******* |
| 0.150 | -0.7740 | -0.6032 | -0.2960 | ******* | ******* |
| 0.200 | -0.7925 | -0.6100 | -0.3463 | ******* | -0.3189 |
| 0.250 | ******* | -0.6277 | -0.3584 | -0.3880 | -0.3755 |
| 0.300 | -0.7690 | -0.6489 | -0.4361 | -0.3746 | -0.3858 |
| 0.350 | -0.7629 | -0.6729 | -0.4770 | -0.4313 | -0.4093 |
| 0.400 | -0.8010 | -0.7597 | -0.5730 | -0.5050 | -0.4523 |
| 0.450 | -0.8327 | -0.8997 | -0.7407 | -0.6601 | -0.5796 |
| 0.500 | -0.9905 | -1.1543 | -1.0495 | -0.9328 | -0.6889 |
| 0.525 | ******* | -1.3758 | -1.2462 | -1.0864 | -0.7899 |
| 0.550 | -1.3869 | -1.6387 | -1.5019 | -1.2665 | -0.8492 |
| 0.575 | ******* | -1.9397 | -1.7501 | -1.4484 | -0.8981 |
| 0.600 | -2.2564 | -2.3098 | -2.0579 | -1.6002 | -0.9056 |
| 0.625 | ******* | ******* | -2.2421 | -1.6985 | -0.8683 |
| 0.650 | -3.3898 | -2.9558 | -2.4293 | -1.6937 | -0.7672 |
| 0.675 | ******* | -3.1549 | -2.4040 | -1.5857 | -0.5928 |
| 0.700 | -4.0158 | -3.0349 | -2.2388 | -1.3742 | -0.4588 |
| 0.725 | ******* | -2.6555 | ******* | -1.0782 | -0.4427 |
| 0.750 | -3.2916 | -2.2397 | ******* | -0.8929 | -0.4837 |
| 0.775 | ******* | -2.1315 | -1.5183 | -0.8840 | -0.4613 |
| 0.800 | -2.7009 | -2.1063 | -1.5077 | -0.8820 | ******* |
| 0.825 | ******* | -2.0986 | -1.4971 | -0.8571 | -0.4648 |
| 0.850 | -2.6658 | -2.1193 | -1.4762 | -0.8425 | -0.4459 |
| 0.875 | ******* | -2.1381 | -1.4903 | -0.8155 | -0.4447 |
| 0.900 | -2.5369 | -2.0698 | -1.4988 | -0.8479 | ******* |
| 0.925 | ******* | -1.9856 | -1.4163 | -0.8097 | -0.4344 |
| 0.950 | -2.4361 | -1.9646 | -1.4112 | -0.7636 | -0.4206 |
| 0.975 | ******* | -1.9658 | -1.4013 | -0.7623 | -0.4033 |
| 1.000 | -2.3626 | -1.9379 | -1.3667 | -0.7452 | -0.4156 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5664 | 0.4911 | 0.4526 | ******* | -0.3236 |
| -0.400 | 0.5462 | 0.5081 | 0.4161 | 0.1970 | -0.3978 |
| -0.600 | 0.5237 | 0.4826 | 0.4170 | 0.2487 | -0.5082 |
| -0.700 | ******* | 0.4638 | 0.4274 | 0.2443 | -0.5060 |
| -0.800 | ******* | ******* | 0.3970 | 0.2747 | -0.4401 |
| -0.850 | ******* | 0.3196 | 0.3543 | 0.2856 | -0.4045 |
| -0.900 | 0.2482 | 0.1595 | 0.2635 | 0.2358 | -0.3111 |
| -0.950 | 0.0352 | -0.1363 | -0.0026 | 0.1308 | -0.0718 |
| -0.975 | ******* | -0.5887 | -0.3114 | -0.0433 | -0.0022 |
| -1.000 | -2.3879 | -1.9254 | -1.3035 | -0.7182 | -0.3766 |



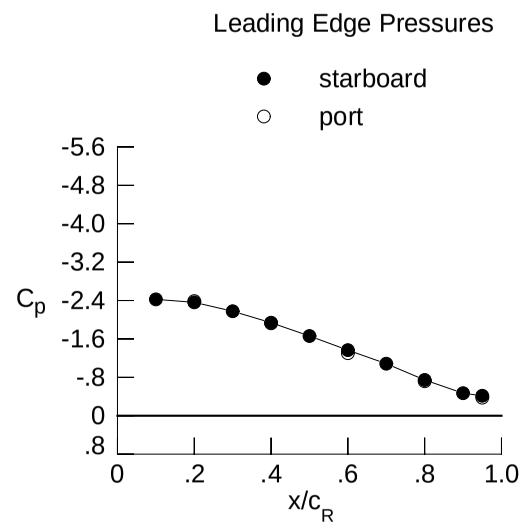

Small Radius L.E.

Run No. = 36 , Point No. = 739

$C_N$ = 1.178, $C_m$ = -0.1350

$\alpha$ = 25.5 °, $M_\infty$ = 0.398

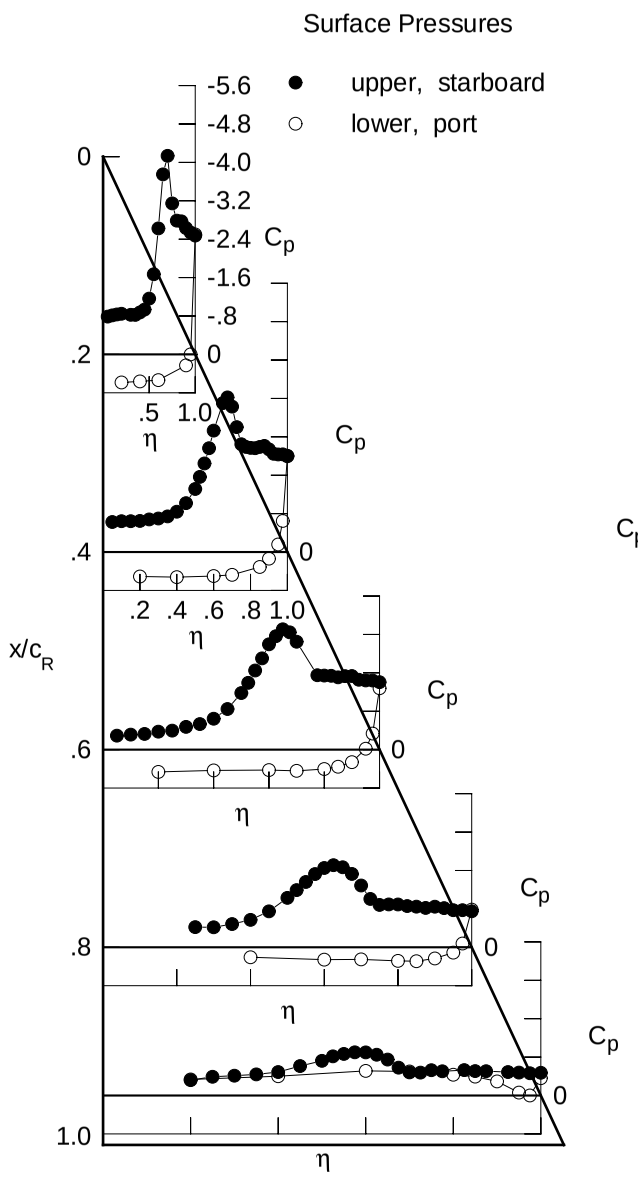
$R_{mac}$ = $5.7 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -2.4242 | ******* |
| 0.20 | -2.3626 | -2.3879 |
| 0.30 | -2.1769 | ******* |
| 0.40 | -1.9379 | -1.9254 |
| 0.50 | -1.6610 | ******* |
| 0.60 | -1.3667 | -1.3035 |
| 0.70 | -1.0839 | ******* |
| 0.80 | -0.7452 | -0.7182 |
| 0.90 | -0.4693 | ******* |
| 0.95 | -0.4156 | -0.3766 |

# Table D1. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.7869 | -0.6256 | -0.2914 | ******* | ******* |
| 0.100 | -0.8127 | -0.6425 | -0.3127 | ******* | ******* |
| 0.150 | -0.8319 | -0.6427 | -0.3269 | ******* | ******* |
| 0.200 | -0.8468 | -0.6481 | -0.3743 | ******* | -0.3202 |
| 0.250 | ******* | -0.6789 | -0.3957 | -0.4199 | -0.3906 |
| 0.300 | -0.8246 | -0.6982 | -0.4746 | -0.4167 | -0.4130 |
| 0.350 | -0.8233 | -0.7420 | -0.5326 | -0.4842 | -0.4399 |
| 0.400 | -0.8743 | -0.8399 | -0.6437 | -0.5709 | -0.4891 |
| 0.450 | -0.9335 | -1.0185 | -0.8462 | -0.7491 | -0.6139 |
| 0.500 | -1.1622 | -1.3135 | -1.1791 | -1.0294 | -0.7227 |
| 0.525 | ******* | -1.5660 | -1.3924 | -1.1911 | -0.8163 |
| 0.550 | -1.6693 | -1.8458 | -1.6484 | -1.3609 | -0.8660 |
| 0.575 | ******* | -2.1633 | -1.9017 | -1.5253 | -0.9003 |
| 0.600 | -2.6247 | -2.5293 | -2.1944 | -1.6520 | -0.8986 |
| 0.625 | ******* | ******* | -2.3628 | -1.7104 | -0.8494 |
| 0.650 | -3.7506 | -3.1032 | -2.5076 | -1.6670 | -0.7487 |
| 0.675 | ******* | -3.2217 | -2.4443 | -1.5283 | -0.5800 |
| 0.700 | -4.1365 | -3.0296 | -2.2477 | -1.2869 | -0.4815 |
| 0.725 | ******* | -2.6022 | ******* | -1.0073 | -0.4765 |
| 0.750 | -3.1453 | -2.2457 | ******* | -0.8822 | -0.5273 |
| 0.775 | ******* | -2.1903 | -1.5507 | -0.8925 | -0.5045 |
| 0.800 | -2.7862 | -2.1702 | -1.5432 | -0.8924 | ******* |
| 0.825 | ******* | -2.1628 | -1.5387 | -0.8596 | -0.5292 |
| 0.850 | -2.7718 | -2.1892 | -1.5066 | -0.8461 | -0.5089 |
| 0.875 | ******* | -2.2109 | -1.5309 | -0.8203 | -0.5066 |
| 0.900 | -2.6314 | -2.1394 | -1.5338 | -0.8458 | ******* |
| 0.925 | ******* | -2.0472 | -1.4557 | -0.8161 | -0.4887 |
| 0.950 | -2.5382 | -2.0330 | -1.4415 | -0.7728 | -0.4779 |
| 0.975 | ******* | -2.0350 | -1.4396 | -0.7725 | -0.4643 |
| 1.000 | -2.4753 | -2.0049 | -1.4054 | -0.7501 | -0.4737 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5849 | 0.5092 | 0.4639 | ******* | -0.3345 |
| -0.400 | 0.5630 | 0.5229 | 0.4331 | 0.2076 | -0.4017 |
| -0.600 | 0.5358 | 0.5003 | 0.4256 | 0.2573 | -0.5132 |
| -0.700 | ******* | 0.4752 | 0.4419 | 0.2524 | -0.5006 |
| -0.800 | ******* | ******* | 0.4042 | 0.2834 | -0.4328 |
| -0.850 | ******* | 0.3112 | 0.3558 | 0.2904 | -0.3934 |
| -0.900 | 0.2292 | 0.1379 | 0.2609 | 0.2331 | -0.2936 |
| -0.950 | -0.0003 | -0.1576 | -0.0189 | 0.1109 | -0.0610 |
| -0.975 | ******* | -0.6477 | -0.3350 | -0.0786 | -0.0007 |
| -1.000 | -2.4992 | -1.9949 | -1.2790 | -0.7847 | -0.3612 |



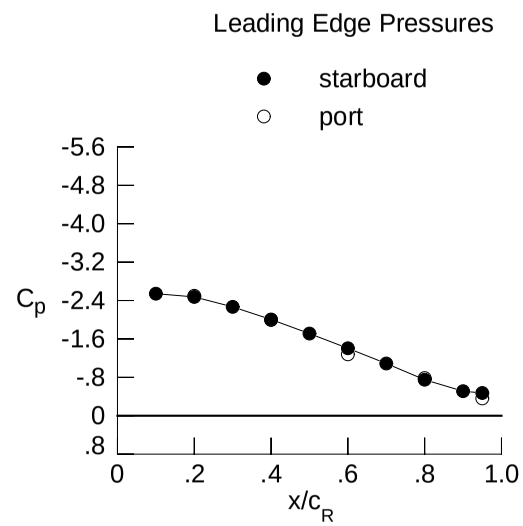

Small Radius L.E.

Run No. = 36 , Point No. = 740

$C_N$ = 1.235, $C_m$ = -0.1464

$\alpha$ = 26.5 °, $M_\infty$ = 0.399

$R_{mac}$ = $5.7 \times 10^6$

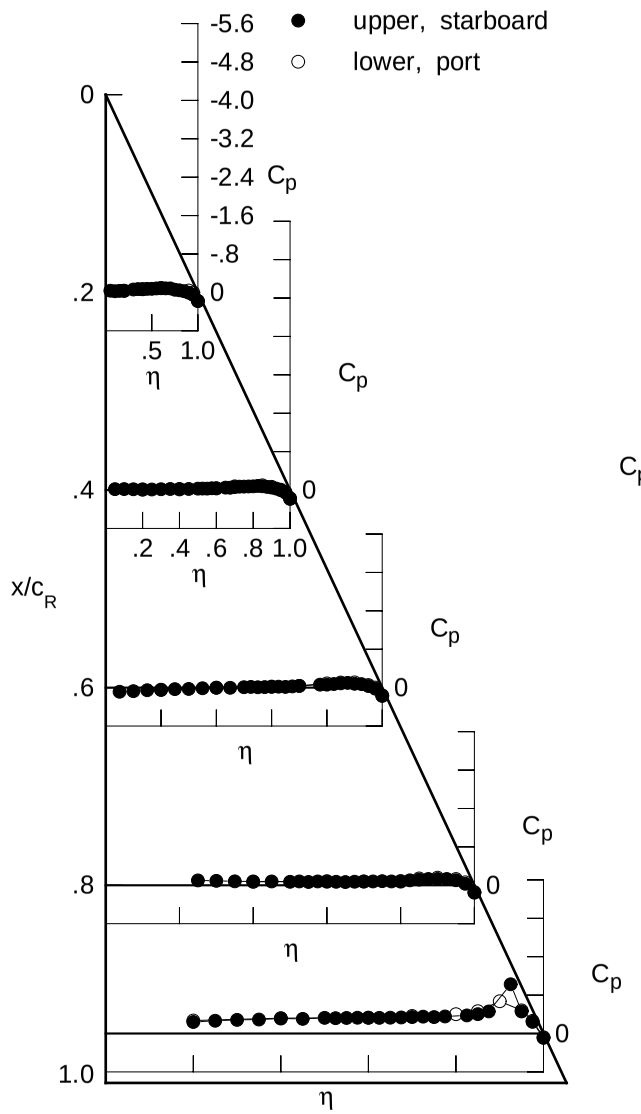



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -2.5426 | ******* |
| 0.20 | -2.4753 | -2.4992 |
| 0.30 | -2.2678 | ******* |
| 0.40 | -2.0049 | -1.9949 |
| 0.50 | -1.7117 | ******* |
| 0.60 | -1.4054 | -1.2790 |
| 0.70 | -1.0879 | ******* |
| 0.80 | -0.7501 | -0.7847 |
| 0.90 | -0.5113 | ******* |
| 0.95 | -0.4737 | -0.3612 |

# Table D1. Concluded.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0354 | -0.0185 | 0.0859 | ******* | ******* |
| 0.100 | -0.0241 | -0.0200 | 0.0739 | ******* | ******* |
| 0.150 | -0.0320 | -0.0160 | 0.0534 | ******* | ******* |
| 0.200 | -0.0314 | -0.0148 | 0.0477 | ******* | -0.2402 |
| 0.250 | ******* | -0.0110 | 0.0310 | -0.1017 | -0.2657 |
| 0.300 | -0.0599 | -0.0166 | 0.0273 | -0.0927 | -0.2843 |
| 0.350 | -0.0686 | -0.0213 | 0.0127 | -0.0823 | -0.2909 |
| 0.400 | -0.0646 | -0.0222 | 0.0014 | -0.0800 | -0.3117 |
| 0.450 | -0.0739 | -0.0227 | 0.0032 | -0.0800 | -0.3049 |
| 0.500 | -0.0747 | -0.0286 | -0.0088 | -0.0731 | -0.3267 |
| 0.525 | ******* | -0.0307 | -0.0148 | -0.0802 | -0.3192 |
| 0.550 | -0.0828 | -0.0298 | -0.0078 | -0.0688 | -0.3238 |
| 0.575 | ******* | -0.0371 | -0.0111 | -0.0801 | -0.3290 |
| 0.600 | -0.0861 | -0.0363 | -0.0175 | -0.0746 | -0.3282 |
| 0.625 | ******* | ******* | -0.0197 | -0.0725 | -0.3263 |
| 0.650 | -0.0840 | -0.0500 | -0.0151 | -0.0671 | -0.3298 |
| 0.675 | ******* | -0.0480 | -0.0256 | -0.0747 | -0.3344 |
| 0.700 | -0.0834 | -0.0623 | -0.0359 | -0.0759 | -0.3424 |
| 0.725 | ******* | -0.0703 | ******* | -0.0800 | -0.3515 |
| 0.750 | -0.0554 | -0.0716 | ******* | -0.0858 | -0.3426 |
| 0.775 | ******* | -0.0741 | -0.0627 | -0.0798 | -0.3549 |
| 0.800 | -0.0435 | -0.0765 | -0.0624 | -0.0763 | ******* |
| 0.825 | ******* | -0.0852 | -0.0752 | -0.1031 | -0.3768 |
| 0.850 | -0.0249 | -0.0784 | -0.0893 | -0.1185 | -0.4033 |
| 0.875 | ******* | -0.0654 | -0.0989 | -0.1311 | -0.4600 |
| 0.900 | 0.0073 | -0.0512 | -0.0809 | -0.1309 | ******* |
| 0.925 | ******* | -0.0305 | -0.0736 | -0.1310 | -1.0254 |
| 0.950 | 0.0530 | 0.0040 | -0.0334 | -0.1051 | -0.4595 |
| 0.975 | ******* | 0.0519 | 0.0219 | -0.0320 | -0.2423 |
| 1.000 | 0.1809 | 0.1855 | 0.1725 | 0.1543 | 0.0908 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0363 | -0.0066 | 0.0428 | ******* | -0.2706 |
| -0.400 | -0.0683 | -0.0128 | 0.0020 | -0.0723 | -0.3197 |
| -0.600 | -0.0939 | -0.0354 | -0.0215 | -0.0858 | -0.3306 |
| -0.700 | ******* | -0.0764 | -0.0379 | -0.0817 | -0.3653 |
| -0.800 | ******* | ******* | -0.0881 | -0.0890 | -0.4022 |
| -0.850 | ******* | -0.0983 | -0.1064 | -0.1423 | -0.4650 |
| -0.900 | -0.0381 | -0.0676 | -0.1095 | -0.1586 | -0.6718 |
| -0.950 | 0.0024 | -0.0076 | -0.0548 | -0.1307 | -0.4819 |
| -0.975 | ******* | 0.0449 | -0.0016 | -0.0619 | -0.2636 |
| -1.000 | 0.1786 | 0.1689 | 0.1596 | 0.1412 | 0.0787 |

Surface Pressures




Small Radius L.E.

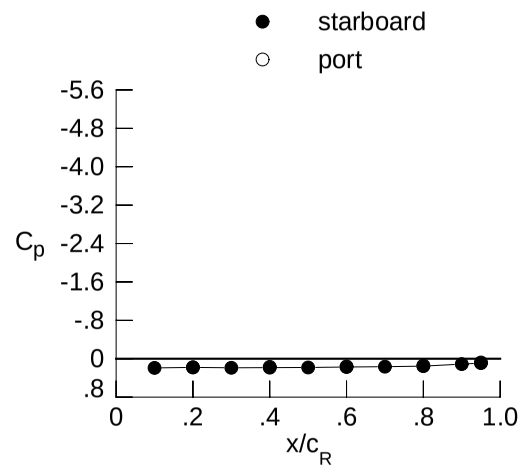
Run No. = 36 , Point No. = 741

$C_N$ = -0.052, $C_m$ = 0.0313

$\alpha$ = 0.1 °, $M_\infty$ = 0.399

$R_{mac}$ = $5.8 \times 10^6$

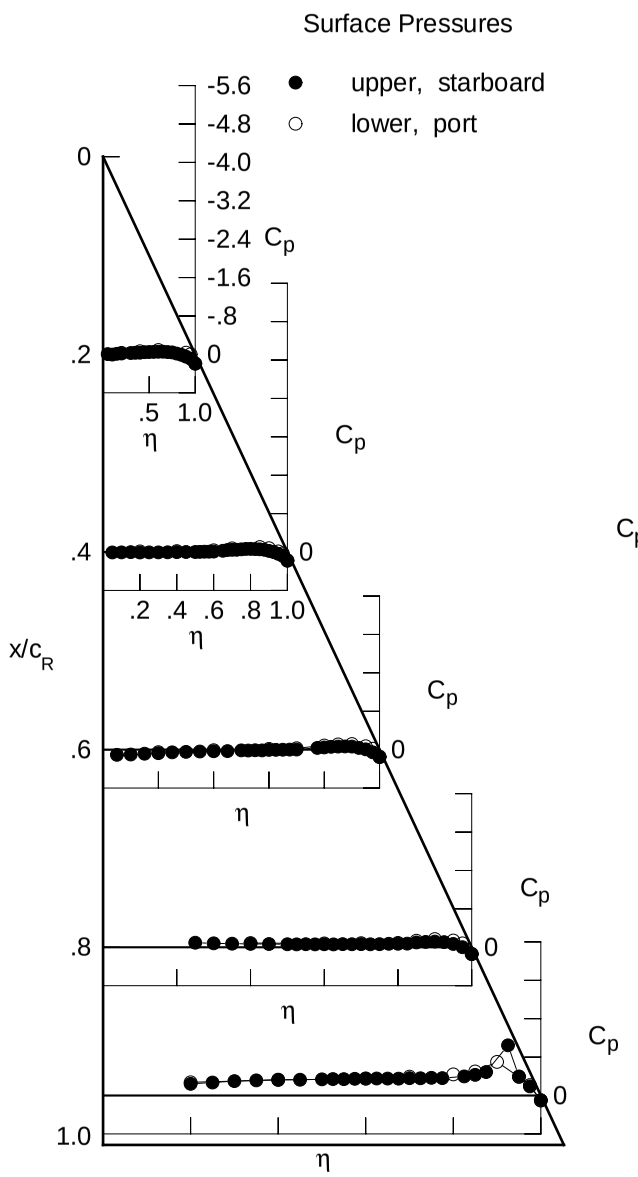
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.1913 | ******* |
| 0.20 | 0.1809 | 0.1786 |
| 0.30 | 0.1887 | ******* |
| 0.40 | 0.1855 | 0.1689 |
| 0.50 | 0.1823 | ******* |
| 0.60 | 0.1725 | 0.1596 |
| 0.70 | 0.1658 | ******* |
| 0.80 | 0.1543 | 0.1412 |
| 0.90 | 0.1121 | ******* |
| 0.95 | 0.0908 | 0.0787 |

# Table D2. Tabulations and Plots of Surface Pressure Coefficients.

| | $x/c_R$ .2 | $x/c_R$ .4 | $x/c_R$ .6 | $x/c_R$ .8 | $x/c_R$ .95 |
|---|---|---|---|---|---|
| $\eta$ | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ |
| 0.050 | -0.0066 | 0.0084 | 0.1082 | ******* | ******* |
| 0.100 | 0.0039 | 0.0074 | 0.1017 | ******* | ******* |
| 0.150 | -0.0129 | 0.0023 | 0.0848 | ******* | ******* |
| 0.200 | -0.0188 | 0.0092 | 0.0734 | ******* | -0.2434 |
| 0.250 | ******* | 0.0071 | 0.0559 | -0.0950 | -0.2704 |
| 0.300 | -0.0289 | 0.0076 | 0.0465 | -0.0823 | -0.2998 |
| 0.350 | -0.0338 | 0.0055 | 0.0390 | -0.0755 | -0.3150 |
| 0.400 | -0.0355 | 0.0015 | 0.0335 | -0.0709 | -0.3302 |
| 0.450 | -0.0456 | -0.0008 | 0.0301 | -0.0676 | -0.3289 |
| 0.500 | -0.0495 | -0.0006 | 0.0153 | -0.0634 | -0.3370 |
| 0.525 | ******* | -0.0044 | 0.0188 | -0.0606 | -0.3424 |
| 0.550 | -0.0523 | -0.0074 | 0.0126 | -0.0638 | -0.3404 |
| 0.575 | ******* | -0.0075 | 0.0159 | -0.0604 | -0.3478 |
| 0.600 | -0.0553 | -0.0093 | 0.0051 | -0.0632 | -0.3563 |
| 0.625 | ******* | ******* | 0.0044 | -0.0602 | -0.3548 |
| 0.650 | -0.0558 | -0.0265 | 0.0020 | -0.0656 | -0.3524 |
| 0.675 | ******* | -0.0422 | -0.0008 | -0.0633 | -0.3512 |
| 0.700 | -0.0491 | -0.0463 | -0.0023 | -0.0654 | -0.3613 |
| 0.725 | ******* | -0.0473 | ******* | -0.0625 | -0.3594 |
| 0.750 | -0.0417 | -0.0564 | ******* | -0.0651 | -0.3692 |
| 0.775 | ******* | -0.0647 | -0.0360 | -0.0727 | -0.3625 |
| 0.800 | -0.0166 | -0.0659 | -0.0454 | -0.0738 | ******* |
| 0.825 | ******* | -0.0613 | -0.0591 | -0.0758 | -0.3977 |
| 0.850 | 0.0097 | -0.0569 | -0.0640 | -0.1006 | -0.4307 |
| 0.875 | ******* | -0.0469 | -0.0661 | -0.1122 | -0.4890 |
| 0.900 | 0.0472 | -0.0242 | -0.0639 | -0.1195 | ******* |
| 0.925 | ******* | -0.0003 | -0.0361 | -0.1074 | -1.0455 |
| 0.950 | 0.0898 | 0.0366 | -0.0062 | -0.0695 | -0.3976 |
| 0.975 | ******* | 0.0807 | 0.0552 | -0.0018 | -0.1905 |
| 1.000 | 0.1956 | 0.1825 | 0.1578 | 0.1447 | 0.0962 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0321 | -0.0125 | 0.0526 | ******* | -0.2755 |
| -0.400 | -0.0657 | -0.0195 | 0.0117 | -0.0879 | -0.3241 |
| -0.600 | -0.0916 | -0.0361 | -0.0149 | -0.0797 | -0.3498 |
| -0.700 | ******* | -0.0763 | -0.0291 | -0.0855 | -0.3930 |
| -0.800 | ******* | ******* | -0.0855 | -0.0914 | -0.4397 |
| -0.850 | ******* | -0.1037 | -0.1089 | -0.1365 | -0.5010 |
| -0.900 | -0.0359 | -0.0797 | -0.1167 | -0.1711 | -0.6998 |
| -0.950 | -0.0035 | -0.0128 | -0.0705 | -0.1408 | -0.3868 |
| -0.975 | ******* | 0.0255 | -0.0188 | -0.0819 | -0.2175 |
| -1.000 | 0.1879 | 0.1703 | 0.1434 | 0.1351 | 0.1063 |



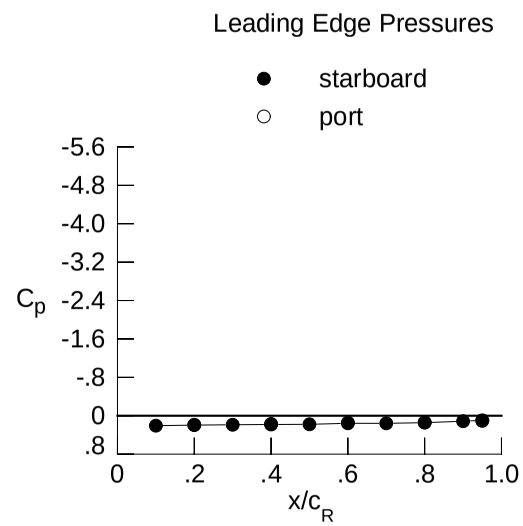

Small Radius L.E.

Run No. = 38 , Point No. = 750

$C_N$ = -0.010, $C_m$ = -0.0075

$\alpha$ = -0.4 °, $M_\infty$ = 0.601

$R_{mac}$ = $6.0 \times 10^6$

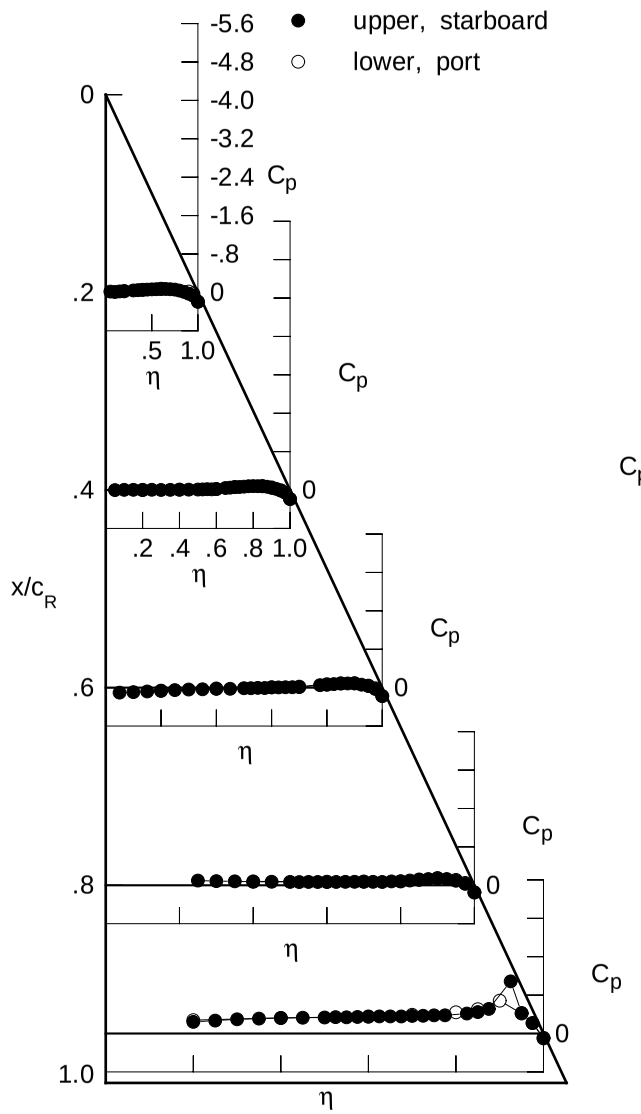



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2075 | ******* |
| 0.20 | 0.1956 | 0.1879 |
| 0.30 | 0.1880 | ******* |
| 0.40 | 0.1825 | 0.1703 |
| 0.50 | 0.1787 | ******* |
| 0.60 | 0.1578 | 0.1434 |
| 0.70 | 0.1584 | ******* |
| 0.80 | 0.1447 | 0.1351 |
| 0.90 | 0.1143 | ******* |
| 0.95 | 0.0962 | 0.1063 |

# Table D2. Continued.

| η | x/c_R .2 C_p,u | x/c_R .4 C_p,u | x/c_R .6 C_p,u | x/c_R .8 C_p,u | x/c_R .95 C_p,u |
|---|---|---|---|---|---|
| 0.050 | -0.0168 | 0.0017 | 0.1041 | ******* | ******* |
| 0.100 | -0.0081 | -0.0036 | 0.0936 | ******* | ******* |
| 0.150 | -0.0198 | -0.0046 | 0.0802 | ******* | ******* |
| 0.200 | -0.0286 | 0.0012 | 0.0681 | ******* | -0.2425 |
| 0.250 | ******* | -0.0056 | 0.0511 | -0.0986 | -0.2689 |
| 0.300 | -0.0400 | -0.0014 | 0.0388 | -0.0868 | -0.2963 |
| 0.350 | -0.0464 | -0.0037 | 0.0345 | -0.0823 | -0.3108 |
| 0.400 | -0.0526 | -0.0072 | 0.0258 | -0.0728 | -0.3218 |
| 0.450 | -0.0576 | -0.0083 | 0.0243 | -0.0732 | -0.3290 |
| 0.500 | -0.0631 | -0.0107 | 0.0124 | -0.0700 | -0.3332 |
| 0.525 | ******* | -0.0129 | 0.0117 | -0.0671 | -0.3405 |
| 0.550 | -0.0660 | -0.0176 | 0.0046 | -0.0700 | -0.3380 |
| 0.575 | ******* | -0.0145 | 0.0077 | -0.0687 | -0.3448 |
| 0.600 | -0.0695 | -0.0214 | -0.0045 | -0.0682 | -0.3545 |
| 0.625 | ******* | ******* | -0.0048 | -0.0695 | -0.3560 |
| 0.650 | -0.0714 | -0.0426 | -0.0080 | -0.0716 | -0.3561 |
| 0.675 | ******* | -0.0493 | -0.0085 | -0.0730 | -0.3552 |
| 0.700 | -0.0654 | -0.0599 | -0.0116 | -0.0722 | -0.3661 |
| 0.725 | ******* | -0.0635 | ******* | -0.0723 | -0.3692 |
| 0.750 | -0.0586 | -0.0701 | ******* | -0.0684 | -0.3781 |
| 0.775 | ******* | -0.0792 | -0.0508 | -0.0811 | -0.3789 |
| 0.800 | -0.0378 | -0.0820 | -0.0595 | -0.0798 | ******* |
| 0.825 | ******* | -0.0799 | -0.0734 | -0.0989 | -0.4159 |
| 0.850 | -0.0103 | -0.0773 | -0.0833 | -0.1129 | -0.4465 |
| 0.875 | ******* | -0.0688 | -0.0872 | -0.1296 | -0.5124 |
| 0.900 | 0.0276 | -0.0458 | -0.0860 | -0.1422 | ******* |
| 0.925 | ******* | -0.0243 | -0.0619 | -0.1307 | -1.0862 |
| 0.950 | 0.0701 | 0.0129 | -0.0324 | -0.0947 | -0.4281 |
| 0.975 | ******* | 0.0543 | 0.0283 | -0.0308 | -0.2178 |
| 1.000 | 0.1937 | 0.1862 | 0.1771 | 0.1447 | 0.0894 |
| | C_p,l | C_p,l | C_p,l | C_p,l | C_p,l |
| -0.200 | -0.0216 | -0.0050 | 0.0620 | ******* | -0.2785 |
| -0.400 | -0.0548 | -0.0082 | 0.0171 | -0.0816 | -0.3259 |
| -0.600 | -0.0767 | -0.0186 | -0.0077 | -0.0747 | -0.3502 |
| -0.700 | ******* | -0.0629 | -0.0211 | -0.0789 | -0.3906 |
| -0.800 | ******* | ******* | -0.0723 | -0.0849 | -0.4414 |
| -0.850 | ******* | -0.0836 | -0.0916 | -0.1218 | -0.5064 |
| -0.900 | -0.0166 | -0.0553 | -0.0940 | -0.1509 | -0.6839 |
| -0.950 | 0.0171 | 0.0049 | -0.0424 | -0.1131 | -0.4161 |
| -0.975 | ******* | 0.0550 | 0.0128 | -0.0494 | -0.2166 |
| -1.000 | 0.1954 | 0.1877 | 0.1739 | 0.1521 | 0.1030 |

Surface Pressures




Small Radius L.E.

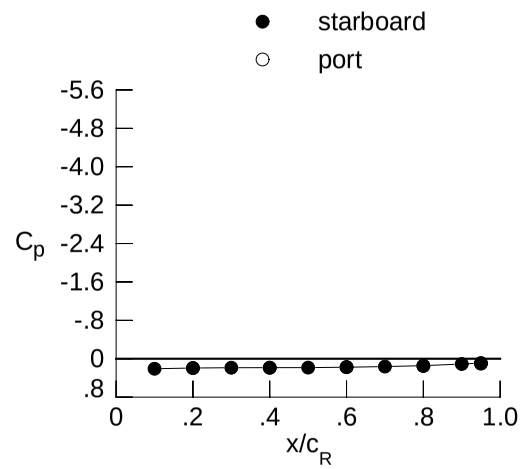
Run No. = 38 , Point No. = 751

$C_N$ = 0.007, $C_m$ = -0.0102

$\alpha$ = 0.1 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

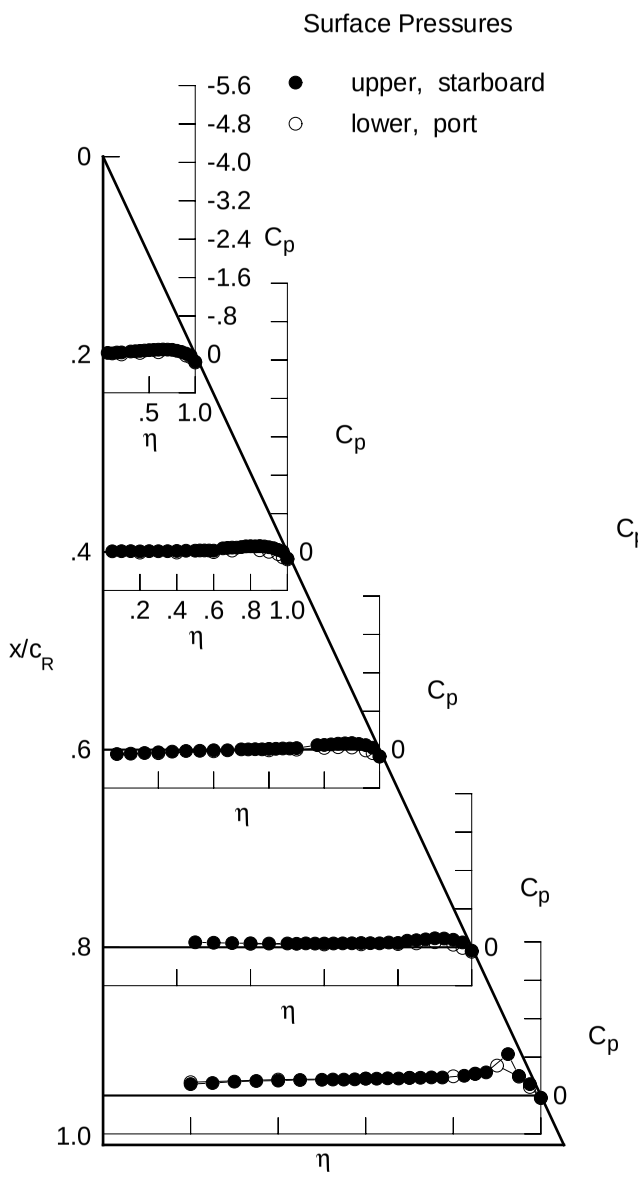
Leading Edge Pressures




| x/c_R | starb'd C_p | port C_p |
|---|---|---|
| 0.10 | 0.2085 | ******* |
| 0.20 | 0.1937 | 0.1954 |
| 0.30 | 0.1871 | ******* |
| 0.40 | 0.1862 | 0.1877 |
| 0.50 | 0.1851 | ******* |
| 0.60 | 0.1771 | 0.1739 |
| 0.70 | 0.1634 | ******* |
| 0.80 | 0.1447 | 0.1521 |
| 0.90 | 0.1098 | ******* |
| 0.95 | 0.0894 | 0.1030 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0316 | -0.0148 | 0.0916 | ******* | ******* |
| 0.100 | -0.0204 | -0.0175 | 0.0837 | ******* | ******* |
| 0.150 | -0.0390 | -0.0183 | 0.0702 | ******* | ******* |
| 0.200 | -0.0410 | -0.0134 | 0.0561 | ******* | -0.2378 |
| 0.250 | ******* | -0.0188 | 0.0413 | -0.1040 | -0.2600 |
| 0.300 | -0.0599 | -0.0166 | 0.0284 | -0.0941 | -0.2886 |
| 0.350 | -0.0654 | -0.0172 | 0.0241 | -0.0870 | -0.3020 |
| 0.400 | -0.0725 | -0.0225 | 0.0124 | -0.0829 | -0.3107 |
| 0.450 | -0.0799 | -0.0269 | 0.0135 | -0.0777 | -0.3234 |
| 0.500 | -0.0879 | -0.0277 | -0.0058 | -0.0793 | -0.3276 |
| 0.525 | ******* | -0.0324 | -0.0048 | -0.0731 | -0.3325 |
| 0.550 | -0.0930 | -0.0327 | -0.0089 | -0.0806 | -0.3316 |
| 0.575 | ******* | -0.0321 | -0.0065 | -0.0768 | -0.3368 |
| 0.600 | -0.0974 | -0.0285 | -0.0162 | -0.0774 | -0.3529 |
| 0.625 | ******* | ******* | -0.0176 | -0.0791 | -0.3505 |
| 0.650 | -0.1017 | -0.0771 | -0.0237 | -0.0819 | -0.3583 |
| 0.675 | ******* | -0.0865 | -0.0231 | -0.0830 | -0.3541 |
| 0.700 | -0.0995 | -0.0917 | -0.0319 | -0.0891 | -0.3663 |
| 0.725 | ******* | -0.0911 | ******* | -0.0856 | -0.3694 |
| 0.750 | -0.0953 | -0.1031 | ******* | -0.0823 | -0.3770 |
| 0.775 | ******* | -0.1188 | -0.0938 | -0.0994 | -0.3756 |
| 0.800 | -0.0749 | -0.1215 | -0.0980 | -0.0903 | ******* |
| 0.825 | ******* | -0.1194 | -0.1094 | -0.1367 | -0.4108 |
| 0.850 | -0.0508 | -0.1245 | -0.1237 | -0.1476 | -0.4487 |
| 0.875 | ******* | -0.1162 | -0.1314 | -0.1646 | -0.4813 |
| 0.900 | -0.0168 | -0.1004 | -0.1369 | -0.1873 | ******* |
| 0.925 | ******* | -0.0800 | -0.1185 | -0.1821 | -0.8622 |
| 0.950 | 0.0235 | -0.0439 | -0.0946 | -0.1564 | -0.4079 |
| 0.975 | ******* | -0.0093 | -0.0399 | -0.1015 | -0.2371 |
| 1.000 | 0.1530 | 0.1333 | 0.1392 | 0.0703 | 0.0459 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0006 | 0.0122 | 0.0732 | ******* | -0.2768 |
| -0.400 | -0.0302 | 0.0106 | 0.0346 | -0.0717 | -0.3321 |
| -0.600 | -0.0452 | 0.0018 | 0.0141 | -0.0588 | -0.3511 |
| -0.700 | ******* | -0.0308 | 0.0001 | -0.0618 | -0.3698 |
| -0.800 | ******* | ******* | -0.0359 | -0.0673 | -0.3997 |
| -0.850 | ******* | -0.0377 | -0.0512 | -0.0818 | -0.4561 |
| -0.900 | 0.0246 | -0.0050 | -0.0447 | -0.1059 | -0.6231 |
| -0.950 | 0.0602 | 0.0430 | 0.0159 | -0.0534 | -0.3928 |
| -0.975 | ******* | 0.1101 | 0.0731 | 0.0138 | -0.1776 |
| -1.000 | 0.1690 | 0.1536 | 0.1459 | 0.0932 | 0.0534 |



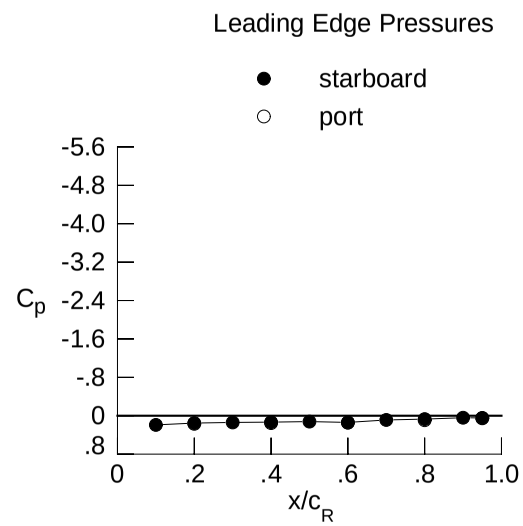

Small Radius L.E.

Run No. = 38 , Point No. = 752

$C_N$ = 0.044, $C_m$ = -0.0149

$\alpha$ = 1.1 °, $M_\infty$ = 0.601

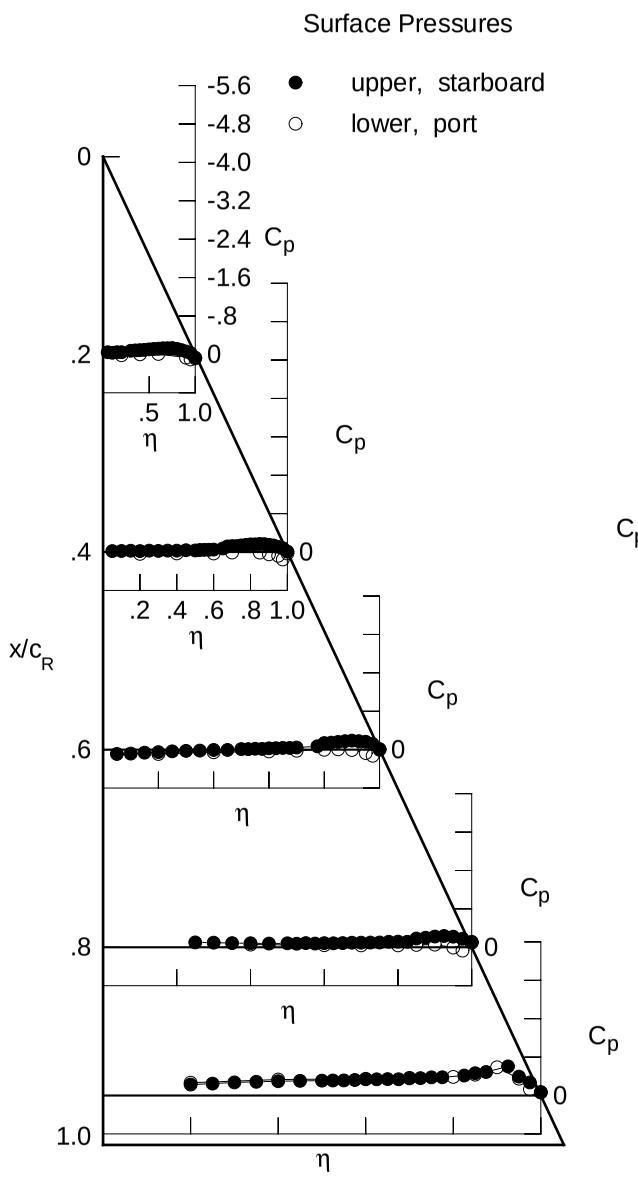
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.1909 | ******* |
| 0.20 | 0.1530 | 0.1690 |
| 0.30 | 0.1396 | ******* |
| 0.40 | 0.1333 | 0.1536 |
| 0.50 | 0.1221 | ******* |
| 0.60 | 0.1392 | 0.1459 |
| 0.70 | 0.0883 | ******* |
| 0.80 | 0.0703 | 0.0932 |
| 0.90 | 0.0416 | ******* |
| 0.95 | 0.0459 | 0.0534 |

# Table D2. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0444 | -0.0199 | 0.0905 | ******* | ******* |
| 0.100 | -0.0333 | -0.0216 | 0.0828 | ******* | ******* |
| 0.150 | -0.0451 | -0.0270 | 0.0629 | ******* | ******* |
| 0.200 | -0.0453 | -0.0199 | 0.0519 | ******* | -0.2279 |
| 0.250 | ******* | -0.0285 | 0.0353 | -0.1016 | -0.2480 |
| 0.300 | -0.0759 | -0.0228 | 0.0259 | -0.0964 | -0.2730 |
| 0.350 | -0.0831 | -0.0295 | 0.0199 | -0.0868 | -0.2856 |
| 0.400 | -0.0881 | -0.0286 | 0.0065 | -0.0838 | -0.2978 |
| 0.450 | -0.0943 | -0.0379 | 0.0060 | -0.0778 | -0.3052 |
| 0.500 | -0.1046 | -0.0325 | -0.0113 | -0.0828 | -0.3093 |
| 0.525 | ******* | -0.0425 | -0.0106 | -0.0746 | -0.3126 |
| 0.550 | -0.1130 | -0.0453 | -0.0180 | -0.0873 | -0.3147 |
| 0.575 | ******* | -0.0473 | -0.0150 | -0.0773 | -0.3231 |
| 0.600 | -0.1189 | -0.0508 | -0.0283 | -0.0853 | -0.3383 |
| 0.625 | ******* | ******* | -0.0294 | -0.0832 | -0.3380 |
| 0.650 | -0.1279 | -0.0745 | -0.0359 | -0.0871 | -0.3418 |
| 0.675 | ******* | -0.1166 | -0.0355 | -0.0951 | -0.3382 |
| 0.700 | -0.1287 | -0.1234 | -0.0439 | -0.0960 | -0.3575 |
| 0.725 | ******* | -0.1236 | ******* | -0.0986 | -0.3616 |
| 0.750 | -0.1320 | -0.1381 | ******* | -0.1001 | -0.3788 |
| 0.775 | ******* | -0.1477 | -0.0700 | -0.1154 | -0.3800 |
| 0.800 | -0.1161 | -0.1596 | -0.1366 | -0.1182 | ******* |
| 0.825 | ******* | -0.1606 | -0.1456 | -0.1148 | -0.4157 |
| 0.850 | -0.0895 | -0.1668 | -0.1600 | -0.1831 | -0.4638 |
| 0.875 | ******* | -0.1648 | -0.1757 | -0.1990 | -0.4898 |
| 0.900 | -0.0607 | -0.1509 | -0.1878 | -0.2236 | ******* |
| 0.925 | ******* | -0.1364 | -0.1760 | -0.2354 | -0.6063 |
| 0.950 | -0.0254 | -0.1088 | -0.1641 | -0.2205 | -0.3939 |
| 0.975 | ******* | -0.0818 | -0.1187 | -0.1777 | -0.2719 |
| 1.000 | 0.0682 | -0.0098 | -0.0123 | -0.1141 | -0.0624 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0176 | 0.0373 | 0.0902 | ******* | -0.2668 |
| -0.400 | -0.0013 | 0.0285 | 0.0545 | -0.0563 | -0.3326 |
| -0.600 | -0.0098 | 0.0299 | 0.0357 | -0.0435 | -0.3479 |
| -0.700 | ******* | 0.0105 | 0.0221 | -0.0401 | -0.3673 |
| -0.800 | ******* | ******* | 0.0032 | -0.0397 | -0.3871 |
| -0.850 | ******* | 0.0110 | -0.0067 | -0.0493 | -0.4343 |
| -0.900 | 0.0677 | 0.0473 | 0.0070 | -0.0557 | -0.5879 |
| -0.950 | 0.1050 | 0.0778 | 0.0715 | 0.0052 | -0.3501 |
| -0.975 | ******* | 0.1552 | 0.1272 | 0.0686 | -0.1304 |
| -1.000 | 0.0835 | 0.0295 | 0.0036 | -0.0938 | -0.0728 |



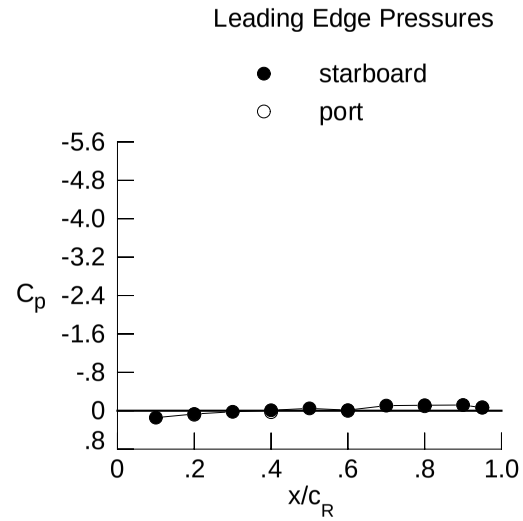

Small Radius L.E.

Run No. = 38 , Point No. = 753

$C_N$ = 0.078, $C_m$ = -0.0181

$\alpha$ = 2.1 °, $M_\infty$ = 0.600

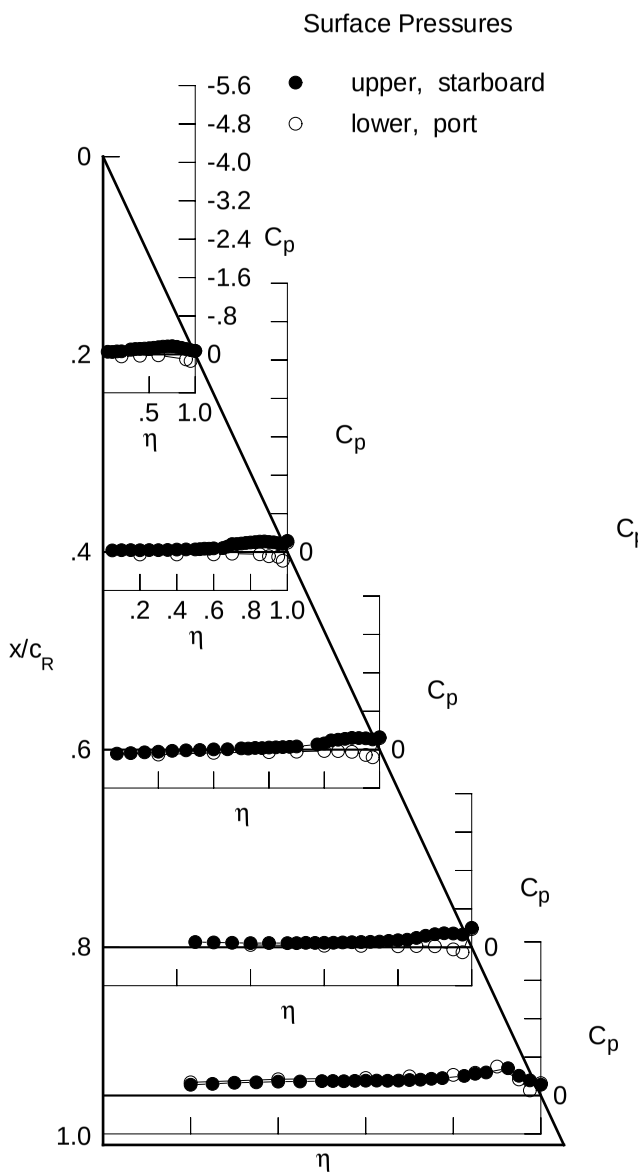
$R_{mac}$ = $6.0 \times 10^6$




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.1443 | ******* |
| 0.20 | 0.0682 | 0.0835 |
| 0.30 | 0.0221 | ******* |
| 0.40 | -0.0098 | 0.0295 |
| 0.50 | -0.0486 | ******* |
| 0.60 | -0.0123 | 0.0036 |
| 0.70 | -0.1063 | ******* |
| 0.80 | -0.1141 | -0.0938 |
| 0.90 | -0.1190 | ******* |
| 0.95 | -0.0624 | -0.0728 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0547 | -0.0337 | 0.0829 | ******* | ******* |
| 0.100 | -0.0505 | -0.0381 | 0.0729 | ******* | ******* |
| 0.150 | -0.0623 | -0.0402 | 0.0558 | ******* | ******* |
| 0.200 | -0.0639 | -0.0376 | 0.0434 | ******* | -0.2239 |
| 0.250 | ******* | -0.0406 | 0.0251 | -0.1094 | -0.2422 |
| 0.300 | -0.1036 | -0.0392 | 0.0147 | -0.1010 | -0.2659 |
| 0.350 | -0.1118 | -0.0434 | 0.0068 | -0.0937 | -0.2743 |
| 0.400 | -0.1152 | -0.0515 | -0.0056 | -0.0867 | -0.2891 |
| 0.450 | -0.1207 | -0.0544 | -0.0082 | -0.0888 | -0.2919 |
| 0.500 | -0.1289 | -0.0548 | -0.0261 | -0.0865 | -0.2998 |
| 0.525 | ******* | -0.0596 | -0.0225 | -0.0866 | -0.3021 |
| 0.550 | -0.1379 | -0.0698 | -0.0352 | -0.0927 | -0.2972 |
| 0.575 | ******* | -0.0689 | -0.0318 | -0.0911 | -0.3050 |
| 0.600 | -0.1492 | -0.0770 | -0.0437 | -0.0939 | -0.3089 |
| 0.625 | ******* | ******* | -0.0479 | -0.0948 | -0.3104 |
| 0.650 | -0.1611 | -0.0831 | -0.0527 | -0.1009 | -0.3071 |
| 0.675 | ******* | -0.1139 | -0.0573 | -0.1059 | -0.3105 |
| 0.700 | -0.1662 | -0.1660 | -0.0661 | -0.1101 | -0.3227 |
| 0.725 | ******* | -0.1668 | ******* | -0.1133 | -0.3296 |
| 0.750 | -0.1711 | -0.1766 | ******* | -0.1181 | -0.3477 |
| 0.775 | ******* | -0.1885 | -0.1085 | -0.1340 | -0.3623 |
| 0.800 | -0.1579 | -0.1981 | -0.1295 | -0.1469 | ******* |
| 0.825 | ******* | -0.2063 | -0.1938 | -0.1574 | -0.4076 |
| 0.850 | -0.1366 | -0.2179 | -0.2065 | -0.1949 | -0.4525 |
| 0.875 | ******* | -0.2205 | -0.2252 | -0.2396 | -0.4799 |
| 0.900 | -0.1132 | -0.2092 | -0.2446 | -0.2725 | ******* |
| 0.925 | ******* | -0.2022 | -0.2416 | -0.2919 | -0.5686 |
| 0.950 | -0.0890 | -0.1846 | -0.2364 | -0.2873 | -0.4112 |
| 0.975 | ******* | -0.1697 | -0.2126 | -0.2641 | -0.3156 |
| 1.000 | -0.0736 | -0.2320 | -0.2594 | -0.4054 | -0.2259 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0415 | 0.0500 | 0.1028 | ******* | -0.2741 |
| -0.400 | 0.0275 | 0.0498 | 0.0661 | -0.0487 | -0.3383 |
| -0.600 | 0.0180 | 0.0483 | 0.0521 | -0.0326 | -0.3651 |
| -0.700 | ******* | 0.0334 | 0.0426 | -0.0297 | -0.3995 |
| -0.800 | ******* | ******* | 0.0282 | -0.0218 | -0.4298 |
| -0.850 | ******* | 0.0464 | 0.0294 | -0.0259 | -0.4733 |
| -0.900 | 0.1029 | 0.0874 | 0.0455 | -0.0216 | -0.6028 |
| -0.950 | 0.1367 | 0.1000 | 0.1104 | 0.0439 | -0.3350 |
| -0.975 | ******* | 0.1820 | 0.1592 | 0.1041 | -0.1062 |
| -1.000 | -0.0711 | -0.1952 | -0.2395 | -0.3790 | -0.2583 |



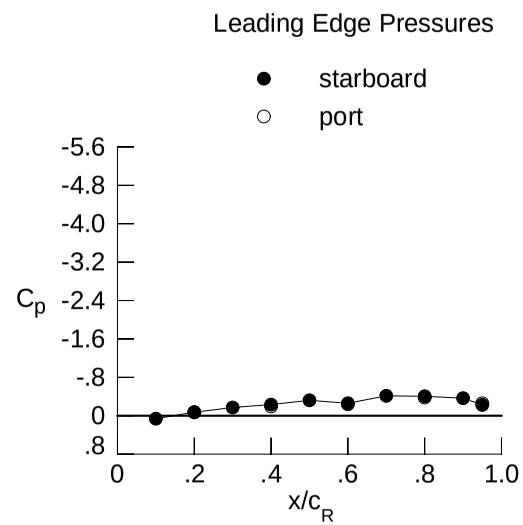

Small Radius L.E.

Run No. = 38 , Point No. = 754

$C_N$ = 0.119, $C_m$ = -0.0281

$\alpha$ = 3.2 °, $M_\infty$ = 0.600

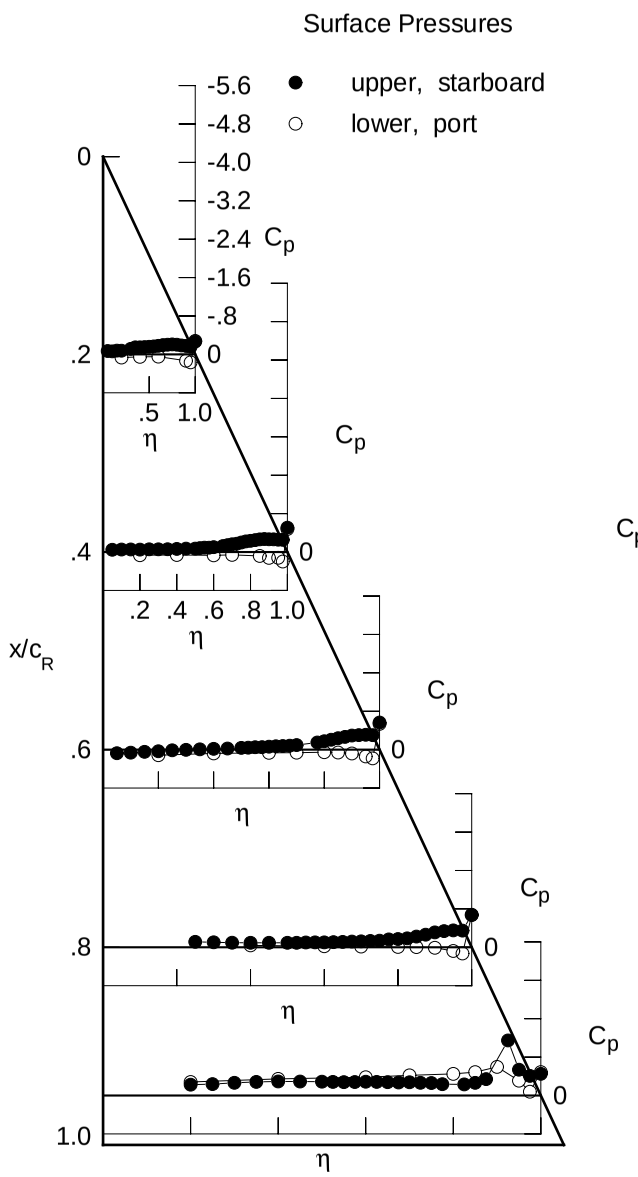
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.0615 | ******* |
| 0.20 | -0.0736 | -0.0711 |
| 0.30 | -0.1714 | ******* |
| 0.40 | -0.2320 | -0.1952 |
| 0.50 | -0.3214 | ******* |
| 0.60 | -0.2594 | -0.2395 |
| 0.70 | -0.4147 | ******* |
| 0.80 | -0.4054 | -0.3790 |
| 0.90 | -0.3655 | ******* |
| 0.95 | -0.2259 | -0.2583 |

# Table D2. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0707 | -0.0472 | 0.0743 | ******* | ******* |
| 0.100 | -0.0632 | -0.0524 | 0.0633 | ******* | ******* |
| 0.150 | -0.0787 | -0.0537 | 0.0457 | ******* | ******* |
| 0.200 | -0.0768 | -0.0502 | 0.0333 | ******* | -0.2255 |
| 0.250 | ******* | -0.0571 | 0.0137 | -0.1133 | -0.2374 |
| 0.300 | -0.1155 | -0.0566 | 0.0040 | -0.1042 | -0.2649 |
| 0.350 | -0.1468 | -0.0584 | -0.0060 | -0.0955 | -0.2828 |
| 0.400 | -0.1472 | -0.0647 | -0.0165 | -0.0939 | -0.2931 |
| 0.450 | -0.1519 | -0.0712 | -0.0232 | -0.0932 | -0.2913 |
| 0.500 | -0.1582 | -0.0712 | -0.0367 | -0.0939 | -0.2877 |
| 0.525 | ******* | -0.0813 | -0.0405 | -0.0940 | -0.2836 |
| 0.550 | -0.1664 | -0.0910 | -0.0501 | -0.1002 | -0.2782 |
| 0.575 | ******* | -0.0902 | -0.0523 | -0.1022 | -0.2811 |
| 0.600 | -0.1781 | -0.1020 | -0.0617 | -0.1020 | -0.2873 |
| 0.625 | ******* | ******* | -0.0704 | -0.1070 | -0.2829 |
| 0.650 | -0.1938 | -0.1239 | -0.0755 | -0.1118 | -0.2779 |
| 0.675 | ******* | -0.1433 | -0.0822 | -0.1194 | -0.2709 |
| 0.700 | -0.2015 | -0.1615 | -0.0955 | -0.1236 | -0.2759 |
| 0.725 | ******* | -0.1731 | ******* | -0.1318 | -0.2652 |
| 0.750 | -0.2083 | -0.1982 | ******* | -0.1375 | -0.2599 |
| 0.775 | ******* | -0.2218 | -0.1487 | -0.1638 | -0.2361 |
| 0.800 | -0.2016 | -0.2338 | -0.1753 | -0.1721 | ******* |
| 0.825 | ******* | -0.2477 | -0.2067 | -0.1860 | -0.2315 |
| 0.850 | -0.1867 | -0.2641 | -0.2385 | -0.2231 | -0.2644 |
| 0.875 | ******* | -0.2714 | -0.2658 | -0.2622 | -0.3419 |
| 0.900 | -0.1758 | -0.2654 | -0.2938 | -0.3103 | ******* |
| 0.925 | ******* | -0.2647 | -0.3028 | -0.3367 | -1.1473 |
| 0.950 | -0.1593 | -0.2564 | -0.3095 | -0.3520 | -0.5374 |
| 0.975 | ******* | -0.2541 | -0.3019 | -0.3468 | -0.4085 |
| 1.000 | -0.2670 | -0.5074 | -0.5646 | -0.6775 | -0.4515 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0658 | 0.0663 | 0.1162 | ******* | -0.2819 |
| -0.400 | 0.0515 | 0.0614 | 0.0785 | -0.0396 | -0.3462 |
| -0.600 | 0.0467 | 0.0686 | 0.0662 | -0.0212 | -0.3810 |
| -0.700 | ******* | 0.0591 | 0.0634 | -0.0153 | -0.4198 |
| -0.800 | ******* | ******* | 0.0540 | -0.0070 | -0.4505 |
| -0.850 | ******* | 0.0814 | 0.0603 | -0.0037 | -0.4871 |
| -0.900 | 0.1323 | 0.1214 | 0.0801 | 0.0100 | -0.5957 |
| -0.950 | 0.1660 | 0.1199 | 0.1419 | 0.0771 | -0.3089 |
| -0.975 | ******* | 0.1977 | 0.1813 | 0.1292 | -0.0791 |
| -1.000 | -0.2811 | -0.4785 | -0.5371 | -0.6709 | -0.4882 |



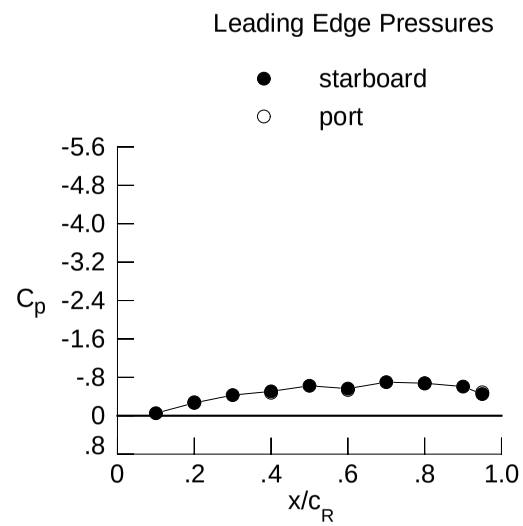

Small Radius L.E.

Run No. = 38 , Point No. = 755

$C_N$ = 0.150, $C_m$ = -0.0305

$\alpha$ = 4.2 °, $M_\infty$ = 0.600

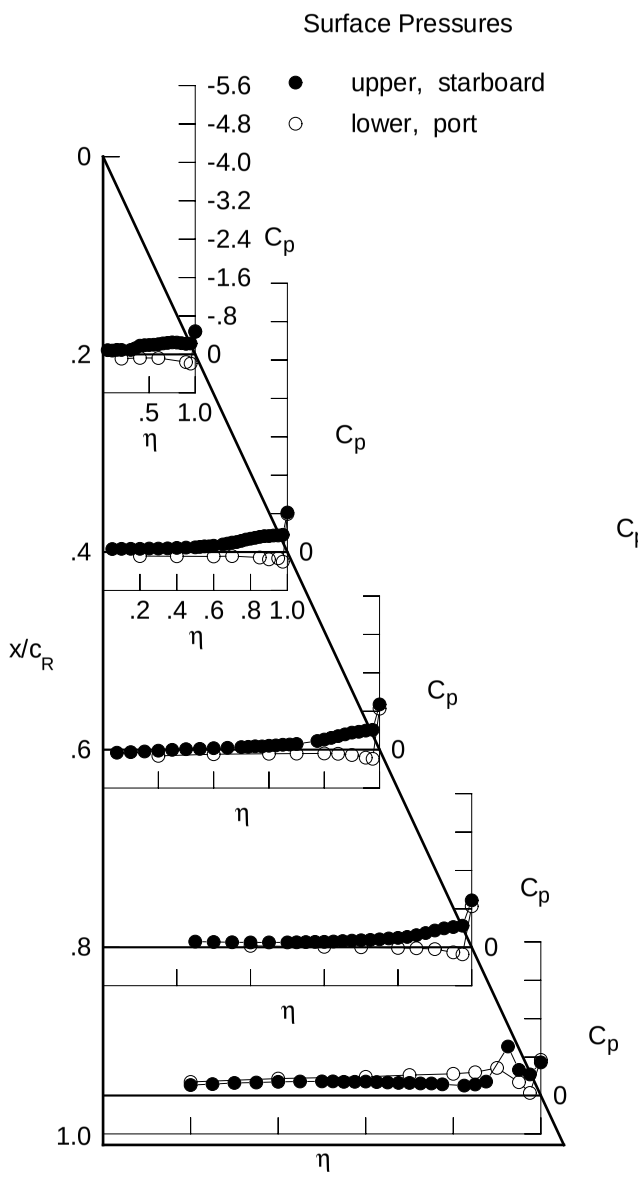
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.0523 | ******* |
| 0.20 | -0.2670 | -0.2811 |
| 0.30 | -0.4297 | ******* |
| 0.40 | -0.5074 | -0.4785 |
| 0.50 | -0.6237 | ******* |
| 0.60 | -0.5646 | -0.5371 |
| 0.70 | -0.6995 | ******* |
| 0.80 | -0.6775 | -0.6709 |
| 0.90 | -0.6072 | ******* |
| 0.95 | -0.4515 | -0.4882 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0882 | -0.0624 | 0.0642 | ******* | ******* |
| 0.100 | -0.0793 | -0.0665 | 0.0516 | ******* | ******* |
| 0.150 | -0.0943 | -0.0676 | 0.0381 | ******* | ******* |
| 0.200 | -0.0929 | -0.0670 | 0.0219 | ******* | -0.2180 |
| 0.250 | ******* | -0.0726 | 0.0041 | -0.1187 | -0.2379 |
| 0.300 | -0.0928 | -0.0720 | -0.0096 | -0.1107 | -0.2615 |
| 0.350 | -0.1268 | -0.0767 | -0.0159 | -0.1050 | -0.2703 |
| 0.400 | -0.1815 | -0.0862 | -0.0304 | -0.1006 | -0.2845 |
| 0.450 | -0.1914 | -0.0925 | -0.0380 | -0.1017 | -0.2918 |
| 0.500 | -0.1953 | -0.0976 | -0.0531 | -0.1014 | -0.2943 |
| 0.525 | ******* | -0.1074 | -0.0581 | -0.1042 | -0.2941 |
| 0.550 | -0.2009 | -0.1182 | -0.0693 | -0.1088 | -0.2849 |
| 0.575 | ******* | -0.1186 | -0.0671 | -0.1127 | -0.2856 |
| 0.600 | -0.2117 | -0.1315 | -0.0809 | -0.1132 | -0.2904 |
| 0.625 | ******* | ******* | -0.0884 | -0.1199 | -0.2797 |
| 0.650 | -0.2288 | -0.1576 | -0.1018 | -0.1294 | -0.2714 |
| 0.675 | ******* | -0.1764 | -0.1063 | -0.1383 | -0.2624 |
| 0.700 | -0.2395 | -0.1965 | -0.1183 | -0.1462 | -0.2627 |
| 0.725 | ******* | -0.2078 | ******* | -0.1534 | -0.2514 |
| 0.750 | -0.2507 | -0.2325 | ******* | -0.1655 | -0.2501 |
| 0.775 | ******* | -0.2598 | -0.1799 | -0.1836 | -0.2332 |
| 0.800 | -0.2467 | -0.2773 | -0.2105 | -0.1963 | ******* |
| 0.825 | ******* | -0.2956 | -0.2449 | -0.2164 | -0.2064 |
| 0.850 | -0.2332 | -0.3158 | -0.2815 | -0.2529 | -0.2295 |
| 0.875 | ******* | -0.3312 | -0.3187 | -0.2966 | -0.2893 |
| 0.900 | -0.2199 | -0.3326 | -0.3542 | -0.3493 | ******* |
| 0.925 | ******* | -0.3443 | -0.3723 | -0.3941 | -1.0209 |
| 0.950 | -0.2269 | -0.3446 | -0.3960 | -0.4217 | -0.5338 |
| 0.975 | ******* | -0.3596 | -0.4131 | -0.4499 | -0.4390 |
| 1.000 | -0.4691 | -0.8235 | -0.9427 | -0.9772 | -0.6895 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0888 | 0.0846 | 0.1300 | ******* | -0.2824 |
| -0.400 | 0.0737 | 0.0882 | 0.0955 | -0.0295 | -0.3530 |
| -0.600 | 0.0757 | 0.0922 | 0.0856 | -0.0095 | -0.3889 |
| -0.700 | ******* | 0.0847 | 0.0824 | -0.0010 | -0.4264 |
| -0.800 | ******* | ******* | 0.0792 | 0.0133 | -0.4521 |
| -0.850 | ******* | 0.1145 | 0.0865 | 0.0197 | -0.4839 |
| -0.900 | 0.1605 | 0.1516 | 0.1117 | 0.0387 | -0.5752 |
| -0.950 | 0.1909 | 0.1307 | 0.1672 | 0.1057 | -0.2777 |
| -0.975 | ******* | 0.2016 | 0.1904 | 0.1467 | -0.0533 |
| -1.000 | -0.4835 | -0.7919 | -0.8538 | -0.8542 | -0.7427 |



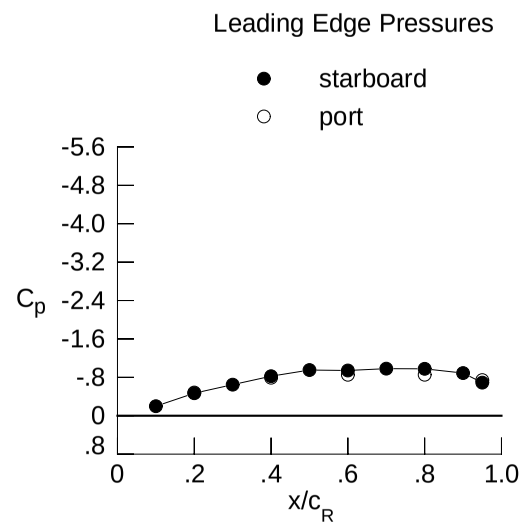

Small Radius L.E.

Run No. = 38 , Point No. = 756

$C_N$ = 0.183, $C_m$ = -0.0323

$\alpha$ = 5.2 °, $M_\infty$ = 0.600

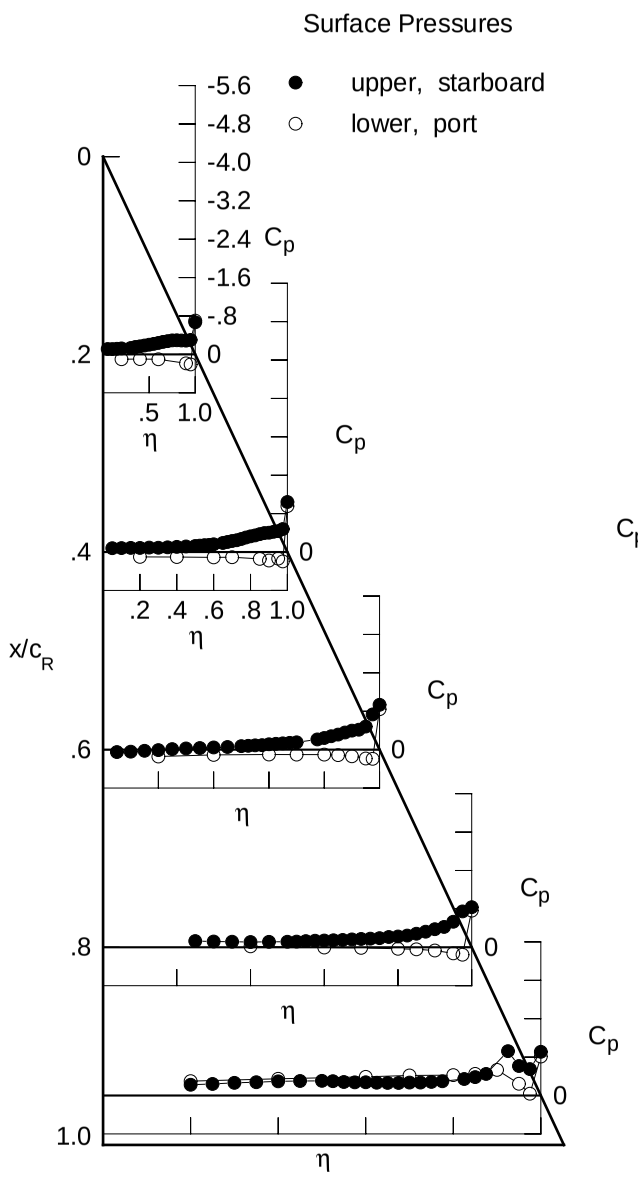
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.1988 | ******* |
| 0.20 | -0.4691 | -0.4835 |
| 0.30 | -0.6474 | ******* |
| 0.40 | -0.8235 | -0.7919 |
| 0.50 | -0.9519 | ******* |
| 0.60 | -0.9427 | -0.8538 |
| 0.70 | -0.9806 | ******* |
| 0.80 | -0.9772 | -0.8542 |
| 0.90 | -0.8887 | ******* |
| 0.95 | -0.6895 | -0.7427 |

# Table D2. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1118 | -0.0799 | 0.0504 | ******* | ******* |
| 0.100 | -0.1104 | -0.0824 | 0.0420 | ******* | ******* |
| 0.150 | -0.1168 | -0.0867 | 0.0242 | ******* | ******* |
| 0.200 | -0.1248 | -0.0853 | 0.0100 | ******* | -0.2244 |
| 0.250 | ******* | -0.0930 | -0.0113 | -0.1299 | -0.2406 |
| 0.300 | -0.1330 | -0.0897 | -0.0244 | -0.1199 | -0.2641 |
| 0.350 | -0.1546 | -0.0983 | -0.0333 | -0.1158 | -0.2770 |
| 0.400 | -0.1681 | -0.1080 | -0.0459 | -0.1098 | -0.2955 |
| 0.450 | -0.1845 | -0.1160 | -0.0549 | -0.1137 | -0.3021 |
| 0.500 | -0.2012 | -0.1255 | -0.0729 | -0.1155 | -0.3052 |
| 0.525 | ******* | -0.1337 | -0.0801 | -0.1184 | -0.2981 |
| 0.550 | -0.2194 | -0.1432 | -0.0898 | -0.1289 | -0.2817 |
| 0.575 | ******* | -0.1478 | -0.0935 | -0.1371 | -0.2742 |
| 0.600 | -0.2384 | -0.1620 | -0.1118 | -0.1411 | -0.2757 |
| 0.625 | ******* | ******* | -0.1216 | -0.1462 | -0.2661 |
| 0.650 | -0.2604 | -0.1891 | -0.1310 | -0.1526 | -0.2627 |
| 0.675 | ******* | -0.2097 | -0.1412 | -0.1637 | -0.2616 |
| 0.700 | -0.2758 | -0.2299 | -0.1525 | -0.1733 | -0.2693 |
| 0.725 | ******* | -0.2458 | ******* | -0.1802 | -0.2699 |
| 0.750 | -0.2917 | -0.2719 | ******* | -0.1906 | -0.2833 |
| 0.775 | ******* | -0.3024 | -0.2125 | -0.2147 | -0.2968 |
| 0.800 | -0.2945 | -0.3276 | -0.2427 | -0.2249 | ******* |
| 0.825 | ******* | -0.3461 | -0.2788 | -0.2438 | -0.3437 |
| 0.850 | -0.2896 | -0.3725 | -0.3136 | -0.2821 | -0.3831 |
| 0.875 | ******* | -0.3955 | -0.3566 | -0.3252 | -0.4497 |
| 0.900 | -0.2863 | -0.4028 | -0.3961 | -0.3769 | ******* |
| 0.925 | ******* | -0.4218 | -0.4149 | -0.4244 | -0.9244 |
| 0.950 | -0.3018 | -0.4351 | -0.4805 | -0.5324 | -0.6148 |
| 0.975 | ******* | -0.4789 | -0.7335 | -0.7468 | -0.5504 |
| 1.000 | -0.6690 | -1.0424 | -0.9347 | -0.8349 | -0.9106 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1005 | 0.1011 | 0.1431 | ******* | -0.2996 |
| -0.400 | 0.0973 | 0.1042 | 0.1094 | -0.0197 | -0.3482 |
| -0.600 | 0.1018 | 0.1115 | 0.1013 | 0.0047 | -0.3890 |
| -0.700 | ******* | 0.1078 | 0.1032 | 0.0116 | -0.4173 |
| -0.800 | ******* | ******* | 0.1033 | 0.0311 | -0.4245 |
| -0.850 | ******* | 0.1427 | 0.1141 | 0.0424 | -0.4507 |
| -0.900 | 0.1862 | 0.1766 | 0.1385 | 0.0669 | -0.5338 |
| -0.950 | 0.2086 | 0.1370 | 0.1846 | 0.1268 | -0.2450 |
| -0.975 | ******* | 0.1950 | 0.1913 | 0.1543 | -0.0377 |
| -1.000 | -0.7028 | -0.9572 | -0.8427 | -0.7632 | -0.8120 |



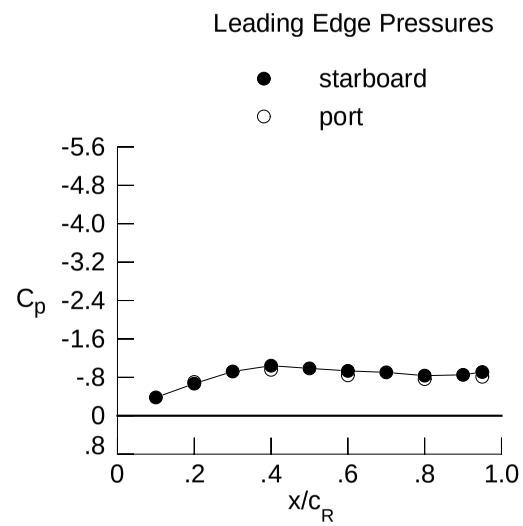

Small Radius L.E.

Run No. = 38 , Point No. = 757

$C_N$ = 0.229, $C_m$ = -0.0413

$\alpha$ = 6.3 °, $M_\infty$ = 0.601

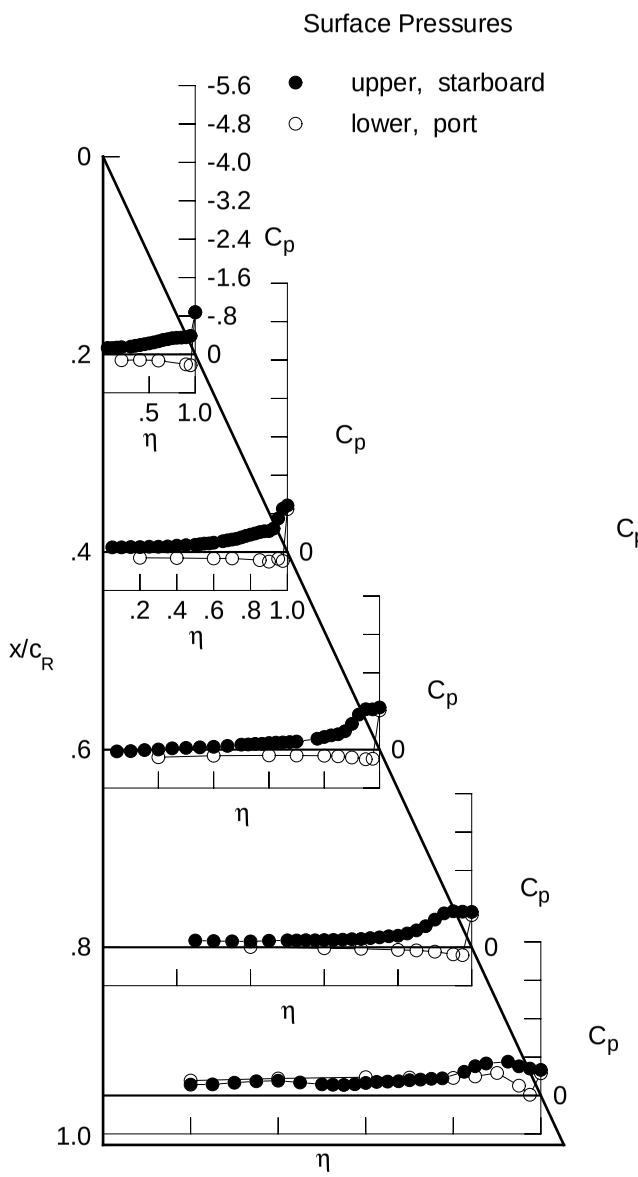
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.3810 | ******* |
| 0.20 | -0.6690 | -0.7028 |
| 0.30 | -0.9216 | ******* |
| 0.40 | -1.0424 | -0.9572 |
| 0.50 | -0.9862 | ******* |
| 0.60 | -0.9347 | -0.8427 |
| 0.70 | -0.9029 | ******* |
| 0.80 | -0.8349 | -0.7632 |
| 0.90 | -0.8519 | ******* |
| 0.95 | -0.9106 | -0.8120 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1342 | -0.0972 | 0.0372 | ******* | ******* |
| 0.100 | -0.1310 | -0.0974 | 0.0308 | ******* | ******* |
| 0.150 | -0.1423 | -0.1037 | 0.0089 | ******* | ******* |
| 0.200 | -0.1496 | -0.1030 | -0.0035 | ******* | -0.2266 |
| 0.250 | ******* | -0.1110 | -0.0270 | -0.1409 | -0.2322 |
| 0.300 | -0.1612 | -0.1114 | -0.0365 | -0.1298 | -0.2663 |
| 0.350 | -0.1795 | -0.1170 | -0.0478 | -0.1237 | -0.2970 |
| 0.400 | -0.1945 | -0.1324 | -0.0593 | -0.1221 | -0.3084 |
| 0.450 | -0.2117 | -0.1425 | -0.0784 | -0.1371 | -0.2709 |
| 0.500 | -0.2304 | -0.1516 | -0.1040 | -0.1446 | -0.2327 |
| 0.525 | ******* | -0.1626 | -0.1084 | -0.1415 | -0.2252 |
| 0.550 | -0.2496 | -0.1758 | -0.1203 | -0.1477 | -0.2198 |
| 0.575 | ******* | -0.1795 | -0.1212 | -0.1453 | -0.2355 |
| 0.600 | -0.2719 | -0.1944 | -0.1379 | -0.1506 | -0.2616 |
| 0.625 | ******* | ******* | -0.1460 | -0.1533 | -0.2829 |
| 0.650 | -0.3003 | -0.2245 | -0.1497 | -0.1582 | -0.2892 |
| 0.675 | ******* | -0.2436 | -0.1575 | -0.1676 | -0.2969 |
| 0.700 | -0.3160 | -0.2601 | -0.1686 | -0.1726 | -0.3181 |
| 0.725 | ******* | -0.2761 | ******* | -0.1912 | -0.3310 |
| 0.750 | -0.3371 | -0.3051 | ******* | -0.2072 | -0.3483 |
| 0.775 | ******* | -0.3359 | -0.2273 | -0.2294 | -0.3577 |
| 0.800 | -0.3468 | -0.3621 | -0.2642 | -0.2407 | ******* |
| 0.825 | ******* | -0.3860 | -0.2974 | -0.2876 | -0.4944 |
| 0.850 | -0.3492 | -0.4140 | -0.3197 | -0.3519 | -0.6104 |
| 0.875 | ******* | -0.4327 | -0.3829 | -0.4395 | -0.6675 |
| 0.900 | -0.3559 | -0.4357 | -0.5368 | -0.5764 | ******* |
| 0.925 | ******* | -0.4890 | -0.7302 | -0.7064 | -0.7045 |
| 0.950 | -0.3867 | -0.6982 | -0.8420 | -0.7507 | -0.6079 |
| 0.975 | ******* | -0.9013 | -0.8389 | -0.7414 | -0.5608 |
| 1.000 | -0.8740 | -0.9714 | -0.8785 | -0.7366 | -0.5336 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1219 | 0.1204 | 0.1586 | ******* | -0.3111 |
| -0.400 | 0.1153 | 0.1251 | 0.1267 | -0.0055 | -0.3548 |
| -0.600 | 0.1281 | 0.1334 | 0.1201 | 0.0201 | -0.3816 |
| -0.700 | ******* | 0.1331 | 0.1226 | 0.0314 | -0.3726 |
| -0.800 | ******* | ******* | 0.1267 | 0.0544 | -0.3662 |
| -0.850 | ******* | 0.1687 | 0.1380 | 0.0647 | -0.3973 |
| -0.900 | 0.2078 | 0.2001 | 0.1642 | 0.0913 | -0.4700 |
| -0.950 | 0.2265 | 0.1412 | 0.2000 | 0.1473 | -0.2050 |
| -0.975 | ******* | 0.1853 | 0.1898 | 0.1620 | -0.0158 |
| -1.000 | -0.8825 | -0.8936 | -0.8182 | -0.6705 | -0.4632 |



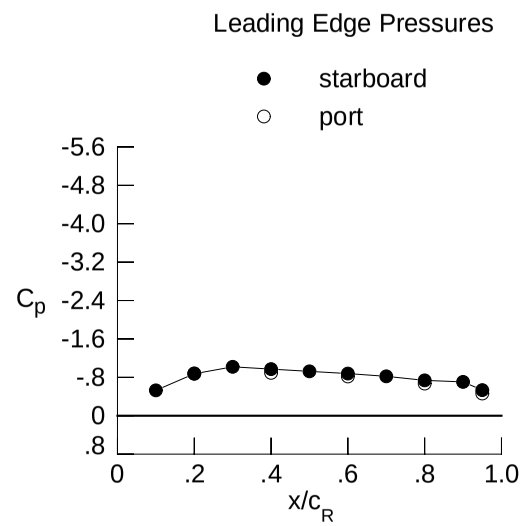

Small Radius L.E.

Run No. = 38 , Point No. = 758

$C_N$ = 0.286, $C_m$ = -0.0563

$\alpha$ = 7.3 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

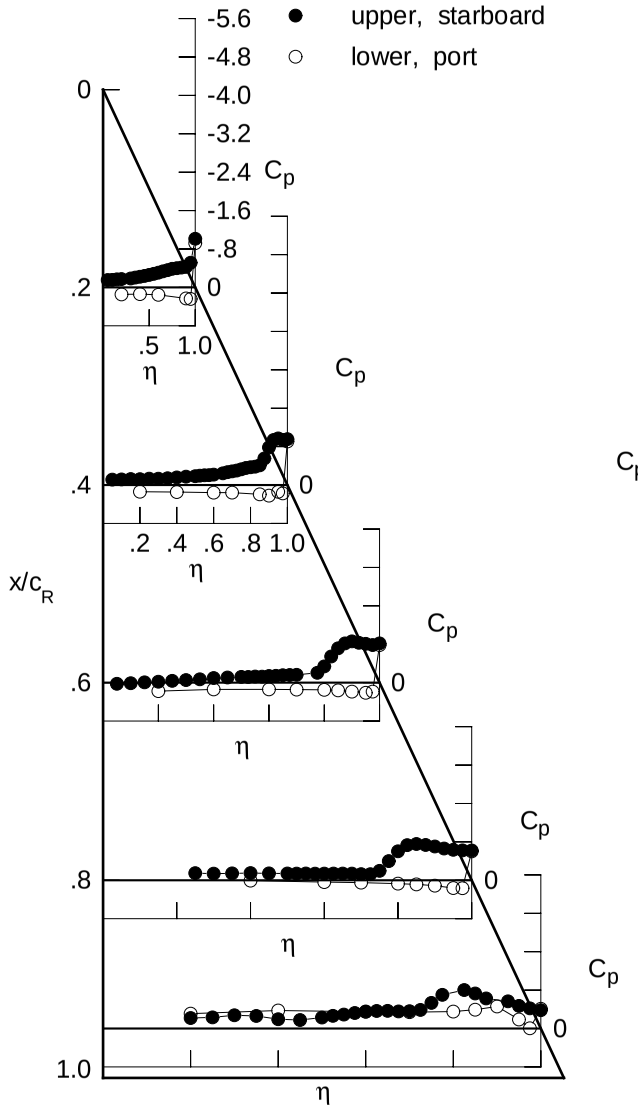



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.5285 | ******* |
| 0.20 | -0.8740 | -0.8825 |
| 0.30 | -1.0191 | ******* |
| 0.40 | -0.9714 | -0.8936 |
| 0.50 | -0.9244 | ******* |
| 0.60 | -0.8785 | -0.8182 |
| 0.70 | -0.8209 | ******* |
| 0.80 | -0.7366 | -0.6705 |
| 0.90 | -0.7050 | ******* |
| 0.95 | -0.5336 | -0.4632 |

# Table D2. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1537 | -0.1132 | 0.0236 | ******* | ******* |
| 0.100 | -0.1557 | -0.1168 | 0.0121 | ******* | ******* |
| 0.150 | -0.1679 | -0.1247 | -0.0061 | ******* | ******* |
| 0.200 | -0.1739 | -0.1222 | -0.0190 | ******* | -0.2187 |
| 0.250 | ******* | -0.1328 | -0.0374 | -0.1488 | -0.2319 |
| 0.300 | -0.1859 | -0.1323 | -0.0535 | -0.1384 | -0.2760 |
| 0.350 | -0.2049 | -0.1417 | -0.0694 | -0.1441 | -0.2613 |
| 0.400 | -0.2216 | -0.1584 | -0.0958 | -0.1502 | -0.1939 |
| 0.450 | -0.2388 | -0.1747 | -0.1074 | -0.1440 | -0.1766 |
| 0.500 | -0.2602 | -0.1839 | -0.1200 | -0.1414 | -0.2291 |
| 0.525 | ******* | -0.1949 | -0.1187 | -0.1392 | -0.2638 |
| 0.550 | -0.2825 | -0.2028 | -0.1275 | -0.1419 | -0.2904 |
| 0.575 | ******* | -0.2053 | -0.1245 | -0.1382 | -0.3235 |
| 0.600 | -0.3062 | -0.2171 | -0.1388 | -0.1389 | -0.3546 |
| 0.625 | ******* | ******* | -0.1423 | -0.1404 | -0.3652 |
| 0.650 | -0.3341 | -0.2441 | -0.1544 | -0.1399 | -0.3682 |
| 0.675 | ******* | -0.2682 | -0.1593 | -0.1389 | -0.3558 |
| 0.700 | -0.3593 | -0.2848 | -0.1631 | -0.1279 | -0.3611 |
| 0.725 | ******* | -0.3013 | ******* | -0.1271 | -0.3872 |
| 0.750 | -0.3870 | -0.3278 | ******* | -0.1966 | -0.5337 |
| 0.775 | ******* | -0.3552 | -0.2051 | -0.4004 | -0.7020 |
| 0.800 | -0.3999 | -0.3703 | -0.3383 | -0.6041 | ******* |
| 0.825 | ******* | -0.3820 | -0.5444 | -0.7323 | -0.8017 |
| 0.850 | -0.4125 | -0.4107 | -0.7150 | -0.7561 | -0.7299 |
| 0.875 | ******* | -0.5532 | -0.8176 | -0.7362 | -0.6262 |
| 0.900 | -0.4274 | -0.7836 | -0.8598 | -0.7036 | ******* |
| 0.925 | ******* | -0.9383 | -0.8308 | -0.6618 | -0.5663 |
| 0.950 | -0.5138 | -0.9712 | -0.8085 | -0.6356 | -0.4714 |
| 0.975 | ******* | -0.9389 | -0.7835 | -0.6232 | -0.4197 |
| 1.000 | -1.0128 | -0.9563 | -0.8175 | -0.6207 | -0.3818 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1463 | 0.1395 | 0.1766 | ******* | -0.3094 |
| -0.400 | 0.1401 | 0.1462 | 0.1410 | 0.0068 | -0.3750 |
| -0.600 | 0.1547 | 0.1580 | 0.1403 | 0.0375 | -0.3482 |
| -0.700 | ******* | 0.1580 | 0.1447 | 0.0490 | -0.3401 |
| -0.800 | ******* | ******* | 0.1497 | 0.0700 | -0.3530 |
| -0.850 | ******* | 0.1936 | 0.1606 | 0.0857 | -0.3920 |
| -0.900 | 0.2300 | 0.2206 | 0.1870 | 0.1117 | -0.4589 |
| -0.950 | 0.2406 | 0.1405 | 0.2110 | 0.1620 | -0.1881 |
| -0.975 | ******* | 0.1735 | 0.1860 | 0.1645 | -0.0051 |
| -1.000 | -0.9214 | -0.9079 | -0.7824 | -0.6026 | -0.4110 |

Surface Pressures




Small Radius L.E.

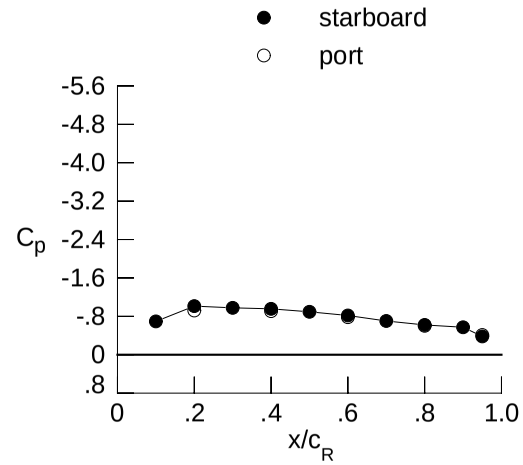
Run No. = 38 , Point No. = 759

$C_N$ = 0.334, $C_m$ = -0.0599

$\alpha$ = 8.3 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

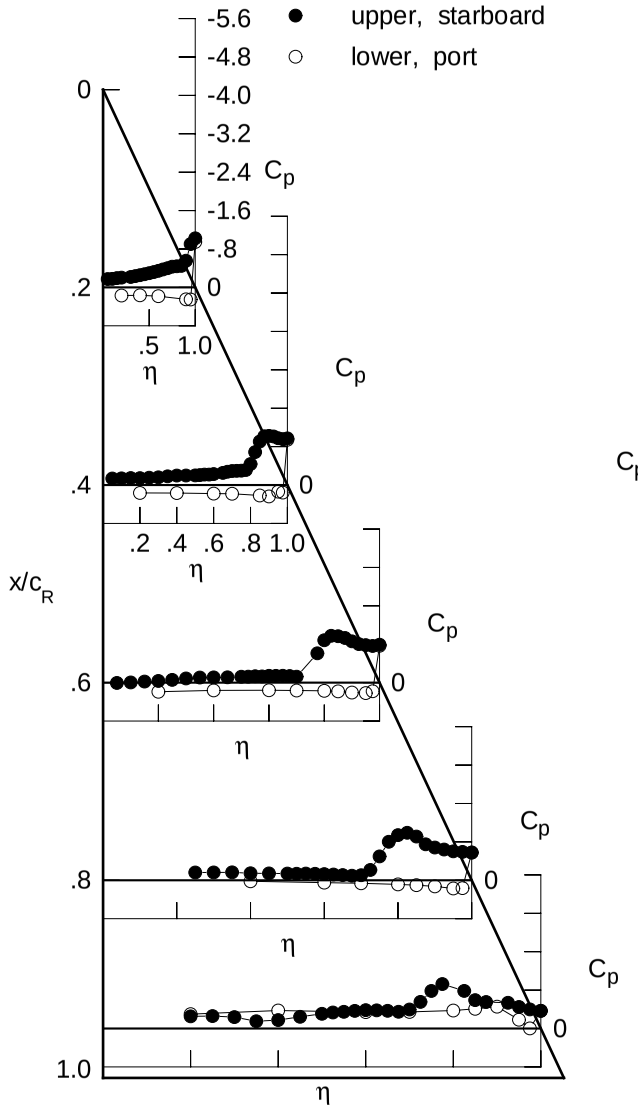



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.6941 | ******* |
| 0.20 | -1.0128 | -0.9214 |
| 0.30 | -0.9771 | ******* |
| 0.40 | -0.9563 | -0.9079 |
| 0.50 | -0.8942 | ******* |
| 0.60 | -0.8175 | -0.7824 |
| 0.70 | -0.7031 | ******* |
| 0.80 | -0.6207 | -0.6026 |
| 0.90 | -0.5724 | ******* |
| 0.95 | -0.3818 | -0.4110 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1739 | -0.1362 | 0.0067 | ******* | ******* |
| 0.100 | -0.1778 | -0.1396 | -0.0044 | ******* | ******* |
| 0.150 | -0.1937 | -0.1455 | -0.0228 | ******* | ******* |
| 0.200 | -0.2033 | -0.1437 | -0.0349 | ******* | -0.2535 |
| 0.250 | ******* | -0.1530 | -0.0574 | -0.1626 | -0.2595 |
| 0.300 | -0.2171 | -0.1607 | -0.0874 | -0.1633 | -0.2374 |
| 0.350 | -0.2349 | -0.1816 | -0.1065 | -0.1654 | -0.1512 |
| 0.400 | -0.2541 | -0.1977 | -0.1098 | -0.1460 | -0.1758 |
| 0.450 | -0.2745 | -0.1981 | -0.1111 | -0.1433 | -0.2440 |
| 0.500 | -0.2960 | -0.2012 | -0.1235 | -0.1399 | -0.3066 |
| 0.525 | ******* | -0.2075 | -0.1245 | -0.1363 | -0.3339 |
| 0.550 | -0.3189 | -0.2177 | -0.1340 | -0.1401 | -0.3478 |
| 0.575 | ******* | -0.2172 | -0.1294 | -0.1353 | -0.3672 |
| 0.600 | -0.3451 | -0.2291 | -0.1425 | -0.1289 | -0.3827 |
| 0.625 | ******* | ******* | -0.1413 | -0.1200 | -0.3786 |
| 0.650 | -0.3738 | -0.2530 | -0.1430 | -0.1090 | -0.3689 |
| 0.675 | ******* | -0.2764 | -0.1377 | -0.0955 | -0.3487 |
| 0.700 | -0.4000 | -0.2924 | -0.1239 | -0.1058 | -0.3959 |
| 0.725 | ******* | -0.2959 | ******* | -0.2153 | -0.5542 |
| 0.750 | -0.4310 | -0.2990 | ******* | -0.4976 | -0.7821 |
| 0.775 | ******* | -0.3138 | -0.6109 | -0.8027 | -0.9263 |
| 0.800 | -0.4403 | -0.4377 | -0.8831 | -0.9411 | ******* |
| 0.825 | ******* | -0.6862 | -0.9760 | -0.9897 | -0.7834 |
| 0.850 | -0.4477 | -0.9066 | -0.9673 | -0.9112 | -0.5912 |
| 0.875 | ******* | -1.0156 | -0.9304 | -0.7498 | -0.5521 |
| 0.900 | -0.5557 | -1.0240 | -0.8606 | -0.6821 | ******* |
| 0.925 | ******* | -1.0120 | -0.8031 | -0.6404 | -0.5358 |
| 0.950 | -0.9025 | -0.9754 | -0.7815 | -0.6034 | -0.4484 |
| 0.975 | ******* | -0.9561 | -0.7640 | -0.5908 | -0.3975 |
| 1.000 | -1.0225 | -0.9720 | -0.7906 | -0.5795 | -0.3684 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1697 | 0.1644 | 0.1894 | ******* | -0.2990 |
| -0.400 | 0.1647 | 0.1671 | 0.1615 | 0.0209 | -0.3748 |
| -0.600 | 0.1831 | 0.1783 | 0.1584 | 0.0491 | -0.3414 |
| -0.700 | ******* | 0.1816 | 0.1637 | 0.0622 | -0.3456 |
| -0.800 | ******* | ******* | 0.1704 | 0.0859 | -0.3745 |
| -0.850 | ******* | 0.2172 | 0.1819 | 0.1018 | -0.4102 |
| -0.900 | 0.2489 | 0.2378 | 0.2063 | 0.1272 | -0.4551 |
| -0.950 | 0.2519 | 0.1377 | 0.2179 | 0.1707 | -0.1829 |
| -0.975 | ******* | 0.1566 | 0.1788 | 0.1633 | -0.0027 |
| -1.000 | -0.9457 | -0.9431 | -0.7683 | -0.5767 | -0.3687 |

Surface Pressures




Small Radius L.E.

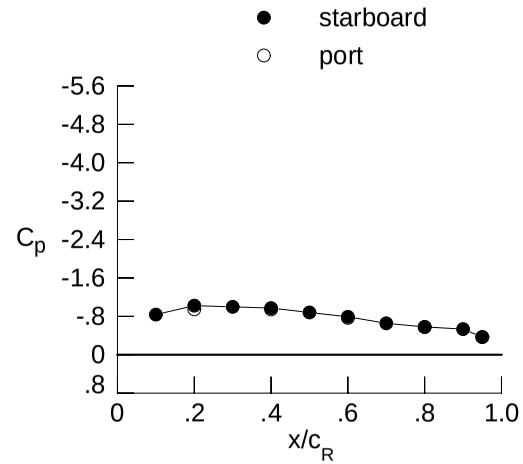
Run No. = 38 , Point No. = 760

$C_N$ = 0.389, $C_m$ = -0.0691

$\alpha$ = 9.3 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

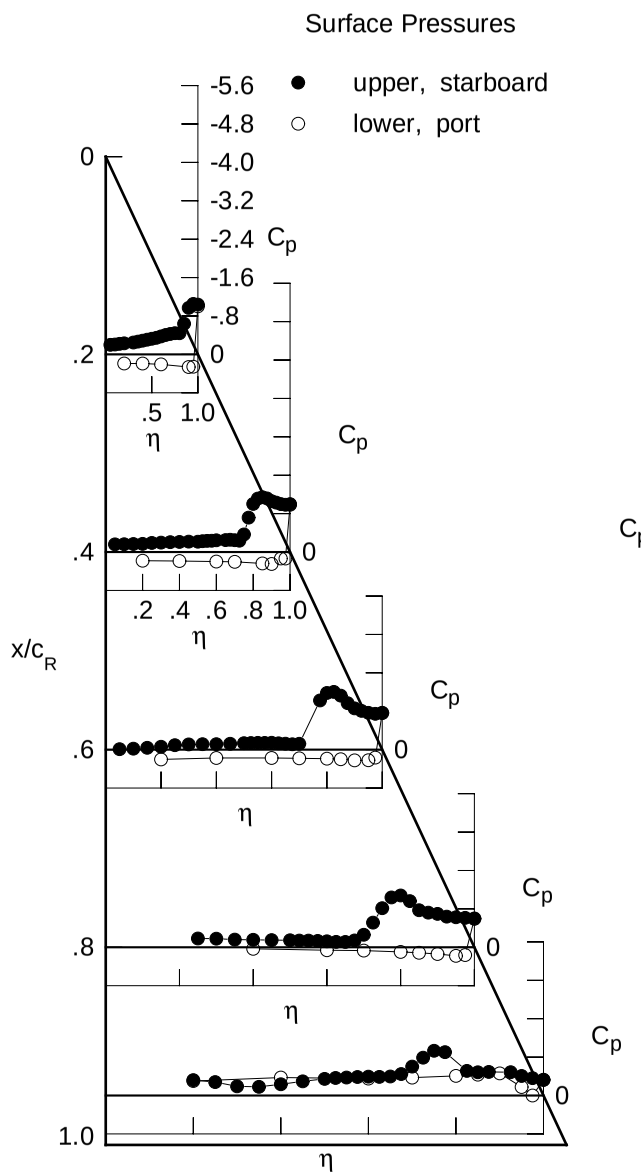
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.8361 | ******* |
| 0.20 | -1.0225 | -0.9457 |
| 0.30 | -0.9976 | ******* |
| 0.40 | -0.9720 | -0.9431 |
| 0.50 | -0.8804 | ******* |
| 0.60 | -0.7906 | -0.7683 |
| 0.70 | -0.6545 | ******* |
| 0.80 | -0.5795 | -0.5767 |
| 0.90 | -0.5339 | ******* |
| 0.95 | -0.3684 | -0.3687 |

# Table D2. Continued.

| η | x/c_R .2 C_p,u | x/c_R .4 C_p,u | x/c_R .6 C_p,u | x/c_R .8 C_p,u | x/c_R .95 C_p,u |
|---|---|---|---|---|---|
| 0.050 | -0.1989 | -0.1601 | -0.0097 | ******* | ******* |
| 0.100 | -0.2054 | -0.1626 | -0.0197 | ******* | ******* |
| 0.150 | -0.2203 | -0.1668 | -0.0384 | ******* | ******* |
| 0.200 | -0.2304 | -0.1701 | -0.0598 | ******* | -0.3211 |
| 0.250 | ******* | -0.1899 | -0.0924 | -0.1835 | -0.2798 |
| 0.300 | -0.2475 | -0.1962 | -0.1089 | -0.1795 | -0.1908 |
| 0.350 | -0.2663 | -0.2058 | -0.1132 | -0.1601 | -0.1812 |
| 0.400 | -0.2857 | -0.2102 | -0.1135 | -0.1557 | -0.2342 |
| 0.450 | -0.3061 | -0.2170 | -0.1228 | -0.1496 | -0.2954 |
| 0.500 | -0.3257 | -0.2149 | -0.1348 | -0.1463 | -0.3467 |
| 0.525 | ******* | -0.2253 | -0.1379 | -0.1401 | -0.3659 |
| 0.550 | -0.3458 | -0.2331 | -0.1415 | -0.1390 | -0.3741 |
| 0.575 | ******* | -0.2351 | -0.1398 | -0.1329 | -0.3853 |
| 0.600 | -0.3742 | -0.2445 | -0.1431 | -0.1244 | -0.3925 |
| 0.625 | ******* | ******* | -0.1316 | -0.1130 | -0.3881 |
| 0.650 | -0.4044 | -0.2486 | -0.1240 | -0.1113 | -0.3960 |
| 0.675 | ******* | -0.2561 | -0.1120 | -0.1421 | -0.4469 |
| 0.700 | -0.4254 | -0.2466 | -0.1220 | -0.2605 | -0.6025 |
| 0.725 | ******* | -0.2358 | ******* | -0.5138 | -0.7878 |
| 0.750 | -0.4416 | -0.3663 | ******* | -0.8144 | -0.9317 |
| 0.775 | ******* | -0.7166 | -1.0245 | -1.0387 | -0.9035 |
| 0.800 | -0.4410 | -1.0021 | -1.1809 | -1.0791 | ******* |
| 0.825 | ******* | -1.1138 | -1.2033 | -0.9616 | -0.5130 |
| 0.850 | -0.6388 | -1.1423 | -1.1244 | -0.7724 | -0.4844 |
| 0.875 | ******* | -1.1169 | -0.9677 | -0.7216 | -0.4912 |
| 0.900 | -0.9695 | -1.0601 | -0.8599 | -0.6959 | ******* |
| 0.925 | ******* | -1.0294 | -0.8082 | -0.6383 | -0.4853 |
| 0.950 | -1.0513 | -0.9995 | -0.7674 | -0.6259 | -0.4073 |
| 0.975 | ******* | -0.9849 | -0.7466 | -0.6138 | -0.3616 |
| 1.000 | -1.0370 | -0.9981 | -0.7674 | -0.6008 | -0.3292 |
| | C_p,l | C_p,l | C_p,l | C_p,l | C_p,l |
| -0.200 | 0.1899 | 0.1805 | 0.2039 | ******* | -0.3013 |
| -0.400 | 0.1902 | 0.1875 | 0.1735 | 0.0318 | -0.3742 |
| -0.600 | 0.2078 | 0.1985 | 0.1734 | 0.0613 | -0.3527 |
| -0.700 | ******* | 0.2038 | 0.1809 | 0.0689 | -0.3726 |
| -0.800 | ******* | ******* | 0.1884 | 0.0965 | -0.4088 |
| -0.850 | ******* | 0.2378 | 0.1998 | 0.1144 | -0.4346 |
| -0.900 | 0.2634 | 0.2492 | 0.2235 | 0.1397 | -0.4611 |
| -0.950 | 0.2568 | 0.1346 | 0.2209 | 0.1785 | -0.1771 |
| -0.975 | ******* | 0.1349 | 0.1659 | 0.1613 | 0.0002 |
| -1.000 | -1.0007 | -0.9847 | -0.7619 | -0.5932 | -0.3239 |



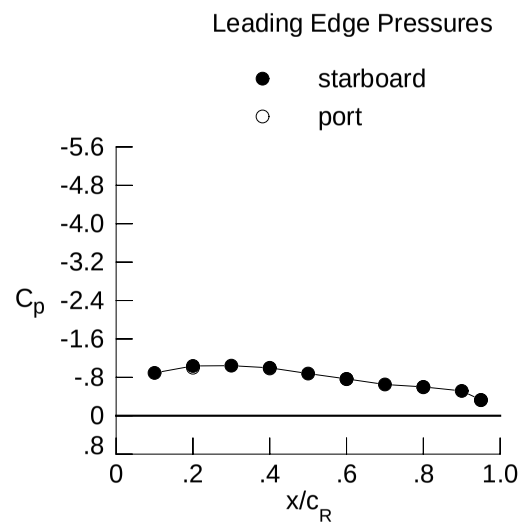

Small Radius L.E.

Run No. = 38 , Point No. = 761

$C_N$ = 0.443, $C_m$ = -0.0787

$\alpha$ = 10.4 °, $M_\infty$ = 0.601

$R_{mac}$ = $6.0 \times 10^6$

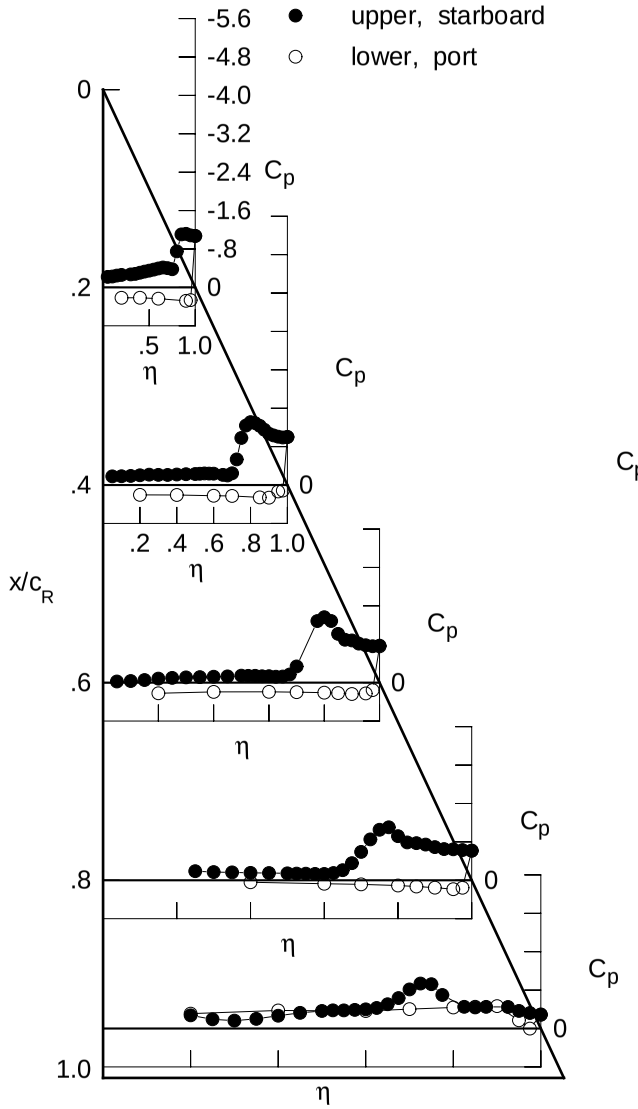



| x/c_R | starb'd C_p | port C_p |
|---|---|---|
| 0.10 | -0.8917 | ******* |
| 0.20 | -1.0370 | -1.0007 |
| 0.30 | -1.0429 | ******* |
| 0.40 | -0.9981 | -0.9847 |
| 0.50 | -0.8787 | ******* |
| 0.60 | -0.7674 | -0.7619 |
| 0.70 | -0.6508 | ******* |
| 0.80 | -0.6008 | -0.5932 |
| 0.90 | -0.5171 | ******* |
| 0.95 | -0.3292 | -0.3239 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2196 | -0.1804 | -0.0239 | ******* | ******* |
| 0.100 | -0.2263 | -0.1832 | -0.0337 | ******* | ******* |
| 0.150 | -0.2460 | -0.1892 | -0.0547 | ******* | ******* |
| 0.200 | -0.2598 | -0.2029 | -0.0842 | ******* | -0.2743 |
| 0.250 | ******* | -0.2163 | -0.0994 | -0.1894 | -0.1917 |
| 0.300 | -0.2702 | -0.2120 | -0.1098 | -0.1713 | -0.1637 |
| 0.350 | -0.2819 | -0.2103 | -0.1148 | -0.1645 | -0.2010 |
| 0.400 | -0.3055 | -0.2191 | -0.1229 | -0.1547 | -0.2663 |
| 0.450 | -0.3286 | -0.2257 | -0.1303 | -0.1513 | -0.3263 |
| 0.500 | -0.3491 | -0.2300 | -0.1460 | -0.1451 | -0.3653 |
| 0.525 | ******* | -0.2351 | -0.1412 | -0.1392 | -0.3780 |
| 0.550 | -0.3703 | -0.2416 | -0.1421 | -0.1372 | -0.3780 |
| 0.575 | ******* | -0.2381 | -0.1324 | -0.1329 | -0.3876 |
| 0.600 | -0.3945 | -0.2366 | -0.1343 | -0.1317 | -0.3991 |
| 0.625 | ******* | ******* | -0.1229 | -0.1509 | -0.4284 |
| 0.650 | -0.4145 | -0.2120 | -0.1268 | -0.2103 | -0.5056 |
| 0.675 | ******* | -0.1991 | -0.1700 | -0.3568 | -0.6347 |
| 0.700 | -0.4010 | -0.2447 | -0.3374 | -0.5909 | -0.8141 |
| 0.725 | ******* | -0.5344 | ******* | -0.8521 | -0.9371 |
| 0.750 | -0.3785 | -0.9807 | ******* | -1.0532 | -0.9232 |
| 0.775 | ******* | -1.2389 | -1.2832 | -1.1039 | -0.6984 |
| 0.800 | -0.7504 | -1.3102 | -1.3630 | -0.9188 | ******* |
| 0.825 | ******* | -1.2894 | -1.2843 | -0.7886 | -0.4516 |
| 0.850 | -1.1039 | -1.2337 | -1.0160 | -0.7739 | -0.4394 |
| 0.875 | ******* | -1.1520 | -0.8933 | -0.7442 | -0.4511 |
| 0.900 | -1.1164 | -1.0688 | -0.8794 | -0.6914 | ******* |
| 0.925 | ******* | -1.0336 | -0.8124 | -0.6506 | -0.4489 |
| 0.950 | -1.0833 | -1.0073 | -0.7793 | -0.6460 | -0.3661 |
| 0.975 | ******* | -0.9900 | -0.7584 | -0.6298 | -0.3228 |
| 1.000 | -1.0736 | -0.9991 | -0.7707 | -0.6159 | -0.2933 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2169 | 0.2051 | 0.2215 | ******* | -0.3097 |
| -0.400 | 0.2159 | 0.2073 | 0.1927 | 0.0412 | -0.3761 |
| -0.600 | 0.2351 | 0.2230 | 0.1910 | 0.0716 | -0.3640 |
| -0.700 | ******* | 0.2275 | 0.1987 | 0.0848 | -0.4041 |
| -0.800 | ******* | ******* | 0.2086 | 0.1091 | -0.4380 |
| -0.850 | ******* | 0.2572 | 0.2179 | 0.1298 | -0.4527 |
| -0.900 | 0.2797 | 0.2632 | 0.2365 | 0.1536 | -0.4661 |
| -0.950 | 0.2649 | 0.1332 | 0.2248 | 0.1854 | -0.1712 |
| -0.975 | ******* | 0.1155 | 0.1552 | 0.1553 | 0.0015 |
| -1.000 | -1.0695 | -1.0030 | -0.7556 | -0.6185 | -0.2853 |

Surface Pressures




Small Radius L.E.

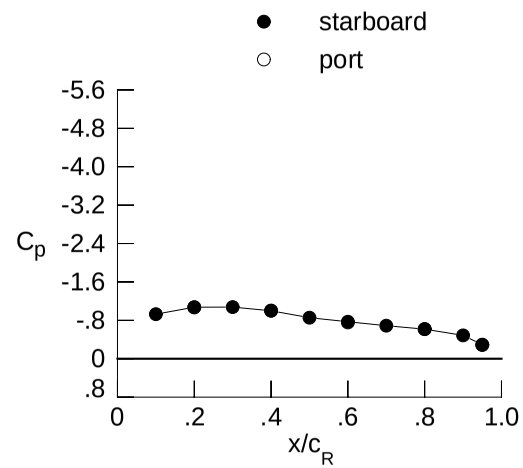
Run No. = 38 , Point No. = 762

$C_N$ = 0.482, $C_m$ = -0.0769

$\alpha$ = 11.4 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

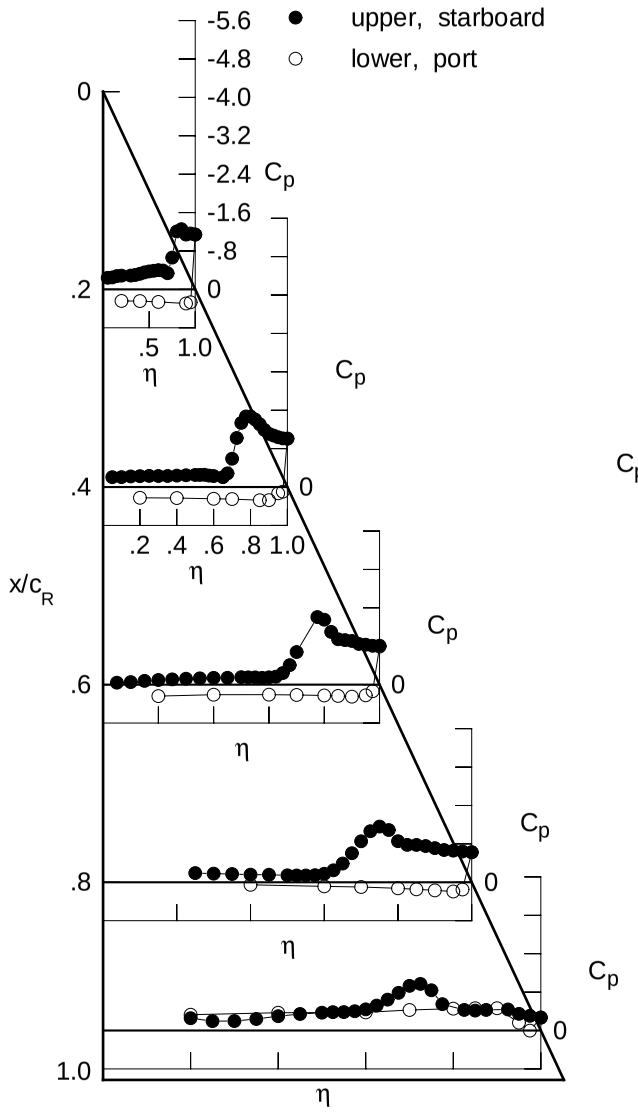



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.9281 | ******* |
| 0.20 | -1.0736 | -1.0695 |
| 0.30 | -1.0760 | ******* |
| 0.40 | -0.9991 | -1.0030 |
| 0.50 | -0.8550 | ******* |
| 0.60 | -0.7707 | -0.7556 |
| 0.70 | -0.6885 | ******* |
| 0.80 | -0.6159 | -0.6185 |
| 0.90 | -0.4865 | ******* |
| 0.95 | -0.2933 | -0.2853 |

# Table D2. Continued.

| η | x/c_R .2 Cp,u | x/c_R .4 Cp,u | x/c_R .6 Cp,u | x/c_R .8 Cp,u | x/c_R .95 Cp,u |
|---|---|---|---|---|---|
| 0.050 | -0.2415 | -0.2055 | -0.0405 | ******* | ******* |
| 0.100 | -0.2490 | -0.2064 | -0.0528 | ******* | ******* |
| 0.150 | -0.2779 | -0.2206 | -0.0785 | ******* | ******* |
| 0.200 | -0.2863 | -0.2263 | -0.0968 | ******* | -0.2560 |
| 0.250 | ******* | -0.2323 | -0.1096 | -0.1919 | -0.1953 |
| 0.300 | -0.2878 | -0.2293 | -0.1231 | -0.1800 | -0.1971 |
| 0.350 | -0.3011 | -0.2304 | -0.1312 | -0.1717 | -0.2402 |
| 0.400 | -0.3251 | -0.2377 | -0.1418 | -0.1593 | -0.2981 |
| 0.450 | -0.3542 | -0.2459 | -0.1429 | -0.1573 | -0.3437 |
| 0.500 | -0.3745 | -0.2524 | -0.1552 | -0.1449 | -0.3709 |
| 0.525 | ******* | -0.2517 | -0.1519 | -0.1419 | -0.3823 |
| 0.550 | -0.3881 | -0.2559 | -0.1516 | -0.1417 | -0.3839 |
| 0.575 | ******* | -0.2381 | -0.1419 | -0.1478 | -0.4014 |
| 0.600 | -0.4005 | -0.2291 | -0.1527 | -0.1779 | -0.4408 |
| 0.625 | ******* | ******* | -0.1658 | -0.2492 | -0.5190 |
| 0.650 | -0.3932 | -0.2049 | -0.2416 | -0.3902 | -0.6433 |
| 0.675 | ******* | -0.2845 | -0.4065 | -0.6060 | -0.7850 |
| 0.700 | -0.3366 | -0.5902 | -0.6794 | -0.8546 | -0.9302 |
| 0.725 | ******* | -1.0218 | ******* | -1.0637 | -0.9700 |
| 0.750 | -0.6621 | -1.3363 | ******* | -1.1607 | -0.8385 |
| 0.775 | ******* | -1.4707 | -1.4081 | -1.0891 | -0.5490 |
| 0.800 | -1.2070 | -1.4702 | -1.3524 | -0.8556 | ******* |
| 0.825 | ******* | -1.4060 | -1.0987 | -0.7798 | -0.4285 |
| 0.850 | -1.2541 | -1.3072 | -0.9460 | -0.7784 | -0.4150 |
| 0.875 | ******* | -1.1911 | -0.9280 | -0.7549 | -0.4287 |
| 0.900 | -1.1416 | -1.1091 | -0.9106 | -0.7121 | ******* |
| 0.925 | ******* | -1.0725 | -0.8484 | -0.6725 | -0.4382 |
| 0.950 | -1.1650 | -1.0373 | -0.8320 | -0.6592 | -0.3470 |
| 0.975 | ******* | -1.0133 | -0.8096 | -0.6415 | -0.3062 |
| 1.000 | -1.1414 | -1.0085 | -0.8103 | -0.6258 | -0.2722 |
| | Cp,l | Cp,l | Cp,l | Cp,l | Cp,l |
| -0.200 | 0.2407 | 0.2239 | 0.2390 | ******* | -0.3292 |
| -0.400 | 0.2433 | 0.2296 | 0.2095 | 0.0527 | -0.3705 |
| -0.600 | 0.2616 | 0.2449 | 0.2086 | 0.0851 | -0.3779 |
| -0.700 | ******* | 0.2507 | 0.2149 | 0.0982 | -0.4272 |
| -0.800 | ******* | ******* | 0.2259 | 0.1258 | -0.4553 |
| -0.850 | ******* | 0.2750 | 0.2350 | 0.1462 | -0.4639 |
| -0.900 | 0.2934 | 0.2738 | 0.2505 | 0.1686 | -0.4638 |
| -0.950 | 0.2681 | 0.1307 | 0.2222 | 0.1917 | -0.1633 |
| -0.975 | ******* | 0.0968 | 0.1368 | 0.1494 | 0.0026 |
| -1.000 | -1.1414 | -1.0072 | -0.7933 | -0.6254 | -0.2665 |

Surface Pressures




Small Radius L.E.

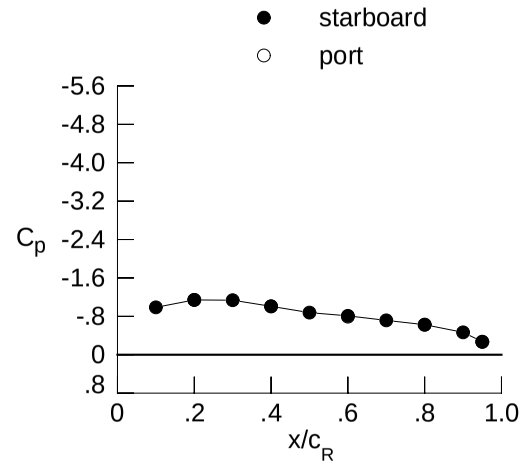
Run No. = 38 , Point No. = 763

$C_N$ = 0.537, $C_m$ = -0.0860

$\alpha$ = 12.4 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

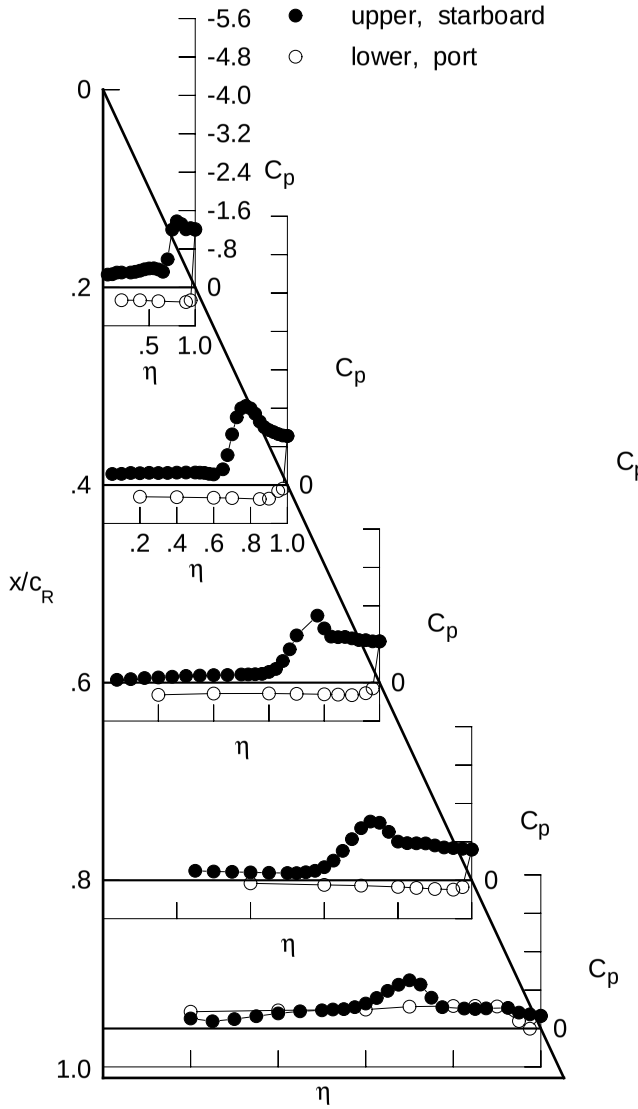



| x/c_R | starb'd Cp | port Cp |
|---|---|---|
| 0.10 | -0.9872 | ******* |
| 0.20 | -1.1414 | -1.1434 |
| 0.30 | -1.1361 | ******* |
| 0.40 | -1.0085 | -1.0072 |
| 0.50 | -0.8772 | ******* |
| 0.60 | -0.8103 | -0.7933 |
| 0.70 | -0.7157 | ******* |
| 0.80 | -0.6258 | -0.6254 |
| 0.90 | -0.4666 | ******* |
| 0.95 | -0.2722 | -0.2665 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2660 | -0.2308 | -0.0580 | ******* | ******* |
| 0.100 | -0.2747 | -0.2327 | -0.0727 | ******* | ******* |
| 0.150 | -0.3086 | -0.2509 | -0.0957 | ******* | ******* |
| 0.200 | -0.3096 | -0.2463 | -0.1082 | ******* | -0.2089 |
| 0.250 | ******* | -0.2541 | -0.1229 | -0.1978 | -0.1506 |
| 0.300 | -0.3092 | -0.2508 | -0.1398 | -0.1827 | -0.1961 |
| 0.350 | -0.3246 | -0.2523 | -0.1470 | -0.1759 | -0.2557 |
| 0.400 | -0.3474 | -0.2585 | -0.1571 | -0.1641 | -0.3144 |
| 0.450 | -0.3767 | -0.2605 | -0.1591 | -0.1558 | -0.3581 |
| 0.500 | -0.3943 | -0.2607 | -0.1697 | -0.1510 | -0.3793 |
| 0.525 | ******* | -0.2576 | -0.1716 | -0.1489 | -0.3961 |
| 0.550 | -0.3977 | -0.2530 | -0.1755 | -0.1675 | -0.4036 |
| 0.575 | ******* | -0.2336 | -0.1822 | -0.1978 | -0.4446 |
| 0.600 | -0.3732 | -0.2212 | -0.2231 | -0.2731 | -0.5201 |
| 0.625 | ******* | ******* | -0.2855 | -0.4096 | -0.6360 |
| 0.650 | -0.3253 | -0.3281 | -0.4502 | -0.6127 | -0.7840 |
| 0.675 | ******* | -0.6237 | -0.6941 | -0.8568 | -0.9118 |
| 0.700 | -0.5853 | -1.0562 | -0.9836 | -1.0859 | -1.0046 |
| 0.725 | ******* | -1.4101 | ******* | -1.2236 | -0.9150 |
| 0.750 | -1.2028 | -1.5987 | ******* | -1.1986 | -0.6413 |
| 0.775 | ******* | -1.6476 | -1.3957 | -1.0085 | -0.4451 |
| 0.800 | -1.3766 | -1.5971 | -1.1296 | -0.8054 | ******* |
| 0.825 | ******* | -1.4854 | -0.9595 | -0.7737 | -0.4162 |
| 0.850 | -1.3191 | -1.3219 | -0.9473 | -0.7706 | -0.4064 |
| 0.875 | ******* | -1.2048 | -0.9521 | -0.7683 | -0.4196 |
| 0.900 | -1.2099 | -1.1445 | -0.9223 | -0.7254 | ******* |
| 0.925 | ******* | -1.1028 | -0.8871 | -0.6842 | -0.4296 |
| 0.950 | -1.2347 | -1.0620 | -0.8850 | -0.6718 | -0.3315 |
| 0.975 | ******* | -1.0320 | -0.8597 | -0.6561 | -0.2951 |
| 1.000 | -1.2003 | -1.0200 | -0.8616 | -0.6399 | -0.2663 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2673 | 0.2441 | 0.2541 | ******* | -0.3497 |
| -0.400 | 0.2679 | 0.2531 | 0.2274 | 0.0632 | -0.3780 |
| -0.600 | 0.2876 | 0.2651 | 0.2253 | 0.0964 | -0.3944 |
| -0.700 | ******* | 0.2713 | 0.2333 | 0.1110 | -0.4554 |
| -0.800 | ******* | ******* | 0.2430 | 0.1380 | -0.4685 |
| -0.850 | ******* | 0.2920 | 0.2495 | 0.1590 | -0.4700 |
| -0.900 | 0.3052 | 0.2841 | 0.2612 | 0.1812 | -0.4589 |
| -0.950 | 0.2681 | 0.1242 | 0.2202 | 0.1949 | -0.1552 |
| -0.975 | ******* | 0.0748 | 0.1199 | 0.1413 | 0.0042 |
| -1.000 | -1.2152 | -1.0247 | -0.8569 | -0.6418 | -0.2587 |

Surface Pressures




Small Radius L.E.

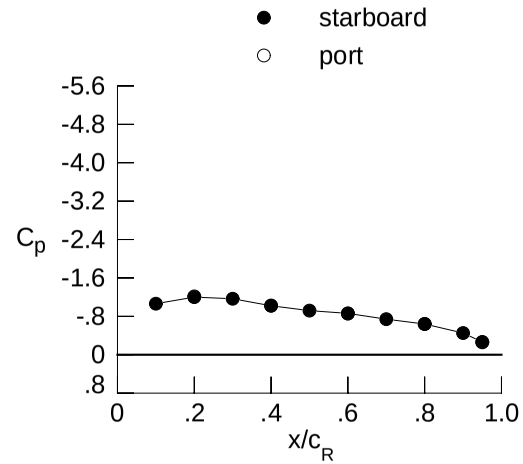
Run No. = 38 , Point No. = 764

$C_N$ = 0.588, $C_m$ = -0.0933

$\alpha$ = 13.4 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

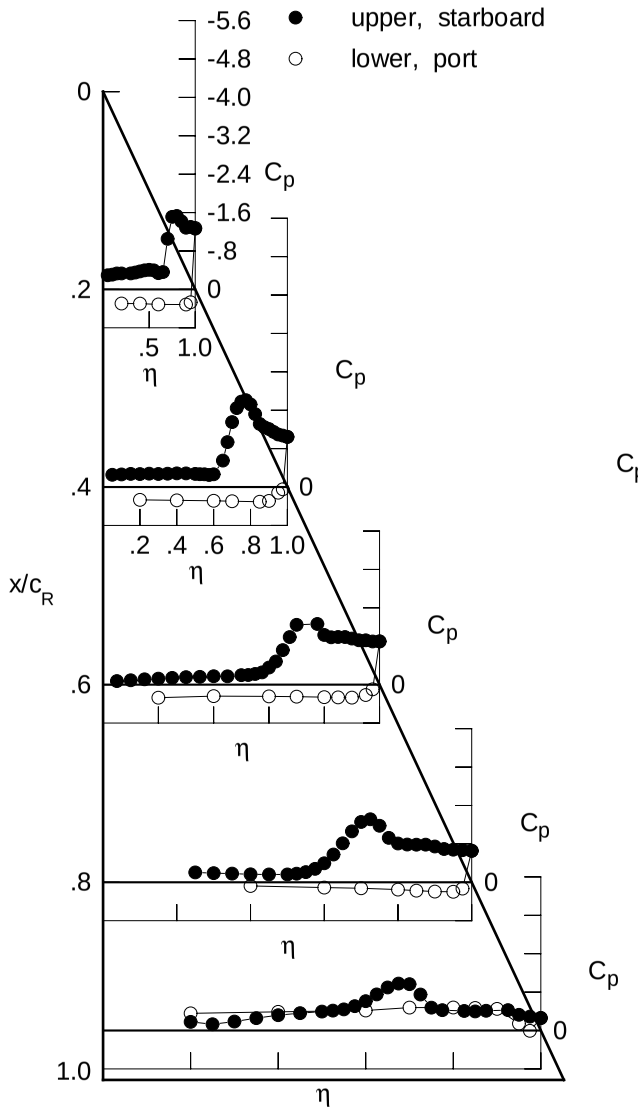



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0629 | ******* |
| 0.20 | -1.2003 | -1.2152 |
| 0.30 | -1.1665 | ******* |
| 0.40 | -1.0200 | -1.0247 |
| 0.50 | -0.9189 | ******* |
| 0.60 | -0.8616 | -0.8569 |
| 0.70 | -0.7405 | ******* |
| 0.80 | -0.6399 | -0.6418 |
| 0.90 | -0.4520 | ******* |
| 0.95 | -0.2663 | -0.2587 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2947 | -0.2550 | -0.0740 | ******* | ******* |
| 0.100 | -0.3070 | -0.2621 | -0.0914 | ******* | ******* |
| 0.150 | -0.3324 | -0.2737 | -0.1111 | ******* | ******* |
| 0.200 | -0.3321 | -0.2705 | -0.1246 | ******* | -0.1803 |
| 0.250 | ******* | -0.2784 | -0.1405 | -0.2053 | -0.1303 |
| 0.300 | -0.3331 | -0.2721 | -0.1557 | -0.1900 | -0.1863 |
| 0.350 | -0.3513 | -0.2775 | -0.1624 | -0.1810 | -0.2576 |
| 0.400 | -0.3748 | -0.2848 | -0.1753 | -0.1660 | -0.3195 |
| 0.450 | -0.3968 | -0.2842 | -0.1740 | -0.1631 | -0.3614 |
| 0.500 | -0.4084 | -0.2739 | -0.1976 | -0.1629 | -0.3942 |
| 0.525 | ******* | -0.2670 | -0.2008 | -0.1788 | -0.4144 |
| 0.550 | -0.3967 | -0.2652 | -0.2227 | -0.2119 | -0.4398 |
| 0.575 | ******* | -0.2515 | -0.2556 | -0.2799 | -0.5072 |
| 0.600 | -0.3385 | -0.2659 | -0.3560 | -0.3963 | -0.6113 |
| 0.625 | ******* | ******* | -0.4827 | -0.5787 | -0.7519 |
| 0.650 | -0.3614 | -0.5513 | -0.7196 | -0.8122 | -0.8967 |
| 0.675 | ******* | -0.9360 | -0.9912 | -1.0610 | -0.9777 |
| 0.700 | -1.0529 | -1.3530 | -1.2467 | -1.2567 | -0.9654 |
| 0.725 | ******* | -1.6452 | ******* | -1.3126 | -0.7499 |
| 0.750 | -1.5115 | -1.7795 | ******* | -1.1774 | -0.4756 |
| 0.775 | ******* | -1.8099 | -1.2640 | -0.9257 | -0.4239 |
| 0.800 | -1.5294 | -1.7211 | -1.0356 | -0.8081 | ******* |
| 0.825 | ******* | -1.5190 | -0.9865 | -0.7863 | -0.4076 |
| 0.850 | -1.4178 | -1.3142 | -0.9925 | -0.7833 | -0.3973 |
| 0.875 | ******* | -1.2481 | -0.9917 | -0.7840 | -0.4114 |
| 0.900 | -1.2849 | -1.2083 | -0.9596 | -0.7456 | ******* |
| 0.925 | ******* | -1.1488 | -0.9252 | -0.6937 | -0.4250 |
| 0.950 | -1.3019 | -1.0955 | -0.9238 | -0.6790 | -0.3271 |
| 0.975 | ******* | -1.0718 | -0.8991 | -0.6688 | -0.2895 |
| 1.000 | -1.2651 | -1.0430 | -0.8991 | -0.6578 | -0.2639 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2943 | 0.2670 | 0.2719 | ******* | -0.3575 |
| -0.400 | 0.2961 | 0.2773 | 0.2393 | 0.0764 | -0.3891 |
| -0.600 | 0.3135 | 0.2865 | 0.2447 | 0.1100 | -0.4168 |
| -0.700 | ******* | 0.2957 | 0.2506 | 0.1245 | -0.4773 |
| -0.800 | ******* | ******* | 0.2608 | 0.1519 | -0.4791 |
| -0.850 | ******* | 0.3064 | 0.2657 | 0.1741 | -0.4699 |
| -0.900 | 0.3156 | 0.2894 | 0.2704 | 0.1936 | -0.4502 |
| -0.950 | 0.2684 | 0.1178 | 0.2162 | 0.1975 | -0.1443 |
| -0.975 | ******* | 0.0475 | 0.0978 | 0.1310 | 0.0061 |
| -1.000 | -1.2798 | -1.0466 | -0.9024 | -0.6539 | -0.2567 |

Surface Pressures




Small Radius L.E.

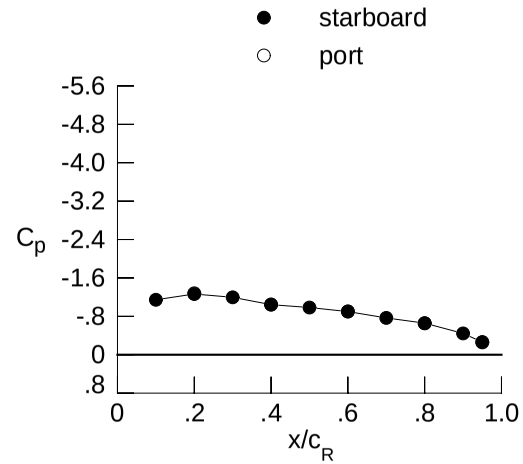
Run No. = 38 , Point No. = 765

$C_N$ = 0.637, $C_m$ = -0.0974

$\alpha$ = 14.4 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

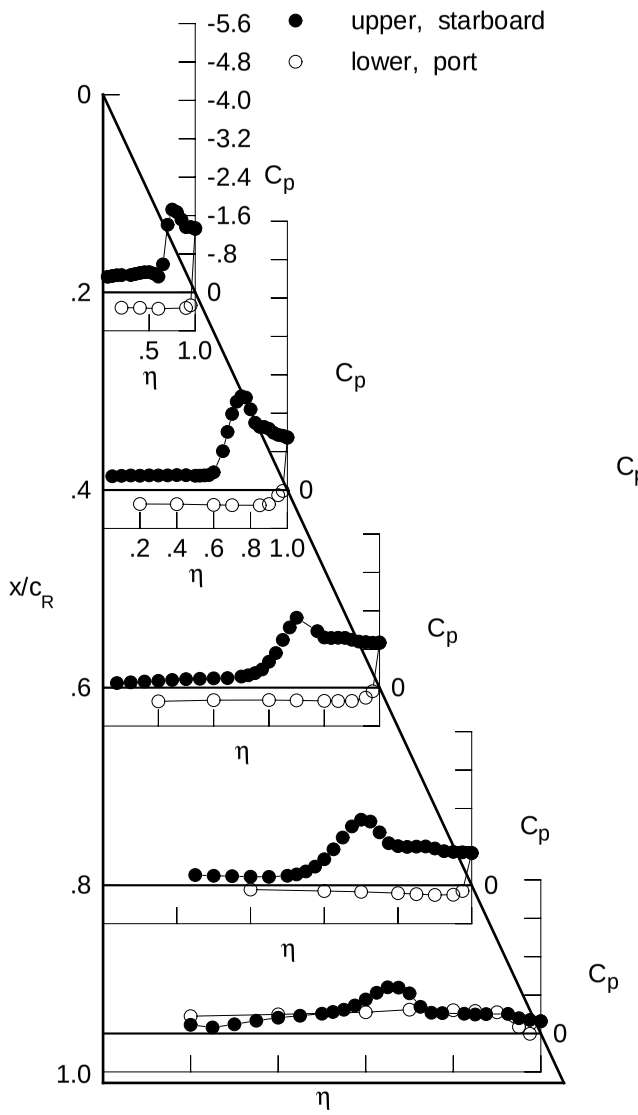



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1451 | ******* |
| 0.20 | -1.2651 | -1.2798 |
| 0.30 | -1.1962 | ******* |
| 0.40 | -1.0430 | -1.0466 |
| 0.50 | -0.9836 | ******* |
| 0.60 | -0.8991 | -0.9024 |
| 0.70 | -0.7668 | ******* |
| 0.80 | -0.6578 | -0.6539 |
| 0.90 | -0.4439 | ******* |
| 0.95 | -0.2639 | -0.2567 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3245 | -0.2872 | -0.0955 | ******* | ******* |
| 0.100 | -0.3418 | -0.2957 | -0.1105 | ******* | ******* |
| 0.150 | -0.3573 | -0.3031 | -0.1276 | ******* | ******* |
| 0.200 | -0.3606 | -0.2986 | -0.1415 | ******* | -0.1810 |
| 0.250 | ******* | -0.3059 | -0.1598 | -0.2135 | -0.1262 |
| 0.300 | -0.3614 | -0.3038 | -0.1766 | -0.1980 | -0.1922 |
| 0.350 | -0.3829 | -0.3055 | -0.1846 | -0.1896 | -0.2666 |
| 0.400 | -0.4038 | -0.3118 | -0.1934 | -0.1784 | -0.3293 |
| 0.450 | -0.4205 | -0.3095 | -0.1989 | -0.1763 | -0.3703 |
| 0.500 | -0.4221 | -0.2979 | -0.2316 | -0.1986 | -0.4130 |
| 0.525 | ******* | -0.2988 | -0.2565 | -0.2266 | -0.4487 |
| 0.550 | -0.3913 | -0.3048 | -0.3028 | -0.2879 | -0.4955 |
| 0.575 | ******* | -0.3127 | -0.3784 | -0.3885 | -0.5844 |
| 0.600 | -0.3291 | -0.3705 | -0.5400 | -0.5420 | -0.7091 |
| 0.625 | ******* | ******* | -0.7204 | -0.7493 | -0.8491 |
| 0.650 | -0.5849 | -0.8098 | -0.9942 | -0.9947 | -0.9621 |
| 0.675 | ******* | -1.2108 | -1.2546 | -1.2268 | -0.9562 |
| 0.700 | -1.4090 | -1.5850 | -1.4570 | -1.3665 | -0.8364 |
| 0.725 | ******* | -1.8399 | ******* | -1.3270 | -0.5560 |
| 0.750 | -1.7257 | -1.9524 | ******* | -1.1026 | -0.4332 |
| 0.775 | ******* | -1.9258 | -1.1768 | -0.8761 | -0.4245 |
| 0.800 | -1.6731 | -1.6816 | -1.0447 | -0.8156 | ******* |
| 0.825 | ******* | -1.4014 | -1.0347 | -0.8003 | -0.4123 |
| 0.850 | -1.5193 | -1.3175 | -1.0393 | -0.8053 | -0.3960 |
| 0.875 | ******* | -1.3129 | -1.0367 | -0.8085 | -0.4042 |
| 0.900 | -1.3599 | -1.2753 | -0.9977 | -0.7666 | ******* |
| 0.925 | ******* | -1.1933 | -0.9600 | -0.7106 | -0.4090 |
| 0.950 | -1.3613 | -1.1495 | -0.9496 | -0.6949 | -0.3189 |
| 0.975 | ******* | -1.1310 | -0.9356 | -0.6871 | -0.2825 |
| 1.000 | -1.3220 | -1.1007 | -0.9310 | -0.6724 | -0.2572 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3189 | 0.2912 | 0.2859 | ******* | -0.3606 |
| -0.400 | 0.3217 | 0.2941 | 0.2610 | 0.0889 | -0.3983 |
| -0.600 | 0.3396 | 0.3092 | 0.2584 | 0.1196 | -0.4433 |
| -0.700 | ******* | 0.3158 | 0.2657 | 0.1360 | -0.4966 |
| -0.800 | ******* | ******* | 0.2762 | 0.1638 | -0.4852 |
| -0.850 | ******* | 0.3176 | 0.2788 | 0.1850 | -0.4691 |
| -0.900 | 0.3249 | 0.2932 | 0.2775 | 0.2013 | -0.4423 |
| -0.950 | 0.2685 | 0.1083 | 0.2096 | 0.1968 | -0.1367 |
| -0.975 | ******* | 0.0181 | 0.0742 | 0.1184 | 0.0064 |
| -1.000 | -1.3420 | -1.0886 | -0.9433 | -0.6710 | -0.2536 |

Surface Pressures




Small Radius L.E.

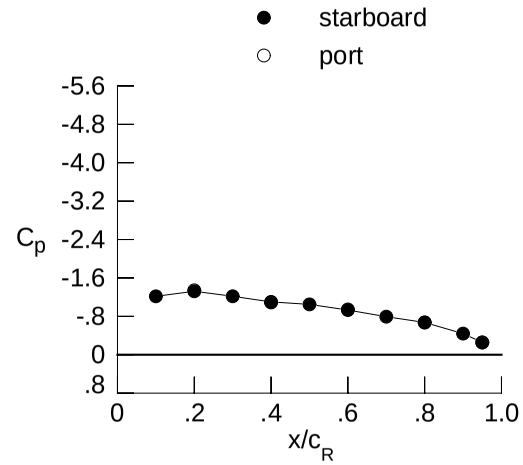
Run No. = 38 , Point No. = 766

$C_N$ = 0.689, $C_m$ = -0.1034

$\alpha$ = 15.5 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

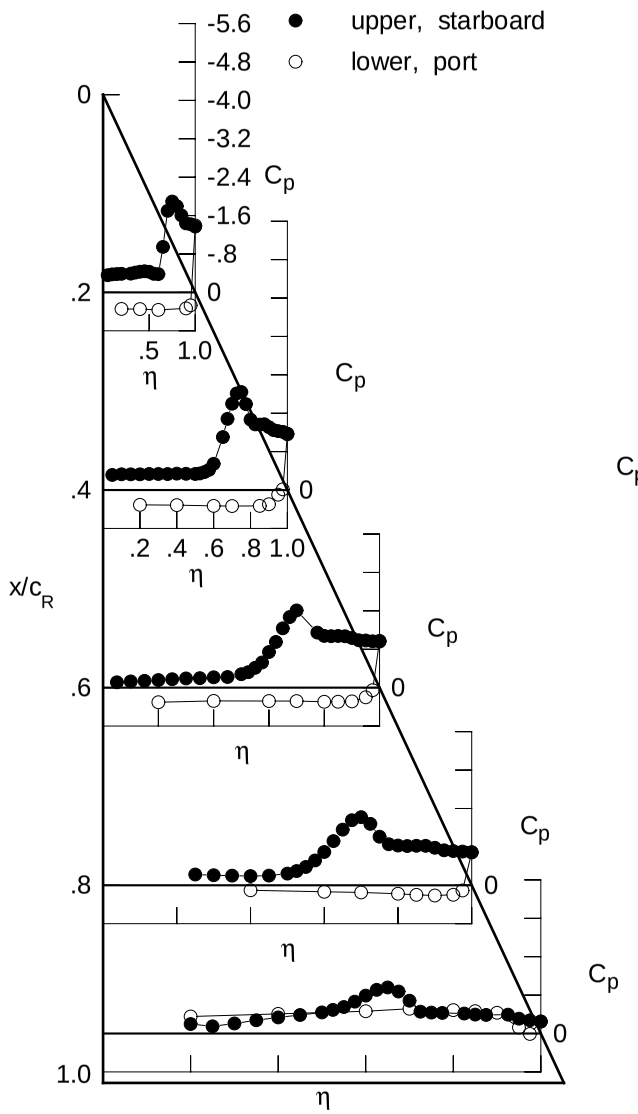



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.2170 | ******* |
| 0.20 | -1.3220 | -1.3420 |
| 0.30 | -1.2179 | ******* |
| 0.40 | -1.1007 | -1.0886 |
| 0.50 | -1.0489 | ******* |
| 0.60 | -0.9310 | -0.9433 |
| 0.70 | -0.7925 | ******* |
| 0.80 | -0.6724 | -0.6710 |
| 0.90 | -0.4396 | ******* |
| 0.95 | -0.2572 | -0.2536 |

# Table D2. Continued.

| η | x/c_R .2 Cp,u | x/c_R .4 Cp,u | x/c_R .6 Cp,u | x/c_R .8 Cp,u | x/c_R .95 Cp,u |
|---|---|---|---|---|---|
| 0.050 | -0.3577 | -0.3142 | -0.1114 | ******* | ******* |
| 0.100 | -0.3760 | -0.3283 | -0.1297 | ******* | ******* |
| 0.150 | -0.3825 | -0.3274 | -0.1419 | ******* | ******* |
| 0.200 | -0.3869 | -0.3270 | -0.1588 | ******* | -0.1979 |
| 0.250 | ******* | -0.3345 | -0.1755 | -0.2244 | -0.1498 |
| 0.300 | -0.3907 | -0.3344 | -0.1921 | -0.2094 | -0.2084 |
| 0.350 | -0.4124 | -0.3325 | -0.1978 | -0.2005 | -0.2761 |
| 0.400 | -0.4305 | -0.3419 | -0.2154 | -0.1919 | -0.3351 |
| 0.450 | -0.4399 | -0.3387 | -0.2215 | -0.2015 | -0.3857 |
| 0.500 | -0.4293 | -0.3347 | -0.2802 | -0.2433 | -0.4389 |
| 0.525 | ******* | -0.3455 | -0.3212 | -0.2967 | -0.4921 |
| 0.550 | -0.3870 | -0.3742 | -0.4129 | -0.3815 | -0.5521 |
| 0.575 | ******* | -0.4214 | -0.5239 | -0.5166 | -0.6641 |
| 0.600 | -0.3809 | -0.5465 | -0.7414 | -0.6939 | -0.7892 |
| 0.625 | ******* | ******* | -0.9519 | -0.9209 | -0.9099 |
| 0.650 | -0.9473 | -1.1032 | -1.2364 | -1.1592 | -0.9593 |
| 0.675 | ******* | -1.4822 | -1.4707 | -1.3551 | -0.8744 |
| 0.700 | -1.6995 | -1.7983 | -1.6090 | -1.4190 | -0.6834 |
| 0.725 | ******* | -2.0129 | ******* | -1.2802 | -0.4546 |
| 0.750 | -1.8924 | -2.0418 | ******* | -1.0119 | -0.4362 |
| 0.775 | ******* | -1.7894 | -1.1466 | -0.8553 | -0.4291 |
| 0.800 | -1.7964 | -1.4663 | -1.0774 | -0.8282 | ******* |
| 0.825 | ******* | -1.3683 | -1.0721 | -0.8174 | -0.4163 |
| 0.850 | -1.6040 | -1.3632 | -1.0772 | -0.8235 | -0.3946 |
| 0.875 | ******* | -1.3707 | -1.0705 | -0.8225 | -0.3874 |
| 0.900 | -1.4377 | -1.3090 | -1.0343 | -0.7813 | ******* |
| 0.925 | ******* | -1.2486 | -0.9872 | -0.7291 | -0.3925 |
| 0.950 | -1.4189 | -1.2271 | -0.9827 | -0.7136 | -0.3087 |
| 0.975 | ******* | -1.2127 | -0.9658 | -0.7023 | -0.2751 |
| 1.000 | -1.3711 | -1.1743 | -0.9602 | -0.6899 | -0.2511 |
| | Cp,l | Cp,l | Cp,l | Cp,l | Cp,l |
| -0.200 | 0.3449 | 0.3091 | 0.3043 | ******* | -0.3542 |
| -0.400 | 0.3484 | 0.3147 | 0.2765 | 0.1038 | -0.4088 |
| -0.600 | 0.3646 | 0.3303 | 0.2788 | 0.1354 | -0.4638 |
| -0.700 | ******* | 0.3338 | 0.2800 | 0.1491 | -0.5159 |
| -0.800 | ******* | ******* | 0.2941 | 0.1761 | -0.4876 |
| -0.850 | ******* | 0.3303 | 0.2939 | 0.1993 | -0.4653 |
| -0.900 | 0.3336 | 0.2960 | 0.2865 | 0.2128 | -0.4322 |
| -0.950 | 0.2687 | 0.0965 | 0.2017 | 0.1976 | -0.1255 |
| -0.975 | ******* | -0.0151 | 0.0531 | 0.1077 | 0.0086 |
| -1.000 | -1.3948 | -1.1608 | -0.9753 | -0.6837 | -0.2478 |

Surface Pressures




Small Radius L.E.

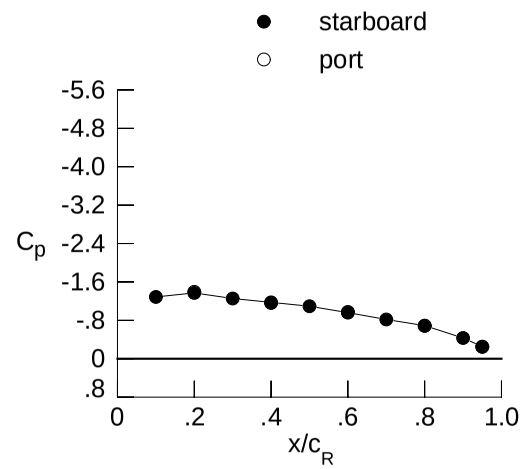
Run No. = 38 , Point No. = 767

$C_N$ = 0.742, $C_m$ = -0.1093

$\alpha$ = 16.5 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

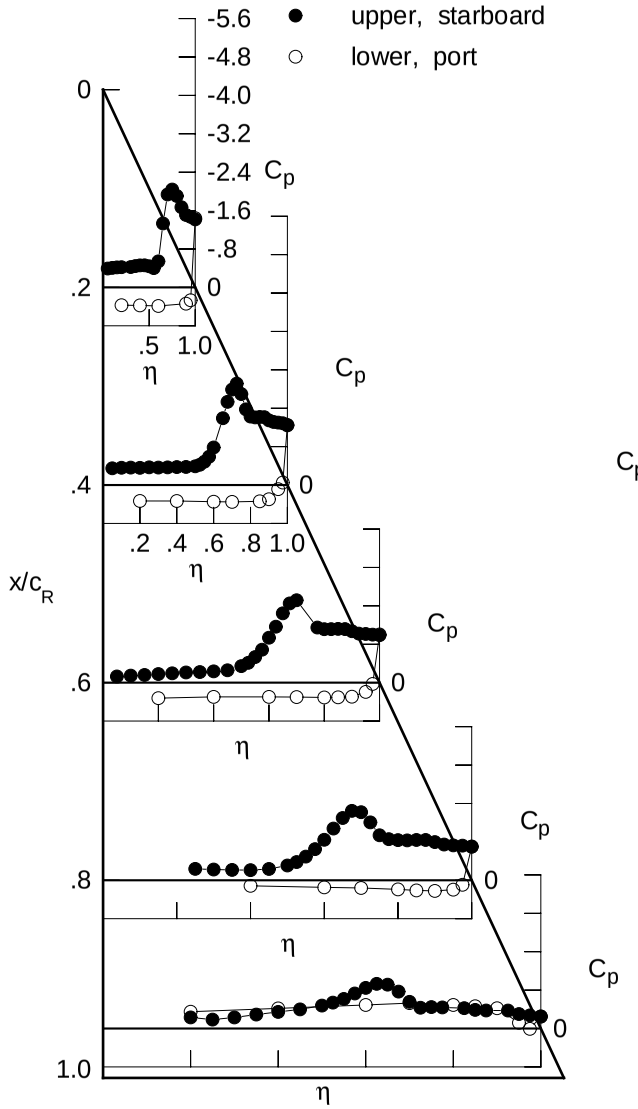



| x/c_R | starb'd Cp | port Cp |
|---|---|---|
| 0.10 | -1.2872 | ******* |
| 0.20 | -1.3711 | -1.3948 |
| 0.30 | -1.2547 | ******* |
| 0.40 | -1.1743 | -1.1608 |
| 0.50 | -1.0939 | ******* |
| 0.60 | -0.9602 | -0.9753 |
| 0.70 | -0.8179 | ******* |
| 0.80 | -0.6899 | -0.6837 |
| 0.90 | -0.4321 | ******* |
| 0.95 | -0.2511 | -0.2478 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3929 | -0.3486 | -0.1287 | ******* | ******* |
| 0.100 | -0.4064 | -0.3598 | -0.1461 | ******* | ******* |
| 0.150 | -0.4168 | -0.3634 | -0.1596 | ******* | ******* |
| 0.200 | -0.4204 | -0.3584 | -0.1790 | ******* | -0.2309 |
| 0.250 | ******* | -0.3685 | -0.1940 | -0.2379 | -0.1854 |
| 0.300 | -0.4238 | -0.3638 | -0.2118 | -0.2240 | -0.2305 |
| 0.350 | -0.4438 | -0.3682 | -0.2206 | -0.2160 | -0.2901 |
| 0.400 | -0.4588 | -0.3741 | -0.2353 | -0.2113 | -0.3458 |
| 0.450 | -0.4602 | -0.3766 | -0.2578 | -0.2360 | -0.3983 |
| 0.500 | -0.4402 | -0.3906 | -0.3438 | -0.3078 | -0.4772 |
| 0.525 | ******* | -0.4227 | -0.4128 | -0.3802 | -0.5395 |
| 0.550 | -0.4018 | -0.4866 | -0.5328 | -0.4932 | -0.6158 |
| 0.575 | ******* | -0.5895 | -0.6866 | -0.6490 | -0.7299 |
| 0.600 | -0.5426 | -0.7820 | -0.9363 | -0.8443 | -0.8462 |
| 0.625 | ******* | ******* | -1.1655 | -1.0777 | -0.9302 |
| 0.650 | -1.3321 | -1.3916 | -1.4441 | -1.2972 | -0.9137 |
| 0.675 | ******* | -1.7325 | -1.6501 | -1.4462 | -0.7686 |
| 0.700 | -1.9363 | -1.9886 | -1.7165 | -1.4180 | -0.5557 |
| 0.725 | ******* | -2.1127 | ******* | -1.2061 | -0.4329 |
| 0.750 | -2.0384 | -1.8953 | ******* | -0.9379 | -0.4466 |
| 0.775 | ******* | -1.5765 | -1.1477 | -0.8572 | -0.4389 |
| 0.800 | -1.9052 | -1.4262 | -1.1138 | -0.8366 | ******* |
| 0.825 | ******* | -1.4086 | -1.1142 | -0.8310 | -0.4237 |
| 0.850 | -1.6708 | -1.4183 | -1.1199 | -0.8403 | -0.3878 |
| 0.875 | ******* | -1.4135 | -1.1160 | -0.8397 | -0.3754 |
| 0.900 | -1.5086 | -1.3475 | -1.0713 | -0.7964 | ******* |
| 0.925 | ******* | -1.3145 | -1.0214 | -0.7451 | -0.3742 |
| 0.950 | -1.4698 | -1.3006 | -1.0141 | -0.7275 | -0.3017 |
| 0.975 | ******* | -1.2873 | -0.9996 | -0.7215 | -0.2739 |
| 1.000 | -1.4165 | -1.2508 | -0.9887 | -0.7036 | -0.2525 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3712 | 0.3320 | 0.3230 | ******* | -0.3498 |
| -0.400 | 0.3754 | 0.3326 | 0.2966 | 0.1154 | -0.4193 |
| -0.600 | 0.3874 | 0.3476 | 0.2970 | 0.1472 | -0.4905 |
| -0.700 | ******* | 0.3514 | 0.3004 | 0.1602 | -0.5291 |
| -0.800 | ******* | ******* | 0.3086 | 0.1895 | -0.4906 |
| -0.850 | ******* | 0.3391 | 0.3057 | 0.2110 | -0.4642 |
| -0.900 | 0.3395 | 0.2962 | 0.2931 | 0.2214 | -0.4226 |
| -0.950 | 0.2679 | 0.0856 | 0.1927 | 0.1954 | -0.1190 |
| -0.975 | ******* | -0.0521 | 0.0271 | 0.0935 | 0.0074 |
| -1.000 | -1.4427 | -1.2430 | -1.0043 | -0.6993 | -0.2475 |

Surface Pressures




Small Radius L.E.

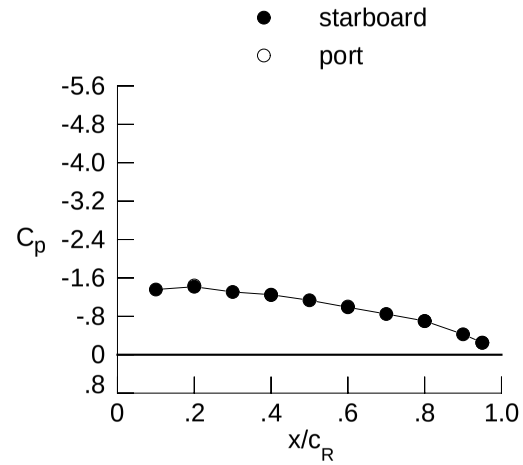
Run No. = 38 , Point No. = 768

$C_N$ = 0.792, $C_m$ = -0.1128

$\alpha$ = 17.5 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

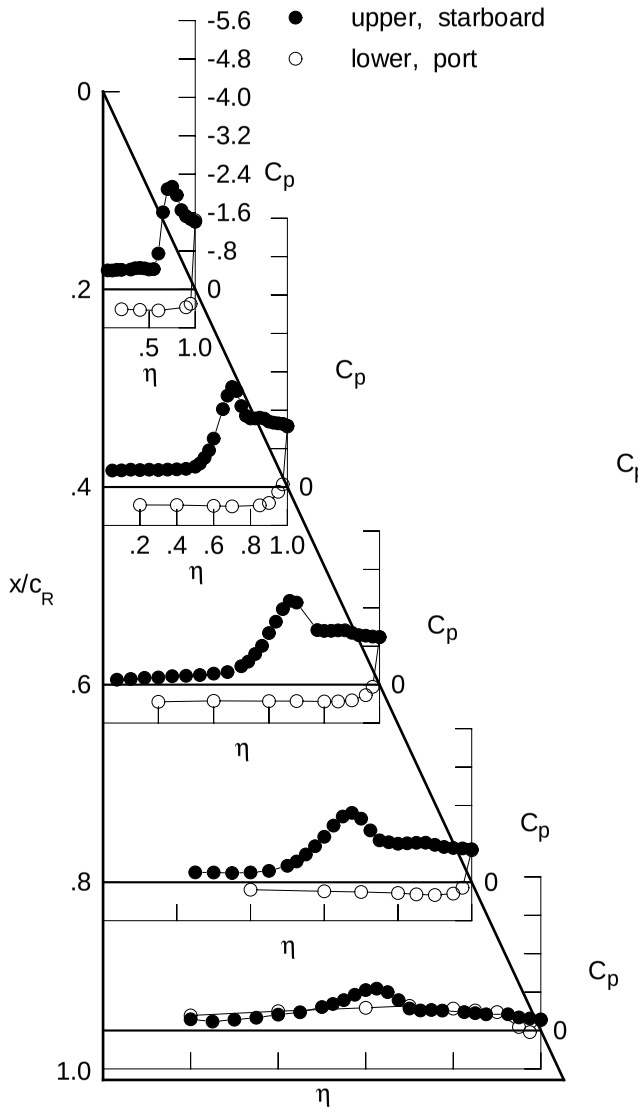



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.3586 | ******* |
| 0.20 | -1.4165 | -1.4427 |
| 0.30 | -1.3074 | ******* |
| 0.40 | -1.2508 | -1.2430 |
| 0.50 | -1.1347 | ******* |
| 0.60 | -0.9887 | -1.0043 |
| 0.70 | -0.8486 | ******* |
| 0.80 | -0.7036 | -0.6993 |
| 0.90 | -0.4258 | ******* |
| 0.95 | -0.2525 | -0.2475 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3960 | -0.3436 | -0.1035 | ******* | ******* |
| 0.100 | -0.3932 | -0.3468 | -0.1180 | ******* | ******* |
| 0.150 | -0.4079 | -0.3615 | -0.1404 | ******* | ******* |
| 0.200 | -0.4071 | -0.3540 | -0.1492 | ******* | -0.2337 |
| 0.250 | ******* | -0.3617 | -0.1760 | -0.2063 | -0.1866 |
| 0.300 | -0.4135 | -0.3551 | -0.1846 | -0.2042 | -0.2258 |
| 0.350 | -0.4412 | -0.3634 | -0.1999 | -0.1926 | -0.2668 |
| 0.400 | -0.4472 | -0.3687 | -0.2296 | -0.2045 | -0.3304 |
| 0.450 | -0.4379 | -0.3793 | -0.2616 | -0.2380 | -0.3799 |
| 0.500 | -0.4141 | -0.4239 | -0.3833 | -0.3429 | -0.4887 |
| 0.525 | ******* | -0.4896 | -0.4792 | -0.4340 | -0.5532 |
| 0.550 | -0.4233 | -0.6075 | -0.6378 | -0.5790 | -0.6331 |
| 0.575 | ******* | -0.7650 | -0.8088 | -0.7513 | -0.7451 |
| 0.600 | -0.7473 | -1.0085 | -1.0755 | -0.9478 | -0.8423 |
| 0.625 | ******* | ******* | -1.3116 | -1.1812 | -0.8719 |
| 0.650 | -1.6063 | -1.6224 | -1.5734 | -1.3700 | -0.8000 |
| 0.675 | ******* | -1.9040 | -1.7457 | -1.4461 | -0.6330 |
| 0.700 | -2.0886 | -2.0837 | -1.7097 | -1.3254 | -0.4583 |
| 0.725 | ******* | -2.0000 | ******* | -1.0807 | -0.4173 |
| 0.750 | -2.1377 | -1.6866 | ******* | -0.8735 | -0.4276 |
| 0.775 | ******* | -1.4853 | -1.1364 | -0.8342 | -0.4151 |
| 0.800 | -1.9643 | -1.4291 | -1.1188 | -0.8032 | ******* |
| 0.825 | ******* | -1.4286 | -1.1216 | -0.8119 | -0.3832 |
| 0.850 | -1.6508 | -1.4448 | -1.1302 | -0.8224 | -0.3619 |
| 0.875 | ******* | -1.4246 | -1.1318 | -0.8248 | -0.3379 |
| 0.900 | -1.5256 | -1.3634 | -1.0797 | -0.7803 | ******* |
| 0.925 | ******* | -1.3401 | -1.0306 | -0.7359 | -0.3380 |
| 0.950 | -1.4661 | -1.3269 | -1.0201 | -0.7150 | -0.2730 |
| 0.975 | ******* | -1.3158 | -1.0020 | -0.7060 | -0.2505 |
| 1.000 | -1.4082 | -1.2778 | -0.9905 | -0.6879 | -0.2314 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4143 | 0.3736 | 0.3575 | ******* | -0.3133 |
| -0.400 | 0.4274 | 0.3756 | 0.3382 | 0.1543 | -0.4023 |
| -0.600 | 0.4389 | 0.3919 | 0.3431 | 0.1884 | -0.4732 |
| -0.700 | ******* | 0.4031 | 0.3425 | 0.2020 | -0.5127 |
| -0.800 | ******* | ******* | 0.3508 | 0.2234 | -0.4571 |
| -0.850 | ******* | 0.3813 | 0.3506 | 0.2522 | -0.4170 |
| -0.900 | 0.3725 | 0.3319 | 0.3268 | 0.2660 | -0.3832 |
| -0.950 | 0.3003 | 0.0993 | 0.2189 | 0.2363 | -0.0734 |
| -0.975 | ******* | -0.0565 | 0.0456 | 0.1139 | 0.0339 |
| -1.000 | -1.4389 | -1.2600 | -0.9906 | -0.6683 | -0.2171 |

Surface Pressures




Small Radius L.E.

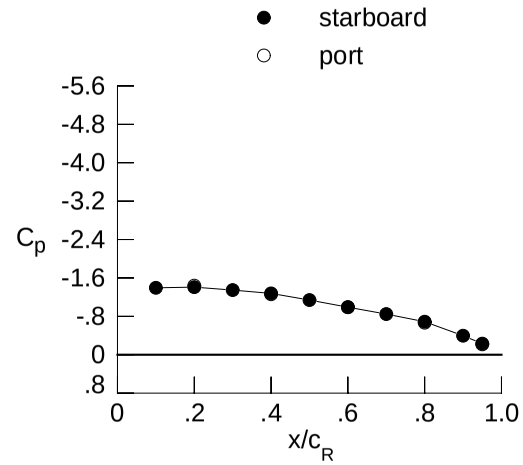
Run No. = 38 , Point No. = 769

$C_N$ = 0.847, $C_m$ = -0.1191

$\alpha$ = 18.5 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

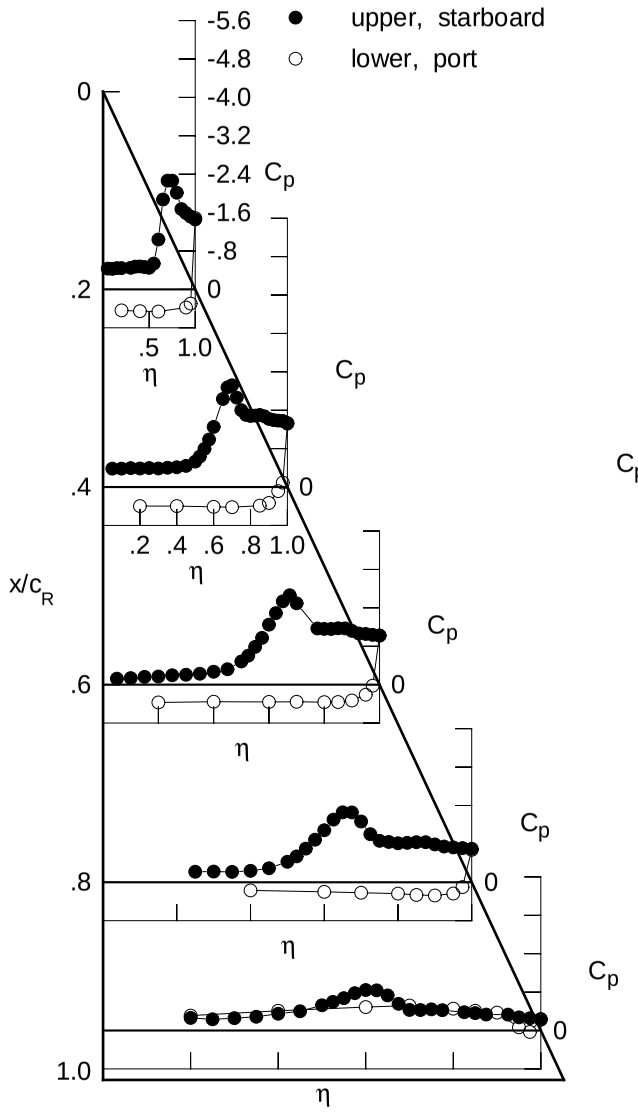



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.3940 | ******* |
| 0.20 | -1.4082 | -1.4389 |
| 0.30 | -1.3470 | ******* |
| 0.40 | -1.2778 | -1.2600 |
| 0.50 | -1.1392 | ******* |
| 0.60 | -0.9905 | -0.9906 |
| 0.70 | -0.8471 | ******* |
| 0.80 | -0.6879 | -0.6683 |
| 0.90 | -0.3963 | ******* |
| 0.95 | -0.2314 | -0.2171 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4330 | -0.3834 | -0.1247 | ******* | ******* |
| 0.100 | -0.4274 | -0.3828 | -0.1361 | ******* | ******* |
| 0.150 | -0.4433 | -0.3947 | -0.1615 | ******* | ******* |
| 0.200 | -0.4439 | -0.3867 | -0.1690 | ******* | -0.2621 |
| 0.250 | ******* | -0.3959 | -0.1951 | -0.2199 | -0.2335 |
| 0.300 | -0.4493 | -0.3867 | -0.2063 | -0.2231 | -0.2572 |
| 0.350 | -0.4743 | -0.4026 | -0.2274 | -0.2165 | -0.2866 |
| 0.400 | -0.4775 | -0.4119 | -0.2691 | -0.2387 | -0.3496 |
| 0.450 | -0.4654 | -0.4410 | -0.3208 | -0.2931 | -0.4010 |
| 0.500 | -0.4504 | -0.5293 | -0.4824 | -0.4269 | -0.5252 |
| 0.525 | ******* | -0.6350 | -0.6031 | -0.5390 | -0.5970 |
| 0.550 | -0.5378 | -0.7944 | -0.7863 | -0.7013 | -0.6747 |
| 0.575 | ******* | -0.9897 | -0.9747 | -0.8872 | -0.7778 |
| 0.600 | -1.0388 | -1.2527 | -1.2492 | -1.0843 | -0.8435 |
| 0.625 | ******* | ******* | -1.4896 | -1.3059 | -0.8366 |
| 0.650 | -1.8730 | -1.8342 | -1.7355 | -1.4580 | -0.7312 |
| 0.675 | ******* | -2.0771 | -1.8621 | -1.4551 | -0.5564 |
| 0.700 | -2.2656 | -2.1202 | -1.6942 | -1.2663 | -0.4287 |
| 0.725 | ******* | -1.8628 | ******* | -1.0017 | -0.4266 |
| 0.750 | -2.2653 | -1.6014 | ******* | -0.8638 | -0.4405 |
| 0.775 | ******* | -1.5039 | -1.1707 | -0.8397 | -0.4235 |
| 0.800 | -2.0138 | -1.4809 | -1.1604 | -0.8132 | ******* |
| 0.825 | ******* | -1.4879 | -1.1599 | -0.8220 | -0.3805 |
| 0.850 | -1.6733 | -1.5017 | -1.1744 | -0.8352 | -0.3622 |
| 0.875 | ******* | -1.4732 | -1.1717 | -0.8349 | -0.3325 |
| 0.900 | -1.5899 | -1.4184 | -1.1210 | -0.7888 | ******* |
| 0.925 | ******* | -1.3953 | -1.0656 | -0.7448 | -0.3314 |
| 0.950 | -1.5166 | -1.3843 | -1.0560 | -0.7262 | -0.2746 |
| 0.975 | ******* | -1.3762 | -1.0369 | -0.7129 | -0.2563 |
| 1.000 | -1.4571 | -1.3345 | -1.0243 | -0.6986 | -0.2397 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4380 | 0.3968 | 0.3712 | ******* | -0.3106 |
| -0.400 | 0.4533 | 0.3968 | 0.3562 | 0.1687 | -0.4107 |
| -0.600 | 0.4617 | 0.4126 | 0.3603 | 0.1991 | -0.4884 |
| -0.700 | ******* | 0.4203 | 0.3567 | 0.2179 | -0.5201 |
| -0.800 | ******* | ******* | 0.3652 | 0.2358 | -0.4550 |
| -0.850 | ******* | 0.3884 | 0.3627 | 0.2638 | -0.4102 |
| -0.900 | 0.3779 | 0.3317 | 0.3305 | 0.2749 | -0.3728 |
| -0.950 | 0.2961 | 0.0850 | 0.2099 | 0.2344 | -0.0663 |
| -0.975 | ******* | -0.0921 | 0.0214 | 0.0992 | 0.0306 |
| -1.000 | -1.4856 | -1.3208 | -1.0215 | -0.6760 | -0.2244 |

Surface Pressures




Small Radius L.E.

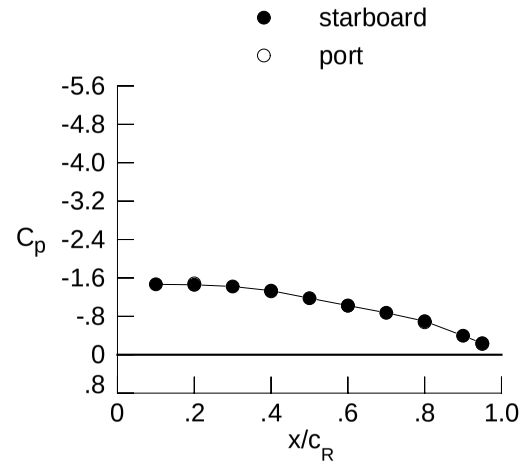
Run No. = 38 , Point No. = 770

$C_N$ = 0.902, $C_m$ = -0.1259

$\alpha$ = 19.5 °, $M_\infty$ = 0.601

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

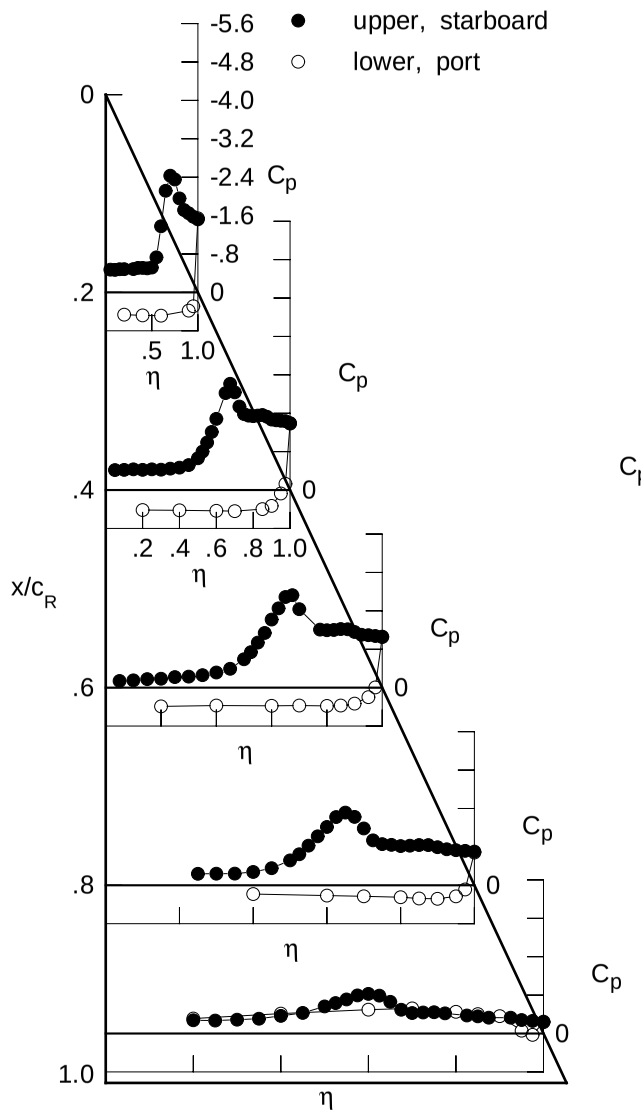



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.4669 | ******* |
| 0.20 | -1.4571 | -1.4856 |
| 0.30 | -1.4219 | ******* |
| 0.40 | -1.3345 | -1.3208 |
| 0.50 | -1.1779 | ******* |
| 0.60 | -1.0243 | -1.0215 |
| 0.70 | -0.8735 | ******* |
| 0.80 | -0.6986 | -0.6760 |
| 0.90 | -0.3963 | ******* |
| 0.95 | -0.2397 | -0.2244 |

# Table D2. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4739 | -0.4157 | -0.1395 | ******* | ******* |
| 0.100 | -0.4686 | -0.4202 | -0.1523 | ******* | ******* |
| 0.150 | -0.4825 | -0.4314 | -0.1772 | ******* | ******* |
| 0.200 | -0.4837 | -0.4209 | -0.1858 | ******* | -0.2757 |
| 0.250 | ******* | -0.4316 | -0.2197 | -0.2393 | -0.2695 |
| 0.300 | -0.4854 | -0.4238 | -0.2294 | -0.2414 | -0.2878 |
| 0.350 | -0.5104 | -0.4456 | -0.2598 | -0.2431 | -0.3082 |
| 0.400 | -0.5108 | -0.4661 | -0.3149 | -0.2773 | -0.3675 |
| 0.450 | -0.5007 | -0.5200 | -0.3930 | -0.3556 | -0.4287 |
| 0.500 | -0.5177 | -0.6616 | -0.5915 | -0.5186 | -0.5643 |
| 0.525 | ******* | -0.8008 | -0.7389 | -0.6467 | -0.6346 |
| 0.550 | -0.7306 | -0.9902 | -0.9383 | -0.8256 | -0.7098 |
| 0.575 | ******* | -1.2104 | -1.1394 | -1.0201 | -0.7938 |
| 0.600 | -1.3772 | -1.4833 | -1.4184 | -1.2155 | -0.8254 |
| 0.625 | ******* | ******* | -1.6519 | -1.4214 | -0.7885 |
| 0.650 | -2.1171 | -2.0202 | -1.8880 | -1.5143 | -0.6597 |
| 0.675 | ******* | -2.2132 | -1.9267 | -1.4249 | -0.4951 |
| 0.700 | -2.4312 | -2.0354 | -1.6347 | -1.1839 | -0.4265 |
| 0.725 | ******* | -1.7393 | ******* | -0.9363 | -0.4375 |
| 0.750 | -2.3521 | -1.5830 | ******* | -0.8579 | -0.4429 |
| 0.775 | ******* | -1.5494 | -1.2086 | -0.8423 | -0.4204 |
| 0.800 | -1.9577 | -1.5392 | -1.1963 | -0.8171 | ******* |
| 0.825 | ******* | -1.5511 | -1.2018 | -0.8251 | -0.3751 |
| 0.850 | -1.7163 | -1.5636 | -1.2205 | -0.8387 | -0.3579 |
| 0.875 | ******* | -1.5267 | -1.2161 | -0.8377 | -0.3299 |
| 0.900 | -1.6485 | -1.4681 | -1.1600 | -0.7939 | ******* |
| 0.925 | ******* | -1.4527 | -1.1016 | -0.7503 | -0.3299 |
| 0.950 | -1.5759 | -1.4430 | -1.0925 | -0.7315 | -0.2806 |
| 0.975 | ******* | -1.4355 | -1.0761 | -0.7177 | -0.2627 |
| 1.000 | -1.5218 | -1.3934 | -1.0628 | -0.7013 | -0.2475 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4638 | 0.4171 | 0.3907 | ******* | -0.3116 |
| -0.400 | 0.4792 | 0.4224 | 0.3731 | 0.1826 | -0.4147 |
| -0.600 | 0.4848 | 0.4327 | 0.3787 | 0.2143 | -0.4967 |
| -0.700 | ******* | 0.4396 | 0.3731 | 0.2297 | -0.5232 |
| -0.800 | ******* | ******* | 0.3804 | 0.2487 | -0.4517 |
| -0.850 | ******* | 0.3975 | 0.3727 | 0.2753 | -0.4041 |
| -0.900 | 0.3800 | 0.3301 | 0.3328 | 0.2813 | -0.3618 |
| -0.950 | 0.2892 | 0.0722 | 0.1982 | 0.2302 | -0.0595 |
| -0.975 | ******* | -0.1288 | -0.0050 | 0.0869 | 0.0281 |
| -1.000 | -1.5442 | -1.3843 | -1.0533 | -0.6819 | -0.2352 |

Surface Pressures




Small Radius L.E.

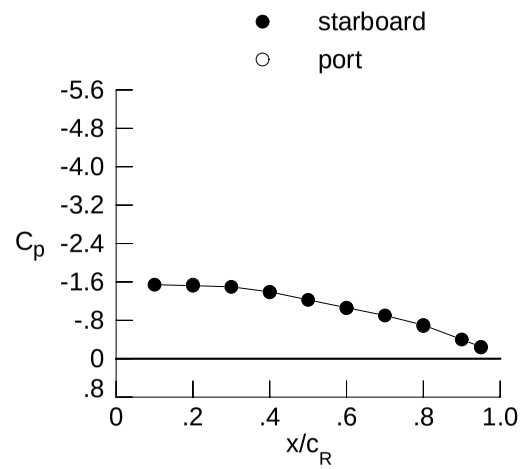
Run No. = 38 , Point No. = 771

$C_N$ = 0.961, $C_m$ = -0.1361

$\alpha$ = 20.5 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

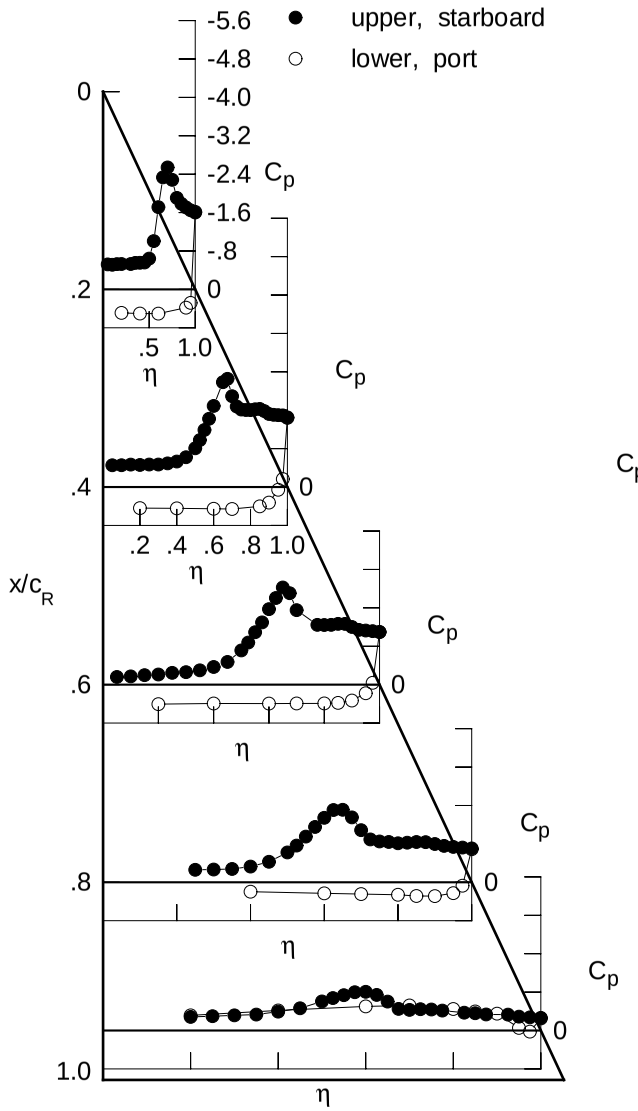



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.5421 | ******* |
| 0.20 | -1.5218 | -1.5442 |
| 0.30 | -1.4977 | ******* |
| 0.40 | -1.3934 | -1.3843 |
| 0.50 | -1.2263 | ******* |
| 0.60 | -1.0628 | -1.0533 |
| 0.70 | -0.9011 | ******* |
| 0.80 | -0.7013 | -0.6819 |
| 0.90 | -0.4008 | ******* |
| 0.95 | -0.2475 | -0.2352 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5205 | -0.4536 | -0.1599 | ******* | ******* |
| 0.100 | -0.5130 | -0.4547 | -0.1718 | ******* | ******* |
| 0.150 | -0.5266 | -0.4676 | -0.1977 | ******* | ******* |
| 0.200 | -0.5290 | -0.4601 | -0.2108 | ******* | -0.2832 |
| 0.250 | ******* | -0.4690 | -0.2455 | -0.2604 | -0.2981 |
| 0.300 | -0.5291 | -0.4684 | -0.2603 | -0.2658 | -0.3163 |
| 0.350 | -0.5523 | -0.4925 | -0.2986 | -0.2777 | -0.3323 |
| 0.400 | -0.5541 | -0.5309 | -0.3676 | -0.3270 | -0.3929 |
| 0.450 | -0.5600 | -0.6210 | -0.4729 | -0.4270 | -0.4629 |
| 0.500 | -0.6414 | -0.8069 | -0.7129 | -0.6212 | -0.6059 |
| 0.525 | ******* | -0.9785 | -0.8765 | -0.7647 | -0.6760 |
| 0.550 | -1.0064 | -1.1891 | -1.0923 | -0.9519 | -0.7361 |
| 0.575 | ******* | -1.4215 | -1.2965 | -1.1526 | -0.7979 |
| 0.600 | -1.7135 | -1.6899 | -1.5728 | -1.3430 | -0.8061 |
| 0.625 | ******* | ******* | -1.8045 | -1.5056 | -0.7415 |
| 0.650 | -2.3335 | -2.1844 | -2.0239 | -1.5102 | -0.6021 |
| 0.675 | ******* | -2.2543 | -1.9050 | -1.3516 | -0.4507 |
| 0.700 | -2.5406 | -1.8918 | -1.5522 | -1.0857 | -0.4299 |
| 0.725 | ******* | -1.6780 | ******* | -0.8931 | -0.4437 |
| 0.750 | -2.2824 | -1.6146 | ******* | -0.8502 | -0.4377 |
| 0.775 | ******* | -1.6047 | -1.2455 | -0.8399 | -0.4156 |
| 0.800 | -1.9061 | -1.6026 | -1.2420 | -0.8126 | ******* |
| 0.825 | ******* | -1.6202 | -1.2455 | -0.8244 | -0.3710 |
| 0.850 | -1.7833 | -1.6271 | -1.2668 | -0.8389 | -0.3598 |
| 0.875 | ******* | -1.5826 | -1.2654 | -0.8361 | -0.3343 |
| 0.900 | -1.7078 | -1.5228 | -1.2019 | -0.7978 | ******* |
| 0.925 | ******* | -1.5051 | -1.1404 | -0.7581 | -0.3313 |
| 0.950 | -1.6477 | -1.4976 | -1.1274 | -0.7370 | -0.2885 |
| 0.975 | ******* | -1.4932 | -1.1147 | -0.7232 | -0.2748 |
| 1.000 | -1.6018 | -1.4509 | -1.0976 | -0.7058 | -0.2641 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4898 | 0.4391 | 0.4061 | ******* | -0.3156 |
| -0.400 | 0.5031 | 0.4438 | 0.3925 | 0.1963 | -0.4177 |
| -0.600 | 0.5051 | 0.4527 | 0.3947 | 0.2301 | -0.5021 |
| -0.700 | ******* | 0.4578 | 0.3921 | 0.2453 | -0.5217 |
| -0.800 | ******* | ******* | 0.3913 | 0.2602 | -0.4476 |
| -0.850 | ******* | 0.4024 | 0.3801 | 0.2854 | -0.3968 |
| -0.900 | 0.3809 | 0.3243 | 0.3308 | 0.2879 | -0.3510 |
| -0.950 | 0.2806 | 0.0571 | 0.1796 | 0.2267 | -0.0547 |
| -0.975 | ******* | -0.1664 | -0.0383 | 0.0712 | 0.0228 |
| -1.000 | -1.6161 | -1.4412 | -1.0940 | -0.6888 | -0.2510 |

Surface Pressures




Small Radius L.E.

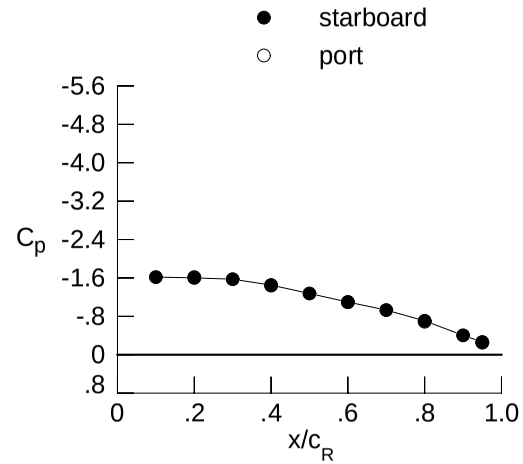
Run No. = 38 , Point No. = 772

$C_N$ = 1.019, $C_m$ = -0.1452

$\alpha$ = 21.6 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

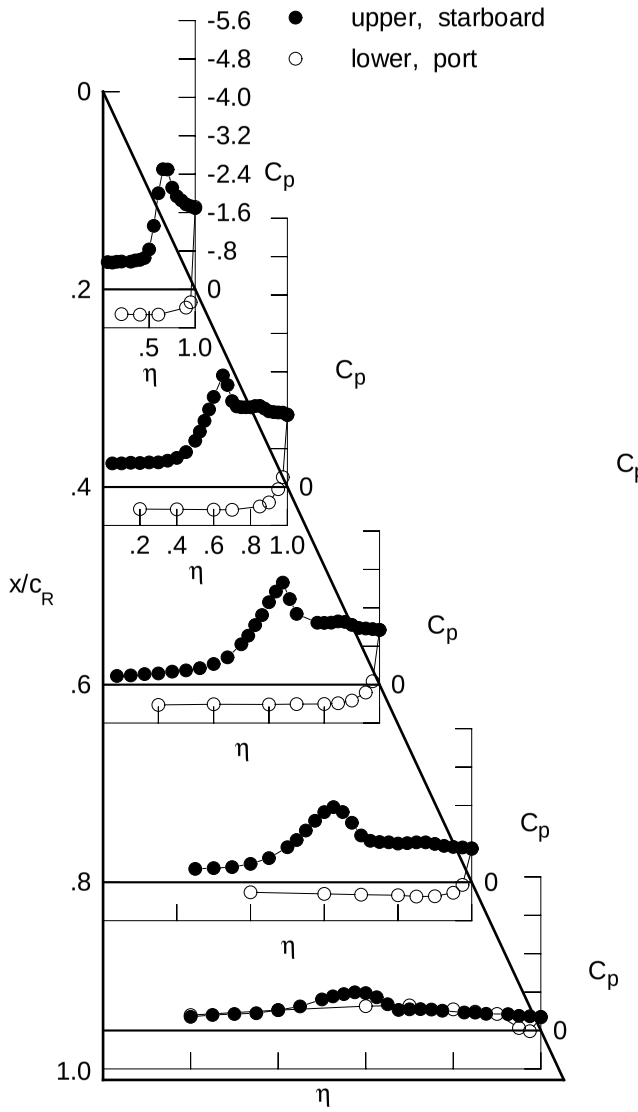



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.6171 | ******* |
| 0.20 | -1.6018 | -1.6161 |
| 0.30 | -1.5734 | ******* |
| 0.40 | -1.4509 | -1.4412 |
| 0.50 | -1.2759 | ******* |
| 0.60 | -1.0976 | -1.0940 |
| 0.70 | -0.9305 | ******* |
| 0.80 | -0.7058 | -0.6888 |
| 0.90 | -0.4041 | ******* |
| 0.95 | -0.2641 | -0.2510 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5680 | -0.4917 | -0.1807 | ******* | ******* |
| 0.100 | -0.5585 | -0.4928 | -0.1918 | ******* | ******* |
| 0.150 | -0.5757 | -0.5059 | -0.2197 | ******* | ******* |
| 0.200 | -0.5800 | -0.5005 | -0.2335 | ******* | -0.2852 |
| 0.250 | ******* | -0.5127 | -0.2712 | -0.2795 | -0.3236 |
| 0.300 | -0.5776 | -0.5140 | -0.2964 | -0.2952 | -0.3438 |
| 0.350 | -0.6028 | -0.5491 | -0.3431 | -0.3161 | -0.3601 |
| 0.400 | -0.6161 | -0.6069 | -0.4307 | -0.3836 | -0.4257 |
| 0.450 | -0.6553 | -0.7282 | -0.5684 | -0.5030 | -0.5015 |
| 0.500 | -0.8327 | -0.9642 | -0.8410 | -0.7300 | -0.6470 |
| 0.525 | ******* | -1.1546 | -1.0196 | -0.8804 | -0.7112 |
| 0.550 | -1.3233 | -1.3788 | -1.2409 | -1.0786 | -0.7584 |
| 0.575 | ******* | -1.6157 | -1.4497 | -1.2815 | -0.7961 |
| 0.600 | -2.0033 | -1.8775 | -1.7170 | -1.4618 | -0.7795 |
| 0.625 | ******* | ******* | -1.9395 | -1.5666 | -0.6930 |
| 0.650 | -2.5029 | -2.3254 | -2.1255 | -1.4634 | -0.5474 |
| 0.675 | ******* | -2.1257 | -1.7829 | -1.2400 | -0.4285 |
| 0.700 | -2.4975 | -1.7900 | -1.4741 | -0.9755 | -0.4416 |
| 0.725 | ******* | -1.6799 | ******* | -0.8648 | -0.4455 |
| 0.750 | -2.1190 | -1.6627 | ******* | -0.8391 | -0.4372 |
| 0.775 | ******* | -1.6626 | -1.2892 | -0.8328 | -0.4131 |
| 0.800 | -1.9399 | -1.6611 | -1.2861 | -0.8067 | ******* |
| 0.825 | ******* | -1.6870 | -1.2915 | -0.8150 | -0.3754 |
| 0.850 | -1.8546 | -1.6900 | -1.3174 | -0.8317 | -0.3728 |
| 0.875 | ******* | -1.6372 | -1.3071 | -0.8319 | -0.3479 |
| 0.900 | -1.7721 | -1.5767 | -1.2451 | -0.7990 | ******* |
| 0.925 | ******* | -1.5616 | -1.1804 | -0.7585 | -0.3410 |
| 0.950 | -1.7328 | -1.5535 | -1.1697 | -0.7372 | -0.3059 |
| 0.975 | ******* | -1.5499 | -1.1576 | -0.7256 | -0.2965 |
| 1.000 | -1.6938 | -1.5115 | -1.1400 | -0.7090 | -0.2856 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5162 | 0.4595 | 0.4225 | ******* | -0.3220 |
| -0.400 | 0.5265 | 0.4645 | 0.4091 | 0.2090 | -0.4242 |
| -0.600 | 0.5254 | 0.4713 | 0.4126 | 0.2417 | -0.5075 |
| -0.700 | ******* | 0.4744 | 0.4056 | 0.2585 | -0.5220 |
| -0.800 | ******* | ******* | 0.4029 | 0.2699 | -0.4411 |
| -0.850 | ******* | 0.4055 | 0.3871 | 0.2964 | -0.3917 |
| -0.900 | 0.3800 | 0.3212 | 0.3314 | 0.2912 | -0.3446 |
| -0.950 | 0.2683 | 0.0448 | 0.1639 | 0.2188 | -0.0523 |
| -0.975 | ******* | -0.2054 | -0.0713 | 0.0547 | 0.0144 |
| -1.000 | -1.7174 | -1.4975 | -1.1381 | -0.6948 | -0.2740 |

Surface Pressures




Small Radius L.E.

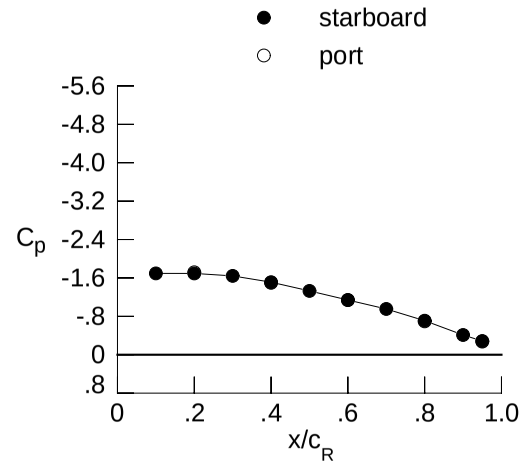
Run No. = 38 , Point No. = 773

$C_N$ = 1.072, $C_m$ = -0.1511

$\alpha$ = 22.6 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

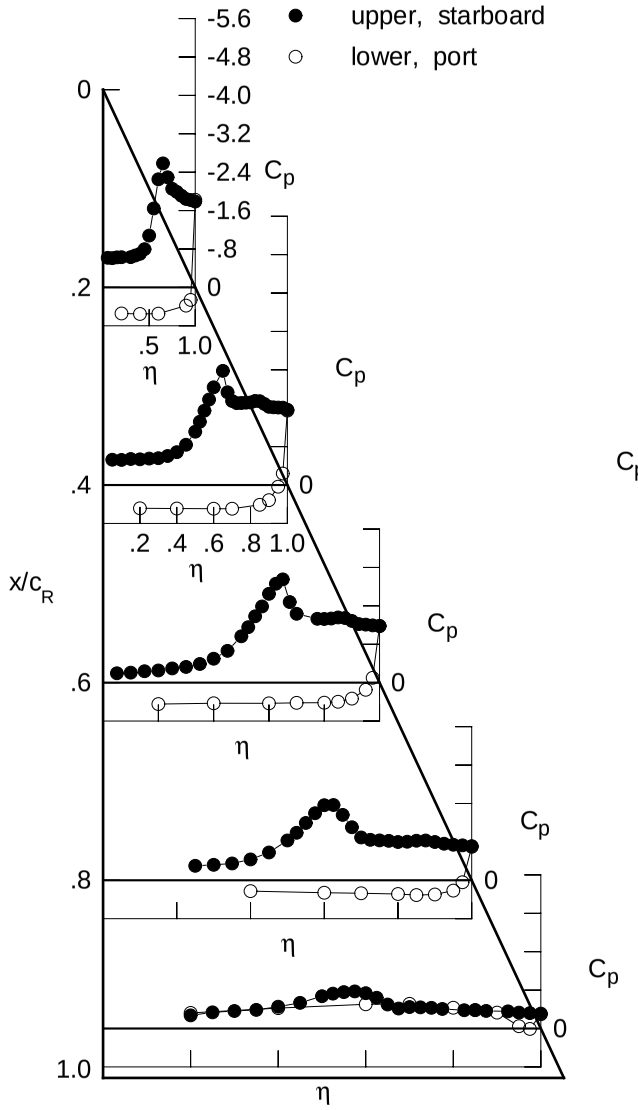



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.6946 | ******* |
| 0.20 | -1.6938 | -1.7174 |
| 0.30 | -1.6422 | ******* |
| 0.40 | -1.5115 | -1.4975 |
| 0.50 | -1.3297 | ******* |
| 0.60 | -1.1400 | -1.1381 |
| 0.70 | -0.9532 | ******* |
| 0.80 | -0.7090 | -0.6948 |
| 0.90 | -0.4114 | ******* |
| 0.95 | -0.2856 | -0.2740 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6167 | -0.5273 | -0.1950 | ******* | ******* |
| 0.100 | -0.6086 | -0.5236 | -0.2082 | ******* | ******* |
| 0.150 | -0.6254 | -0.5426 | -0.2377 | ******* | ******* |
| 0.200 | -0.6286 | -0.5364 | -0.2536 | ******* | -0.2734 |
| 0.250 | ******* | -0.5512 | -0.2956 | -0.3016 | -0.3368 |
| 0.300 | -0.6303 | -0.5592 | -0.3275 | -0.3223 | -0.3651 |
| 0.350 | -0.6644 | -0.6045 | -0.3887 | -0.3501 | -0.3879 |
| 0.400 | -0.6992 | -0.6847 | -0.4984 | -0.4342 | -0.4548 |
| 0.450 | -0.7959 | -0.8392 | -0.6621 | -0.5793 | -0.5347 |
| 0.500 | -1.0792 | -1.1112 | -0.9659 | -0.8297 | -0.6731 |
| 0.525 | ******* | -1.3185 | -1.1553 | -0.9895 | -0.7265 |
| 0.550 | -1.6438 | -1.5488 | -1.3824 | -1.1941 | -0.7587 |
| 0.575 | ******* | -1.7806 | -1.5872 | -1.3965 | -0.7729 |
| 0.600 | -2.2524 | -2.0362 | -1.8501 | -1.5637 | -0.7362 |
| 0.625 | ******* | ******* | -2.0606 | -1.5678 | -0.6410 |
| 0.650 | -2.5832 | -2.3782 | -2.1515 | -1.3627 | -0.4996 |
| 0.675 | ******* | -1.9326 | -1.6793 | -1.1044 | -0.4164 |
| 0.700 | -2.2934 | -1.7515 | -1.4341 | -0.8922 | -0.4472 |
| 0.725 | ******* | -1.7066 | ******* | -0.8429 | -0.4410 |
| 0.750 | -2.0536 | -1.7089 | ******* | -0.8314 | -0.4313 |
| 0.775 | ******* | -1.7160 | -1.3304 | -0.8215 | -0.4076 |
| 0.800 | -1.9899 | -1.7201 | -1.3266 | -0.7974 | ******* |
| 0.825 | ******* | -1.7518 | -1.3352 | -0.8033 | -0.3804 |
| 0.850 | -1.9101 | -1.7466 | -1.3588 | -0.8242 | -0.3851 |
| 0.875 | ******* | -1.6892 | -1.3466 | -0.8287 | -0.3667 |
| 0.900 | -1.8427 | -1.6296 | -1.2853 | -0.7972 | ******* |
| 0.925 | ******* | -1.6191 | -1.2200 | -0.7612 | -0.3577 |
| 0.950 | -1.8202 | -1.6144 | -1.2085 | -0.7405 | -0.3310 |
| 0.975 | ******* | -1.6116 | -1.1925 | -0.7279 | -0.3206 |
| 1.000 | -1.7880 | -1.5685 | -1.1759 | -0.7114 | -0.3104 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5433 | 0.4846 | 0.4464 | ******* | -0.3247 |
| -0.400 | 0.5534 | 0.4894 | 0.4293 | 0.2259 | -0.4249 |
| -0.600 | 0.5476 | 0.4934 | 0.4308 | 0.2596 | -0.5047 |
| -0.700 | ******* | 0.4939 | 0.4207 | 0.2702 | -0.5146 |
| -0.800 | ******* | ******* | 0.4176 | 0.2859 | -0.4324 |
| -0.850 | ******* | 0.4116 | 0.3982 | 0.3084 | -0.3817 |
| -0.900 | 0.3798 | 0.3151 | 0.3327 | 0.2960 | -0.3313 |
| -0.950 | 0.2607 | 0.0341 | 0.1487 | 0.2156 | -0.0481 |
| -0.975 | ******* | -0.2404 | -0.1002 | 0.0408 | 0.0088 |
| -1.000 | -1.8250 | -1.5508 | -1.1838 | -0.6968 | -0.2970 |

Surface Pressures




Small Radius L.E.

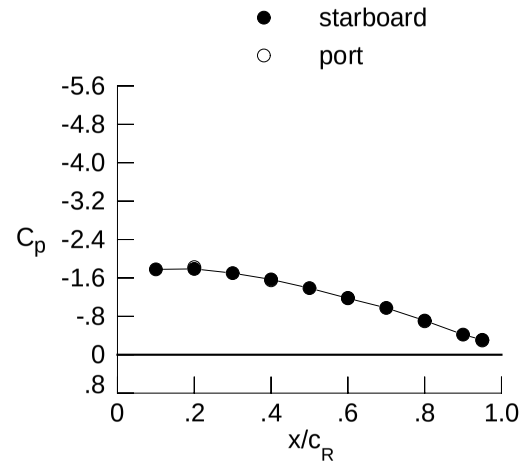
Run No. = 38 , Point No. = 774

$C_N$ = 1.125, $C_m$ = -0.1560

$\alpha$ = 23.6 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

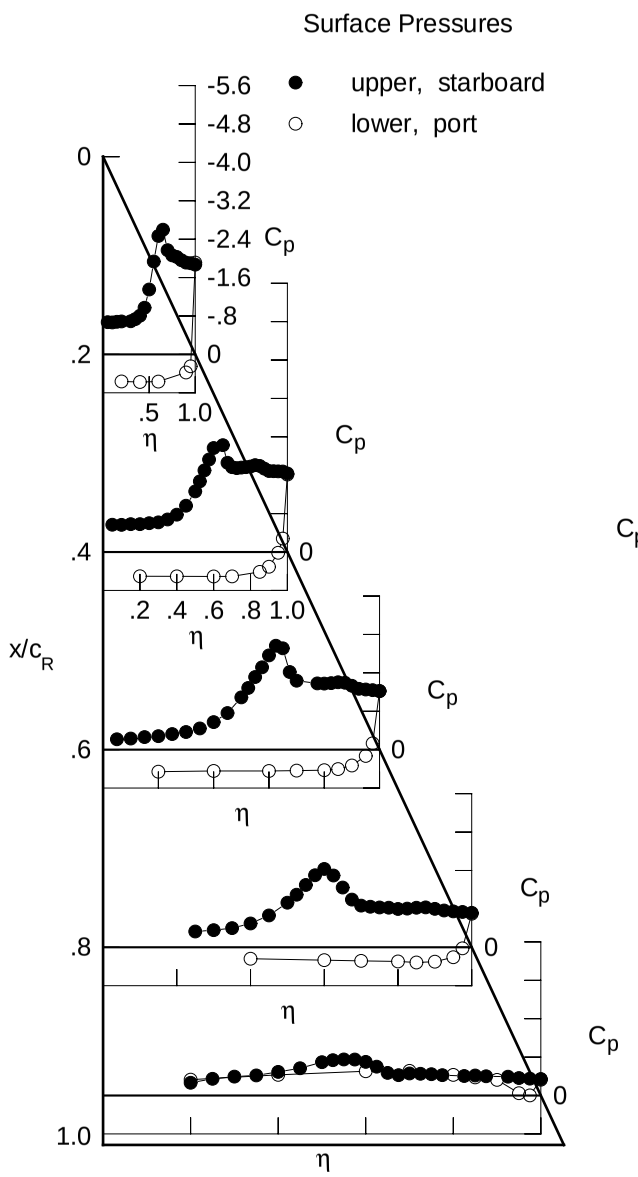
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.7781 | ******* |
| 0.20 | -1.7880 | -1.8250 |
| 0.30 | -1.7001 | ******* |
| 0.40 | -1.5685 | -1.5508 |
| 0.50 | -1.3877 | ******* |
| 0.60 | -1.1759 | -1.1838 |
| 0.70 | -0.9750 | ******* |
| 0.80 | -0.7114 | -0.6968 |
| 0.90 | -0.4196 | ******* |
| 0.95 | -0.3104 | -0.2970 |

# Table D2. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6712 | -0.5692 | -0.2158 | ******* | ******* |
| 0.100 | -0.6655 | -0.5662 | -0.2313 | ******* | ******* |
| 0.150 | -0.6790 | -0.5810 | -0.2613 | ******* | ******* |
| 0.200 | -0.6863 | -0.5805 | -0.2809 | ******* | -0.2657 |
| 0.250 | ******* | -0.6007 | -0.3252 | -0.3287 | -0.3479 |
| 0.300 | -0.6906 | -0.6186 | -0.3673 | -0.3565 | -0.3938 |
| 0.350 | -0.7354 | -0.6784 | -0.4418 | -0.3989 | -0.4186 |
| 0.400 | -0.8059 | -0.7786 | -0.5737 | -0.4958 | -0.4919 |
| 0.450 | -0.9723 | -0.9648 | -0.7623 | -0.6628 | -0.5680 |
| 0.500 | -1.3518 | -1.2629 | -1.0891 | -0.9286 | -0.6946 |
| 0.525 | ******* | -1.4726 | -1.2852 | -1.0954 | -0.7361 |
| 0.550 | -1.9352 | -1.7010 | -1.5130 | -1.2988 | -0.7509 |
| 0.575 | ******* | -1.9271 | -1.7148 | -1.5005 | -0.7496 |
| 0.600 | -2.4673 | -2.1670 | -1.9630 | -1.6317 | -0.7008 |
| 0.625 | ******* | ******* | -2.1648 | -1.4950 | -0.6005 |
| 0.650 | -2.5974 | -2.2267 | -2.1109 | -1.2451 | -0.4713 |
| 0.675 | ******* | -1.8597 | -1.6173 | -0.9939 | -0.4240 |
| 0.700 | -2.1713 | -1.7679 | -1.4364 | -0.8678 | -0.4594 |
| 0.725 | ******* | -1.7476 | ******* | -0.8452 | -0.4526 |
| 0.750 | -2.0636 | -1.7591 | ******* | -0.8296 | -0.4440 |
| 0.775 | ******* | -1.7681 | -1.3797 | -0.8244 | -0.4243 |
| 0.800 | -2.0296 | -1.7809 | -1.3756 | -0.7985 | ******* |
| 0.825 | ******* | -1.8105 | -1.3853 | -0.8056 | -0.4065 |
| 0.850 | -1.9618 | -1.7939 | -1.4037 | -0.8238 | -0.4165 |
| 0.875 | ******* | -1.7378 | -1.3936 | -0.8314 | -0.4009 |
| 0.900 | -1.9122 | -1.6882 | -1.3303 | -0.8008 | ******* |
| 0.925 | ******* | -1.6837 | -1.2672 | -0.7668 | -0.3919 |
| 0.950 | -1.8990 | -1.6811 | -1.2531 | -0.7480 | -0.3643 |
| 0.975 | ******* | -1.6773 | -1.2390 | -0.7356 | -0.3514 |
| 1.000 | -1.8693 | -1.6369 | -1.2178 | -0.7185 | -0.3437 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5641 | 0.5046 | 0.4592 | ******* | -0.3304 |
| -0.400 | 0.5751 | 0.5062 | 0.4444 | 0.2384 | -0.4304 |
| -0.600 | 0.5663 | 0.5089 | 0.4445 | 0.2682 | -0.5057 |
| -0.700 | ******* | 0.5071 | 0.4369 | 0.2833 | -0.5132 |
| -0.800 | ******* | ******* | 0.4281 | 0.2949 | -0.4298 |
| -0.850 | ******* | 0.4134 | 0.4047 | 0.3167 | -0.3773 |
| -0.900 | 0.3769 | 0.3066 | 0.3307 | 0.3004 | -0.3256 |
| -0.950 | 0.2481 | 0.0151 | 0.1311 | 0.2076 | -0.0484 |
| -0.975 | ******* | -0.2812 | -0.1312 | 0.0218 | -0.0027 |
| -1.000 | -1.9129 | -1.6148 | -1.2223 | -0.6994 | -0.3289 |



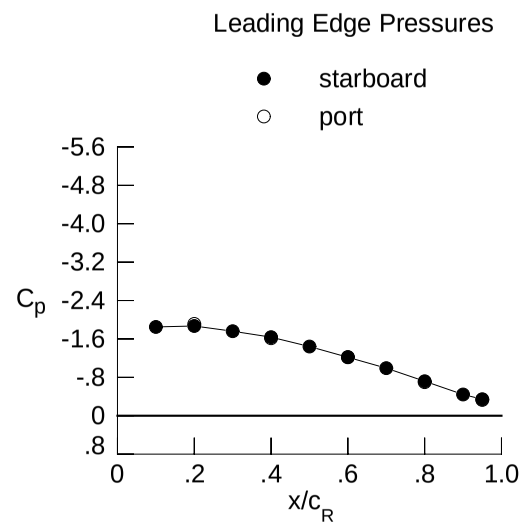

Small Radius L.E.

Run No. = 38 , Point No. = 775

$C_N$ = 1.177, $C_m$ = -0.1624

$\alpha$ = 24.6 °, $M_\infty$ = 0.600

$R_{mac}$ = $6.0 \times 10^6$

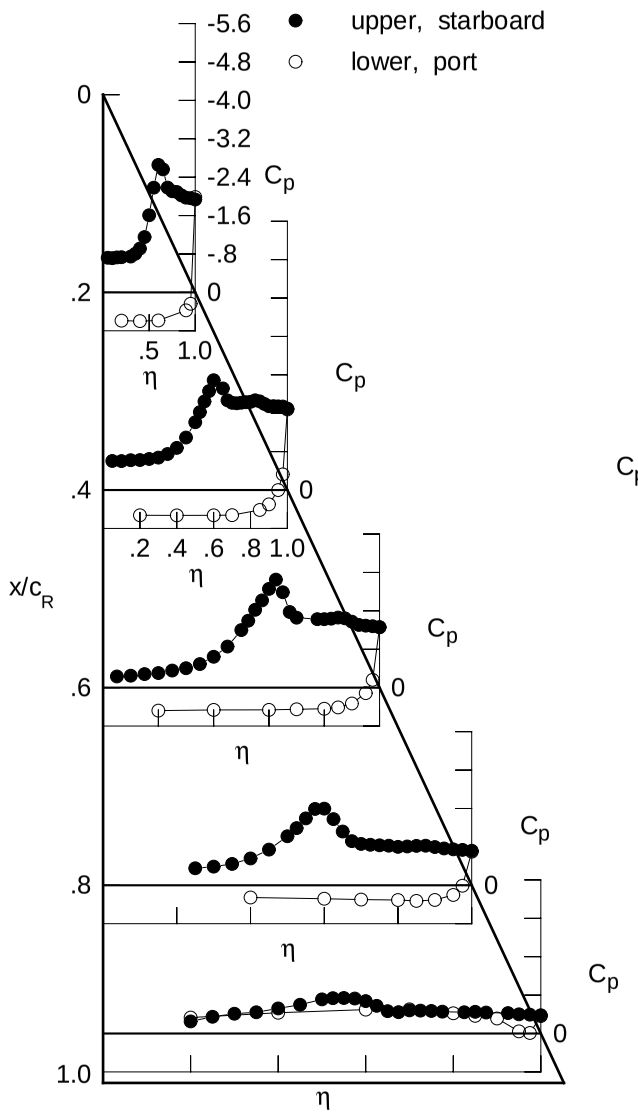



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.8500 | ******* |
| 0.20 | -1.8693 | -1.9129 |
| 0.30 | -1.7607 | ******* |
| 0.40 | -1.6369 | -1.6148 |
| 0.50 | -1.4417 | ******* |
| 0.60 | -1.2178 | -1.2223 |
| 0.70 | -0.9910 | ******* |
| 0.80 | -0.7185 | -0.6994 |
| 0.90 | -0.4424 | ******* |
| 0.95 | -0.3437 | -0.3289 |

# Table D2. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.7219 | -0.6053 | -0.2327 | ******* | ******* |
| 0.100 | -0.7130 | -0.6030 | -0.2490 | ******* | ******* |
| 0.150 | -0.7285 | -0.6214 | -0.2820 | ******* | ******* |
| 0.200 | -0.7330 | -0.6251 | -0.3042 | ******* | -0.2518 |
| 0.250 | ******* | -0.6473 | -0.3558 | -0.3544 | -0.3491 |
| 0.300 | -0.7462 | -0.6754 | -0.4051 | -0.3891 | -0.4123 |
| 0.350 | -0.8058 | -0.7506 | -0.4914 | -0.4446 | -0.4421 |
| 0.400 | -0.9137 | -0.8783 | -0.6430 | -0.5589 | -0.5224 |
| 0.450 | -1.1532 | -1.0936 | -0.8563 | -0.7429 | -0.5992 |
| 0.500 | -1.6075 | -1.4123 | -1.1994 | -1.0213 | -0.7112 |
| 0.525 | ******* | -1.6233 | -1.3943 | -1.1908 | -0.7359 |
| 0.550 | -2.1820 | -1.8459 | -1.6214 | -1.3934 | -0.7401 |
| 0.575 | ******* | -2.0612 | -1.8179 | -1.5902 | -0.7289 |
| 0.600 | -2.6562 | -2.2878 | -2.0567 | -1.5969 | -0.6756 |
| 0.625 | ******* | ******* | -2.2503 | -1.3786 | -0.5765 |
| 0.650 | -2.5627 | -2.1169 | -1.9872 | -1.1196 | -0.4655 |
| 0.675 | ******* | -1.8690 | -1.5762 | -0.9196 | -0.4451 |
| 0.700 | -2.1836 | -1.8179 | -1.4574 | -0.8613 | -0.4823 |
| 0.725 | ******* | -1.8072 | ******* | -0.8436 | -0.4767 |
| 0.750 | -2.1075 | -1.8194 | ******* | -0.8330 | -0.4699 |
| 0.775 | ******* | -1.8300 | -1.4266 | -0.8250 | -0.4548 |
| 0.800 | -2.0914 | -1.8379 | -1.4262 | -0.8011 | ******* |
| 0.825 | ******* | -1.8694 | -1.4368 | -0.8087 | -0.4426 |
| 0.850 | -2.0219 | -1.8469 | -1.4597 | -0.8209 | -0.4521 |
| 0.875 | ******* | -1.7940 | -1.4436 | -0.8251 | -0.4365 |
| 0.900 | -1.9740 | -1.7456 | -1.3748 | -0.7967 | ******* |
| 0.925 | ******* | -1.7471 | -1.3065 | -0.7675 | -0.4258 |
| 0.950 | -1.9621 | -1.7430 | -1.2912 | -0.7485 | -0.3998 |
| 0.975 | ******* | -1.7402 | -1.2789 | -0.7376 | -0.3930 |
| 1.000 | -1.9356 | -1.6968 | -1.2585 | -0.7197 | -0.3812 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5886 | 0.5258 | 0.4787 | ******* | -0.3323 |
| -0.400 | 0.5986 | 0.5284 | 0.4644 | 0.2547 | -0.4329 |
| -0.600 | 0.5850 | 0.5266 | 0.4629 | 0.2803 | -0.4977 |
| -0.700 | ******* | 0.5229 | 0.4509 | 0.2979 | -0.5039 |
| -0.800 | ******* | ******* | 0.4396 | 0.3070 | -0.4214 |
| -0.850 | ******* | 0.4154 | 0.4120 | 0.3259 | -0.3678 |
| -0.900 | 0.3744 | 0.2986 | 0.3304 | 0.3059 | -0.3131 |
| -0.950 | 0.2366 | 0.0004 | 0.1142 | 0.2015 | -0.0444 |
| -0.975 | ******* | -0.3268 | -0.1626 | 0.0089 | -0.0110 |
| -1.000 | -1.9864 | -1.6786 | -1.2592 | -0.6989 | -0.3630 |

Surface Pressures




Small Radius L.E.

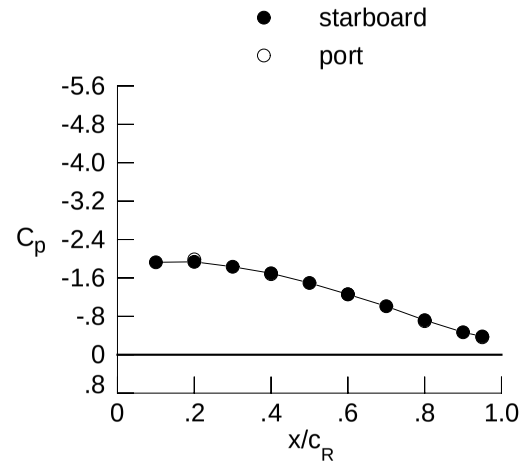
Run No. = 38 , Point No. = 776

$C_N$ = 1.234, $C_m$ = -0.1720

$\alpha$ = 25.6 °, $M_\infty$ = 0.599

$R_{mac}$ = $6.0 \times 10^6$

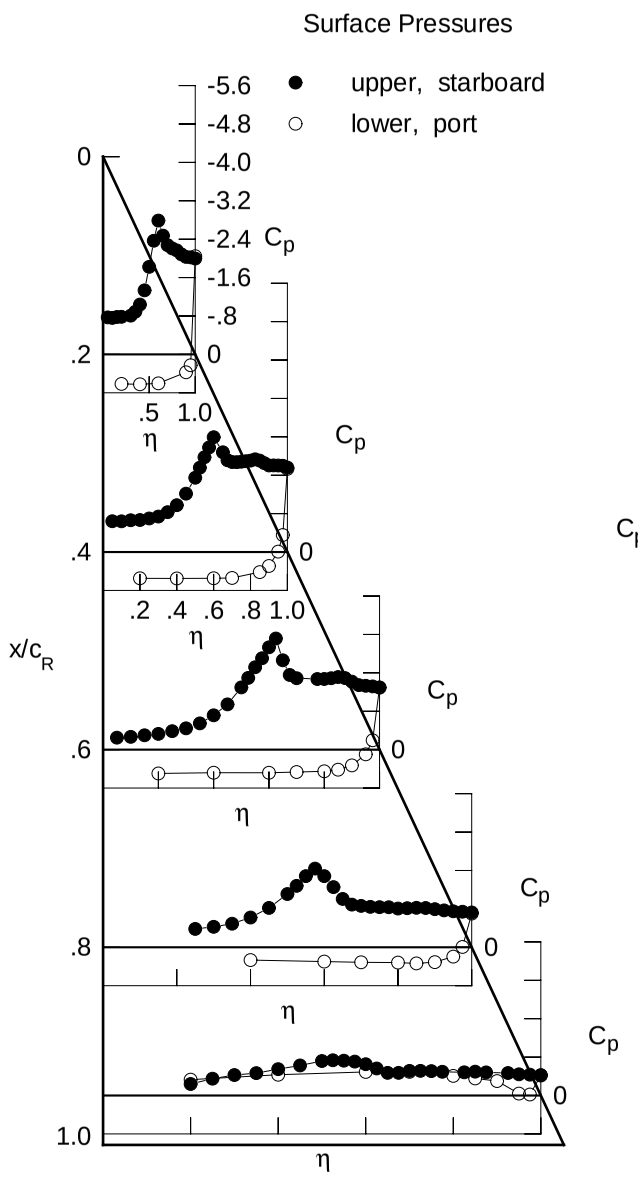
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.9255 | ******* |
| 0.20 | -1.9356 | -1.9864 |
| 0.30 | -1.8329 | ******* |
| 0.40 | -1.6968 | -1.6786 |
| 0.50 | -1.4953 | ******* |
| 0.60 | -1.2585 | -1.2592 |
| 0.70 | -1.0101 | ******* |
| 0.80 | -0.7197 | -0.6989 |
| 0.90 | -0.4684 | ******* |
| 0.95 | -0.3812 | -0.3630 |

# Table D2. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.7716 | -0.6416 | -0.2493 | ******* | ******* |
| 0.100 | -0.7599 | -0.6398 | -0.2665 | ******* | ******* |
| 0.150 | -0.7792 | -0.6626 | -0.2993 | ******* | ******* |
| 0.200 | -0.7831 | -0.6668 | -0.3281 | ******* | -0.2400 |
| 0.250 | ******* | -0.6989 | -0.3847 | -0.3824 | -0.3506 |
| 0.300 | -0.8071 | -0.7389 | -0.4443 | -0.4260 | -0.4267 |
| 0.350 | -0.8890 | -0.8306 | -0.5469 | -0.4915 | -0.4661 |
| 0.400 | -1.0382 | -0.9763 | -0.7155 | -0.6201 | -0.5490 |
| 0.450 | -1.3348 | -1.2160 | -0.9435 | -0.8198 | -0.6261 |
| 0.500 | -1.8232 | -1.5483 | -1.2970 | -1.1097 | -0.7185 |
| 0.525 | ******* | -1.7576 | -1.4943 | -1.2798 | -0.7347 |
| 0.550 | -2.3674 | -1.9747 | -1.7165 | -1.4828 | -0.7253 |
| 0.575 | ******* | -2.1782 | -1.9043 | -1.6391 | -0.7065 |
| 0.600 | -2.7878 | -2.3921 | -2.1319 | -1.4828 | -0.6520 |
| 0.625 | ******* | ******* | -2.3156 | -1.2534 | -0.5628 |
| 0.650 | -2.4746 | -2.0780 | -1.8618 | -1.0074 | -0.4716 |
| 0.675 | ******* | -1.9118 | -1.5558 | -0.8889 | -0.4719 |
| 0.700 | -2.2754 | -1.8749 | -1.4884 | -0.8620 | -0.5125 |
| 0.725 | ******* | -1.8716 | ******* | -0.8423 | -0.5137 |
| 0.750 | -2.2076 | -1.8815 | ******* | -0.8357 | -0.5081 |
| 0.775 | ******* | -1.8920 | -1.4714 | -0.8347 | -0.4941 |
| 0.800 | -2.1660 | -1.9036 | -1.4718 | -0.8075 | ******* |
| 0.825 | ******* | -1.9320 | -1.4882 | -0.8147 | -0.4835 |
| 0.850 | -2.0841 | -1.9047 | -1.5127 | -0.8222 | -0.4965 |
| 0.875 | ******* | -1.8521 | -1.4908 | -0.8183 | -0.4812 |
| 0.900 | -2.0311 | -1.8032 | -1.4169 | -0.7941 | ******* |
| 0.925 | ******* | -1.8047 | -1.3440 | -0.7689 | -0.4685 |
| 0.950 | -2.0213 | -1.8024 | -1.3302 | -0.7498 | -0.4420 |
| 0.975 | ******* | -1.7975 | -1.3174 | -0.7405 | -0.4340 |
| 1.000 | -1.9965 | -1.7601 | -1.2956 | -0.7259 | -0.4256 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.6154 | 0.5476 | 0.4962 | ******* | -0.3303 |
| -0.400 | 0.6231 | 0.5504 | 0.4807 | 0.2665 | -0.4330 |
| -0.600 | 0.6035 | 0.5466 | 0.4816 | 0.2976 | -0.4910 |
| -0.700 | ******* | 0.5403 | 0.4668 | 0.3130 | -0.4926 |
| -0.800 | ******* | ******* | 0.4510 | 0.3187 | -0.4090 |
| -0.850 | ******* | 0.4182 | 0.4178 | 0.3361 | -0.3561 |
| -0.900 | 0.3727 | 0.2906 | 0.3281 | 0.3096 | -0.3009 |
| -0.950 | 0.2263 | -0.0086 | 0.0976 | 0.1942 | -0.0398 |
| -0.975 | ******* | -0.3546 | -0.1953 | -0.0068 | -0.0207 |
| -1.000 | -2.0460 | -1.7326 | -1.2924 | -0.7021 | -0.4163 |



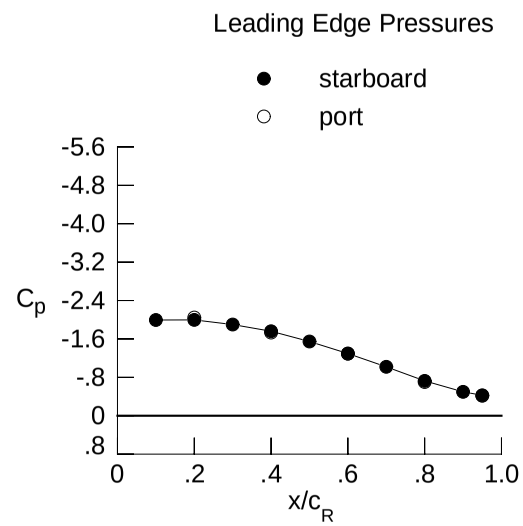

Small Radius L.E.

Run No. = 38 , Point No. = 777

$C_N$ = 1.284, $C_m$ = -0.1776

$\alpha$ = 26.7 °, $M_\infty$ = 0.600

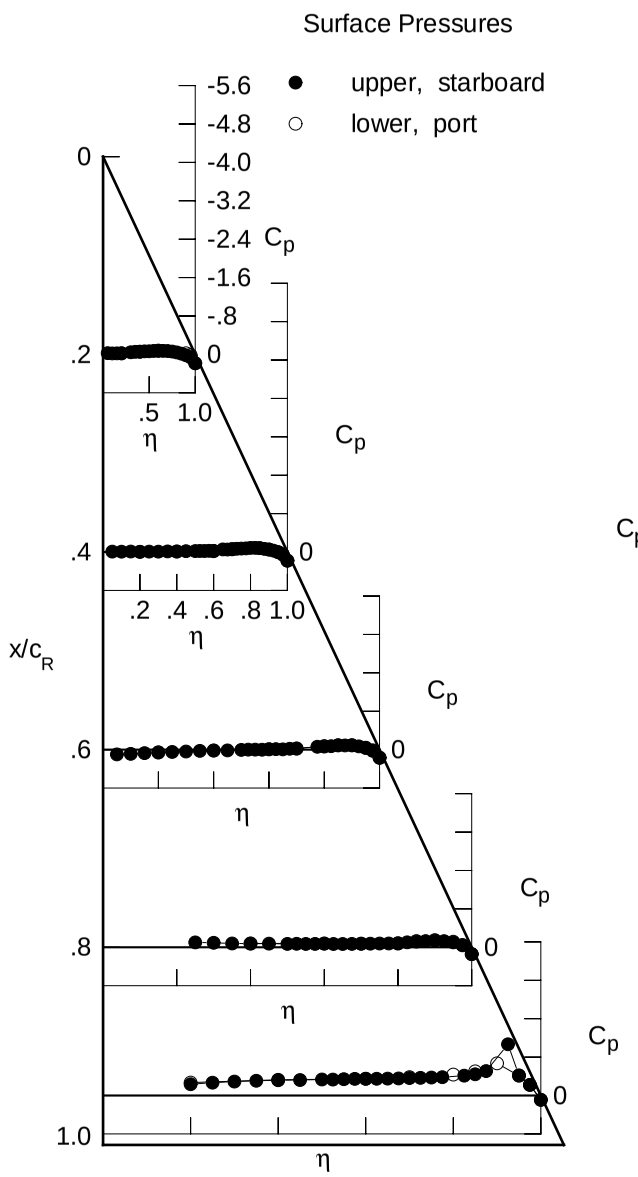
$R_{mac}$ = $6.0 \times 10^6$




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.9940 | ******* |
| 0.20 | -1.9965 | -2.0460 |
| 0.30 | -1.8998 | ******* |
| 0.40 | -1.7601 | -1.7326 |
| 0.50 | -1.5464 | ******* |
| 0.60 | -1.2956 | -1.2924 |
| 0.70 | -1.0188 | ******* |
| 0.80 | -0.7259 | -0.7021 |
| 0.90 | -0.4979 | ******* |
| 0.95 | -0.4256 | -0.4163 |

# Table D2. Concluded.

| η | x/c_R .2 Cp,u | x/c_R .4 Cp,u | x/c_R .6 Cp,u | x/c_R .8 Cp,u | x/c_R .95 Cp,u |
|---|---|---|---|---|---|
| 0.050 | -0.0254 | -0.0089 | 0.0996 | ******* | ******* |
| 0.100 | -0.0200 | -0.0070 | 0.0884 | ******* | ******* |
| 0.150 | -0.0218 | -0.0105 | 0.0727 | ******* | ******* |
| 0.200 | -0.0243 | -0.0052 | 0.0599 | ******* | -0.2356 |
| 0.250 | ******* | -0.0087 | 0.0480 | -0.1014 | -0.2670 |
| 0.300 | -0.0439 | -0.0079 | 0.0392 | -0.0938 | -0.2905 |
| 0.350 | -0.0539 | -0.0128 | 0.0257 | -0.0793 | -0.3068 |
| 0.400 | -0.0554 | -0.0120 | 0.0171 | -0.0763 | -0.3181 |
| 0.450 | -0.0633 | -0.0175 | 0.0164 | -0.0760 | -0.3226 |
| 0.500 | -0.0646 | -0.0197 | 0.0056 | -0.0707 | -0.3334 |
| 0.525 | ******* | -0.0220 | 0.0002 | -0.0724 | -0.3322 |
| 0.550 | -0.0717 | -0.0217 | -0.0001 | -0.0696 | -0.3402 |
| 0.575 | ******* | -0.0252 | 0.0018 | -0.0705 | -0.3461 |
| 0.600 | -0.0746 | -0.0247 | -0.0054 | -0.0744 | -0.3493 |
| 0.625 | ******* | ******* | -0.0102 | -0.0687 | -0.3487 |
| 0.650 | -0.0739 | -0.0545 | -0.0052 | -0.0689 | -0.3518 |
| 0.675 | ******* | -0.0523 | -0.0182 | -0.0706 | -0.3548 |
| 0.700 | -0.0704 | -0.0562 | -0.0250 | -0.0737 | -0.3641 |
| 0.725 | ******* | -0.0681 | ******* | -0.0751 | -0.3679 |
| 0.750 | -0.0590 | -0.0722 | ******* | -0.0787 | -0.3741 |
| 0.775 | ******* | -0.0764 | -0.0604 | -0.0794 | -0.3816 |
| 0.800 | -0.0408 | -0.0861 | -0.0638 | -0.0765 | ******* |
| 0.825 | ******* | -0.0871 | -0.0718 | -0.1035 | -0.4136 |
| 0.850 | -0.0152 | -0.0814 | -0.0883 | -0.1183 | -0.4421 |
| 0.875 | ******* | -0.0661 | -0.0873 | -0.1288 | -0.5089 |
| 0.900 | 0.0183 | -0.0510 | -0.0869 | -0.1376 | ******* |
| 0.925 | ******* | -0.0290 | -0.0682 | -0.1282 | -1.0669 |
| 0.950 | 0.0614 | 0.0012 | -0.0345 | -0.1025 | -0.4196 |
| 0.975 | ******* | 0.0461 | 0.0247 | -0.0404 | -0.2221 |
| 1.000 | 0.1842 | 0.1817 | 0.1722 | 0.1400 | 0.0899 |
| | Cp,l | Cp,l | Cp,l | Cp,l | Cp,l |
| -0.200 | -0.0200 | -0.0035 | 0.0556 | ******* | -0.2699 |
| -0.400 | -0.0558 | -0.0093 | 0.0200 | -0.0798 | -0.3273 |
| -0.600 | -0.0789 | -0.0168 | -0.0094 | -0.0802 | -0.3484 |
| -0.700 | ******* | -0.0632 | -0.0209 | -0.0760 | -0.3822 |
| -0.800 | ******* | ******* | -0.0747 | -0.0863 | -0.4357 |
| -0.850 | ******* | -0.0809 | -0.0930 | -0.1289 | -0.5034 |
| -0.900 | -0.0231 | -0.0535 | -0.0946 | -0.1485 | -0.6700 |
| -0.950 | 0.0131 | 0.0047 | -0.0405 | -0.1159 | -0.4118 |
| -0.975 | ******* | 0.0545 | 0.0128 | -0.0483 | -0.2201 |
| -1.000 | 0.1853 | 0.1761 | 0.1635 | 0.1447 | 0.0897 |



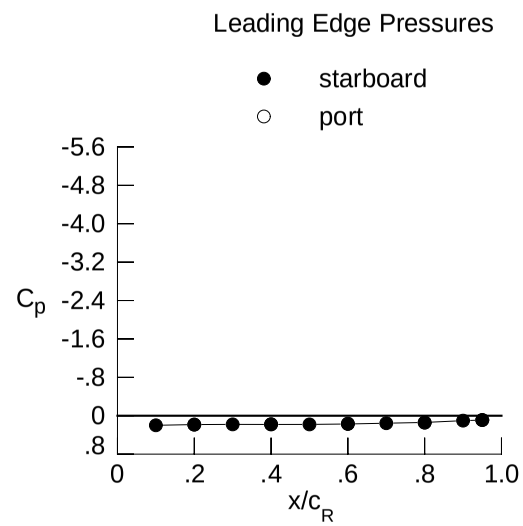

Small Radius L.E.

Run No. = 38 , Point No. = 778

$C_N$ = 0.001, $C_m$ = -0.0069

$\alpha$ = 0.1 °, $M_\infty$ = 0.600

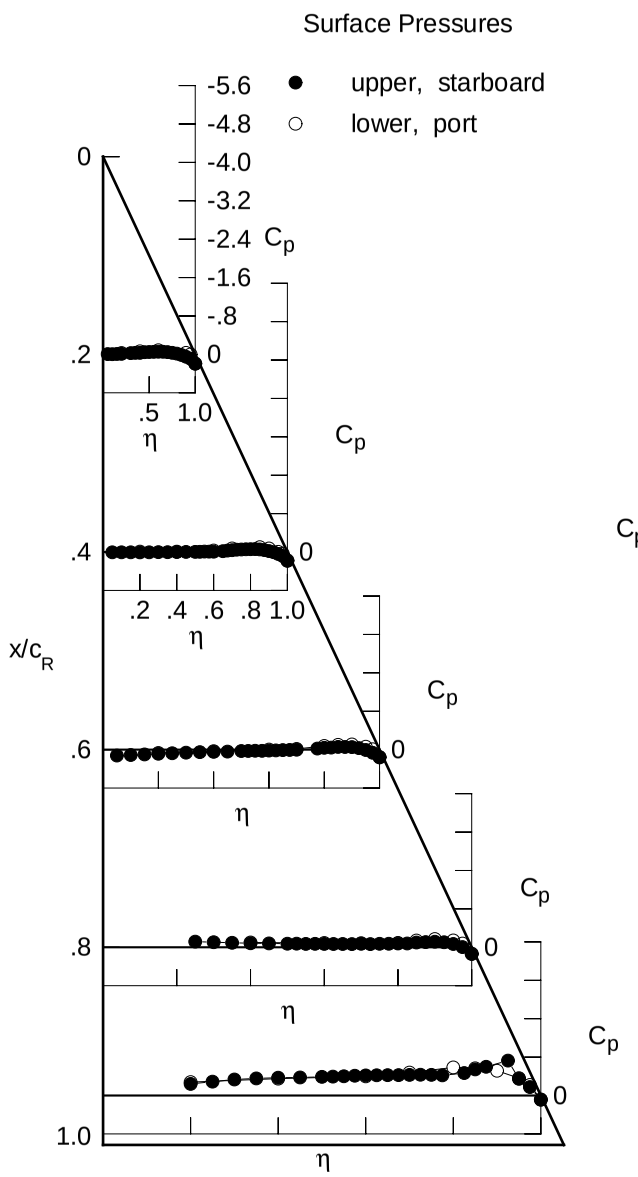
$R_{mac}$ = $6.0 \times 10^6$




| x/c_R | starb'd Cp | port Cp |
|---|---|---|
| 0.10 | 0.1995 | ******* |
| 0.20 | 0.1842 | 0.1853 |
| 0.30 | 0.1803 | ******* |
| 0.40 | 0.1817 | 0.1761 |
| 0.50 | 0.1809 | ******* |
| 0.60 | 0.1722 | 0.1635 |
| 0.70 | 0.1558 | ******* |
| 0.80 | 0.1400 | 0.1447 |
| 0.90 | 0.1025 | ******* |
| 0.95 | 0.0899 | 0.0897 |

# Table D3. Tabulations and Plots of Surface Pressure Coefficients.

| | $x/c_R$ .2 | $x/c_R$ .4 | $x/c_R$ .6 | $x/c_R$ .8 | $x/c_R$ .95 |
|---|---|---|---|---|---|
| $\eta$ | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ |
| 0.050 | -0.0062 | 0.0058 | 0.1235 | ******* | ******* |
| 0.100 | -0.0039 | 0.0054 | 0.1121 | ******* | ******* |
| 0.150 | -0.0089 | 0.0055 | 0.0998 | ******* | ******* |
| 0.200 | -0.0115 | 0.0070 | 0.0854 | ******* | -0.2415 |
| 0.250 | ******* | 0.0055 | 0.0750 | -0.1174 | -0.2884 |
| 0.300 | -0.0261 | 0.0025 | 0.0632 | -0.1059 | -0.3338 |
| 0.350 | -0.0323 | 0.0029 | 0.0520 | -0.0938 | -0.3563 |
| 0.400 | -0.0322 | -0.0007 | 0.0453 | -0.0844 | -0.3714 |
| 0.450 | -0.0456 | -0.0023 | 0.0404 | -0.0807 | -0.3759 |
| 0.500 | -0.0494 | -0.0036 | 0.0290 | -0.0746 | -0.3887 |
| 0.525 | ******* | -0.0047 | 0.0273 | -0.0753 | -0.3934 |
| 0.550 | -0.0531 | -0.0095 | 0.0229 | -0.0702 | -0.4011 |
| 0.575 | ******* | -0.0084 | 0.0250 | -0.0722 | -0.4121 |
| 0.600 | -0.0549 | -0.0075 | 0.0189 | -0.0706 | -0.4183 |
| 0.625 | ******* | ******* | 0.0158 | -0.0689 | -0.4217 |
| 0.650 | -0.0541 | -0.0175 | 0.0099 | -0.0686 | -0.4243 |
| 0.675 | ******* | -0.0300 | 0.0063 | -0.0661 | -0.4247 |
| 0.700 | -0.0470 | -0.0387 | 0.0012 | -0.0725 | -0.4299 |
| 0.725 | ******* | -0.0484 | ******* | -0.0664 | -0.4331 |
| 0.750 | -0.0330 | -0.0529 | ******* | -0.0731 | -0.4302 |
| 0.775 | ******* | -0.0572 | -0.0228 | -0.0736 | -0.4201 |
| 0.800 | -0.0161 | -0.0591 | -0.0386 | -0.0794 | ******* |
| 0.825 | ******* | -0.0620 | -0.0427 | -0.0789 | -0.4680 |
| 0.850 | 0.0122 | -0.0540 | -0.0564 | -0.0994 | -0.5444 |
| 0.875 | ******* | -0.0408 | -0.0553 | -0.1083 | -0.5988 |
| 0.900 | 0.0488 | -0.0198 | -0.0531 | -0.1163 | ******* |
| 0.925 | ******* | 0.0029 | -0.0323 | -0.1046 | -0.7274 |
| 0.950 | 0.0914 | 0.0396 | 0.0068 | -0.0686 | -0.3474 |
| 0.975 | ******* | 0.0839 | 0.0658 | -0.0043 | -0.1758 |
| 1.000 | 0.1955 | 0.1838 | 0.1620 | 0.1400 | 0.0876 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0286 | -0.0090 | 0.0697 | ******* | -0.2793 |
| -0.400 | -0.0637 | -0.0082 | 0.0318 | -0.0999 | -0.3513 |
| -0.600 | -0.0866 | -0.0310 | -0.0013 | -0.0893 | -0.3990 |
| -0.700 | ******* | -0.0747 | -0.0146 | -0.0853 | -0.4773 |
| -0.800 | ******* | ******* | -0.0771 | -0.0914 | -0.5848 |
| -0.850 | ******* | -0.1012 | -0.0999 | -0.1407 | -0.5664 |
| -0.900 | -0.0321 | -0.0748 | -0.1083 | -0.1720 | -0.5163 |
| -0.950 | 0.0004 | -0.0039 | -0.0608 | -0.1424 | -0.3614 |
| -0.975 | ******* | 0.0332 | -0.0079 | -0.0777 | -0.2197 |
| -1.000 | 0.1890 | 0.1723 | 0.1527 | 0.1323 | 0.0828 |



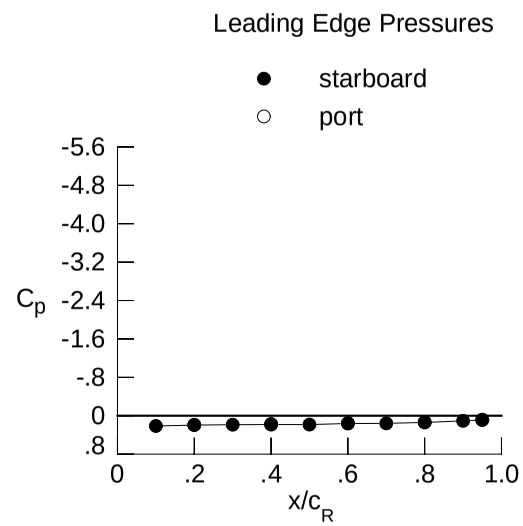

Small Radius L.E.

Run No. = 39 , Point No. = 779

$C_N$ = -0.029, $C_m$ = 0.0062

$\alpha$ = -0.4 °, $M_\infty$ = 0.799

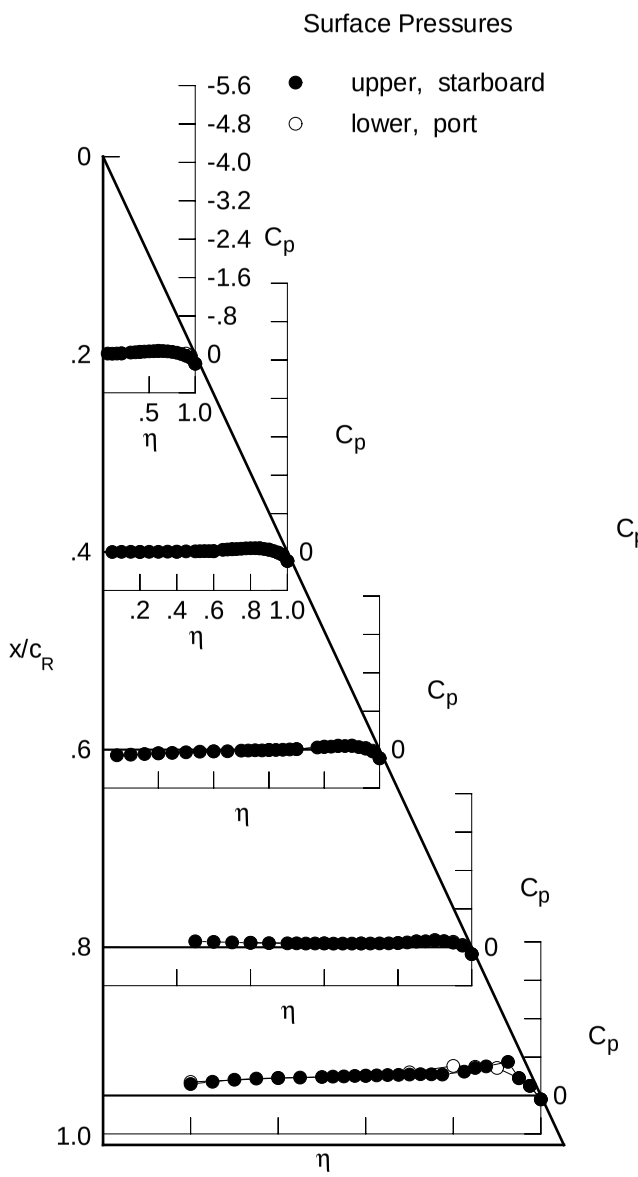
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2136 | ******* |
| 0.20 | 0.1955 | 0.1890 |
| 0.30 | 0.1868 | ******* |
| 0.40 | 0.1838 | 0.1723 |
| 0.50 | 0.1842 | ******* |
| 0.60 | 0.1620 | 0.1527 |
| 0.70 | 0.1592 | ******* |
| 0.80 | 0.1400 | 0.1323 |
| 0.90 | 0.1066 | ******* |
| 0.95 | 0.0876 | 0.0828 |

# Table D3. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0171 | -0.0005 | 0.1172 | ******* | ******* |
| 0.100 | -0.0134 | -0.0044 | 0.1047 | ******* | ******* |
| 0.150 | -0.0176 | -0.0050 | 0.0912 | ******* | ******* |
| 0.200 | -0.0212 | -0.0007 | 0.0784 | ******* | -0.2390 |
| 0.250 | ******* | -0.0051 | 0.0683 | -0.1241 | -0.2868 |
| 0.300 | -0.0381 | -0.0039 | 0.0556 | -0.1126 | -0.3292 |
| 0.350 | -0.0443 | -0.0083 | 0.0424 | -0.1018 | -0.3529 |
| 0.400 | -0.0506 | -0.0091 | 0.0369 | -0.0923 | -0.3666 |
| 0.450 | -0.0574 | -0.0132 | 0.0335 | -0.0867 | -0.3735 |
| 0.500 | -0.0632 | -0.0146 | 0.0209 | -0.0826 | -0.3859 |
| 0.525 | ******* | -0.0166 | 0.0185 | -0.0827 | -0.3935 |
| 0.550 | -0.0665 | -0.0192 | 0.0129 | -0.0778 | -0.3978 |
| 0.575 | ******* | -0.0183 | 0.0163 | -0.0791 | -0.4081 |
| 0.600 | -0.0694 | -0.0196 | 0.0093 | -0.0799 | -0.4150 |
| 0.625 | ******* | ******* | 0.0065 | -0.0762 | -0.4195 |
| 0.650 | -0.0695 | -0.0464 | 0.0026 | -0.0770 | -0.4264 |
| 0.675 | ******* | -0.0528 | -0.0044 | -0.0767 | -0.4303 |
| 0.700 | -0.0631 | -0.0572 | -0.0097 | -0.0801 | -0.4368 |
| 0.725 | ******* | -0.0628 | ******* | -0.0782 | -0.4440 |
| 0.750 | -0.0524 | -0.0688 | ******* | -0.0804 | -0.4416 |
| 0.775 | ******* | -0.0766 | -0.0449 | -0.0817 | -0.4365 |
| 0.800 | -0.0341 | -0.0792 | -0.0546 | -0.0880 | ******* |
| 0.825 | ******* | -0.0802 | -0.0623 | -0.1012 | -0.4970 |
| 0.850 | -0.0071 | -0.0748 | -0.0734 | -0.1202 | -0.5735 |
| 0.875 | ******* | -0.0628 | -0.0748 | -0.1258 | -0.6065 |
| 0.900 | 0.0298 | -0.0445 | -0.0776 | -0.1385 | ******* |
| 0.925 | ******* | -0.0209 | -0.0526 | -0.1296 | -0.7008 |
| 0.950 | 0.0723 | 0.0149 | -0.0204 | -0.0962 | -0.3660 |
| 0.975 | ******* | 0.0583 | 0.0377 | -0.0343 | -0.2013 |
| 1.000 | 0.1925 | 0.1873 | 0.1823 | 0.1413 | 0.0791 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0202 | -0.0030 | 0.0739 | ******* | -0.2824 |
| -0.400 | -0.0547 | -0.0034 | 0.0342 | -0.0955 | -0.3629 |
| -0.600 | -0.0750 | -0.0154 | 0.0040 | -0.0828 | -0.4075 |
| -0.700 | ******* | -0.0611 | -0.0112 | -0.0790 | -0.4828 |
| -0.800 | ******* | ******* | -0.0631 | -0.0897 | -0.6158 |
| -0.850 | ******* | -0.0809 | -0.0838 | -0.1251 | -0.5977 |
| -0.900 | -0.0157 | -0.0535 | -0.0857 | -0.1524 | -0.5744 |
| -0.950 | 0.0179 | 0.0116 | -0.0343 | -0.1146 | -0.3595 |
| -0.975 | ******* | 0.0590 | 0.0209 | -0.0477 | -0.2018 |
| -1.000 | 0.1942 | 0.1850 | 0.1761 | 0.1443 | 0.0809 |



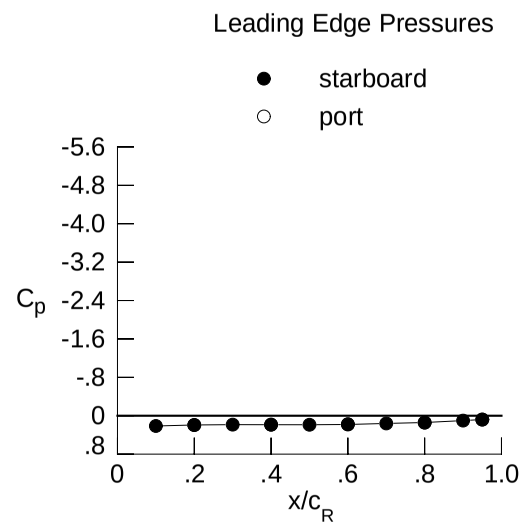

Small Radius L.E.

Run No. = 39 , Point No. = 780

$C_N$ = -0.011, $C_m$ = 0.0026

$\alpha$ = 0.1 °, $M_\infty$ = 0.799

$R_{mac}$ = $6.0 \times 10^6$

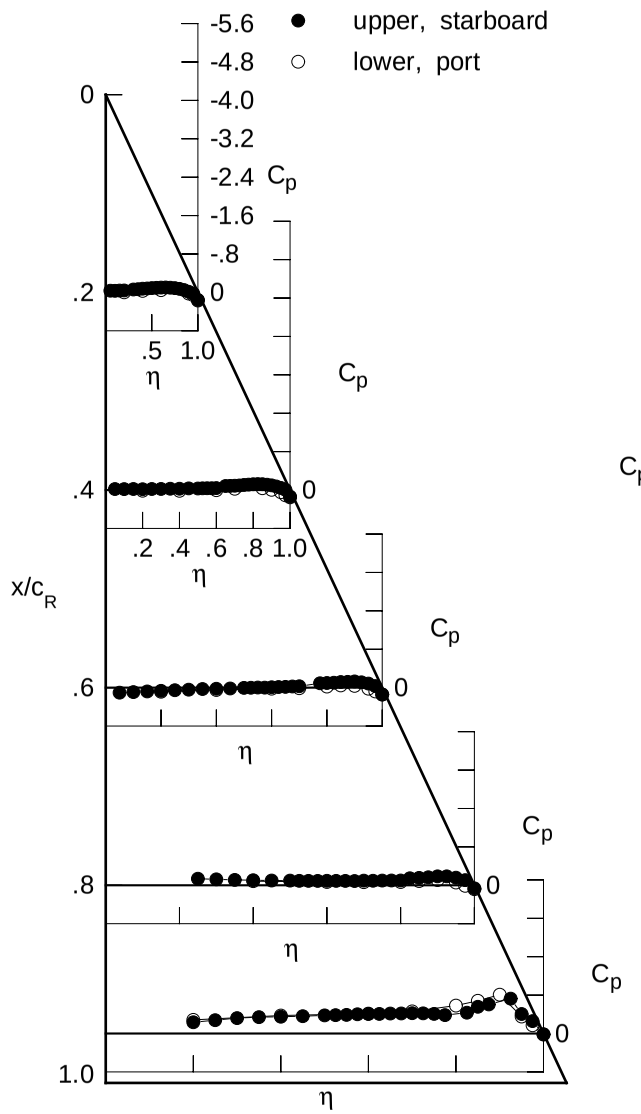



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2139 | ******* |
| 0.20 | 0.1925 | 0.1942 |
| 0.30 | 0.1858 | ******* |
| 0.40 | 0.1873 | 0.1850 |
| 0.50 | 0.1879 | ******* |
| 0.60 | 0.1823 | 0.1761 |
| 0.70 | 0.1607 | ******* |
| 0.80 | 0.1413 | 0.1443 |
| 0.90 | 0.1012 | ******* |
| 0.95 | 0.0791 | 0.0809 |

# Table D3. Continued.

| η | x/c_R .2 C_p,u | x/c_R .4 C_p,u | x/c_R .6 C_p,u | x/c_R .8 C_p,u | x/c_R .95 C_p,u |
|---|---|---|---|---|---|
| 0.050 | -0.0349 | -0.0208 | 0.1045 | ******* | ******* |
| 0.100 | -0.0328 | -0.0194 | 0.0924 | ******* | ******* |
| 0.150 | -0.0386 | -0.0219 | 0.0789 | ******* | ******* |
| 0.200 | -0.0401 | -0.0171 | 0.0661 | ******* | -0.2341 |
| 0.250 | ******* | -0.0220 | 0.0540 | -0.1365 | -0.2779 |
| 0.300 | -0.0603 | -0.0220 | 0.0423 | -0.1240 | -0.3210 |
| 0.350 | -0.0663 | -0.0274 | 0.0289 | -0.1123 | -0.3404 |
| 0.400 | -0.0770 | -0.0276 | 0.0228 | -0.1056 | -0.3492 |
| 0.450 | -0.0813 | -0.0340 | 0.0179 | -0.0991 | -0.3607 |
| 0.500 | -0.0900 | -0.0320 | 0.0052 | -0.0978 | -0.3775 |
| 0.525 | ******* | -0.0363 | 0.0020 | -0.0927 | -0.3823 |
| 0.550 | -0.0951 | -0.0372 | -0.0027 | -0.0923 | -0.3883 |
| 0.575 | ******* | -0.0379 | 0.0001 | -0.0911 | -0.4004 |
| 0.600 | -0.0997 | -0.0404 | -0.0083 | -0.0937 | -0.4074 |
| 0.625 | ******* | ******* | -0.0128 | -0.0922 | -0.4077 |
| 0.650 | -0.1026 | -0.0840 | -0.0159 | -0.0911 | -0.4160 |
| 0.675 | ******* | -0.0867 | -0.0244 | -0.0886 | -0.4174 |
| 0.700 | -0.0976 | -0.0894 | -0.0287 | -0.0969 | -0.4233 |
| 0.725 | ******* | -0.0950 | ******* | -0.0947 | -0.4196 |
| 0.750 | -0.0888 | -0.1057 | ******* | -0.0981 | -0.4085 |
| 0.775 | ******* | -0.1124 | -0.0911 | -0.1000 | -0.3833 |
| 0.800 | -0.0737 | -0.1209 | -0.0965 | -0.1002 | ******* |
| 0.825 | ******* | -0.1238 | -0.1021 | -0.1460 | -0.4336 |
| 0.850 | -0.0485 | -0.1220 | -0.1164 | -0.1547 | -0.5571 |
| 0.875 | ******* | -0.1114 | -0.1207 | -0.1672 | -0.6054 |
| 0.900 | -0.0129 | -0.0977 | -0.1297 | -0.1867 | ******* |
| 0.925 | ******* | -0.0747 | -0.1109 | -0.1863 | -0.7267 |
| 0.950 | 0.0243 | -0.0440 | -0.0849 | -0.1586 | -0.4065 |
| 0.975 | ******* | -0.0049 | -0.0331 | -0.1072 | -0.2581 |
| 1.000 | 0.1566 | 0.1367 | 0.1421 | 0.0636 | 0.0155 |
| | C_p,l | C_p,l | C_p,l | C_p,l | C_p,l |
| -0.200 | -0.0013 | 0.0142 | 0.0859 | ******* | -0.2840 |
| -0.400 | -0.0316 | 0.0159 | 0.0489 | -0.0860 | -0.3746 |
| -0.600 | -0.0467 | 0.0029 | 0.0216 | -0.0690 | -0.4147 |
| -0.700 | ******* | -0.0265 | 0.0118 | -0.0645 | -0.4605 |
| -0.800 | ******* | ******* | -0.0227 | -0.0683 | -0.5818 |
| -0.850 | ******* | -0.0379 | -0.0462 | -0.0882 | -0.6814 |
| -0.900 | 0.0240 | -0.0048 | -0.0370 | -0.1089 | -0.8086 |
| -0.950 | 0.0579 | 0.0451 | 0.0216 | -0.0573 | -0.3537 |
| -0.975 | ******* | 0.1100 | 0.0789 | 0.0113 | -0.1712 |
| -1.000 | 0.1697 | 0.1517 | 0.1436 | 0.0819 | 0.0216 |

Surface Pressures




Small Radius L.E.

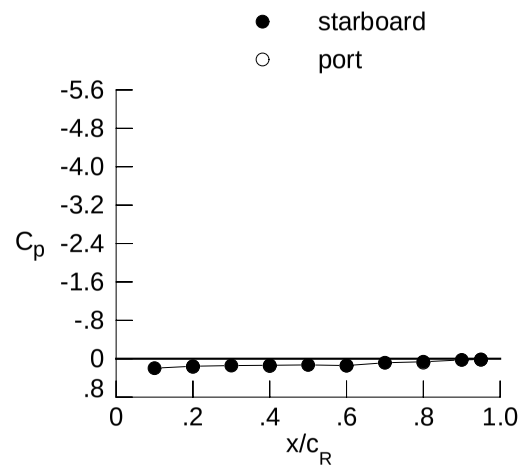
Run No. = 39 , Point No. = 781

$C_N$ = 0.029, $C_m$ = -0.0027

$\alpha$ = 1.1 °, $M_\infty$ = 0.799

$R_{mac}$ = $6.0 \times 10^6$

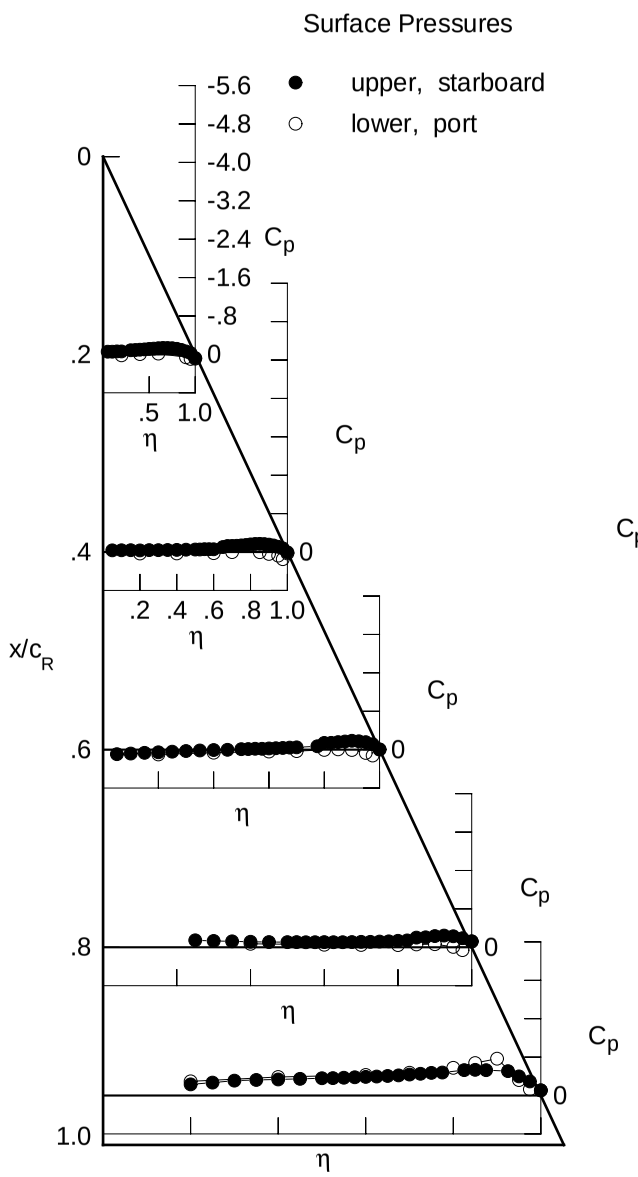
Leading Edge Pressures




| x/c_R | starb'd C_p | port C_p |
|---|---|---|
| 0.10 | 0.1968 | ******* |
| 0.20 | 0.1566 | 0.1697 |
| 0.30 | 0.1428 | ******* |
| 0.40 | 0.1367 | 0.1517 |
| 0.50 | 0.1288 | ******* |
| 0.60 | 0.1421 | 0.1436 |
| 0.70 | 0.0840 | ******* |
| 0.80 | 0.0636 | 0.0819 |
| 0.90 | 0.0250 | ******* |
| 0.95 | 0.0155 | 0.0216 |

# Table D3. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0557 | -0.0349 | 0.0946 | ******* | ******* |
| 0.100 | -0.0561 | -0.0365 | 0.0813 | ******* | ******* |
| 0.150 | -0.0621 | -0.0384 | 0.0661 | ******* | ******* |
| 0.200 | -0.0616 | -0.0332 | 0.0550 | ******* | -0.2320 |
| 0.250 | ******* | -0.0400 | 0.0421 | -0.1452 | -0.2685 |
| 0.300 | -0.0867 | -0.0389 | 0.0287 | -0.1320 | -0.3095 |
| 0.350 | -0.0909 | -0.0421 | 0.0173 | -0.1240 | -0.3242 |
| 0.400 | -0.0974 | -0.0446 | 0.0079 | -0.1149 | -0.3346 |
| 0.450 | -0.1041 | -0.0484 | 0.0032 | -0.1092 | -0.3469 |
| 0.500 | -0.1132 | -0.0521 | -0.0095 | -0.1073 | -0.3598 |
| 0.525 | ******* | -0.0530 | -0.0122 | -0.1080 | -0.3623 |
| 0.550 | -0.1201 | -0.0588 | -0.0187 | -0.1045 | -0.3706 |
| 0.575 | ******* | -0.0593 | -0.0178 | -0.1056 | -0.3799 |
| 0.600 | -0.1291 | -0.0574 | -0.0248 | -0.1078 | -0.3879 |
| 0.625 | ******* | ******* | -0.0296 | -0.1055 | -0.3949 |
| 0.650 | -0.1347 | -0.1039 | -0.0354 | -0.1058 | -0.4069 |
| 0.675 | ******* | -0.1255 | -0.0425 | -0.1092 | -0.4189 |
| 0.700 | -0.1327 | -0.1261 | -0.0483 | -0.1136 | -0.4370 |
| 0.725 | ******* | -0.1304 | ******* | -0.1138 | -0.4528 |
| 0.750 | -0.1287 | -0.1380 | ******* | -0.1196 | -0.4715 |
| 0.775 | ******* | -0.1465 | -0.0700 | -0.1242 | -0.4781 |
| 0.800 | -0.1158 | -0.1591 | -0.1396 | -0.1355 | ******* |
| 0.825 | ******* | -0.1677 | -0.1417 | -0.1432 | -0.5285 |
| 0.850 | -0.0929 | -0.1701 | -0.1568 | -0.2017 | -0.5348 |
| 0.875 | ******* | -0.1653 | -0.1695 | -0.2082 | -0.5283 |
| 0.900 | -0.0615 | -0.1547 | -0.1849 | -0.2332 | ******* |
| 0.925 | ******* | -0.1369 | -0.1744 | -0.2444 | -0.5083 |
| 0.950 | -0.0262 | -0.1097 | -0.1560 | -0.2294 | -0.3981 |
| 0.975 | ******* | -0.0779 | -0.1127 | -0.1895 | -0.2928 |
| 1.000 | 0.0751 | 0.0060 | -0.0045 | -0.1268 | -0.1048 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0195 | 0.0302 | 0.1000 | ******* | -0.2954 |
| -0.400 | -0.0068 | 0.0288 | 0.0636 | -0.0728 | -0.3857 |
| -0.600 | -0.0168 | 0.0229 | 0.0391 | -0.0538 | -0.4281 |
| -0.700 | ******* | 0.0018 | 0.0303 | -0.0488 | -0.4744 |
| -0.800 | ******* | ******* | 0.0053 | -0.0457 | -0.5772 |
| -0.850 | ******* | 0.0036 | -0.0064 | -0.0600 | -0.6763 |
| -0.900 | 0.0598 | 0.0392 | 0.0069 | -0.0649 | -0.7669 |
| -0.950 | 0.0944 | 0.0745 | 0.0688 | -0.0082 | -0.3214 |
| -0.975 | ******* | 0.1492 | 0.1225 | 0.0595 | -0.1295 |
| -1.000 | 0.0889 | 0.0291 | -0.0023 | -0.1169 | -0.1096 |



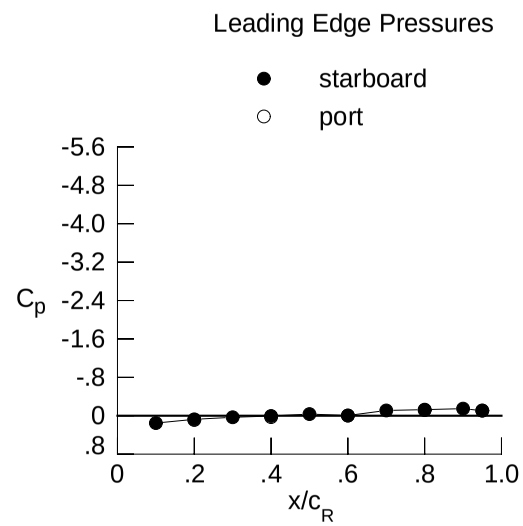

Small Radius L.E.

Run No. = 39 , Point No. = 782

$C_N$ = 0.068, $C_m$ = -0.0087

$\alpha$ = 2.2 °, $M_\infty$ = 0.799

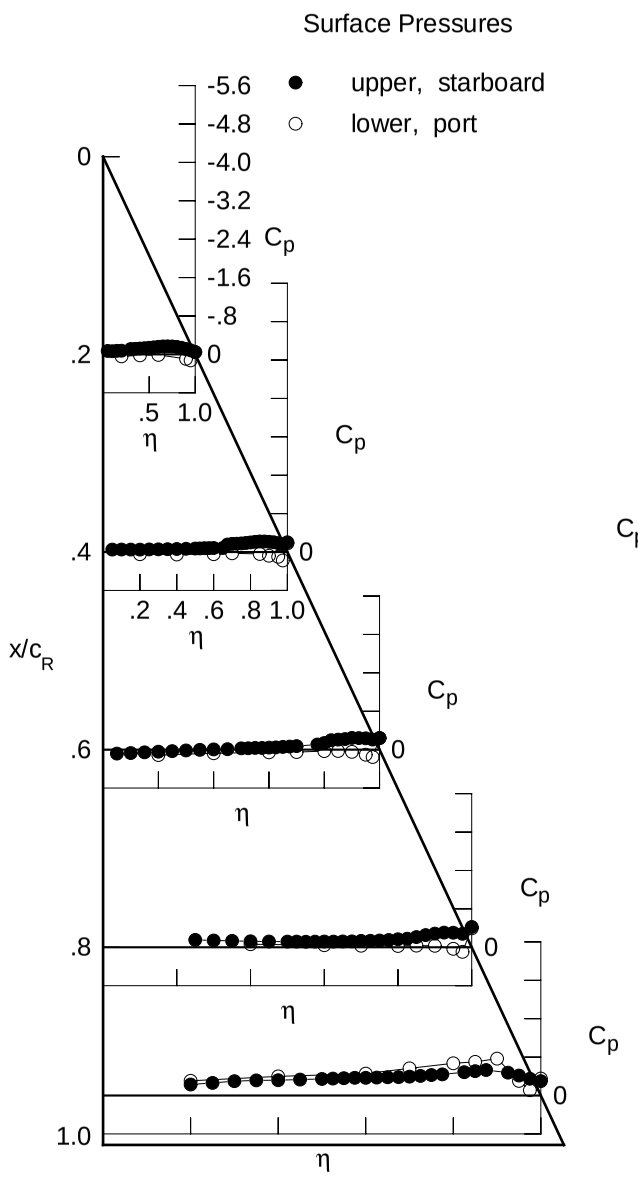
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.1529 | ******* |
| 0.20 | 0.0751 | 0.0889 |
| 0.30 | 0.0323 | ******* |
| 0.40 | 0.0060 | 0.0291 |
| 0.50 | -0.0344 | ******* |
| 0.60 | -0.0045 | -0.0023 |
| 0.70 | -0.1098 | ******* |
| 0.80 | -0.1268 | -0.1169 |
| 0.90 | -0.1478 | ******* |
| 0.95 | -0.1048 | -0.1096 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0721 | -0.0512 | 0.0826 | ******* | ******* |
| 0.100 | -0.0654 | -0.0520 | 0.0709 | ******* | ******* |
| 0.150 | -0.0745 | -0.0516 | 0.0564 | ******* | ******* |
| 0.200 | -0.0765 | -0.0500 | 0.0424 | ******* | -0.2290 |
| 0.250 | ******* | -0.0544 | 0.0314 | -0.1548 | -0.2626 |
| 0.300 | -0.1117 | -0.0560 | 0.0165 | -0.1419 | -0.2988 |
| 0.350 | -0.1160 | -0.0594 | 0.0036 | -0.1333 | -0.3151 |
| 0.400 | -0.1223 | -0.0634 | -0.0052 | -0.1251 | -0.3187 |
| 0.450 | -0.1285 | -0.0681 | -0.0097 | -0.1196 | -0.3324 |
| 0.500 | -0.1382 | -0.0729 | -0.0268 | -0.1183 | -0.3452 |
| 0.525 | ******* | -0.0754 | -0.0291 | -0.1184 | -0.3531 |
| 0.550 | -0.1469 | -0.0803 | -0.0363 | -0.1155 | -0.3609 |
| 0.575 | ******* | -0.0818 | -0.0353 | -0.1179 | -0.3689 |
| 0.600 | -0.1578 | -0.0841 | -0.0428 | -0.1201 | -0.3692 |
| 0.625 | ******* | ******* | -0.0470 | -0.1185 | -0.3738 |
| 0.650 | -0.1661 | -0.0859 | -0.0565 | -0.1213 | -0.3802 |
| 0.675 | ******* | -0.1569 | -0.0638 | -0.1233 | -0.3835 |
| 0.700 | -0.1680 | -0.1704 | -0.0734 | -0.1333 | -0.3930 |
| 0.725 | ******* | -0.1734 | ******* | -0.1351 | -0.4078 |
| 0.750 | -0.1652 | -0.1797 | ******* | -0.1420 | -0.4267 |
| 0.775 | ******* | -0.1890 | -0.1072 | -0.1524 | -0.4396 |
| 0.800 | -0.1559 | -0.2002 | -0.1374 | -0.1672 | ******* |
| 0.825 | ******* | -0.2131 | -0.1968 | -0.1790 | -0.4856 |
| 0.850 | -0.1381 | -0.2207 | -0.2089 | -0.2127 | -0.5074 |
| 0.875 | ******* | -0.2196 | -0.2201 | -0.2541 | -0.5313 |
| 0.900 | -0.1118 | -0.2133 | -0.2445 | -0.2851 | ******* |
| 0.925 | ******* | -0.2038 | -0.2411 | -0.3059 | -0.4758 |
| 0.950 | -0.0852 | -0.1847 | -0.2361 | -0.3036 | -0.4161 |
| 0.975 | ******* | -0.1648 | -0.2100 | -0.2812 | -0.3491 |
| 1.000 | -0.0504 | -0.2032 | -0.2430 | -0.4236 | -0.2990 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0411 | 0.0457 | 0.1132 | ******* | -0.3062 |
| -0.400 | 0.0200 | 0.0510 | 0.0754 | -0.0637 | -0.3984 |
| -0.600 | 0.0111 | 0.0444 | 0.0563 | -0.0429 | -0.4563 |
| -0.700 | ******* | 0.0264 | 0.0505 | -0.0328 | -0.5659 |
| -0.800 | ******* | ******* | 0.0306 | -0.0276 | -0.6712 |
| -0.850 | ******* | 0.0397 | 0.0278 | -0.0347 | -0.7009 |
| -0.900 | 0.0928 | 0.0771 | 0.0457 | -0.0311 | -0.7680 |
| -0.950 | 0.1246 | 0.0985 | 0.1058 | 0.0318 | -0.3044 |
| -0.975 | ******* | 0.1755 | 0.1535 | 0.0940 | -0.1101 |
| -1.000 | -0.0454 | -0.1797 | -0.2387 | -0.3943 | -0.3539 |



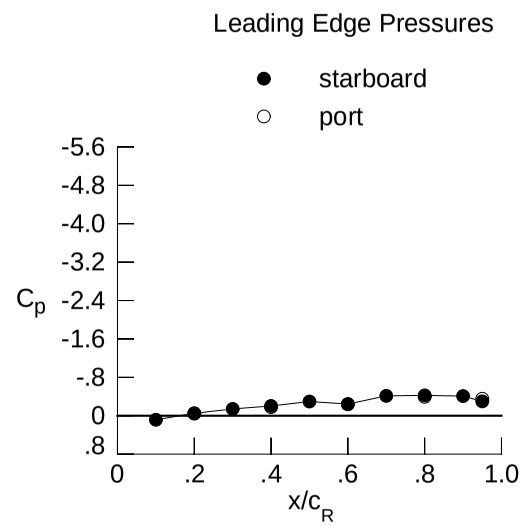

Small Radius L.E.

Run No. = 39 , Point No. = 783

$C_N$ = 0.113, $C_m$ = -0.0197

$\alpha$ = 3.2 °, $M_\infty$ = 0.799

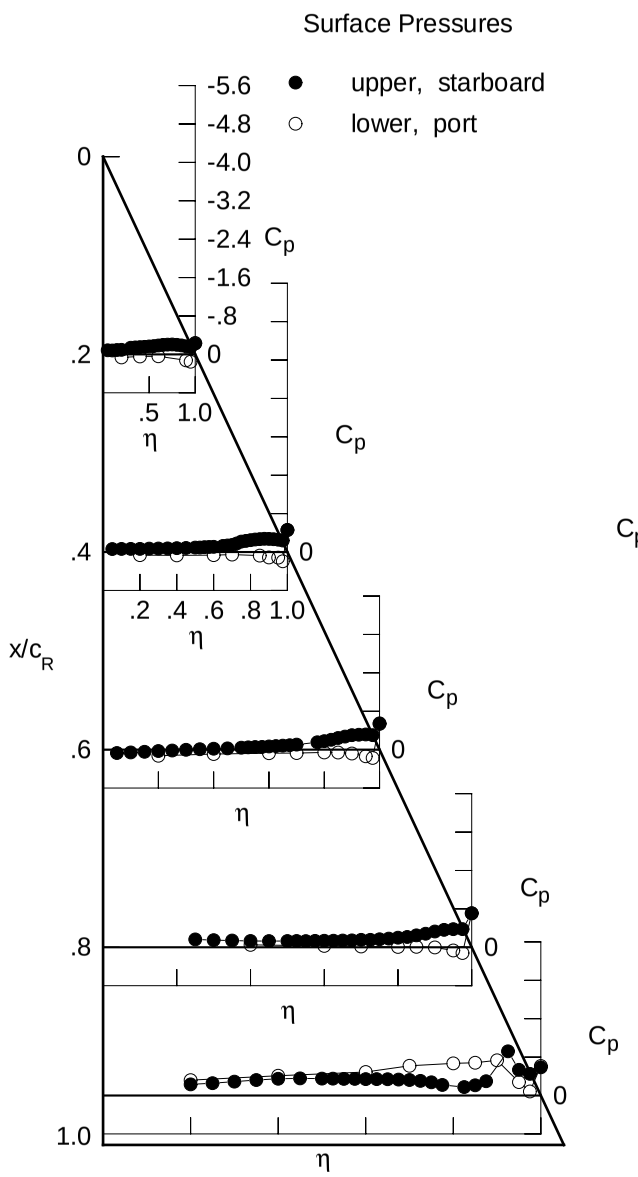
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.0842 | ******* |
| 0.20 | -0.0504 | -0.0454 |
| 0.30 | -0.1416 | ******* |
| 0.40 | -0.2032 | -0.1797 |
| 0.50 | -0.2960 | ******* |
| 0.60 | -0.2430 | -0.2387 |
| 0.70 | -0.4138 | ******* |
| 0.80 | -0.4236 | -0.3943 |
| 0.90 | -0.4093 | ******* |
| 0.95 | -0.2990 | -0.3539 |

# Table D3. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0853 | -0.0627 | 0.0705 | ******* | ******* |
| 0.100 | -0.0816 | -0.0644 | 0.0584 | ******* | ******* |
| 0.150 | -0.0911 | -0.0653 | 0.0451 | ******* | ******* |
| 0.200 | -0.0948 | -0.0658 | 0.0291 | ******* | -0.2324 |
| 0.250 | ******* | -0.0709 | 0.0181 | -0.1643 | -0.2564 |
| 0.300 | -0.1386 | -0.0733 | 0.0029 | -0.1485 | -0.2890 |
| 0.350 | -0.1459 | -0.0761 | -0.0084 | -0.1404 | -0.3224 |
| 0.400 | -0.1513 | -0.0812 | -0.0194 | -0.1312 | -0.3488 |
| 0.450 | -0.1567 | -0.0844 | -0.0260 | -0.1292 | -0.3565 |
| 0.500 | -0.1657 | -0.0927 | -0.0406 | -0.1303 | -0.3521 |
| 0.525 | ******* | -0.0939 | -0.0478 | -0.1309 | -0.3513 |
| 0.550 | -0.1726 | -0.1015 | -0.0545 | -0.1287 | -0.3465 |
| 0.575 | ******* | -0.1058 | -0.0565 | -0.1335 | -0.3461 |
| 0.600 | -0.1853 | -0.1088 | -0.0662 | -0.1361 | -0.3416 |
| 0.625 | ******* | ******* | -0.0743 | -0.1368 | -0.3417 |
| 0.650 | -0.1974 | -0.1268 | -0.0835 | -0.1406 | -0.3390 |
| 0.675 | ******* | -0.1367 | -0.0918 | -0.1436 | -0.3321 |
| 0.700 | -0.2031 | -0.1473 | -0.1046 | -0.1548 | -0.3233 |
| 0.725 | ******* | -0.1784 | ******* | -0.1548 | -0.3051 |
| 0.750 | -0.2061 | -0.2172 | ******* | -0.1673 | -0.2754 |
| 0.775 | ******* | -0.2323 | -0.1536 | -0.1808 | -0.2201 |
| 0.800 | -0.1994 | -0.2471 | -0.1768 | -0.1997 | ******* |
| 0.825 | ******* | -0.2609 | -0.2054 | -0.2150 | -0.1756 |
| 0.850 | -0.1874 | -0.2691 | -0.2428 | -0.2486 | -0.2128 |
| 0.875 | ******* | -0.2758 | -0.2718 | -0.2821 | -0.2974 |
| 0.900 | -0.1687 | -0.2736 | -0.3017 | -0.3292 | ******* |
| 0.925 | ******* | -0.2672 | -0.3107 | -0.3630 | -0.9206 |
| 0.950 | -0.1525 | -0.2571 | -0.3162 | -0.3778 | -0.5354 |
| 0.975 | ******* | -0.2400 | -0.3016 | -0.3782 | -0.4511 |
| 1.000 | -0.2263 | -0.4616 | -0.5478 | -0.7060 | -0.5872 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0630 | 0.0646 | 0.1274 | ******* | -0.3203 |
| -0.400 | 0.0433 | 0.0695 | 0.0914 | -0.0506 | -0.4118 |
| -0.600 | 0.0390 | 0.0646 | 0.0745 | -0.0291 | -0.4897 |
| -0.700 | ******* | 0.0528 | 0.0714 | -0.0165 | -0.6191 |
| -0.800 | ******* | ******* | 0.0580 | -0.0069 | -0.6695 |
| -0.850 | ******* | 0.0742 | 0.0600 | -0.0094 | -0.6825 |
| -0.900 | 0.1237 | 0.1125 | 0.0807 | 0.0030 | -0.7337 |
| -0.950 | 0.1530 | 0.1168 | 0.1383 | 0.0662 | -0.2791 |
| -0.975 | ******* | 0.1928 | 0.1726 | 0.1192 | -0.0840 |
| -1.000 | -0.2388 | -0.4549 | -0.5362 | -0.7109 | -0.6149 |



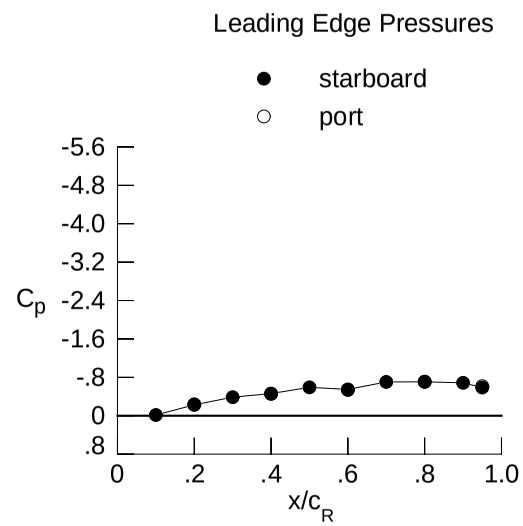

Small Radius L.E.

Run No. = 39 , Point No. = 784

$C_N$ = 0.147, $C_m$ = -0.0210

$\alpha$ = 4.2 °, $M_\infty$ = 0.800

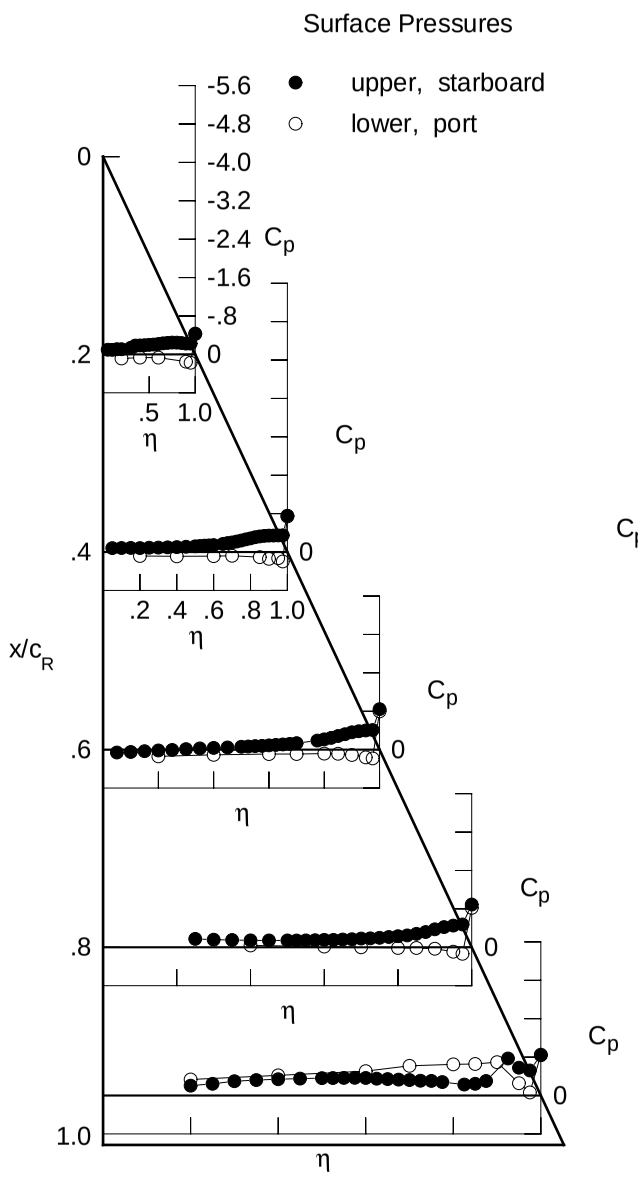
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.0154 | ******* |
| 0.20 | -0.2263 | -0.2388 |
| 0.30 | -0.3868 | ******* |
| 0.40 | -0.4616 | -0.4549 |
| 0.50 | -0.5912 | ******* |
| 0.60 | -0.5478 | -0.5362 |
| 0.70 | -0.7039 | ******* |
| 0.80 | -0.7060 | -0.7109 |
| 0.90 | -0.6857 | ******* |
| 0.95 | -0.5872 | -0.6149 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0965 | -0.0814 | 0.0597 | ******* | ******* |
| 0.100 | -0.0942 | -0.0842 | 0.0487 | ******* | ******* |
| 0.150 | -0.1088 | -0.0859 | 0.0316 | ******* | ******* |
| 0.200 | -0.1079 | -0.0827 | 0.0167 | ******* | -0.2048 |
| 0.250 | ******* | -0.0901 | 0.0062 | -0.1751 | -0.2440 |
| 0.300 | -0.1372 | -0.0927 | -0.0103 | -0.1584 | -0.2973 |
| 0.350 | -0.1837 | -0.0975 | -0.0258 | -0.1519 | -0.3220 |
| 0.400 | -0.1865 | -0.1029 | -0.0356 | -0.1438 | -0.3393 |
| 0.450 | -0.1913 | -0.1104 | -0.0454 | -0.1421 | -0.3522 |
| 0.500 | -0.1984 | -0.1190 | -0.0602 | -0.1426 | -0.3619 |
| 0.525 | ******* | -0.1253 | -0.0655 | -0.1406 | -0.3638 |
| 0.550 | -0.2045 | -0.1334 | -0.0737 | -0.1433 | -0.3669 |
| 0.575 | ******* | -0.1386 | -0.0781 | -0.1473 | -0.3688 |
| 0.600 | -0.2157 | -0.1449 | -0.0885 | -0.1543 | -0.3653 |
| 0.625 | ******* | ******* | -0.0981 | -0.1540 | -0.3507 |
| 0.650 | -0.2302 | -0.1680 | -0.1083 | -0.1615 | -0.3427 |
| 0.675 | ******* | -0.1866 | -0.1198 | -0.1680 | -0.3313 |
| 0.700 | -0.2395 | -0.2001 | -0.1351 | -0.1824 | -0.3227 |
| 0.725 | ******* | -0.2196 | ******* | -0.1862 | -0.3078 |
| 0.750 | -0.2467 | -0.2401 | ******* | -0.1973 | -0.3038 |
| 0.775 | ******* | -0.2637 | -0.1885 | -0.2143 | -0.2798 |
| 0.800 | -0.2451 | -0.2851 | -0.2148 | -0.2315 | ******* |
| 0.825 | ******* | -0.3086 | -0.2448 | -0.2473 | -0.2278 |
| 0.850 | -0.2379 | -0.3249 | -0.2841 | -0.2802 | -0.2440 |
| 0.875 | ******* | -0.3364 | -0.3219 | -0.3175 | -0.3027 |
| 0.900 | -0.2252 | -0.3421 | -0.3618 | -0.3744 | ******* |
| 0.925 | ******* | -0.3434 | -0.3830 | -0.4206 | -0.7708 |
| 0.950 | -0.2248 | -0.3457 | -0.3991 | -0.4519 | -0.5791 |
| 0.975 | ******* | -0.3495 | -0.4089 | -0.4753 | -0.5215 |
| 1.000 | -0.4338 | -0.7566 | -0.8433 | -0.8906 | -0.8386 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0851 | 0.0824 | 0.1400 | ******* | -0.3338 |
| -0.400 | 0.0664 | 0.0894 | 0.1078 | -0.0384 | -0.4197 |
| -0.600 | 0.0673 | 0.0853 | 0.0917 | -0.0149 | -0.5076 |
| -0.700 | ******* | 0.0776 | 0.0914 | -0.0004 | -0.6187 |
| -0.800 | ******* | ******* | 0.0821 | 0.0143 | -0.6489 |
| -0.850 | ******* | 0.1067 | 0.0858 | 0.0144 | -0.6569 |
| -0.900 | 0.1508 | 0.1416 | 0.1109 | 0.0305 | -0.6941 |
| -0.950 | 0.1740 | 0.1289 | 0.1616 | 0.0924 | -0.2559 |
| -0.975 | ******* | 0.1964 | 0.1827 | 0.1351 | -0.0640 |
| -1.000 | -0.4232 | -0.7409 | -0.7974 | -0.8211 | -0.8503 |



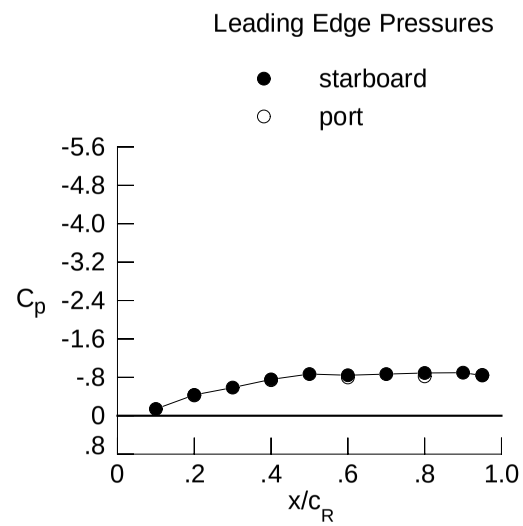

Small Radius L.E.

Run No. = 39 , Point No. = 785

$C_N$ = 0.186, $C_m$ = -0.0268

$\alpha$ = 5.2 °, $M_\infty$ = 0.799

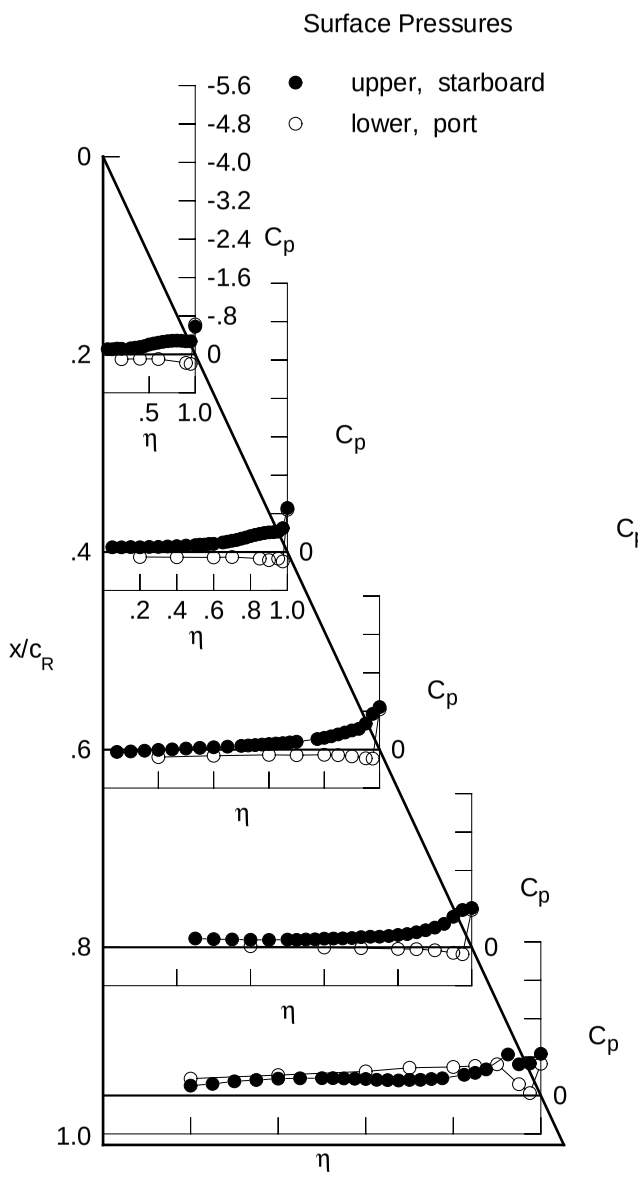
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.1410 | ******* |
| 0.20 | -0.4338 | -0.4232 |
| 0.30 | -0.5861 | ******* |
| 0.40 | -0.7566 | -0.7409 |
| 0.50 | -0.8683 | ******* |
| 0.60 | -0.8433 | -0.7974 |
| 0.70 | -0.8673 | ******* |
| 0.80 | -0.8906 | -0.8211 |
| 0.90 | -0.8966 | ******* |
| 0.95 | -0.8386 | -0.8503 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1083 | -0.0994 | 0.0471 | ******* | ******* |
| 0.100 | -0.1062 | -0.0980 | 0.0379 | ******* | ******* |
| 0.150 | -0.1210 | -0.1031 | 0.0220 | ******* | ******* |
| 0.200 | -0.1177 | -0.0995 | 0.0051 | ******* | -0.2054 |
| 0.250 | ******* | -0.1070 | -0.0054 | -0.1835 | -0.2423 |
| 0.300 | -0.1262 | -0.1081 | -0.0230 | -0.1693 | -0.2956 |
| 0.350 | -0.1404 | -0.1160 | -0.0378 | -0.1633 | -0.3230 |
| 0.400 | -0.1530 | -0.1234 | -0.0497 | -0.1560 | -0.3513 |
| 0.450 | -0.1726 | -0.1344 | -0.0623 | -0.1535 | -0.3584 |
| 0.500 | -0.2057 | -0.1432 | -0.0788 | -0.1601 | -0.3611 |
| 0.525 | ******* | -0.1536 | -0.0868 | -0.1545 | -0.3617 |
| 0.550 | -0.2262 | -0.1556 | -0.0955 | -0.1617 | -0.3557 |
| 0.575 | ******* | -0.1684 | -0.1053 | -0.1655 | -0.3496 |
| 0.600 | -0.2439 | -0.1712 | -0.1165 | -0.1801 | -0.3440 |
| 0.625 | ******* | ******* | -0.1272 | -0.1824 | -0.3270 |
| 0.650 | -0.2626 | -0.1983 | -0.1355 | -0.1857 | -0.3208 |
| 0.675 | ******* | -0.2158 | -0.1500 | -0.1925 | -0.3125 |
| 0.700 | -0.2746 | -0.2353 | -0.1646 | -0.2116 | -0.3247 |
| 0.725 | ******* | -0.2521 | ******* | -0.2204 | -0.3262 |
| 0.750 | -0.2843 | -0.2788 | ******* | -0.2211 | -0.3435 |
| 0.775 | ******* | -0.3015 | -0.2207 | -0.2352 | -0.3584 |
| 0.800 | -0.2873 | -0.3324 | -0.2468 | -0.2572 | ******* |
| 0.825 | ******* | -0.3568 | -0.2776 | -0.2752 | -0.4312 |
| 0.850 | -0.2841 | -0.3778 | -0.3164 | -0.3130 | -0.4716 |
| 0.875 | ******* | -0.3965 | -0.3572 | -0.3549 | -0.5438 |
| 0.900 | -0.2723 | -0.4095 | -0.3997 | -0.4094 | ******* |
| 0.925 | ******* | -0.4146 | -0.4330 | -0.4870 | -0.8547 |
| 0.950 | -0.2728 | -0.4248 | -0.5420 | -0.6352 | -0.6497 |
| 0.975 | ******* | -0.4983 | -0.7451 | -0.7766 | -0.6688 |
| 1.000 | -0.5785 | -0.9181 | -0.8874 | -0.8187 | -0.8686 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0996 | 0.1030 | 0.1558 | ******* | -0.3521 |
| -0.400 | 0.0914 | 0.1088 | 0.1274 | -0.0221 | -0.4254 |
| -0.600 | 0.0966 | 0.1122 | 0.1091 | 0.0041 | -0.5022 |
| -0.700 | ******* | 0.1043 | 0.1151 | 0.0176 | -0.5782 |
| -0.800 | ******* | ******* | 0.1070 | 0.0336 | -0.5947 |
| -0.850 | ******* | 0.1369 | 0.1152 | 0.0389 | -0.6163 |
| -0.900 | 0.1767 | 0.1691 | 0.1401 | 0.0620 | -0.6506 |
| -0.950 | 0.1974 | 0.1377 | 0.1807 | 0.1152 | -0.2351 |
| -0.975 | ******* | 0.1955 | 0.1863 | 0.1444 | -0.0501 |
| -1.000 | -0.6224 | -0.8813 | -0.8384 | -0.7783 | -0.6614 |



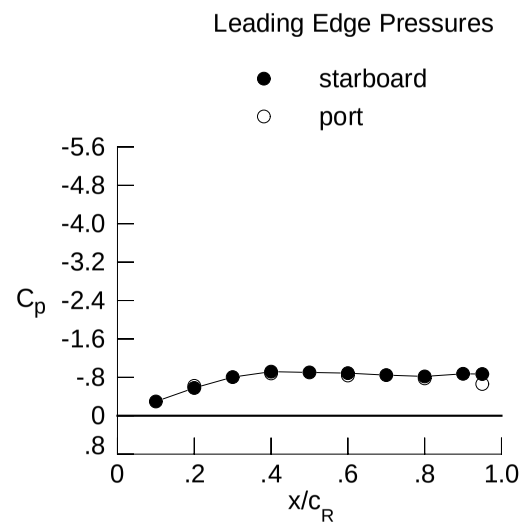

Small Radius L.E.

Run No. = 39 , Point No. = 786

$C_N$ = 0.237, $C_m$ = -0.0375

$\alpha$ = 6.3 °, $M_\infty$ = 0.799

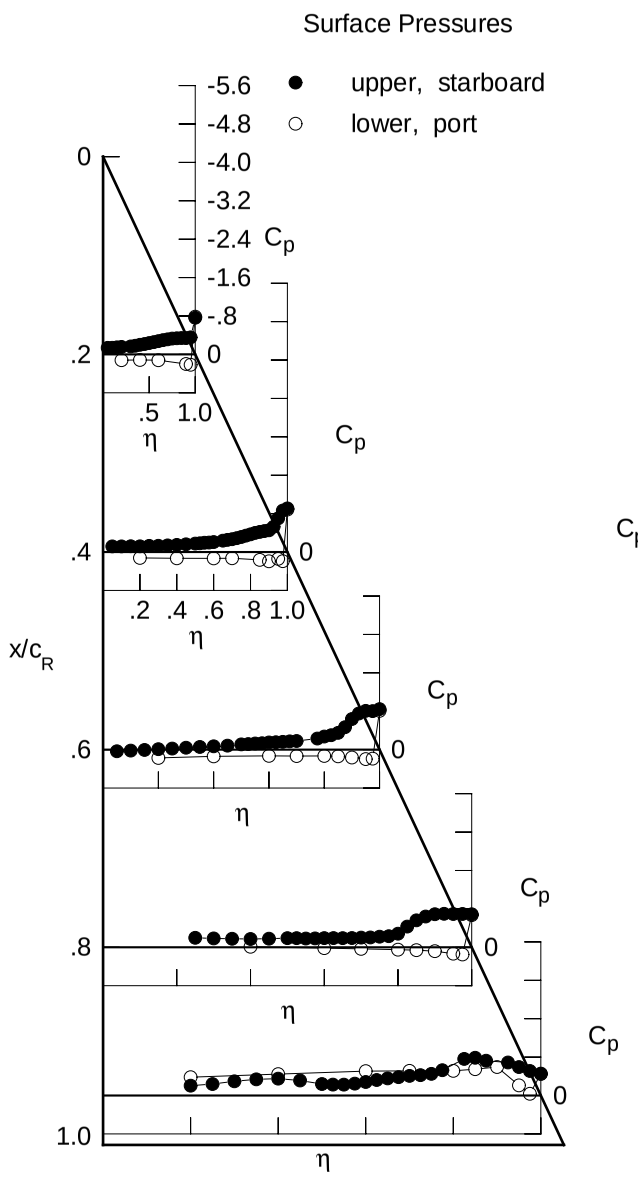
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.2969 | ******* |
| 0.20 | -0.5785 | -0.6224 |
| 0.30 | -0.8047 | ******* |
| 0.40 | -0.9181 | -0.8813 |
| 0.50 | -0.9021 | ******* |
| 0.60 | -0.8874 | -0.8384 |
| 0.70 | -0.8460 | ******* |
| 0.80 | -0.8187 | -0.7783 |
| 0.90 | -0.8732 | ******* |
| 0.95 | -0.8686 | -0.6614 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1365 | -0.1176 | 0.0337 | ******* | ******* |
| 0.100 | -0.1373 | -0.1176 | 0.0201 | ******* | ******* |
| 0.150 | -0.1471 | -0.1208 | 0.0065 | ******* | ******* |
| 0.200 | -0.1563 | -0.1191 | -0.0096 | ******* | -0.2046 |
| 0.250 | ******* | -0.1288 | -0.0226 | -0.1979 | -0.2393 |
| 0.300 | -0.1659 | -0.1304 | -0.0403 | -0.1844 | -0.2964 |
| 0.350 | -0.1803 | -0.1386 | -0.0556 | -0.1775 | -0.3369 |
| 0.400 | -0.1997 | -0.1485 | -0.0695 | -0.1731 | -0.3515 |
| 0.450 | -0.2162 | -0.1607 | -0.0832 | -0.1793 | -0.3125 |
| 0.500 | -0.2362 | -0.1757 | -0.1095 | -0.1908 | -0.2390 |
| 0.525 | ******* | -0.1823 | -0.1161 | -0.1904 | -0.2272 |
| 0.550 | -0.2550 | -0.1940 | -0.1279 | -0.1825 | -0.2266 |
| 0.575 | ******* | -0.1974 | -0.1336 | -0.1850 | -0.2472 |
| 0.600 | -0.2763 | -0.2082 | -0.1493 | -0.1910 | -0.2816 |
| 0.625 | ******* | ******* | -0.1543 | -0.1922 | -0.3229 |
| 0.650 | -0.2972 | -0.2364 | -0.1624 | -0.1907 | -0.3564 |
| 0.675 | ******* | -0.2533 | -0.1726 | -0.1924 | -0.3826 |
| 0.700 | -0.3135 | -0.2673 | -0.1803 | -0.2014 | -0.4085 |
| 0.725 | ******* | -0.2889 | ******* | -0.2049 | -0.4242 |
| 0.750 | -0.3298 | -0.3139 | ******* | -0.2205 | -0.4510 |
| 0.775 | ******* | -0.3415 | -0.2310 | -0.2314 | -0.5269 |
| 0.800 | -0.3359 | -0.3685 | -0.2730 | -0.2831 | ******* |
| 0.825 | ******* | -0.3983 | -0.3010 | -0.4311 | -0.7624 |
| 0.850 | -0.3405 | -0.4196 | -0.3496 | -0.5614 | -0.7864 |
| 0.875 | ******* | -0.4371 | -0.4674 | -0.6410 | -0.7251 |
| 0.900 | -0.3401 | -0.4524 | -0.6380 | -0.6884 | ******* |
| 0.925 | ******* | -0.5259 | -0.7531 | -0.6976 | -0.6878 |
| 0.950 | -0.3550 | -0.7012 | -0.8080 | -0.6934 | -0.5930 |
| 0.975 | ******* | -0.8638 | -0.8024 | -0.6943 | -0.5113 |
| 1.000 | -0.7631 | -0.9089 | -0.8438 | -0.6878 | -0.4559 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1211 | 0.1226 | 0.1725 | ******* | -0.3818 |
| -0.400 | 0.1157 | 0.1304 | 0.1396 | -0.0113 | -0.4460 |
| -0.600 | 0.1213 | 0.1319 | 0.1297 | 0.0172 | -0.5080 |
| -0.700 | ******* | 0.1296 | 0.1336 | 0.0330 | -0.5133 |
| -0.800 | ******* | ******* | 0.1309 | 0.0496 | -0.5140 |
| -0.850 | ******* | 0.1635 | 0.1390 | 0.0596 | -0.5486 |
| -0.900 | 0.1999 | 0.1930 | 0.1640 | 0.0811 | -0.5932 |
| -0.950 | 0.2156 | 0.1418 | 0.1968 | 0.1331 | -0.2116 |
| -0.975 | ******* | 0.1902 | 0.1873 | 0.1495 | -0.0359 |
| -1.000 | -0.7854 | -0.8853 | -0.8083 | -0.6696 | -0.4489 |



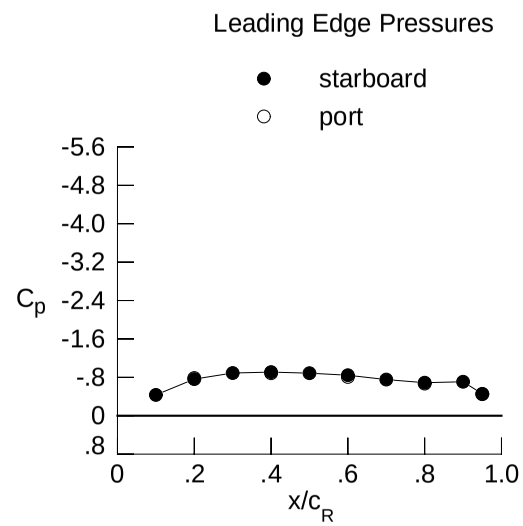

Small Radius L.E.

Run No. = 39 , Point No. = 787

$C_N$ = 0.296, $C_m$ = -0.0524

$\alpha$ = 7.3 °, $M_\infty$ = 0.800

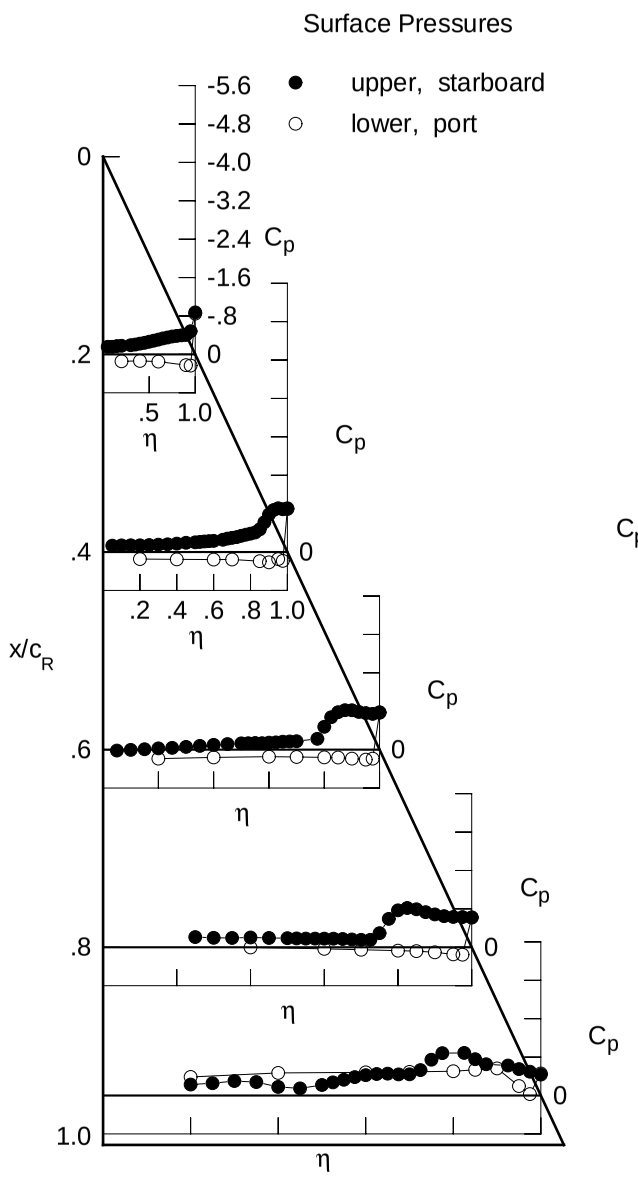
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.4339 | ******* |
| 0.20 | -0.7631 | -0.7854 |
| 0.30 | -0.8898 | ******* |
| 0.40 | -0.9089 | -0.8853 |
| 0.50 | -0.8866 | ******* |
| 0.60 | -0.8438 | -0.8083 |
| 0.70 | -0.7533 | ******* |
| 0.80 | -0.6878 | -0.6696 |
| 0.90 | -0.7080 | ******* |
| 0.95 | -0.4559 | -0.4489 |

# Table D3. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1586 | -0.1325 | 0.0189 | ******* | ******* |
| 0.100 | -0.1588 | -0.1383 | 0.0047 | ******* | ******* |
| 0.150 | -0.1729 | -0.1404 | -0.0081 | ******* | ******* |
| 0.200 | -0.1793 | -0.1401 | -0.0267 | ******* | -0.2292 |
| 0.250 | ******* | -0.1458 | -0.0377 | -0.2130 | -0.2559 |
| 0.300 | -0.1910 | -0.1537 | -0.0578 | -0.1980 | -0.3013 |
| 0.350 | -0.2052 | -0.1608 | -0.0780 | -0.1942 | -0.2798 |
| 0.400 | -0.2243 | -0.1755 | -0.1002 | -0.2041 | -0.1794 |
| 0.450 | -0.2418 | -0.1926 | -0.1158 | -0.1944 | -0.1482 |
| 0.500 | -0.2640 | -0.2021 | -0.1312 | -0.1897 | -0.2191 |
| 0.525 | ******* | -0.2102 | -0.1339 | -0.1848 | -0.2739 |
| 0.550 | -0.2858 | -0.2199 | -0.1387 | -0.1811 | -0.3278 |
| 0.575 | ******* | -0.2275 | -0.1343 | -0.1806 | -0.3830 |
| 0.600 | -0.3081 | -0.2324 | -0.1452 | -0.1802 | -0.4243 |
| 0.625 | ******* | ******* | -0.1509 | -0.1790 | -0.4478 |
| 0.650 | -0.3331 | -0.2558 | -0.1654 | -0.1725 | -0.4550 |
| 0.675 | ******* | -0.2803 | -0.1705 | -0.1624 | -0.4403 |
| 0.700 | -0.3518 | -0.2958 | -0.1750 | -0.1550 | -0.4415 |
| 0.725 | ******* | -0.3114 | ******* | -0.1550 | -0.5294 |
| 0.750 | -0.3729 | -0.3383 | ******* | -0.2948 | -0.7460 |
| 0.775 | ******* | -0.3613 | -0.2254 | -0.5918 | -0.8828 |
| 0.800 | -0.3859 | -0.3834 | -0.4761 | -0.7698 | ******* |
| 0.825 | ******* | -0.4073 | -0.6754 | -0.8183 | -0.8871 |
| 0.850 | -0.3966 | -0.4718 | -0.7804 | -0.7917 | -0.7568 |
| 0.875 | ******* | -0.6195 | -0.8218 | -0.7321 | -0.6511 |
| 0.900 | -0.4047 | -0.7828 | -0.8208 | -0.6847 | ******* |
| 0.925 | ******* | -0.8753 | -0.7858 | -0.6489 | -0.6251 |
| 0.950 | -0.4833 | -0.9123 | -0.7614 | -0.6317 | -0.5507 |
| 0.975 | ******* | -0.8910 | -0.7448 | -0.6293 | -0.4959 |
| 1.000 | -0.8749 | -0.9113 | -0.7793 | -0.6230 | -0.4357 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1436 | 0.1461 | 0.1876 | ******* | -0.3861 |
| -0.400 | 0.1358 | 0.1525 | 0.1619 | 0.0034 | -0.4705 |
| -0.600 | 0.1499 | 0.1568 | 0.1467 | 0.0322 | -0.4825 |
| -0.700 | ******* | 0.1552 | 0.1528 | 0.0509 | -0.4924 |
| -0.800 | ******* | ******* | 0.1611 | 0.0701 | -0.5056 |
| -0.850 | ******* | 0.1904 | 0.1643 | 0.0803 | -0.5351 |
| -0.900 | 0.2243 | 0.2145 | 0.1871 | 0.1045 | -0.5649 |
| -0.950 | 0.2332 | 0.1464 | 0.2084 | 0.1474 | -0.1964 |
| -0.975 | ******* | 0.1842 | 0.1873 | 0.1532 | -0.0295 |
| -1.000 | -0.8492 | -0.8962 | -0.7682 | -0.6200 | -0.4594 |



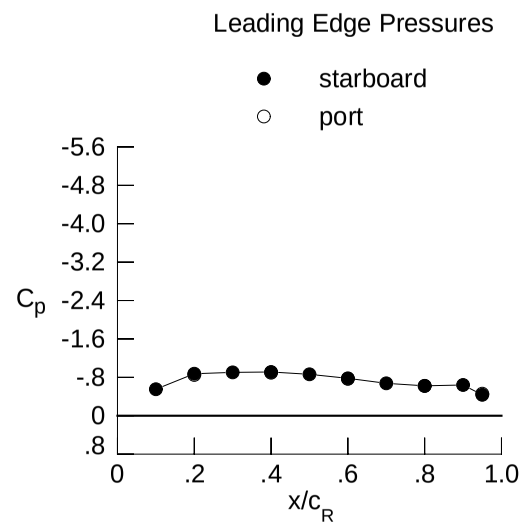

Small Radius L.E.

Run No. = 39 , Point No. = 788

$C_N$ = 0.351, $C_m$ = -0.0621

$\alpha$ = 8.3 °, $M_\infty$ = 0.798

$R_{mac}$ = $6.0 \times 10^6$

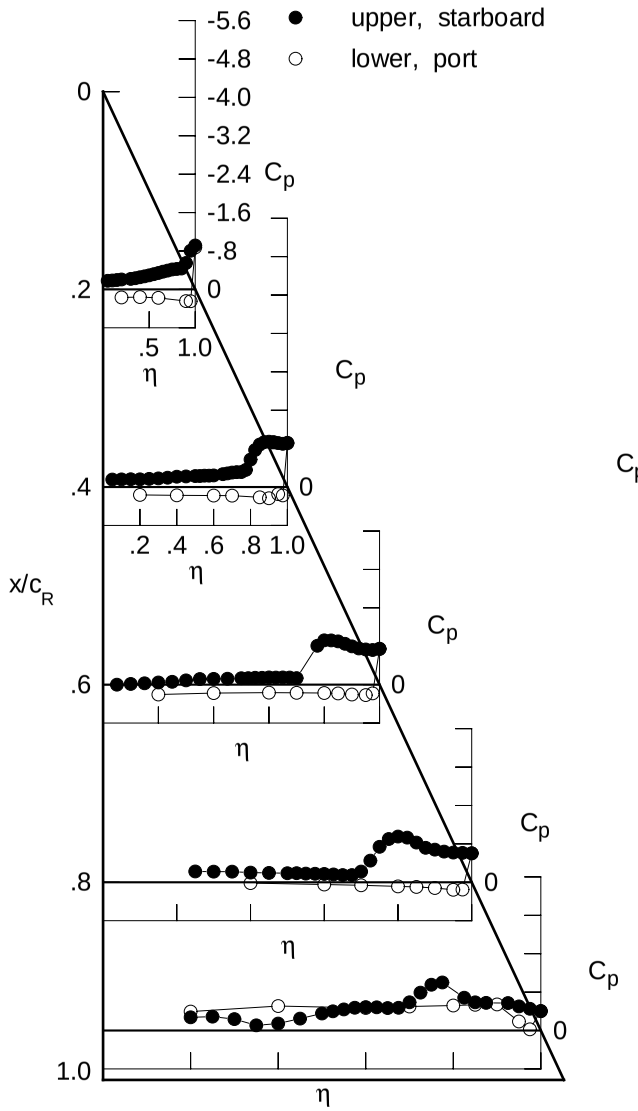



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.5521 | ******* |
| 0.20 | -0.8749 | -0.8492 |
| 0.30 | -0.9032 | ******* |
| 0.40 | -0.9113 | -0.8962 |
| 0.50 | -0.8628 | ******* |
| 0.60 | -0.7793 | -0.7682 |
| 0.70 | -0.6751 | ******* |
| 0.80 | -0.6230 | -0.6200 |
| 0.90 | -0.6404 | ******* |
| 0.95 | -0.4357 | -0.4594 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1794 | -0.1563 | 0.0005 | ******* | ******* |
| 0.100 | -0.1859 | -0.1593 | -0.0146 | ******* | ******* |
| 0.150 | -0.1955 | -0.1621 | -0.0281 | ******* | ******* |
| 0.200 | -0.2063 | -0.1607 | -0.0452 | ******* | -0.2749 |
| 0.250 | ******* | -0.1708 | -0.0591 | -0.2254 | -0.2888 |
| 0.300 | -0.2181 | -0.1802 | -0.0887 | -0.2214 | -0.2374 |
| 0.350 | -0.2328 | -0.1947 | -0.1169 | -0.2215 | -0.1076 |
| 0.400 | -0.2528 | -0.2156 | -0.1200 | -0.2017 | -0.1449 |
| 0.450 | -0.2716 | -0.2210 | -0.1236 | -0.1951 | -0.2483 |
| 0.500 | -0.2925 | -0.2284 | -0.1335 | -0.1890 | -0.3546 |
| 0.525 | ******* | -0.2300 | -0.1350 | -0.1897 | -0.4003 |
| 0.550 | -0.3165 | -0.2371 | -0.1428 | -0.1807 | -0.4390 |
| 0.575 | ******* | -0.2369 | -0.1420 | -0.1780 | -0.4744 |
| 0.600 | -0.3420 | -0.2419 | -0.1502 | -0.1733 | -0.4869 |
| 0.625 | ******* | ******* | -0.1469 | -0.1629 | -0.4831 |
| 0.650 | -0.3688 | -0.2677 | -0.1493 | -0.1503 | -0.4680 |
| 0.675 | ******* | -0.2839 | -0.1476 | -0.1501 | -0.4738 |
| 0.700 | -0.3912 | -0.3018 | -0.1358 | -0.2231 | -0.5876 |
| 0.725 | ******* | -0.3104 | ******* | -0.4511 | -0.7885 |
| 0.750 | -0.4154 | -0.3118 | ******* | -0.7393 | -0.9536 |
| 0.775 | ******* | -0.3574 | -0.8096 | -0.9014 | -1.0006 |
| 0.800 | -0.4260 | -0.5719 | -0.9232 | -0.9529 | ******* |
| 0.825 | ******* | -0.7714 | -0.9214 | -0.9305 | -0.6831 |
| 0.850 | -0.4342 | -0.8860 | -0.9016 | -0.8274 | -0.5871 |
| 0.875 | ******* | -0.9362 | -0.8514 | -0.7187 | -0.5756 |
| 0.900 | -0.5502 | -0.9445 | -0.7978 | -0.6802 | ******* |
| 0.925 | ******* | -0.9372 | -0.7539 | -0.6395 | -0.5717 |
| 0.950 | -0.8046 | -0.9165 | -0.7325 | -0.6189 | -0.5024 |
| 0.975 | ******* | -0.9007 | -0.7218 | -0.6127 | -0.4530 |
| 1.000 | -0.9145 | -0.9219 | -0.7489 | -0.6028 | -0.4016 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1680 | 0.1643 | 0.2059 | ******* | -0.3943 |
| -0.400 | 0.1602 | 0.1730 | 0.1757 | 0.0165 | -0.5098 |
| -0.600 | 0.1763 | 0.1774 | 0.1664 | 0.0466 | -0.4697 |
| -0.700 | ******* | 0.1790 | 0.1701 | 0.0625 | -0.5001 |
| -0.800 | ******* | ******* | 0.1747 | 0.0854 | -0.5205 |
| -0.850 | ******* | 0.2142 | 0.1831 | 0.0966 | -0.5363 |
| -0.900 | 0.2437 | 0.2332 | 0.2054 | 0.1191 | -0.5433 |
| -0.950 | 0.2462 | 0.1469 | 0.2178 | 0.1560 | -0.1877 |
| -0.975 | ******* | 0.1748 | 0.1819 | 0.1509 | -0.0247 |
| -1.000 | -0.8732 | -0.9112 | -0.7414 | -0.6051 | -0.4074 |

Surface Pressures




Small Radius L.E.

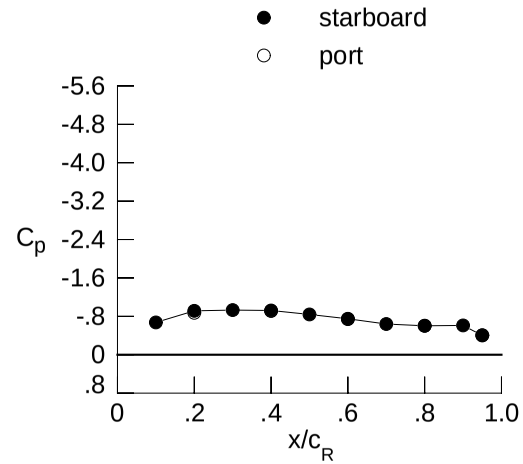
Run No. = 39 , Point No. = 789

$C_N$ = 0.405, $C_m$ = -0.0705

$\alpha$ = 9.3 °, $M_\infty$ = 0.799

$R_{mac}$ = $6.0 \times 10^6$

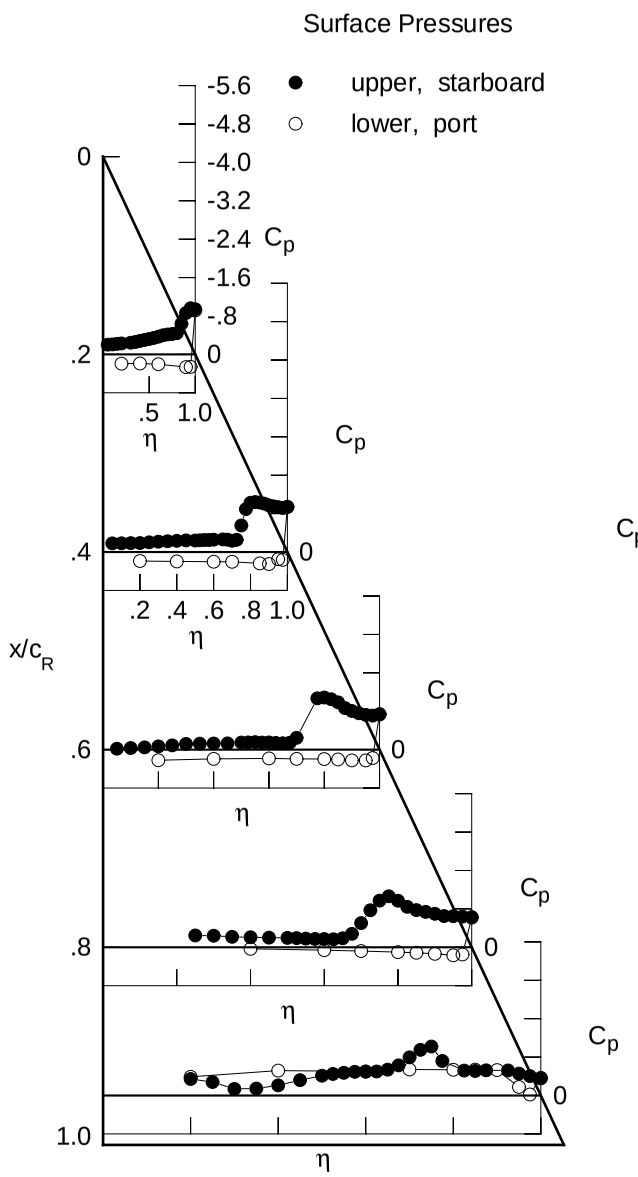
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.6728 | ******* |
| 0.20 | -0.9145 | -0.8732 |
| 0.30 | -0.9300 | ******* |
| 0.40 | -0.9219 | -0.9112 |
| 0.50 | -0.8393 | ******* |
| 0.60 | -0.7489 | -0.7414 |
| 0.70 | -0.6397 | ******* |
| 0.80 | -0.6028 | -0.6051 |
| 0.90 | -0.6104 | ******* |
| 0.95 | -0.4016 | -0.4074 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2023 | -0.1810 | -0.0195 | ******* | ******* |
| 0.100 | -0.2078 | -0.1820 | -0.0340 | ******* | ******* |
| 0.150 | -0.2185 | -0.1855 | -0.0472 | ******* | ******* |
| 0.200 | -0.2281 | -0.1873 | -0.0683 | ******* | -0.3442 |
| 0.250 | ******* | -0.2027 | -0.0889 | -0.2464 | -0.2807 |
| 0.300 | -0.2436 | -0.2157 | -0.1185 | -0.2404 | -0.1379 |
| 0.350 | -0.2580 | -0.2247 | -0.1251 | -0.2172 | -0.1452 |
| 0.400 | -0.2810 | -0.2335 | -0.1277 | -0.2087 | -0.2114 |
| 0.450 | -0.3007 | -0.2424 | -0.1302 | -0.2011 | -0.3198 |
| 0.500 | -0.3207 | -0.2400 | -0.1484 | -0.1957 | -0.4126 |
| 0.525 | ******* | -0.2444 | -0.1507 | -0.1912 | -0.4490 |
| 0.550 | -0.3421 | -0.2501 | -0.1557 | -0.1810 | -0.4726 |
| 0.575 | ******* | -0.2507 | -0.1477 | -0.1742 | -0.4938 |
| 0.600 | -0.3691 | -0.2572 | -0.1504 | -0.1717 | -0.4972 |
| 0.625 | ******* | ******* | -0.1399 | -0.1662 | -0.5001 |
| 0.650 | -0.3973 | -0.2636 | -0.1331 | -0.1876 | -0.5382 |
| 0.675 | ******* | -0.2578 | -0.1434 | -0.2804 | -0.6279 |
| 0.700 | -0.4155 | -0.2356 | -0.2461 | -0.5029 | -0.7953 |
| 0.725 | ******* | -0.2552 | ******* | -0.7708 | -0.9508 |
| 0.750 | -0.4246 | -0.5538 | ******* | -0.9721 | -1.0210 |
| 0.775 | ******* | -0.8943 | -1.0690 | -1.0624 | -0.7201 |
| 0.800 | -0.4413 | -1.0261 | -1.0855 | -0.9705 | ******* |
| 0.825 | ******* | -1.0417 | -1.0493 | -0.8436 | -0.5191 |
| 0.850 | -0.6369 | -1.0315 | -0.9860 | -0.7743 | -0.5111 |
| 0.875 | ******* | -1.0082 | -0.8653 | -0.7373 | -0.5251 |
| 0.900 | -0.8626 | -0.9721 | -0.8058 | -0.6975 | ******* |
| 0.925 | ******* | -0.9522 | -0.7582 | -0.6505 | -0.5221 |
| 0.950 | -0.9616 | -0.9343 | -0.7250 | -0.6487 | -0.4571 |
| 0.975 | ******* | -0.9189 | -0.7086 | -0.6393 | -0.4045 |
| 1.000 | -0.9404 | -0.9370 | -0.7309 | -0.6278 | -0.3567 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1937 | 0.1875 | 0.2212 | ******* | -0.3897 |
| -0.400 | 0.1892 | 0.1958 | 0.1926 | 0.0317 | -0.5189 |
| -0.600 | 0.2045 | 0.2015 | 0.1831 | 0.0602 | -0.5010 |
| -0.700 | ******* | 0.2036 | 0.1921 | 0.0788 | -0.5427 |
| -0.800 | ******* | ******* | 0.1956 | 0.1009 | -0.5358 |
| -0.850 | ******* | 0.2366 | 0.2043 | 0.1144 | -0.5389 |
| -0.900 | 0.2646 | 0.2503 | 0.2238 | 0.1359 | -0.5296 |
| -0.950 | 0.2602 | 0.1495 | 0.2239 | 0.1674 | -0.1784 |
| -0.975 | ******* | 0.1630 | 0.1742 | 0.1496 | -0.0219 |
| -1.000 | -0.9163 | -0.9431 | -0.7407 | -0.6183 | -0.3688 |



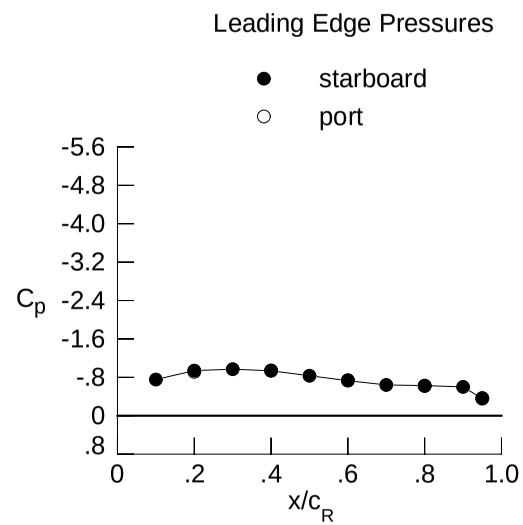

Small Radius L.E.

Run No. = 39 , Point No. = 790

$C_N$ = 0.459, $C_m$ = -0.0790

$\alpha$ = 10.4 °, $M_\infty$ = 0.799

$R_{mac}$ = $6.0 \times 10^6$

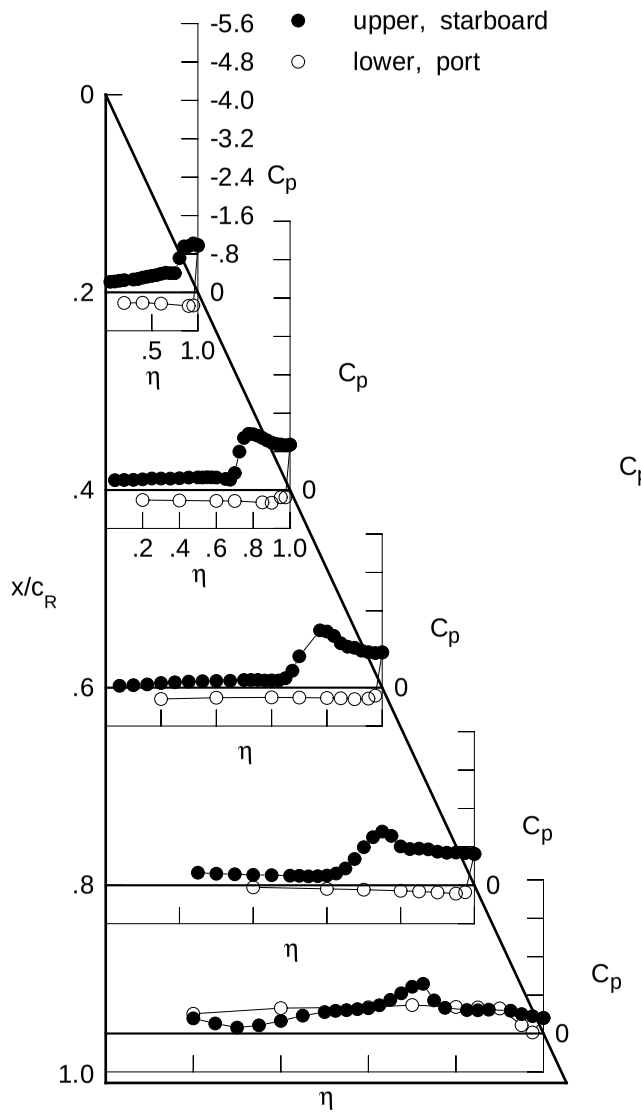



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.7534 | ******* |
| 0.20 | -0.9404 | -0.9163 |
| 0.30 | -0.9694 | ******* |
| 0.40 | -0.9370 | -0.9431 |
| 0.50 | -0.8330 | ******* |
| 0.60 | -0.7309 | -0.7407 |
| 0.70 | -0.6415 | ******* |
| 0.80 | -0.6278 | -0.6183 |
| 0.90 | -0.6008 | ******* |
| 0.95 | -0.3567 | -0.3688 |

# Table D3. Continued.

| η | x/c_R .2 C_p,u | x/c_R .4 C_p,u | x/c_R .6 C_p,u | x/c_R .8 C_p,u | x/c_R .95 C_p,u |
|---|---|---|---|---|---|
| 0.050 | -0.2216 | -0.2053 | -0.0384 | ******* | ******* |
| 0.100 | -0.2273 | -0.2093 | -0.0510 | ******* | ******* |
| 0.150 | -0.2430 | -0.2118 | -0.0668 | ******* | ******* |
| 0.200 | -0.2545 | -0.2221 | -0.0958 | ******* | -0.3154 |
| 0.250 | ******* | -0.2397 | -0.1111 | -0.2625 | -0.2091 |
| 0.300 | -0.2678 | -0.2393 | -0.1258 | -0.2409 | -0.1230 |
| 0.350 | -0.2801 | -0.2386 | -0.1337 | -0.2295 | -0.1696 |
| 0.400 | -0.3073 | -0.2460 | -0.1392 | -0.2159 | -0.2624 |
| 0.450 | -0.3264 | -0.2597 | -0.1432 | -0.2102 | -0.3721 |
| 0.500 | -0.3440 | -0.2636 | -0.1592 | -0.2001 | -0.4467 |
| 0.525 | ******* | -0.2619 | -0.1590 | -0.1978 | -0.4720 |
| 0.550 | -0.3601 | -0.2665 | -0.1596 | -0.1864 | -0.4864 |
| 0.575 | ******* | -0.2641 | -0.1482 | -0.1897 | -0.5069 |
| 0.600 | -0.3874 | -0.2608 | -0.1515 | -0.2028 | -0.5264 |
| 0.625 | ******* | ******* | -0.1491 | -0.2446 | -0.5878 |
| 0.650 | -0.4087 | -0.2313 | -0.1967 | -0.3504 | -0.7007 |
| 0.675 | ******* | -0.2153 | -0.3531 | -0.5469 | -0.8373 |
| 0.700 | -0.3997 | -0.3546 | -0.6528 | -0.7939 | -0.9746 |
| 0.725 | ******* | -0.8002 | ******* | -1.0016 | -1.0350 |
| 0.750 | -0.4005 | -1.0856 | ******* | -1.1191 | -0.6892 |
| 0.775 | ******* | -1.1721 | -1.1938 | -1.0287 | -0.5355 |
| 0.800 | -0.7145 | -1.1624 | -1.1690 | -0.8093 | ******* |
| 0.825 | ******* | -1.1306 | -1.0779 | -0.7551 | -0.4886 |
| 0.850 | -0.9586 | -1.0861 | -0.9244 | -0.7637 | -0.4837 |
| 0.875 | ******* | -1.0352 | -0.8517 | -0.7489 | -0.4967 |
| 0.900 | -0.9640 | -0.9882 | -0.8308 | -0.6999 | ******* |
| 0.925 | ******* | -0.9600 | -0.7706 | -0.6785 | -0.4749 |
| 0.950 | -1.0208 | -0.9485 | -0.7394 | -0.6813 | -0.4042 |
| 0.975 | ******* | -0.9311 | -0.7211 | -0.6705 | -0.3614 |
| 1.000 | -0.9883 | -0.9434 | -0.7349 | -0.6562 | -0.3225 |
| | C_p,l | C_p,l | C_p,l | C_p,l | C_p,l |
| -0.200 | 0.2204 | 0.2079 | 0.2370 | ******* | -0.4110 |
| -0.400 | 0.2161 | 0.2181 | 0.2097 | 0.0428 | -0.5289 |
| -0.600 | 0.2341 | 0.2261 | 0.2034 | 0.0743 | -0.5466 |
| -0.700 | ******* | 0.2280 | 0.2068 | 0.0923 | -0.5927 |
| -0.800 | ******* | ******* | 0.2151 | 0.1141 | -0.5525 |
| -0.850 | ******* | 0.2580 | 0.2219 | 0.1281 | -0.5434 |
| -0.900 | 0.2826 | 0.2651 | 0.2399 | 0.1488 | -0.5224 |
| -0.950 | 0.2723 | 0.1504 | 0.2277 | 0.1737 | -0.1726 |
| -0.975 | ******* | 0.1517 | 0.1664 | 0.1442 | -0.0213 |
| -1.000 | -0.9678 | -0.9456 | -0.7327 | -0.6506 | -0.3252 |

Surface Pressures




Small Radius L.E.

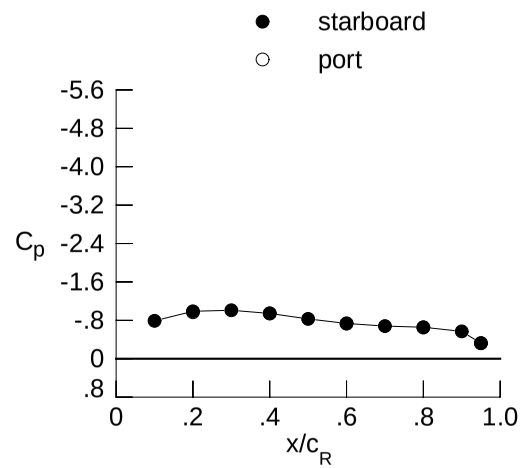
Run No. = 39 , Point No. = 791

$C_N$ = 0.505, $C_m$ = -0.0812

$\alpha$ = 11.4 °, $M_\infty$ = 0.799

$R_{mac}$ = $6.0 \times 10^6$

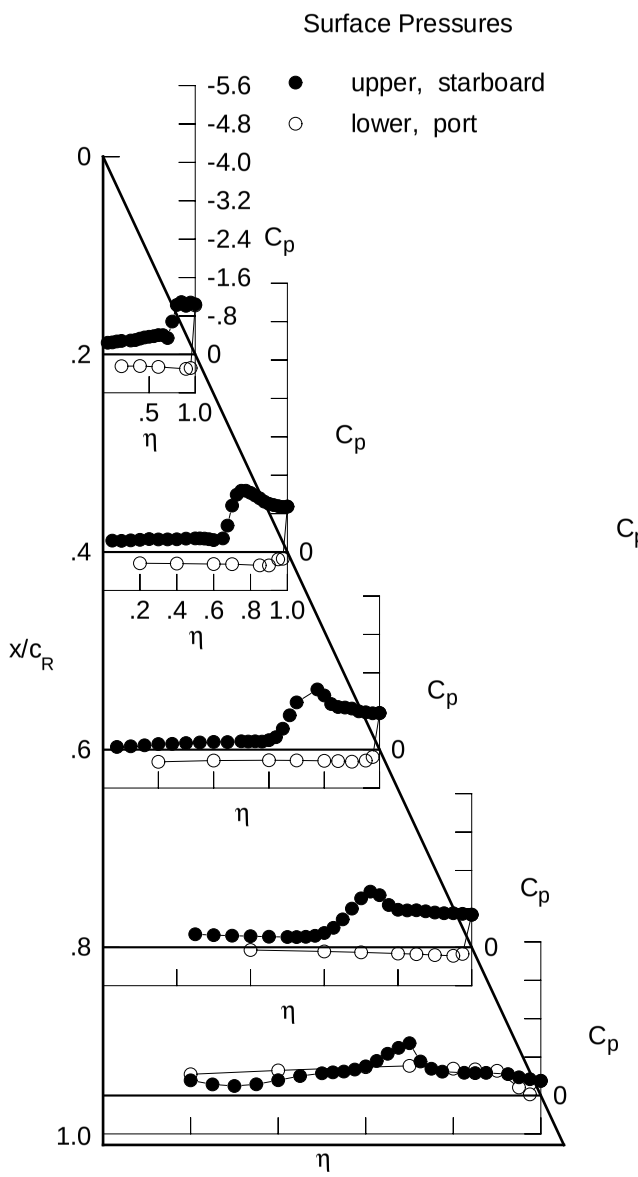
Leading Edge Pressures




| x/c_R | starb'd C_p | port C_p |
|---|---|---|
| 0.10 | -0.7898 | ******* |
| 0.20 | -0.9883 | -0.9678 |
| 0.30 | -1.0098 | ******* |
| 0.40 | -0.9434 | -0.9456 |
| 0.50 | -0.8296 | ******* |
| 0.60 | -0.7349 | -0.7327 |
| 0.70 | -0.6801 | ******* |
| 0.80 | -0.6562 | -0.6506 |
| 0.90 | -0.5694 | ******* |
| 0.95 | -0.3225 | -0.3252 |

# Table D3. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2426 | -0.2376 | -0.0559 | ******* | ******* |
| 0.100 | -0.2500 | -0.2328 | -0.0699 | ******* | ******* |
| 0.150 | -0.2692 | -0.2432 | -0.0907 | ******* | ******* |
| 0.200 | -0.2810 | -0.2547 | -0.1166 | ******* | -0.3160 |
| 0.250 | ******* | -0.2701 | -0.1210 | -0.2709 | -0.2309 |
| 0.300 | -0.2886 | -0.2624 | -0.1368 | -0.2528 | -0.1986 |
| 0.350 | -0.2986 | -0.2630 | -0.1495 | -0.2415 | -0.2335 |
| 0.400 | -0.3278 | -0.2655 | -0.1604 | -0.2312 | -0.3186 |
| 0.450 | -0.3527 | -0.2789 | -0.1574 | -0.2201 | -0.4058 |
| 0.500 | -0.3675 | -0.2842 | -0.1745 | -0.2142 | -0.4631 |
| 0.525 | ******* | -0.2843 | -0.1690 | -0.2126 | -0.4826 |
| 0.550 | -0.3792 | -0.2796 | -0.1734 | -0.2181 | -0.4995 |
| 0.575 | ******* | -0.2674 | -0.1673 | -0.2394 | -0.5404 |
| 0.600 | -0.4014 | -0.2487 | -0.1976 | -0.2977 | -0.6074 |
| 0.625 | ******* | ******* | -0.2591 | -0.4055 | -0.7200 |
| 0.650 | -0.4010 | -0.2841 | -0.4363 | -0.5819 | -0.8693 |
| 0.675 | ******* | -0.5509 | -0.7150 | -0.8053 | -0.9930 |
| 0.700 | -0.3404 | -0.9672 | -0.9841 | -1.0195 | -1.0897 |
| 0.725 | ******* | -1.1937 | ******* | -1.1595 | -0.7085 |
| 0.750 | -0.6837 | -1.2766 | ******* | -1.0859 | -0.5576 |
| 0.775 | ******* | -1.2771 | -1.2545 | -0.8807 | -0.4965 |
| 0.800 | -1.0299 | -1.2328 | -1.1288 | -0.7816 | ******* |
| 0.825 | ******* | -1.1792 | -0.9503 | -0.7681 | -0.4738 |
| 0.850 | -1.0896 | -1.1182 | -0.8884 | -0.7709 | -0.4664 |
| 0.875 | ******* | -1.0493 | -0.8771 | -0.7499 | -0.4723 |
| 0.900 | -1.0119 | -1.0044 | -0.8563 | -0.7241 | ******* |
| 0.925 | ******* | -0.9795 | -0.7976 | -0.7097 | -0.4458 |
| 0.950 | -1.0803 | -0.9571 | -0.7784 | -0.7094 | -0.3788 |
| 0.975 | ******* | -0.9393 | -0.7577 | -0.6970 | -0.3403 |
| 1.000 | -1.0434 | -0.9470 | -0.7657 | -0.6776 | -0.3075 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2462 | 0.2336 | 0.2540 | ******* | -0.4423 |
| -0.400 | 0.2424 | 0.2403 | 0.2273 | 0.0568 | -0.5224 |
| -0.600 | 0.2611 | 0.2504 | 0.2211 | 0.0868 | -0.5905 |
| -0.700 | ******* | 0.2527 | 0.2251 | 0.1059 | -0.6175 |
| -0.800 | ******* | ******* | 0.2328 | 0.1303 | -0.5594 |
| -0.850 | ******* | 0.2776 | 0.2382 | 0.1433 | -0.5443 |
| -0.900 | 0.3013 | 0.2789 | 0.2512 | 0.1621 | -0.5144 |
| -0.950 | 0.2838 | 0.1516 | 0.2280 | 0.1773 | -0.1684 |
| -0.975 | ******* | 0.1401 | 0.1540 | 0.1372 | -0.0239 |
| -1.000 | -1.0197 | -0.9453 | -0.7581 | -0.6803 | -0.3042 |



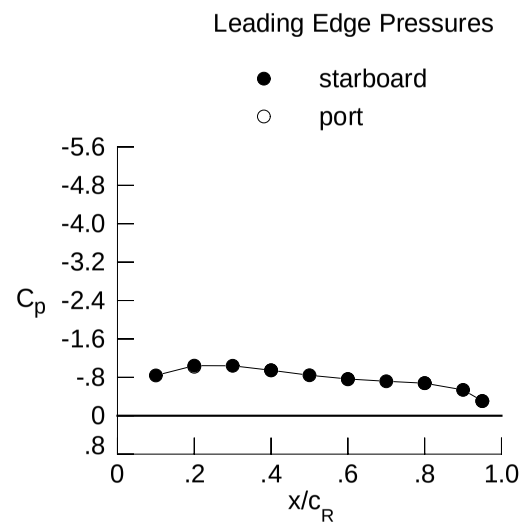

Small Radius L.E.

Run No. = 39 , Point No. = 792

$C_N$ = 0.560, $C_m$ = -0.0899

$\alpha$ = 12.4 °, $M_\infty$ = 0.798

$R_{mac}$ = $6.0 \times 10^6$

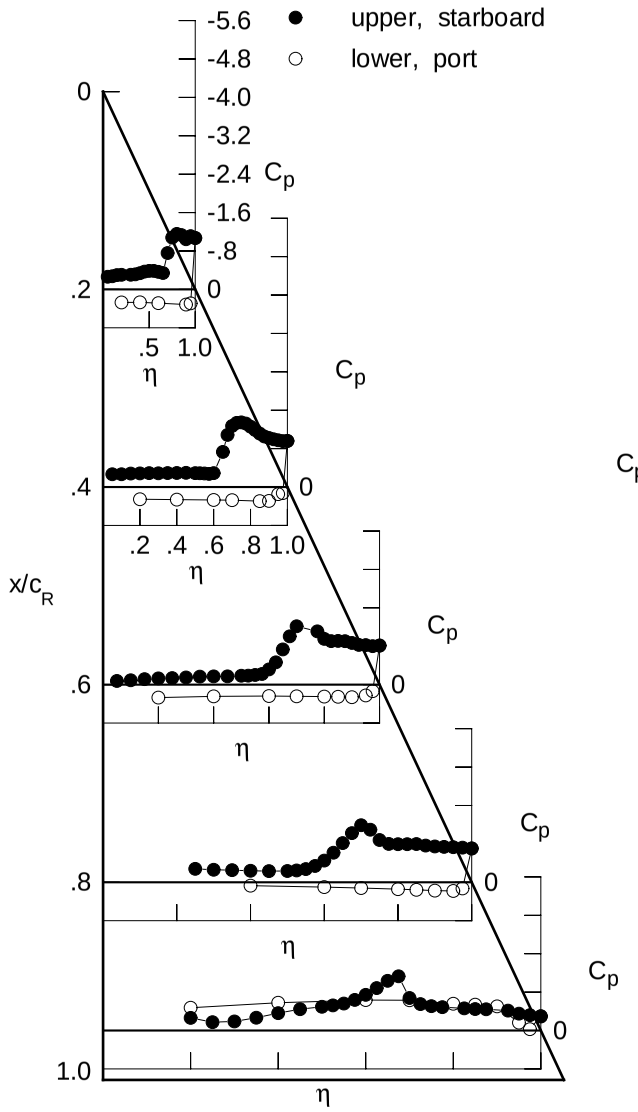



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.8393 | ******* |
| 0.20 | -1.0434 | -1.0197 |
| 0.30 | -1.0406 | ******* |
| 0.40 | -0.9470 | -0.9453 |
| 0.50 | -0.8433 | ******* |
| 0.60 | -0.7657 | -0.7581 |
| 0.70 | -0.7179 | ******* |
| 0.80 | -0.6776 | -0.6803 |
| 0.90 | -0.5384 | ******* |
| 0.95 | -0.3075 | -0.3042 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2630 | -0.2666 | -0.0768 | ******* | ******* |
| 0.100 | -0.2740 | -0.2667 | -0.0915 | ******* | ******* |
| 0.150 | -0.2979 | -0.2808 | -0.1143 | ******* | ******* |
| 0.200 | -0.3039 | -0.2839 | -0.1302 | ******* | -0.2629 |
| 0.250 | ******* | -0.2896 | -0.1367 | -0.2799 | -0.1738 |
| 0.300 | -0.3046 | -0.2862 | -0.1500 | -0.2607 | -0.1888 |
| 0.350 | -0.3137 | -0.2909 | -0.1671 | -0.2526 | -0.2665 |
| 0.400 | -0.3376 | -0.2926 | -0.1719 | -0.2396 | -0.3617 |
| 0.450 | -0.3704 | -0.2957 | -0.1730 | -0.2331 | -0.4443 |
| 0.500 | -0.3860 | -0.2899 | -0.1856 | -0.2349 | -0.4947 |
| 0.525 | ******* | -0.2870 | -0.1868 | -0.2461 | -0.5236 |
| 0.550 | -0.3853 | -0.2828 | -0.2016 | -0.2751 | -0.5619 |
| 0.575 | ******* | -0.2735 | -0.2221 | -0.3397 | -0.6375 |
| 0.600 | -0.3652 | -0.2893 | -0.3173 | -0.4522 | -0.7433 |
| 0.625 | ******* | ******* | -0.4645 | -0.6163 | -0.8840 |
| 0.650 | -0.3418 | -0.7319 | -0.7337 | -0.8166 | -1.0356 |
| 0.675 | ******* | -1.0858 | -1.0061 | -1.0239 | -1.1296 |
| 0.700 | -0.7578 | -1.2718 | -1.2161 | -1.1890 | -0.6777 |
| 0.725 | ******* | -1.3368 | ******* | -1.0952 | -0.5503 |
| 0.750 | -1.0796 | -1.3474 | ******* | -0.8810 | -0.5071 |
| 0.775 | ******* | -1.3225 | -1.1101 | -0.7988 | -0.4866 |
| 0.800 | -1.1559 | -1.2577 | -0.9539 | -0.7932 | ******* |
| 0.825 | ******* | -1.1881 | -0.9064 | -0.7933 | -0.4614 |
| 0.850 | -1.1318 | -1.1136 | -0.9109 | -0.7964 | -0.4472 |
| 0.875 | ******* | -1.0537 | -0.9058 | -0.7646 | -0.4421 |
| 0.900 | -1.0447 | -1.0216 | -0.8687 | -0.7465 | ******* |
| 0.925 | ******* | -0.9948 | -0.8277 | -0.7375 | -0.4148 |
| 0.950 | -1.1093 | -0.9743 | -0.8236 | -0.7311 | -0.3510 |
| 0.975 | ******* | -0.9569 | -0.8013 | -0.7217 | -0.3201 |
| 1.000 | -1.0732 | -0.9611 | -0.8109 | -0.7054 | -0.2914 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2721 | 0.2540 | 0.2699 | ******* | -0.4742 |
| -0.400 | 0.2695 | 0.2622 | 0.2443 | 0.0704 | -0.5786 |
| -0.600 | 0.2863 | 0.2699 | 0.2374 | 0.1003 | -0.6343 |
| -0.700 | ******* | 0.2740 | 0.2432 | 0.1198 | -0.6302 |
| -0.800 | ******* | ******* | 0.2486 | 0.1429 | -0.5579 |
| -0.850 | ******* | 0.2938 | 0.2528 | 0.1568 | -0.5381 |
| -0.900 | 0.3157 | 0.2893 | 0.2620 | 0.1737 | -0.5034 |
| -0.950 | 0.2905 | 0.1476 | 0.2248 | 0.1805 | -0.1644 |
| -0.975 | ******* | 0.1261 | 0.1359 | 0.1281 | -0.0279 |
| -1.000 | -1.0679 | -0.9592 | -0.8171 | -0.7042 | -0.3002 |

Surface Pressures




Small Radius L.E.

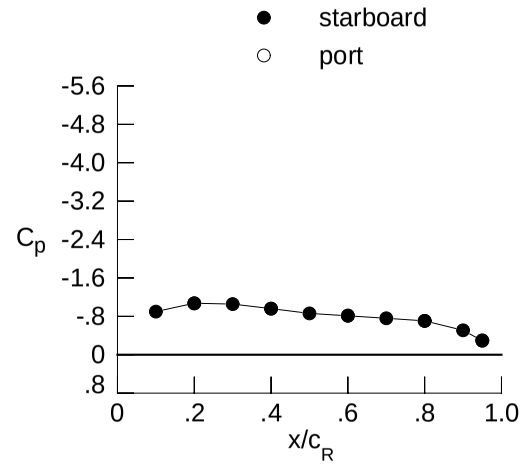
Run No. = 39 , Point No. = 793

$C_N$ = 0.606, $C_m$ = -0.0929

$\alpha$ = 13.4 °, $M_\infty$ = 0.798

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

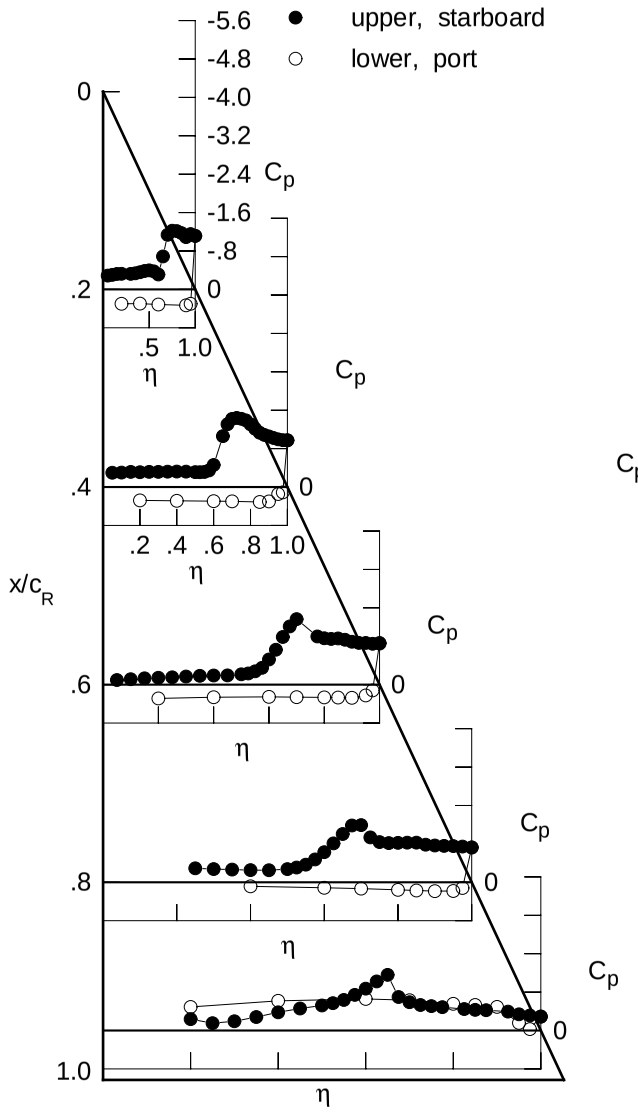



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.8985 | ******* |
| 0.20 | -1.0732 | -1.0679 |
| 0.30 | -1.0549 | ******* |
| 0.40 | -0.9611 | -0.9592 |
| 0.50 | -0.8608 | ******* |
| 0.60 | -0.8109 | -0.8171 |
| 0.70 | -0.7596 | ******* |
| 0.80 | -0.7054 | -0.7042 |
| 0.90 | -0.5088 | ******* |
| 0.95 | -0.2914 | -0.3002 |

# Table D3. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2872 | -0.2978 | -0.0964 | ******* | ******* |
| 0.100 | -0.3023 | -0.3005 | -0.1130 | ******* | ******* |
| 0.150 | -0.3219 | -0.3149 | -0.1319 | ******* | ******* |
| 0.200 | -0.3249 | -0.3084 | -0.1434 | ******* | -0.2371 |
| 0.250 | ******* | -0.3161 | -0.1525 | -0.2912 | -0.1527 |
| 0.300 | -0.3232 | -0.3161 | -0.1687 | -0.2754 | -0.1928 |
| 0.350 | -0.3350 | -0.3198 | -0.1836 | -0.2645 | -0.2805 |
| 0.400 | -0.3575 | -0.3221 | -0.1904 | -0.2534 | -0.3792 |
| 0.450 | -0.3832 | -0.3205 | -0.1927 | -0.2513 | -0.4584 |
| 0.500 | -0.3964 | -0.3104 | -0.2148 | -0.2748 | -0.5217 |
| 0.525 | ******* | -0.3088 | -0.2326 | -0.3071 | -0.5694 |
| 0.550 | -0.3757 | -0.3148 | -0.2779 | -0.3671 | -0.6368 |
| 0.575 | ******* | -0.3463 | -0.3502 | -0.4761 | -0.7420 |
| 0.600 | -0.3102 | -0.4599 | -0.5238 | -0.6271 | -0.8718 |
| 0.625 | ******* | ******* | -0.7274 | -0.8105 | -1.0221 |
| 0.650 | -0.6865 | -1.0600 | -0.9925 | -1.0055 | -1.1595 |
| 0.675 | ******* | -1.3080 | -1.2117 | -1.1833 | -0.6974 |
| 0.700 | -1.1371 | -1.4189 | -1.3649 | -1.1909 | -0.5893 |
| 0.725 | ******* | -1.4398 | ******* | -0.9352 | -0.5310 |
| 0.750 | -1.2222 | -1.4219 | ******* | -0.8375 | -0.5082 |
| 0.775 | ******* | -1.3891 | -1.0038 | -0.8164 | -0.4863 |
| 0.800 | -1.2145 | -1.3062 | -0.9667 | -0.8214 | ******* |
| 0.825 | ******* | -1.2136 | -0.9521 | -0.8253 | -0.4470 |
| 0.850 | -1.1739 | -1.1315 | -0.9624 | -0.8252 | -0.4302 |
| 0.875 | ******* | -1.0856 | -0.9349 | -0.7831 | -0.4230 |
| 0.900 | -1.0885 | -1.0547 | -0.8939 | -0.7666 | ******* |
| 0.925 | ******* | -1.0219 | -0.8697 | -0.7585 | -0.3935 |
| 0.950 | -1.1531 | -0.9934 | -0.8688 | -0.7546 | -0.3374 |
| 0.975 | ******* | -0.9767 | -0.8509 | -0.7440 | -0.3127 |
| 1.000 | -1.1147 | -0.9746 | -0.8549 | -0.7259 | -0.2872 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2997 | 0.2782 | 0.2871 | ******* | -0.4906 |
| -0.400 | 0.2964 | 0.2870 | 0.2622 | 0.0844 | -0.6180 |
| -0.600 | 0.3150 | 0.2943 | 0.2547 | 0.1143 | -0.6575 |
| -0.700 | ******* | 0.2981 | 0.2606 | 0.1317 | -0.6308 |
| -0.800 | ******* | ******* | 0.2658 | 0.1574 | -0.5562 |
| -0.850 | ******* | 0.3113 | 0.2691 | 0.1709 | -0.5322 |
| -0.900 | 0.3319 | 0.2999 | 0.2745 | 0.1844 | -0.4917 |
| -0.950 | 0.2998 | 0.1454 | 0.2245 | 0.1813 | -0.1587 |
| -0.975 | ******* | 0.1111 | 0.1202 | 0.1182 | -0.0297 |
| -1.000 | -1.1152 | -0.9725 | -0.8687 | -0.7260 | -0.2932 |

Surface Pressures




Small Radius L.E.

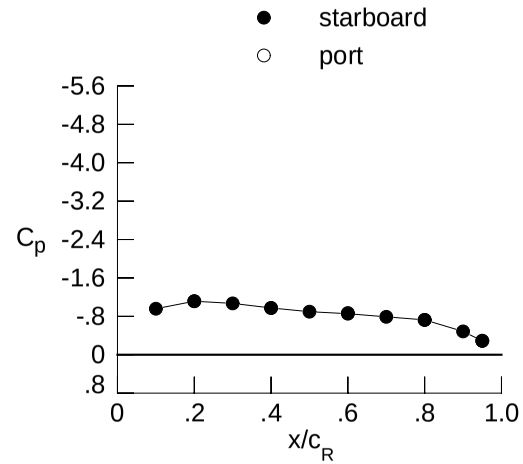
Run No. = 39 , Point No. = 794

$C_N$ = 0.657, $C_m$ = -0.0998

$\alpha$ = 14.5 °, $M_\infty$ = 0.798

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

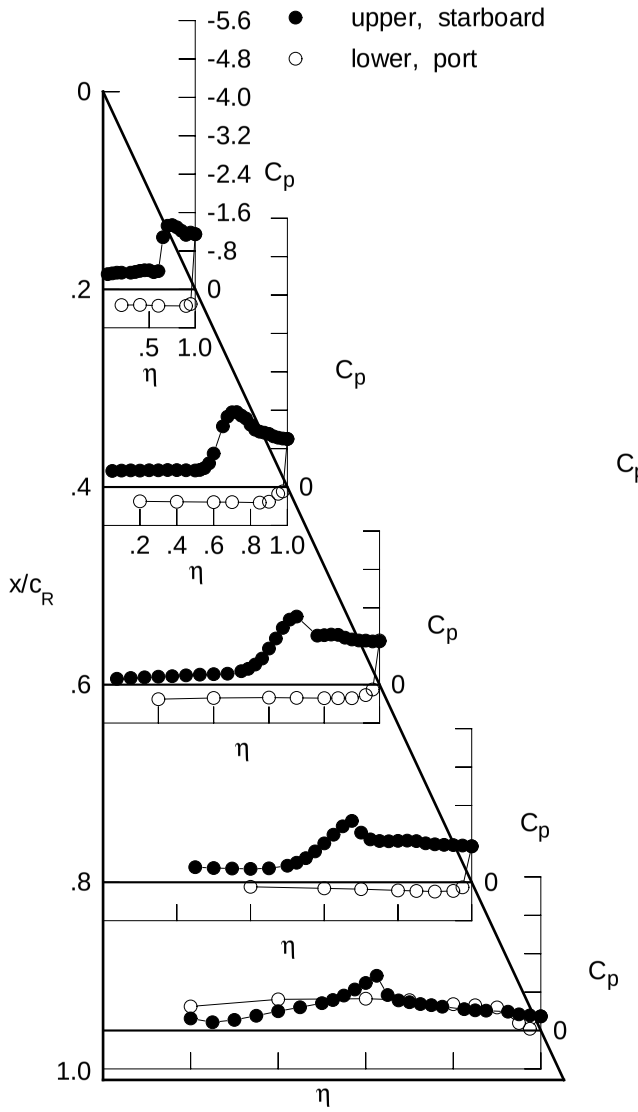



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.9580 | ******* |
| 0.20 | -1.1147 | -1.1152 |
| 0.30 | -1.0693 | ******* |
| 0.40 | -0.9746 | -0.9725 |
| 0.50 | -0.8966 | ******* |
| 0.60 | -0.8549 | -0.8687 |
| 0.70 | -0.7894 | ******* |
| 0.80 | -0.7259 | -0.7260 |
| 0.90 | -0.4859 | ******* |
| 0.95 | -0.2872 | -0.2932 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3175 | -0.3349 | -0.1220 | ******* | ******* |
| 0.100 | -0.3338 | -0.3427 | -0.1382 | ******* | ******* |
| 0.150 | -0.3481 | -0.3470 | -0.1526 | ******* | ******* |
| 0.200 | -0.3483 | -0.3424 | -0.1654 | ******* | -0.2510 |
| 0.250 | ******* | -0.3499 | -0.1760 | -0.3146 | -0.1717 |
| 0.300 | -0.3483 | -0.3491 | -0.1933 | -0.2971 | -0.2208 |
| 0.350 | -0.3635 | -0.3542 | -0.2080 | -0.2867 | -0.3075 |
| 0.400 | -0.3855 | -0.3530 | -0.2185 | -0.2794 | -0.4016 |
| 0.450 | -0.3984 | -0.3493 | -0.2284 | -0.2902 | -0.4837 |
| 0.500 | -0.3985 | -0.3447 | -0.2802 | -0.3451 | -0.5692 |
| 0.525 | ******* | -0.3572 | -0.3294 | -0.4075 | -0.6350 |
| 0.550 | -0.3589 | -0.3956 | -0.4184 | -0.5024 | -0.7277 |
| 0.575 | ******* | -0.4941 | -0.5433 | -0.6433 | -0.8547 |
| 0.600 | -0.3811 | -0.6973 | -0.7518 | -0.8108 | -0.9908 |
| 0.625 | ******* | ******* | -0.9607 | -0.9910 | -1.1400 |
| 0.650 | -1.0860 | -1.2644 | -1.1820 | -1.1657 | -0.7390 |
| 0.675 | ******* | -1.4652 | -1.3544 | -1.2794 | -0.6273 |
| 0.700 | -1.3254 | -1.5579 | -1.4188 | -1.0346 | -0.5898 |
| 0.725 | ******* | -1.5606 | ******* | -0.8939 | -0.5511 |
| 0.750 | -1.3389 | -1.4888 | ******* | -0.8597 | -0.5281 |
| 0.775 | ******* | -1.4286 | -1.0205 | -0.8546 | -0.4960 |
| 0.800 | -1.2938 | -1.2987 | -1.0301 | -0.8635 | ******* |
| 0.825 | ******* | -1.1951 | -1.0433 | -0.8679 | -0.4449 |
| 0.850 | -1.2212 | -1.1526 | -1.0378 | -0.8577 | -0.4207 |
| 0.875 | ******* | -1.1323 | -0.9780 | -0.8118 | -0.4132 |
| 0.900 | -1.1361 | -1.1063 | -0.9411 | -0.7909 | ******* |
| 0.925 | ******* | -1.0564 | -0.9198 | -0.7799 | -0.3920 |
| 0.950 | -1.1835 | -1.0283 | -0.9177 | -0.7752 | -0.3372 |
| 0.975 | ******* | -1.0102 | -0.8998 | -0.7659 | -0.3142 |
| 1.000 | -1.1479 | -1.0001 | -0.9014 | -0.7471 | -0.2941 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3271 | 0.2980 | 0.3029 | ******* | -0.5012 |
| -0.400 | 0.3231 | 0.3070 | 0.2779 | 0.0940 | -0.6490 |
| -0.600 | 0.3405 | 0.3141 | 0.2698 | 0.1267 | -0.6625 |
| -0.700 | ******* | 0.3146 | 0.2762 | 0.1434 | -0.6322 |
| -0.800 | ******* | ******* | 0.2814 | 0.1694 | -0.5488 |
| -0.850 | ******* | 0.3251 | 0.2815 | 0.1809 | -0.5253 |
| -0.900 | 0.3447 | 0.3064 | 0.2820 | 0.1934 | -0.4807 |
| -0.950 | 0.3053 | 0.1409 | 0.2176 | 0.1804 | -0.1558 |
| -0.975 | ******* | 0.0916 | 0.1017 | 0.1049 | -0.0363 |
| -1.000 | -1.1525 | -1.0035 | -0.9207 | -0.7522 | -0.2956 |

Surface Pressures




Small Radius L.E.

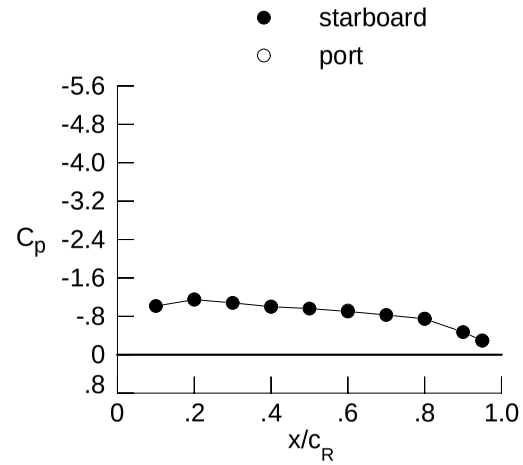
Run No. = 39 , Point No. = 795

$C_N$ = 0.708, $C_m$ = -0.1051

$\alpha$ = 15.5 °, $M_\infty$ = 0.798

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

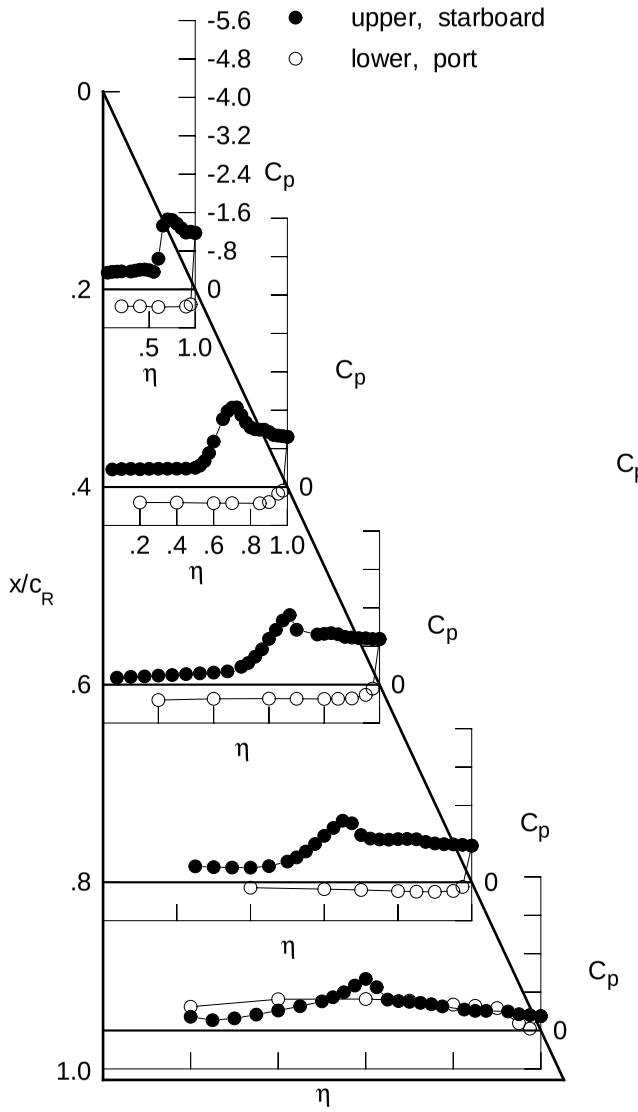



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0150 | ******* |
| 0.20 | -1.1479 | -1.1525 |
| 0.30 | -1.0803 | ******* |
| 0.40 | -1.0001 | -1.0035 |
| 0.50 | -0.9618 | ******* |
| 0.60 | -0.9014 | -0.9207 |
| 0.70 | -0.8286 | ******* |
| 0.80 | -0.7471 | -0.7522 |
| 0.90 | -0.4722 | ******* |
| 0.95 | -0.2941 | -0.2956 |

# Table D3. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3482 | -0.3653 | -0.1448 | ******* | ******* |
| 0.100 | -0.3655 | -0.3746 | -0.1621 | ******* | ******* |
| 0.150 | -0.3700 | -0.3791 | -0.1720 | ******* | ******* |
| 0.200 | -0.3750 | -0.3716 | -0.1880 | ******* | -0.2867 |
| 0.250 | ******* | -0.3804 | -0.1997 | -0.3316 | -0.2142 |
| 0.300 | -0.3731 | -0.3809 | -0.2193 | -0.3152 | -0.2530 |
| 0.350 | -0.3902 | -0.3816 | -0.2355 | -0.3070 | -0.3311 |
| 0.400 | -0.4097 | -0.3826 | -0.2511 | -0.3053 | -0.4163 |
| 0.450 | -0.4143 | -0.3840 | -0.2760 | -0.3357 | -0.5055 |
| 0.500 | -0.3994 | -0.4004 | -0.3722 | -0.4315 | -0.6074 |
| 0.525 | ******* | -0.4457 | -0.4508 | -0.5186 | -0.6931 |
| 0.550 | -0.3645 | -0.5373 | -0.5824 | -0.6417 | -0.7969 |
| 0.575 | ******* | -0.7070 | -0.7370 | -0.7978 | -0.9357 |
| 0.600 | -0.6392 | -0.9482 | -0.9528 | -0.9675 | -1.0748 |
| 0.625 | ******* | ******* | -1.1419 | -1.1328 | -0.9016 |
| 0.650 | -1.3272 | -1.4135 | -1.3349 | -1.2833 | -0.6435 |
| 0.675 | ******* | -1.5769 | -1.4494 | -1.2284 | -0.6138 |
| 0.700 | -1.4587 | -1.6542 | -1.1430 | -0.9844 | -0.5974 |
| 0.725 | ******* | -1.6593 | ******* | -0.9102 | -0.5761 |
| 0.750 | -1.4462 | -1.4996 | ******* | -0.8922 | -0.5472 |
| 0.775 | ******* | -1.3464 | -1.0451 | -0.8877 | -0.5017 |
| 0.800 | -1.3683 | -1.2415 | -1.0589 | -0.8989 | ******* |
| 0.825 | ******* | -1.2032 | -1.0731 | -0.9020 | -0.4365 |
| 0.850 | -1.2745 | -1.1937 | -1.0493 | -0.8958 | -0.4099 |
| 0.875 | ******* | -1.1939 | -0.9946 | -0.8410 | -0.4093 |
| 0.900 | -1.1822 | -1.1466 | -0.9806 | -0.8086 | ******* |
| 0.925 | ******* | -1.0863 | -0.9689 | -0.7938 | -0.3967 |
| 0.950 | -1.2026 | -1.0709 | -0.9662 | -0.7887 | -0.3400 |
| 0.975 | ******* | -1.0592 | -0.9503 | -0.7801 | -0.3214 |
| 1.000 | -1.1718 | -1.0479 | -0.9439 | -0.7622 | -0.2995 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3527 | 0.3220 | 0.3219 | ******* | -0.4952 |
| -0.400 | 0.3511 | 0.3241 | 0.2954 | 0.1127 | -0.6517 |
| -0.600 | 0.3675 | 0.3362 | 0.2911 | 0.1426 | -0.6551 |
| -0.700 | ******* | 0.3351 | 0.2947 | 0.1600 | -0.6230 |
| -0.800 | ******* | ******* | 0.2981 | 0.1832 | -0.5403 |
| -0.850 | ******* | 0.3392 | 0.2956 | 0.1952 | -0.5141 |
| -0.900 | 0.3580 | 0.3133 | 0.2870 | 0.1996 | -0.4666 |
| -0.950 | 0.3131 | 0.1374 | 0.2133 | 0.1807 | -0.1504 |
| -0.975 | ******* | 0.0751 | 0.0833 | 0.0950 | -0.0389 |
| -1.000 | -1.1830 | -1.0424 | -0.9545 | -0.7628 | -0.2991 |

Surface Pressures




Small Radius L.E.

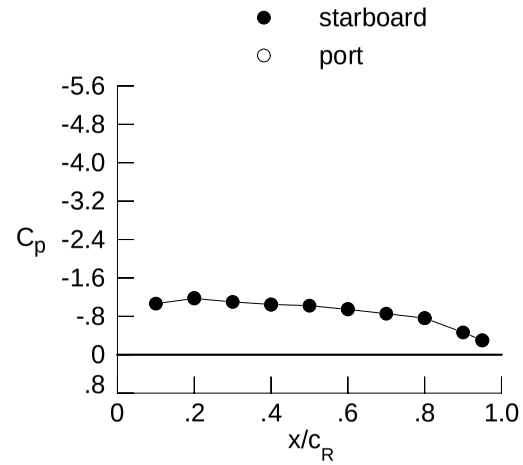
Run No. = 39 , Point No. = 796

$C_N$ = 0.762, $C_m$ = -0.1123

$\alpha$ = 16.5 °, $M_\infty$ = 0.798

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

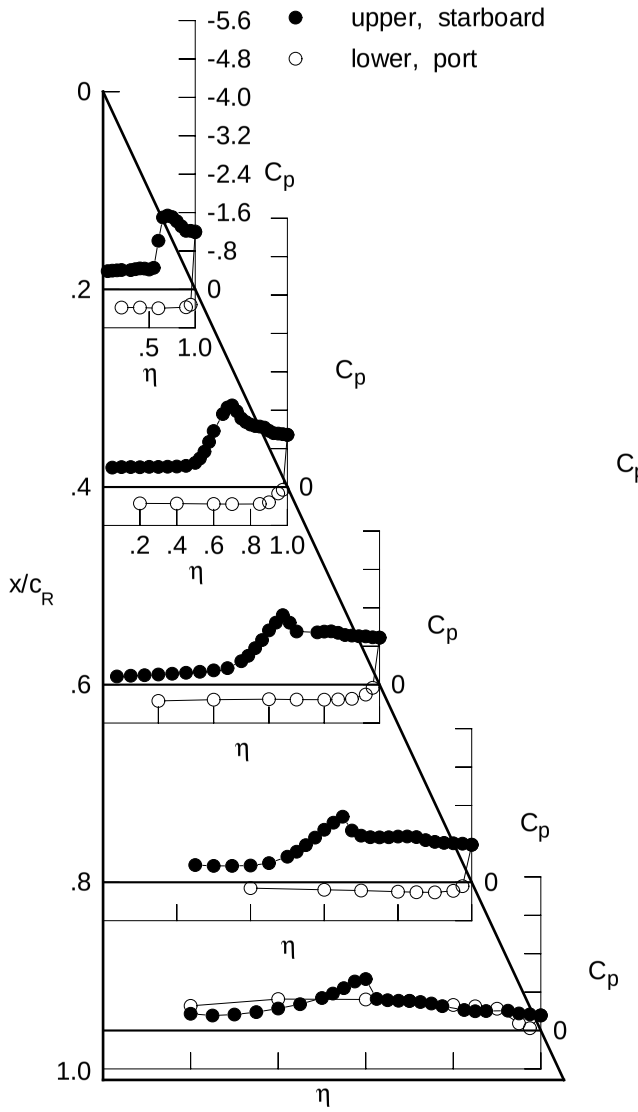



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0650 | ******* |
| 0.20 | -1.1718 | -1.1830 |
| 0.30 | -1.0998 | ******* |
| 0.40 | -1.0479 | -1.0424 |
| 0.50 | -1.0220 | ******* |
| 0.60 | -0.9439 | -0.9545 |
| 0.70 | -0.8552 | ******* |
| 0.80 | -0.7622 | -0.7628 |
| 0.90 | -0.4641 | ******* |
| 0.95 | -0.2995 | -0.2991 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3796 | -0.4051 | -0.1707 | ******* | ******* |
| 0.100 | -0.3906 | -0.4148 | -0.1852 | ******* | ******* |
| 0.150 | -0.3965 | -0.4157 | -0.1967 | ******* | ******* |
| 0.200 | -0.4037 | -0.4124 | -0.2114 | ******* | -0.3491 |
| 0.250 | ******* | -0.4211 | -0.2270 | -0.3593 | -0.3120 |
| 0.300 | -0.4017 | -0.4195 | -0.2471 | -0.3418 | -0.3324 |
| 0.350 | -0.4207 | -0.4233 | -0.2681 | -0.3416 | -0.3830 |
| 0.400 | -0.4364 | -0.4269 | -0.2975 | -0.3485 | -0.4577 |
| 0.450 | -0.4337 | -0.4414 | -0.3443 | -0.3991 | -0.5484 |
| 0.500 | -0.4136 | -0.5028 | -0.4882 | -0.5326 | -0.6770 |
| 0.525 | ******* | -0.5934 | -0.6008 | -0.6368 | -0.7693 |
| 0.550 | -0.4498 | -0.7369 | -0.7598 | -0.7736 | -0.8823 |
| 0.575 | ******* | -0.9401 | -0.9284 | -0.9306 | -1.0205 |
| 0.600 | -1.0132 | -1.1674 | -1.1305 | -1.0942 | -1.0717 |
| 0.625 | ******* | ******* | -1.2915 | -1.2418 | -0.6579 |
| 0.650 | -1.4982 | -1.5204 | -1.4476 | -1.3666 | -0.6315 |
| 0.675 | ******* | -1.6568 | -1.2908 | -1.0783 | -0.6201 |
| 0.700 | -1.5386 | -1.7010 | -1.1073 | -0.9711 | -0.6191 |
| 0.725 | ******* | -1.5789 | ******* | -0.9395 | -0.5932 |
| 0.750 | -1.5061 | -1.4294 | ******* | -0.9360 | -0.5625 |
| 0.775 | ******* | -1.3548 | -1.0886 | -0.9382 | -0.5075 |
| 0.800 | -1.4190 | -1.3013 | -1.1044 | -0.9530 | ******* |
| 0.825 | ******* | -1.2709 | -1.1103 | -0.9547 | -0.4275 |
| 0.850 | -1.3146 | -1.2602 | -1.0800 | -0.9417 | -0.4018 |
| 0.875 | ******* | -1.2386 | -1.0333 | -0.8784 | -0.4059 |
| 0.900 | -1.2201 | -1.1720 | -1.0223 | -0.8418 | ******* |
| 0.925 | ******* | -1.1220 | -1.0086 | -0.8206 | -0.4130 |
| 0.950 | -1.2203 | -1.1139 | -1.0059 | -0.8125 | -0.3556 |
| 0.975 | ******* | -1.1015 | -0.9863 | -0.8043 | -0.3359 |
| 1.000 | -1.1905 | -1.0898 | -0.9786 | -0.7838 | -0.3130 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3780 | 0.3408 | 0.3390 | ******* | -0.5135 |
| -0.400 | 0.3781 | 0.3447 | 0.3134 | 0.1220 | -0.6549 |
| -0.600 | 0.3932 | 0.3531 | 0.3032 | 0.1563 | -0.6467 |
| -0.700 | ******* | 0.3555 | 0.3114 | 0.1722 | -0.6141 |
| -0.800 | ******* | ******* | 0.3133 | 0.1961 | -0.5319 |
| -0.850 | ******* | 0.3528 | 0.3087 | 0.2074 | -0.5038 |
| -0.900 | 0.3720 | 0.3186 | 0.2950 | 0.2102 | -0.4537 |
| -0.950 | 0.3189 | 0.1330 | 0.2072 | 0.1781 | -0.1488 |
| -0.975 | ******* | 0.0578 | 0.0657 | 0.0811 | -0.0483 |
| -1.000 | -1.2065 | -1.0850 | -0.9792 | -0.7789 | -0.3168 |

Surface Pressures




Small Radius L.E.

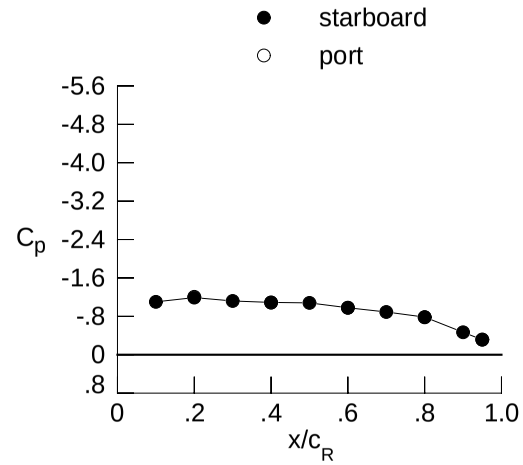
Run No. = 39 , Point No. = 797

$C_N$ = 0.823, $C_m$ = -0.1250

$\alpha$ = 17.5 °, $M_\infty$ = 0.802

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

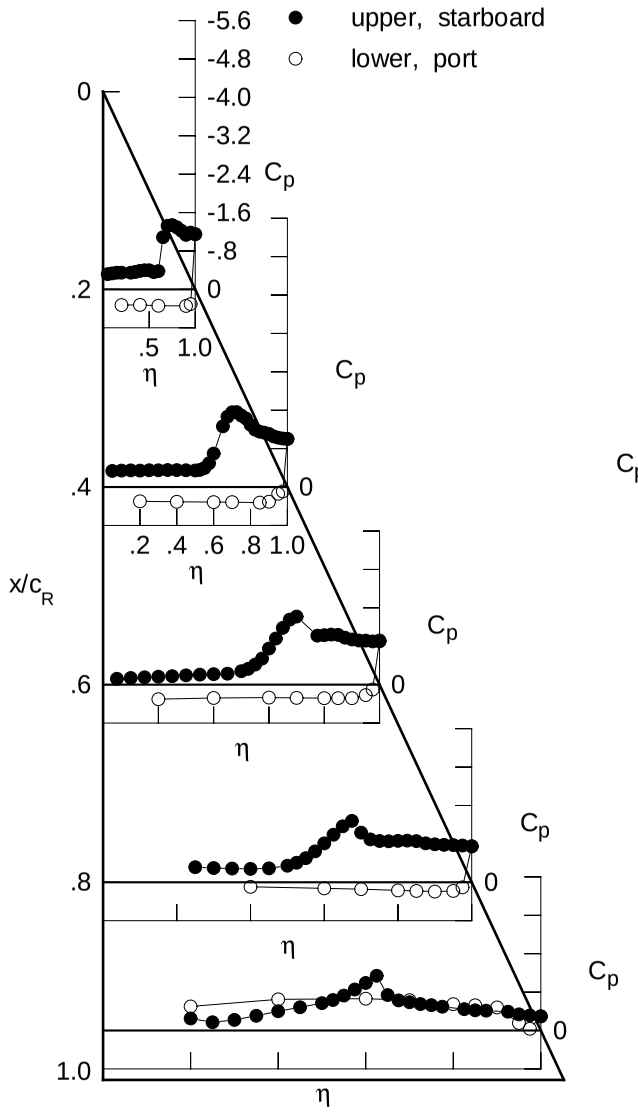



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1018 | ******* |
| 0.20 | -1.1905 | -1.2065 |
| 0.30 | -1.1198 | ******* |
| 0.40 | -1.0898 | -1.0850 |
| 0.50 | -1.0801 | ******* |
| 0.60 | -0.9786 | -0.9792 |
| 0.70 | -0.8907 | ******* |
| 0.80 | -0.7838 | -0.7789 |
| 0.90 | -0.4676 | ******* |
| 0.95 | -0.3130 | -0.3168 |

# Table D3. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3175 | -0.3349 | -0.1220 | ******* | ******* |
| 0.100 | -0.3338 | -0.3427 | -0.1382 | ******* | ******* |
| 0.150 | -0.3481 | -0.3470 | -0.1526 | ******* | ******* |
| 0.200 | -0.3483 | -0.3424 | -0.1654 | ******* | -0.2510 |
| 0.250 | ******* | -0.3499 | -0.1760 | -0.3146 | -0.1717 |
| 0.300 | -0.3483 | -0.3491 | -0.1933 | -0.2971 | -0.2208 |
| 0.350 | -0.3635 | -0.3542 | -0.2080 | -0.2867 | -0.3075 |
| 0.400 | -0.3855 | -0.3530 | -0.2185 | -0.2794 | -0.4016 |
| 0.450 | -0.3984 | -0.3493 | -0.2284 | -0.2902 | -0.4837 |
| 0.500 | -0.3985 | -0.3447 | -0.2802 | -0.3451 | -0.5692 |
| 0.525 | ******* | -0.3572 | -0.3294 | -0.4075 | -0.6350 |
| 0.550 | -0.3589 | -0.3956 | -0.4184 | -0.5024 | -0.7277 |
| 0.575 | ******* | -0.4941 | -0.5433 | -0.6433 | -0.8547 |
| 0.600 | -0.3811 | -0.6973 | -0.7518 | -0.8108 | -0.9908 |
| 0.625 | ******* | ******* | -0.9607 | -0.9910 | -1.1400 |
| 0.650 | -1.0860 | -1.2644 | -1.1820 | -1.1657 | -0.7390 |
| 0.675 | ******* | -1.4652 | -1.3544 | -1.2794 | -0.6273 |
| 0.700 | -1.3254 | -1.5579 | -1.4188 | -1.0346 | -0.5898 |
| 0.725 | ******* | -1.5606 | ******* | -0.8939 | -0.5511 |
| 0.750 | -1.3389 | -1.4888 | ******* | -0.8597 | -0.5281 |
| 0.775 | ******* | -1.4286 | -1.0205 | -0.8546 | -0.4960 |
| 0.800 | -1.2938 | -1.2987 | -1.0301 | -0.8635 | ******* |
| 0.825 | ******* | -1.1951 | -1.0433 | -0.8679 | -0.4449 |
| 0.850 | -1.2212 | -1.1526 | -1.0378 | -0.8577 | -0.4207 |
| 0.875 | ******* | -1.1323 | -0.9780 | -0.8118 | -0.4132 |
| 0.900 | -1.1361 | -1.1063 | -0.9411 | -0.7909 | ******* |
| 0.925 | ******* | -1.0564 | -0.9198 | -0.7799 | -0.3920 |
| 0.950 | -1.1835 | -1.0283 | -0.9177 | -0.7752 | -0.3372 |
| 0.975 | ******* | -1.0102 | -0.8998 | -0.7659 | -0.3142 |
| 1.000 | -1.1479 | -1.0001 | -0.9014 | -0.7471 | -0.2941 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3271 | 0.2980 | 0.3029 | ******* | -0.5012 |
| -0.400 | 0.3231 | 0.3070 | 0.2779 | 0.0940 | -0.6490 |
| -0.600 | 0.3405 | 0.3141 | 0.2698 | 0.1267 | -0.6625 |
| -0.700 | ******* | 0.3146 | 0.2762 | 0.1434 | -0.6322 |
| -0.800 | ******* | ******* | 0.2814 | 0.1694 | -0.5488 |
| -0.850 | ******* | 0.3251 | 0.2815 | 0.1809 | -0.5253 |
| -0.900 | 0.3447 | 0.3064 | 0.2820 | 0.1934 | -0.4807 |
| -0.950 | 0.3053 | 0.1409 | 0.2176 | 0.1804 | -0.1558 |
| -0.975 | ******* | 0.0916 | 0.1017 | 0.1049 | -0.0363 |
| -1.000 | -1.1525 | -1.0035 | -0.9207 | -0.7522 | -0.2956 |

Surface Pressures




Small Radius L.E.

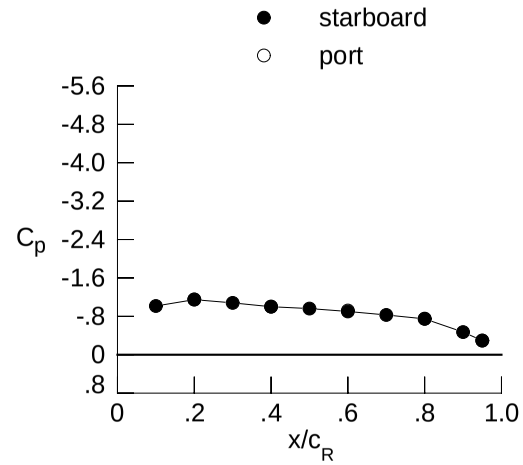
Run No. = 39 , Point No. = 795

$C_N$ = 0.708, $C_m$ = -0.1051

$\alpha$ = 15.5 °, $M_\infty$ = 0.798

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

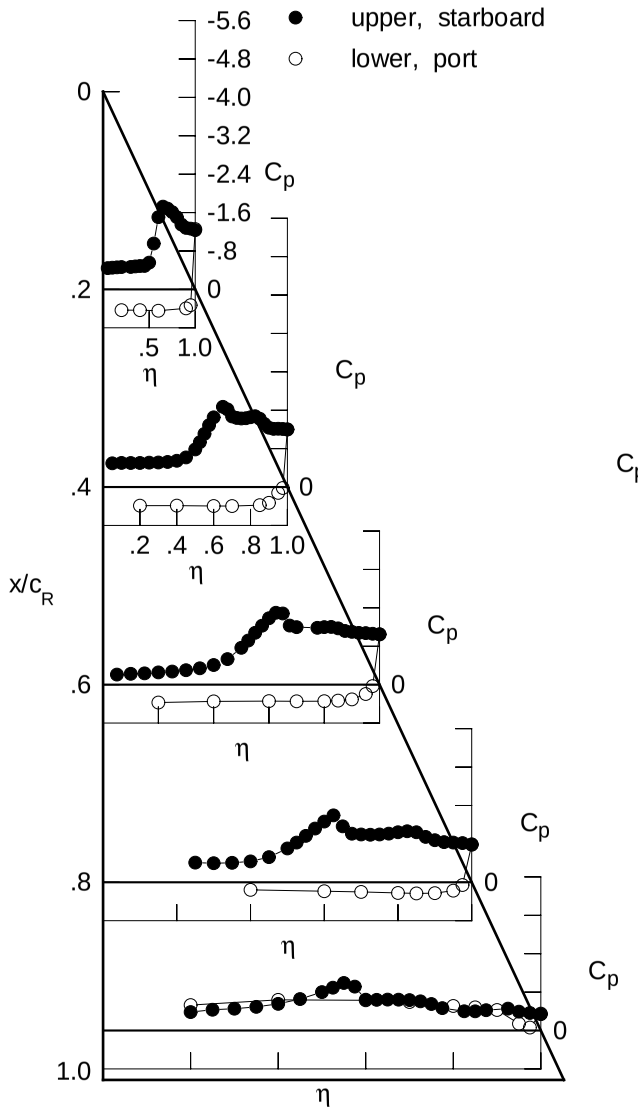



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0150 | ******* |
| 0.20 | -1.1479 | -1.1525 |
| 0.30 | -1.0803 | ******* |
| 0.40 | -1.0001 | -1.0035 |
| 0.50 | -0.9618 | ******* |
| 0.60 | -0.9014 | -0.9207 |
| 0.70 | -0.8286 | ******* |
| 0.80 | -0.7471 | -0.7522 |
| 0.90 | -0.4722 | ******* |
| 0.95 | -0.2941 | -0.2956 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4431 | -0.4946 | -0.2099 | ******* | ******* |
| 0.100 | -0.4523 | -0.5025 | -0.2254 | ******* | ******* |
| 0.150 | -0.4591 | -0.5011 | -0.2349 | ******* | ******* |
| 0.200 | -0.4653 | -0.5014 | -0.2549 | ******* | -0.3843 |
| 0.250 | ******* | -0.5079 | -0.2727 | -0.4092 | -0.4327 |
| 0.300 | -0.4668 | -0.5115 | -0.3008 | -0.3974 | -0.4542 |
| 0.350 | -0.4786 | -0.5224 | -0.3408 | -0.4056 | -0.4924 |
| 0.400 | -0.4869 | -0.5475 | -0.4086 | -0.4355 | -0.5552 |
| 0.450 | -0.4886 | -0.6169 | -0.5317 | -0.5240 | -0.6554 |
| 0.500 | -0.5574 | -0.7835 | -0.7675 | -0.7048 | -0.7999 |
| 0.525 | ******* | -0.9336 | -0.9182 | -0.8272 | -0.8917 |
| 0.550 | -0.9552 | -1.1076 | -1.0800 | -0.9674 | -0.9904 |
| 0.575 | ******* | -1.2877 | -1.2282 | -1.1196 | -0.9143 |
| 0.600 | -1.5051 | -1.4523 | -1.3832 | -1.2647 | -0.6417 |
| 0.625 | ******* | ******* | -1.4972 | -1.3940 | -0.6396 |
| 0.650 | -1.7243 | -1.6712 | -1.4821 | -1.1657 | -0.6444 |
| 0.675 | ******* | -1.6178 | -1.2306 | -1.0116 | -0.6426 |
| 0.700 | -1.6825 | -1.4701 | -1.1978 | -0.9960 | -0.6335 |
| 0.725 | ******* | -1.4398 | ******* | -0.9902 | -0.6082 |
| 0.750 | -1.6097 | -1.4282 | ******* | -0.9956 | -0.5522 |
| 0.775 | ******* | -1.4339 | -1.1840 | -1.0138 | -0.4667 |
| 0.800 | -1.5055 | -1.4546 | -1.1987 | -1.0420 | ******* |
| 0.825 | ******* | -1.4755 | -1.2023 | -1.0630 | -0.4008 |
| 0.850 | -1.3512 | -1.4229 | -1.1724 | -1.0426 | -0.4003 |
| 0.875 | ******* | -1.3155 | -1.1181 | -0.9456 | -0.4234 |
| 0.900 | -1.2816 | -1.2360 | -1.0997 | -0.8771 | ******* |
| 0.925 | ******* | -1.2124 | -1.0786 | -0.8370 | -0.4561 |
| 0.950 | -1.2657 | -1.2148 | -1.0737 | -0.8274 | -0.3929 |
| 0.975 | ******* | -1.2099 | -1.0602 | -0.8169 | -0.3658 |
| 1.000 | -1.2343 | -1.1999 | -1.0468 | -0.7913 | -0.3400 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4325 | 0.3877 | 0.3730 | ******* | -0.5300 |
| -0.400 | 0.4332 | 0.3874 | 0.3491 | 0.1577 | -0.6387 |
| -0.600 | 0.4444 | 0.3951 | 0.3433 | 0.1862 | -0.6296 |
| -0.700 | ******* | 0.3962 | 0.3472 | 0.2006 | -0.5935 |
| -0.800 | ******* | ******* | 0.3448 | 0.2222 | -0.5112 |
| -0.850 | ******* | 0.3776 | 0.3325 | 0.2320 | -0.4825 |
| -0.900 | 0.3949 | 0.3287 | 0.3074 | 0.2266 | -0.4274 |
| -0.950 | 0.3286 | 0.1216 | 0.1954 | 0.1744 | -0.1415 |
| -0.975 | ******* | 0.0204 | 0.0303 | 0.0566 | -0.0617 |
| -1.000 | -1.2568 | -1.1995 | -1.0484 | -0.7826 | -0.3517 |

Surface Pressures




Small Radius L.E.

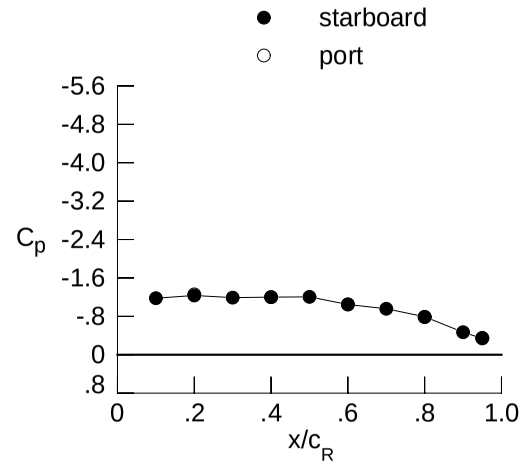
Run No. = 39 , Point No. = 799

$C_N$ = 0.934, $C_m$ = -0.1422

$\alpha$ = 19.6 °, $M_\infty$ = 0.801

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

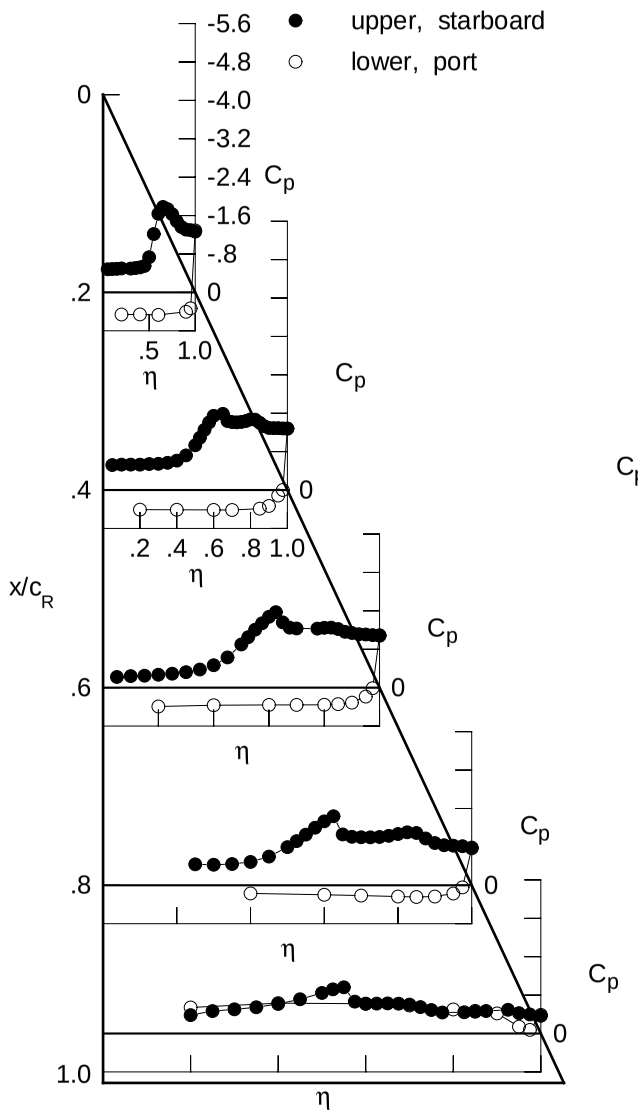



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1778 | ******* |
| 0.20 | -1.2343 | -1.2568 |
| 0.30 | -1.1896 | ******* |
| 0.40 | -1.1999 | -1.1995 |
| 0.50 | -1.2053 | ******* |
| 0.60 | -1.0468 | -1.0484 |
| 0.70 | -0.9578 | ******* |
| 0.80 | -0.7913 | -0.7826 |
| 0.90 | -0.4686 | ******* |
| 0.95 | -0.3400 | -0.3517 |

# Table D3. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4816 | -0.5212 | -0.2224 | ******* | ******* |
| 0.100 | -0.4865 | -0.5292 | -0.2402 | ******* | ******* |
| 0.150 | -0.4901 | -0.5294 | -0.2488 | ******* | ******* |
| 0.200 | -0.4991 | -0.5291 | -0.2690 | ******* | -0.3836 |
| 0.250 | ******* | -0.5415 | -0.2905 | -0.4365 | -0.4675 |
| 0.300 | -0.4962 | -0.5462 | -0.3222 | -0.4277 | -0.5039 |
| 0.350 | -0.5076 | -0.5673 | -0.3780 | -0.4433 | -0.5462 |
| 0.400 | -0.5208 | -0.6117 | -0.4669 | -0.4867 | -0.6161 |
| 0.450 | -0.5513 | -0.7213 | -0.6297 | -0.5979 | -0.7135 |
| 0.500 | -0.7335 | -0.9316 | -0.8991 | -0.7948 | -0.8445 |
| 0.525 | ******* | -1.0896 | -1.0516 | -0.9203 | -0.9204 |
| 0.550 | -1.2163 | -1.2529 | -1.2071 | -1.0556 | -0.9625 |
| 0.575 | ******* | -1.4077 | -1.3410 | -1.1989 | -0.6638 |
| 0.600 | -1.6374 | -1.5461 | -1.4753 | -1.3319 | -0.6206 |
| 0.625 | ******* | ******* | -1.5717 | -1.4382 | -0.6230 |
| 0.650 | -1.7802 | -1.5870 | -1.3594 | -1.0595 | -0.6272 |
| 0.675 | ******* | -1.4374 | -1.2493 | -1.0103 | -0.6214 |
| 0.700 | -1.7346 | -1.4163 | -1.2326 | -1.0011 | -0.6027 |
| 0.725 | ******* | -1.4107 | ******* | -0.9991 | -0.5501 |
| 0.750 | -1.6280 | -1.4186 | ******* | -1.0066 | -0.4895 |
| 0.775 | ******* | -1.4387 | -1.2295 | -1.0306 | -0.4377 |
| 0.800 | -1.4833 | -1.4720 | -1.2464 | -1.0683 | ******* |
| 0.825 | ******* | -1.4656 | -1.2504 | -1.1030 | -0.4425 |
| 0.850 | -1.3629 | -1.4011 | -1.2208 | -1.0899 | -0.4539 |
| 0.875 | ******* | -1.3296 | -1.1636 | -0.9749 | -0.4684 |
| 0.900 | -1.3084 | -1.2939 | -1.1388 | -0.8812 | ******* |
| 0.925 | ******* | -1.2897 | -1.1128 | -0.8346 | -0.4945 |
| 0.950 | -1.2957 | -1.2897 | -1.1072 | -0.8253 | -0.4244 |
| 0.975 | ******* | -1.2829 | -1.0940 | -0.8147 | -0.3968 |
| 1.000 | -1.2658 | -1.2787 | -1.0804 | -0.7857 | -0.3686 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4606 | 0.4086 | 0.3931 | ******* | -0.5421 |
| -0.400 | 0.4595 | 0.4112 | 0.3666 | 0.1693 | -0.6327 |
| -0.600 | 0.4685 | 0.4143 | 0.3599 | 0.1975 | -0.6201 |
| -0.700 | ******* | 0.4158 | 0.3602 | 0.2147 | -0.5832 |
| -0.800 | ******* | ******* | 0.3572 | 0.2345 | -0.5007 |
| -0.850 | ******* | 0.3883 | 0.3429 | 0.2438 | -0.4724 |
| -0.900 | 0.4048 | 0.3323 | 0.3121 | 0.2342 | -0.4186 |
| -0.950 | 0.3318 | 0.1150 | 0.1868 | 0.1718 | -0.1425 |
| -0.975 | ******* | -0.0007 | 0.0109 | 0.0439 | -0.0749 |
| -1.000 | -1.2900 | -1.2818 | -1.0909 | -0.7696 | -0.3887 |

Surface Pressures




Small Radius L.E.

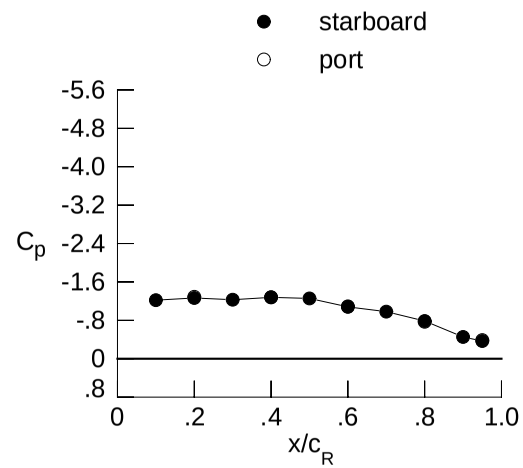
Run No. = 39 , Point No. = 800

$C_N$ = 0.984, $C_m$ = -0.1488

$\alpha$ = 20.6 °, $M_\infty$ = 0.801

$R_{mac}$ = $6.0 \times 10^6$

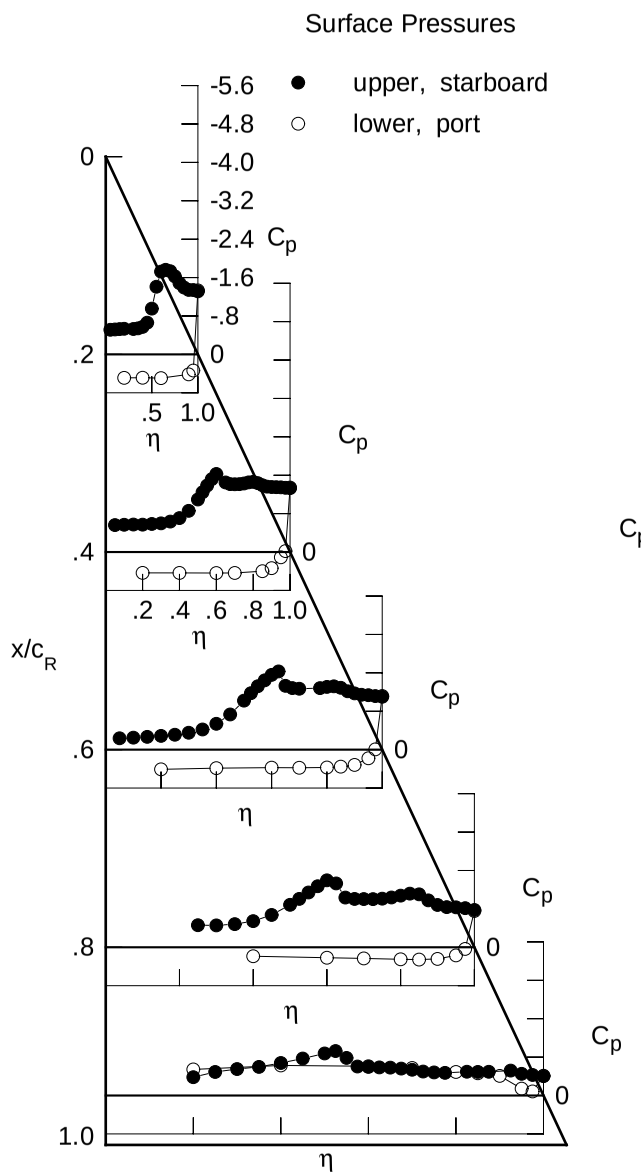
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.2200 | ******* |
| 0.20 | -1.2658 | -1.2900 |
| 0.30 | -1.2294 | ******* |
| 0.40 | -1.2787 | -1.2818 |
| 0.50 | -1.2564 | ******* |
| 0.60 | -1.0804 | -1.0909 |
| 0.70 | -0.9807 | ******* |
| 0.80 | -0.7857 | -0.7696 |
| 0.90 | -0.4537 | ******* |
| 0.95 | -0.3686 | -0.3887 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5131 | -0.5617 | -0.2366 | ******* | ******* |
| 0.100 | -0.5191 | -0.5683 | -0.2498 | ******* | ******* |
| 0.150 | -0.5274 | -0.5729 | -0.2663 | ******* | ******* |
| 0.200 | -0.5339 | -0.5705 | -0.2866 | ******* | -0.3819 |
| 0.250 | ******* | -0.5847 | -0.3103 | -0.4603 | -0.4905 |
| 0.300 | -0.5285 | -0.5977 | -0.3520 | -0.4564 | -0.5509 |
| 0.350 | -0.5426 | -0.6345 | -0.4201 | -0.4826 | -0.5963 |
| 0.400 | -0.5726 | -0.7072 | -0.5386 | -0.5446 | -0.6774 |
| 0.450 | -0.6609 | -0.8585 | -0.7330 | -0.6737 | -0.7701 |
| 0.500 | -0.9533 | -1.0946 | -1.0205 | -0.8845 | -0.8760 |
| 0.525 | ******* | -1.2451 | -1.1762 | -1.0083 | -0.9268 |
| 0.550 | -1.4097 | -1.3853 | -1.3208 | -1.1414 | -0.7830 |
| 0.575 | ******* | -1.5174 | -1.4437 | -1.2717 | -0.6041 |
| 0.600 | -1.7250 | -1.6266 | -1.5574 | -1.3955 | -0.5961 |
| 0.625 | ******* | ******* | -1.6297 | -1.3303 | -0.5857 |
| 0.650 | -1.7626 | -1.4497 | -1.3299 | -1.0359 | -0.5808 |
| 0.675 | ******* | -1.4149 | -1.2825 | -1.0072 | -0.5609 |
| 0.700 | -1.7328 | -1.4118 | -1.2690 | -1.0048 | -0.5371 |
| 0.725 | ******* | -1.4145 | ******* | -1.0034 | -0.4994 |
| 0.750 | -1.6254 | -1.4279 | ******* | -1.0126 | -0.4811 |
| 0.775 | ******* | -1.4511 | -1.2815 | -1.0377 | -0.4716 |
| 0.800 | -1.4845 | -1.4627 | -1.3070 | -1.0764 | ******* |
| 0.825 | ******* | -1.4349 | -1.3190 | -1.1176 | -0.4953 |
| 0.850 | -1.3930 | -1.3920 | -1.2890 | -1.1035 | -0.4909 |
| 0.875 | ******* | -1.3625 | -1.2161 | -0.9778 | -0.4948 |
| 0.900 | -1.3434 | -1.3541 | -1.1719 | -0.8818 | ******* |
| 0.925 | ******* | -1.3511 | -1.1434 | -0.8366 | -0.5191 |
| 0.950 | -1.3405 | -1.3476 | -1.1345 | -0.8326 | -0.4519 |
| 0.975 | ******* | -1.3387 | -1.1161 | -0.8153 | -0.4278 |
| 1.000 | -1.3139 | -1.3314 | -1.1020 | -0.7776 | -0.4028 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4886 | 0.4343 | 0.4105 | ******* | -0.5433 |
| -0.400 | 0.4865 | 0.4348 | 0.3855 | 0.1865 | -0.6262 |
| -0.600 | 0.4943 | 0.4373 | 0.3751 | 0.2175 | -0.6096 |
| -0.700 | ******* | 0.4358 | 0.3775 | 0.2319 | -0.5738 |
| -0.800 | ******* | ******* | 0.3718 | 0.2504 | -0.4903 |
| -0.850 | ******* | 0.3992 | 0.3546 | 0.2558 | -0.4635 |
| -0.900 | 0.4160 | 0.3359 | 0.3182 | 0.2421 | -0.4088 |
| -0.950 | 0.3363 | 0.1097 | 0.1801 | 0.1691 | -0.1429 |
| -0.975 | ******* | -0.0194 | -0.0057 | 0.0346 | -0.0847 |
| -1.000 | -1.3333 | -1.3429 | -1.1177 | -0.7564 | -0.4121 |



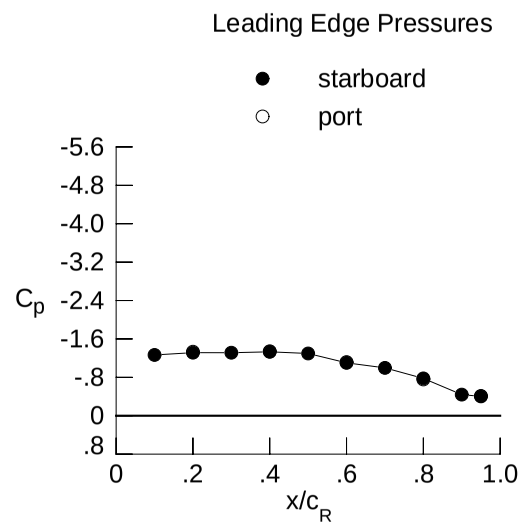

Small Radius L.E.

Run No. = 39 , Point No. = 801

$C_N$ = 1.033, $C_m$ = -0.1547

$\alpha$ = 21.6 °, $M_\infty$ = 0.800

$R_{mac}$ = $6.0 \times 10^6$

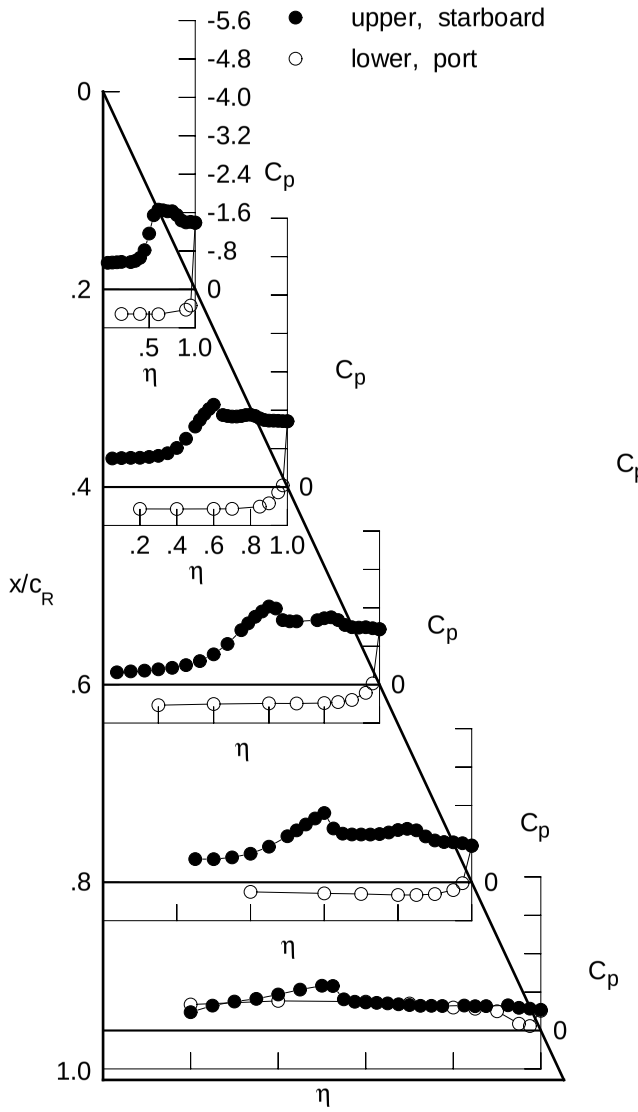



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.2662 | ******* |
| 0.20 | -1.3139 | -1.3333 |
| 0.30 | -1.3126 | ******* |
| 0.40 | -1.3314 | -1.3429 |
| 0.50 | -1.2969 | ******* |
| 0.60 | -1.1020 | -1.1177 |
| 0.70 | -0.9971 | ******* |
| 0.80 | -0.7776 | -0.7564 |
| 0.90 | -0.4403 | ******* |
| 0.95 | -0.4028 | -0.4121 |

# Table D3. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5534 | -0.5954 | -0.2569 | ******* | ******* |
| 0.100 | -0.5589 | -0.6032 | -0.2760 | ******* | ******* |
| 0.150 | -0.5645 | -0.6078 | -0.2919 | ******* | ******* |
| 0.200 | -0.5728 | -0.6097 | -0.3193 | ******* | -0.3819 |
| 0.250 | ******* | -0.6272 | -0.3504 | -0.4833 | -0.5181 |
| 0.300 | -0.5692 | -0.6494 | -0.4063 | -0.4818 | -0.6031 |
| 0.350 | -0.5946 | -0.7039 | -0.4904 | -0.5183 | -0.6594 |
| 0.400 | -0.6570 | -0.8142 | -0.6315 | -0.5942 | -0.7504 |
| 0.450 | -0.8166 | -1.0061 | -0.8471 | -0.7418 | -0.8518 |
| 0.500 | -1.1629 | -1.2597 | -1.1345 | -0.9594 | -0.9332 |
| 0.525 | ******* | -1.3985 | -1.2776 | -1.0813 | -0.9276 |
| 0.550 | -1.5447 | -1.5195 | -1.4137 | -1.2044 | -0.6494 |
| 0.575 | ******* | -1.6249 | -1.5239 | -1.3290 | -0.5994 |
| 0.600 | -1.6615 | -1.7140 | -1.6287 | -1.4433 | -0.5848 |
| 0.625 | ******* | ******* | -1.5860 | -1.1209 | -0.5759 |
| 0.650 | -1.6480 | -1.4997 | -1.3437 | -1.0126 | -0.5647 |
| 0.675 | ******* | -1.4797 | -1.3192 | -0.9958 | -0.5464 |
| 0.700 | -1.6262 | -1.4680 | -1.3184 | -0.9955 | -0.5306 |
| 0.725 | ******* | -1.4691 | ******* | -0.9941 | -0.5143 |
| 0.750 | -1.6281 | -1.4795 | ******* | -1.0051 | -0.5140 |
| 0.775 | ******* | -1.5002 | -1.3422 | -1.0379 | -0.5105 |
| 0.800 | -1.5503 | -1.5063 | -1.3831 | -1.0890 | ******* |
| 0.825 | ******* | -1.4811 | -1.4032 | -1.1137 | -0.5203 |
| 0.850 | -1.4361 | -1.4312 | -1.3456 | -1.0825 | -0.5063 |
| 0.875 | ******* | -1.3968 | -1.2430 | -0.9550 | -0.5080 |
| 0.900 | -1.3952 | -1.3834 | -1.1968 | -0.8713 | ******* |
| 0.925 | ******* | -1.3826 | -1.1882 | -0.8383 | -0.5255 |
| 0.950 | -1.4075 | -1.3789 | -1.1962 | -0.8327 | -0.4731 |
| 0.975 | ******* | -1.3724 | -1.1755 | -0.8140 | -0.4555 |
| 1.000 | -1.3843 | -1.3683 | -1.1499 | -0.7672 | -0.4321 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5131 | 0.4560 | 0.4284 | ******* | -0.5415 |
| -0.400 | 0.5122 | 0.4576 | 0.4042 | 0.1999 | -0.6166 |
| -0.600 | 0.5176 | 0.4553 | 0.3906 | 0.2314 | -0.6007 |
| -0.700 | ******* | 0.4545 | 0.3927 | 0.2433 | -0.5623 |
| -0.800 | ******* | ******* | 0.3836 | 0.2646 | -0.4784 |
| -0.850 | ******* | 0.4089 | 0.3635 | 0.2644 | -0.4539 |
| -0.900 | 0.4229 | 0.3390 | 0.3195 | 0.2459 | -0.4005 |
| -0.950 | 0.3370 | 0.1101 | 0.1716 | 0.1623 | -0.1405 |
| -0.975 | ******* | -0.0355 | -0.0260 | 0.0184 | -0.0929 |
| -1.000 | -1.3939 | -1.3710 | -1.1578 | -0.7560 | -0.4108 |

Surface Pressures




Small Radius L.E.

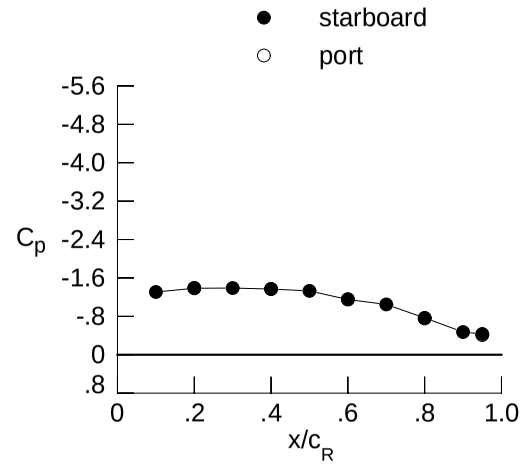
Run No. = 39 , Point No. = 802

$C_N$ = 1.086, $C_m$ = -0.1641

$\alpha$ = 22.6 °, $M_\infty$ = 0.801

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

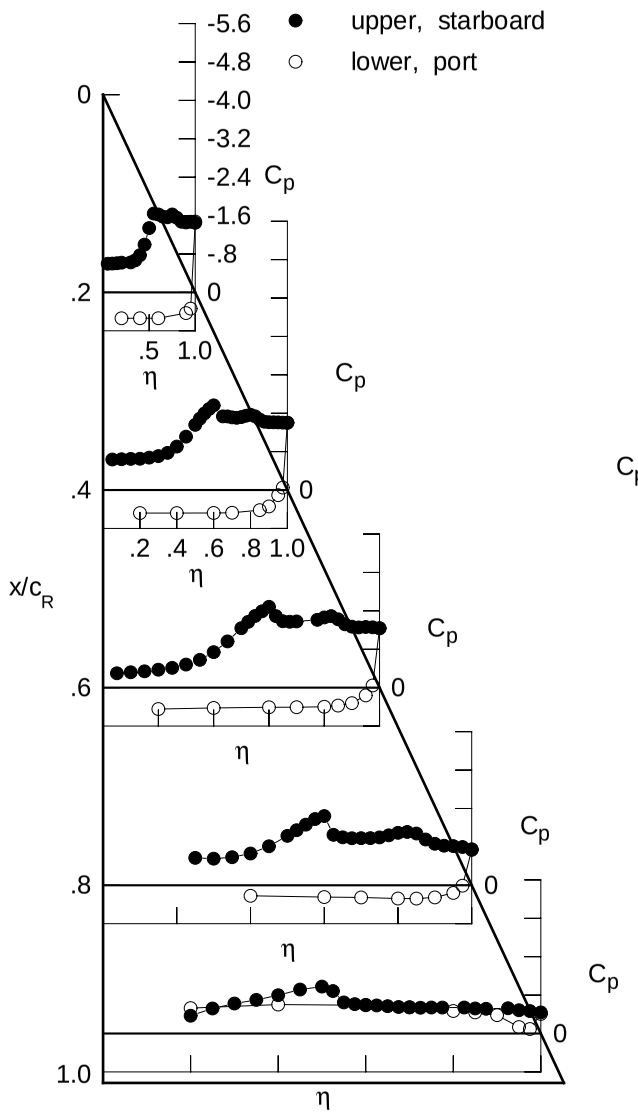



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.3070 | ******* |
| 0.20 | -1.3843 | -1.3939 |
| 0.30 | -1.3895 | ******* |
| 0.40 | -1.3683 | -1.3710 |
| 0.50 | -1.3303 | ******* |
| 0.60 | -1.1499 | -1.1578 |
| 0.70 | -1.0479 | ******* |
| 0.80 | -0.7672 | -0.7560 |
| 0.90 | -0.4728 | ******* |
| 0.95 | -0.4321 | -0.4108 |

# Table D3. Continued.

| η | x/c_R .2 Cp,u | x/c_R .4 Cp,u | x/c_R .6 Cp,u | x/c_R .8 Cp,u | x/c_R .95 Cp,u |
|---|---|---|---|---|---|
| 0.050 | -0.5964 | -0.6359 | -0.2991 | ******* | ******* |
| 0.100 | -0.6010 | -0.6412 | -0.3202 | ******* | ******* |
| 0.150 | -0.6071 | -0.6489 | -0.3399 | ******* | ******* |
| 0.200 | -0.6188 | -0.6521 | -0.3738 | ******* | -0.3707 |
| 0.250 | ******* | -0.6750 | -0.4123 | -0.5715 | -0.5216 |
| 0.300 | -0.6245 | -0.7075 | -0.4805 | -0.5546 | -0.6245 |
| 0.350 | -0.6679 | -0.7748 | -0.5790 | -0.5846 | -0.6996 |
| 0.400 | -0.7748 | -0.9059 | -0.7392 | -0.6616 | -0.7975 |
| 0.450 | -0.9950 | -1.1117 | -0.9631 | -0.8127 | -0.9156 |
| 0.500 | -1.3403 | -1.3586 | -1.2386 | -1.0298 | -0.9772 |
| 0.525 | ******* | -1.4864 | -1.3700 | -1.1469 | -0.8844 |
| 0.550 | -1.6425 | -1.5950 | -1.4935 | -1.2631 | -0.6472 |
| 0.575 | ******* | -1.6878 | -1.5905 | -1.3798 | -0.6123 |
| 0.600 | -1.6228 | -1.7642 | -1.6844 | -1.4424 | -0.5978 |
| 0.625 | ******* | ******* | -1.4903 | -1.0512 | -0.5846 |
| 0.650 | -1.5773 | -1.5342 | -1.3835 | -0.9989 | -0.5699 |
| 0.675 | ******* | -1.5336 | -1.3732 | -0.9798 | -0.5526 |
| 0.700 | -1.5648 | -1.5136 | -1.3794 | -0.9815 | -0.5432 |
| 0.725 | ******* | -1.5051 | ******* | -0.9823 | -0.5368 |
| 0.750 | -1.6230 | -1.5201 | ******* | -0.9977 | -0.5417 |
| 0.775 | ******* | -1.5483 | -1.4131 | -1.0407 | -0.5404 |
| 0.800 | -1.5544 | -1.5687 | -1.4626 | -1.0924 | ******* |
| 0.825 | ******* | -1.5350 | -1.4903 | -1.1114 | -0.5412 |
| 0.850 | -1.4723 | -1.4683 | -1.4238 | -1.0784 | -0.5215 |
| 0.875 | ******* | -1.4235 | -1.3196 | -0.9535 | -0.5155 |
| 0.900 | -1.4568 | -1.4128 | -1.2703 | -0.8650 | ******* |
| 0.925 | ******* | -1.4113 | -1.2546 | -0.8251 | -0.5267 |
| 0.950 | -1.4721 | -1.4096 | -1.2639 | -0.8165 | -0.4846 |
| 0.975 | ******* | -1.4043 | -1.2570 | -0.7977 | -0.4682 |
| 1.000 | -1.4500 | -1.4016 | -1.2362 | -0.7500 | -0.4395 |
| | Cp,l | Cp,l | Cp,l | Cp,l | Cp,l |
| -0.200 | 0.5391 | 0.4799 | 0.4460 | ******* | -0.5291 |
| -0.400 | 0.5384 | 0.4800 | 0.4232 | 0.2188 | -0.6032 |
| -0.600 | 0.5387 | 0.4779 | 0.4089 | 0.2455 | -0.5883 |
| -0.700 | ******* | 0.4736 | 0.4079 | 0.2535 | -0.5491 |
| -0.800 | ******* | ******* | 0.3982 | 0.2759 | -0.4689 |
| -0.850 | ******* | 0.4190 | 0.3733 | 0.2771 | -0.4399 |
| -0.900 | 0.4314 | 0.3417 | 0.3230 | 0.2530 | -0.3821 |
| -0.950 | 0.3380 | 0.1069 | 0.1613 | 0.1593 | -0.1347 |
| -0.975 | ******* | -0.0513 | -0.0457 | 0.0076 | -0.0932 |
| -1.000 | -1.4748 | -1.4027 | -1.2377 | -0.7376 | -0.4075 |

Surface Pressures




Small Radius L.E.

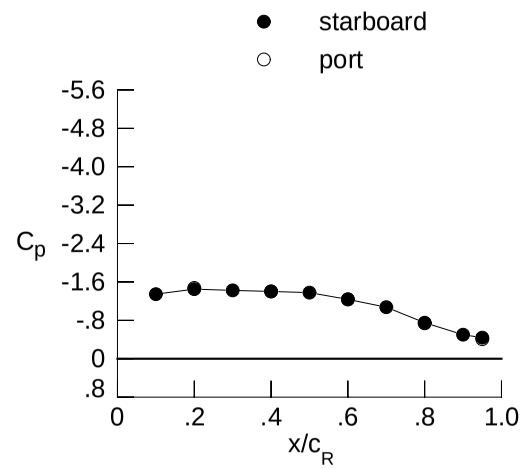
Run No. = 39 , Point No. = 803

$C_N$ = 1.139, $C_m$ = -0.1728

$\alpha$ = 23.6 °, $M_\infty$ = 0.801

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

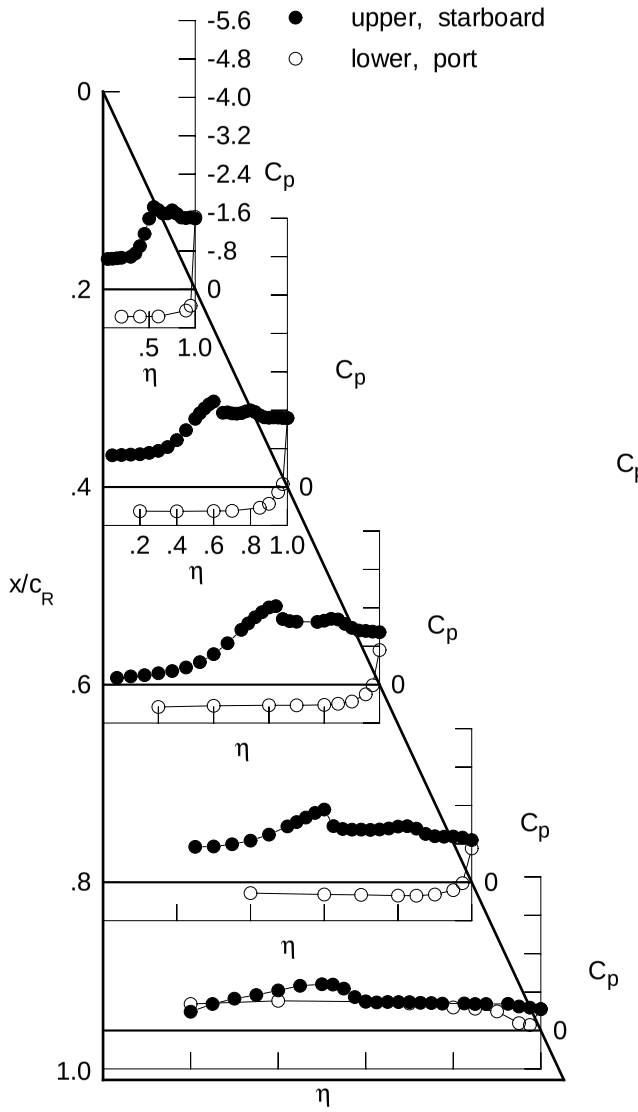



| x/c_R | starb'd Cp | port Cp |
|---|---|---|
| 0.10 | -1.3451 | ******* |
| 0.20 | -1.4500 | -1.4748 |
| 0.30 | -1.4237 | ******* |
| 0.40 | -1.4016 | -1.4027 |
| 0.50 | -1.3769 | ******* |
| 0.60 | -1.2362 | -1.2377 |
| 0.70 | -1.0737 | ******* |
| 0.80 | -0.7500 | -0.7376 |
| 0.90 | -0.5007 | ******* |
| 0.95 | -0.4395 | -0.4075 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6336 | -0.6610 | -0.1412 | ******* | ******* |
| 0.100 | -0.6381 | -0.6675 | -0.1711 | ******* | ******* |
| 0.150 | -0.6477 | -0.6753 | -0.1973 | ******* | ******* |
| 0.200 | -0.6589 | -0.6836 | -0.2380 | ******* | -0.3916 |
| 0.250 | ******* | -0.7111 | -0.2833 | -0.7383 | -0.5527 |
| 0.300 | -0.6791 | -0.7539 | -0.3572 | -0.7455 | -0.6634 |
| 0.350 | -0.7477 | -0.8332 | -0.4690 | -0.7921 | -0.7395 |
| 0.400 | -0.9010 | -0.9779 | -0.6349 | -0.8670 | -0.8353 |
| 0.450 | -1.1565 | -1.1850 | -0.8622 | -0.9929 | -0.9318 |
| 0.500 | -1.4732 | -1.4205 | -1.1408 | -1.1642 | -0.9643 |
| 0.525 | ******* | -1.5371 | -1.2764 | -1.2544 | -0.9569 |
| 0.550 | -1.7160 | -1.6364 | -1.4029 | -1.3484 | -0.8727 |
| 0.575 | ******* | -1.7227 | -1.5099 | -1.4445 | -0.6970 |
| 0.600 | -1.6529 | -1.7827 | -1.6084 | -1.5155 | -0.6057 |
| 0.625 | ******* | ******* | -1.6348 | -1.1703 | -0.5848 |
| 0.650 | -1.5790 | -1.5474 | -1.3669 | -1.1104 | -0.5943 |
| 0.675 | ******* | -1.5555 | -1.3224 | -1.0970 | -0.5932 |
| 0.700 | -1.5842 | -1.5332 | -1.3115 | -1.0975 | -0.5909 |
| 0.725 | ******* | -1.5287 | ******* | -1.0913 | -0.5765 |
| 0.750 | -1.6471 | -1.5391 | ******* | -1.1002 | -0.5721 |
| 0.775 | ******* | -1.5759 | -1.3061 | -1.1205 | -0.5603 |
| 0.800 | -1.5743 | -1.5982 | -1.3319 | -1.1608 | ******* |
| 0.825 | ******* | -1.5624 | -1.3709 | -1.1689 | -0.5642 |
| 0.850 | -1.4978 | -1.4944 | -1.3579 | -1.1174 | -0.5518 |
| 0.875 | ******* | -1.4528 | -1.2659 | -1.0075 | -0.5517 |
| 0.900 | -1.4856 | -1.4431 | -1.1828 | -0.9593 | ******* |
| 0.925 | ******* | -1.4502 | -1.1275 | -0.9493 | -0.5558 |
| 0.950 | -1.5007 | -1.4470 | -1.1190 | -0.9533 | -0.4998 |
| 0.975 | ******* | -1.4384 | -1.1039 | -0.9314 | -0.4762 |
| 1.000 | -1.4769 | -1.4377 | -1.0923 | -0.8793 | -0.4475 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5676 | 0.5030 | 0.4655 | ******* | -0.5524 |
| -0.400 | 0.5652 | 0.5065 | 0.4406 | 0.2257 | -0.6185 |
| -0.600 | 0.5640 | 0.5000 | 0.4296 | 0.2541 | -0.6004 |
| -0.700 | ******* | 0.4959 | 0.4311 | 0.2623 | -0.5632 |
| -0.800 | ******* | ******* | 0.4216 | 0.2777 | -0.4802 |
| -0.850 | ******* | 0.4317 | 0.3986 | 0.2791 | -0.4547 |
| -0.900 | 0.4414 | 0.3494 | 0.3518 | 0.2548 | -0.3975 |
| -0.950 | 0.3410 | 0.1074 | 0.2020 | 0.1637 | -0.1524 |
| -0.975 | ******* | -0.0623 | 0.0130 | 0.0183 | -0.1155 |
| -1.000 | -1.5086 | -1.4362 | -0.7198 | -0.7065 | -0.4441 |

Surface Pressures




Small Radius L.E.

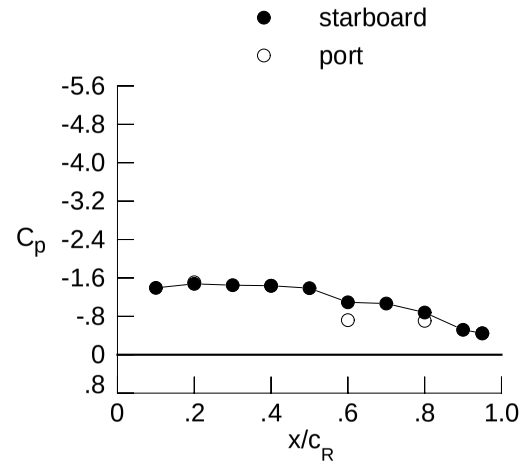
Run No. = 39 , Point No. = 804

$C_N$ = 1.142, $C_m$ = -0.1801

$\alpha$ = 24.6 °, $M_\infty$ = 0.800

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

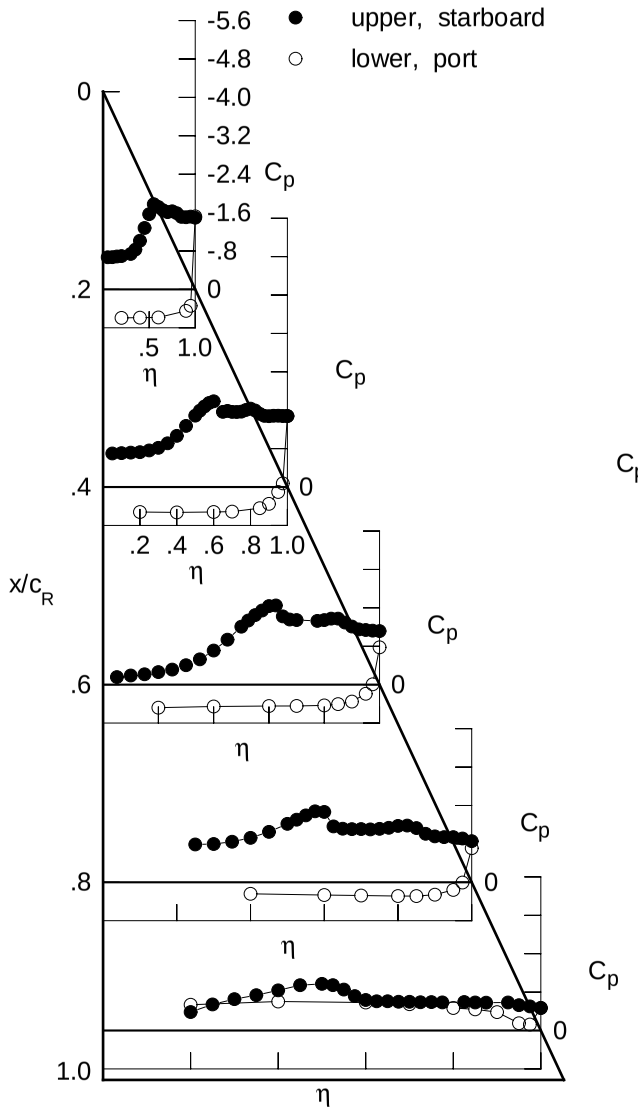



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.3931 | ******* |
| 0.20 | -1.4769 | -1.5086 |
| 0.30 | -1.4485 | ******* |
| 0.40 | -1.4377 | -1.4362 |
| 0.50 | -1.3867 | ******* |
| 0.60 | -1.0923 | -0.7198 |
| 0.70 | -1.0663 | ******* |
| 0.80 | -0.8793 | -0.7065 |
| 0.90 | -0.5189 | ******* |
| 0.95 | -0.4475 | -0.4441 |

# Table D3. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6697 | -0.6996 | -0.1575 | ******* | ******* |
| 0.100 | -0.6715 | -0.7063 | -0.1903 | ******* | ******* |
| 0.150 | -0.6858 | -0.7171 | -0.2162 | ******* | ******* |
| 0.200 | -0.6946 | -0.7261 | -0.2616 | ******* | -0.3848 |
| 0.250 | ******* | -0.7621 | -0.3137 | -0.7880 | -0.5435 |
| 0.300 | -0.7385 | -0.8166 | -0.4048 | -0.7974 | -0.6538 |
| 0.350 | -0.8289 | -0.9110 | -0.5270 | -0.8447 | -0.7358 |
| 0.400 | -1.0137 | -1.0668 | -0.7105 | -0.9258 | -0.8365 |
| 0.450 | -1.2792 | -1.2737 | -0.9371 | -1.0504 | -0.9442 |
| 0.500 | -1.5673 | -1.4874 | -1.2073 | -1.2176 | -0.9717 |
| 0.525 | ******* | -1.5903 | -1.3350 | -1.3041 | -0.9447 |
| 0.550 | -1.7753 | -1.6786 | -1.4489 | -1.3934 | -0.8525 |
| 0.575 | ******* | -1.7514 | -1.5438 | -1.4785 | -0.7171 |
| 0.600 | -1.7171 | -1.7862 | -1.6367 | -1.4655 | -0.6359 |
| 0.625 | ******* | ******* | -1.6497 | -1.1641 | -0.6092 |
| 0.650 | -1.6495 | -1.5667 | -1.4226 | -1.1161 | -0.6096 |
| 0.675 | ******* | -1.5867 | -1.3565 | -1.1075 | -0.5993 |
| 0.700 | -1.6098 | -1.5658 | -1.3459 | -1.1086 | -0.5983 |
| 0.725 | ******* | -1.5633 | ******* | -1.1013 | -0.5884 |
| 0.750 | -1.6269 | -1.5707 | ******* | -1.1133 | -0.5919 |
| 0.775 | ******* | -1.6053 | -1.3280 | -1.1352 | -0.5856 |
| 0.800 | -1.5876 | -1.6334 | -1.3447 | -1.1743 | ******* |
| 0.825 | ******* | -1.5947 | -1.3751 | -1.1812 | -0.5935 |
| 0.850 | -1.5114 | -1.5245 | -1.3755 | -1.1299 | -0.5837 |
| 0.875 | ******* | -1.4833 | -1.2933 | -1.0101 | -0.5796 |
| 0.900 | -1.5030 | -1.4762 | -1.2106 | -0.9567 | ******* |
| 0.925 | ******* | -1.4849 | -1.1511 | -0.9406 | -0.5838 |
| 0.950 | -1.5160 | -1.4852 | -1.1380 | -0.9407 | -0.5277 |
| 0.975 | ******* | -1.4783 | -1.1252 | -0.9118 | -0.5023 |
| 1.000 | -1.4935 | -1.4794 | -1.1164 | -0.8569 | -0.4722 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5936 | 0.5207 | 0.4796 | ******* | -0.5367 |
| -0.400 | 0.5885 | 0.5285 | 0.4556 | 0.2402 | -0.6044 |
| -0.600 | 0.5851 | 0.5197 | 0.4455 | 0.2658 | -0.5832 |
| -0.700 | ******* | 0.5120 | 0.4444 | 0.2757 | -0.5479 |
| -0.800 | ******* | ******* | 0.4326 | 0.2867 | -0.4684 |
| -0.850 | ******* | 0.4405 | 0.4059 | 0.2873 | -0.4411 |
| -0.900 | 0.4479 | 0.3503 | 0.3532 | 0.2586 | -0.3835 |
| -0.950 | 0.3423 | 0.1030 | 0.1903 | 0.1592 | -0.1508 |
| -0.975 | ******* | -0.0766 | -0.0070 | 0.0045 | -0.1251 |
| -1.000 | -1.5216 | -1.4780 | -0.7773 | -0.7103 | -0.4682 |

Surface Pressures




Small Radius L.E.

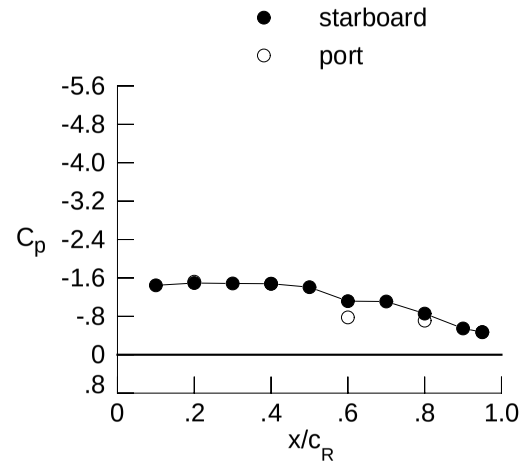
Run No. = 39 , Point No. = 805

$C_N$ = 1.140, $C_m$ = -0.1824

$\alpha$ = 25.6 °, $M_\infty$ = 0.802

$R_{mac}$ = $6.0 \times 10^6$

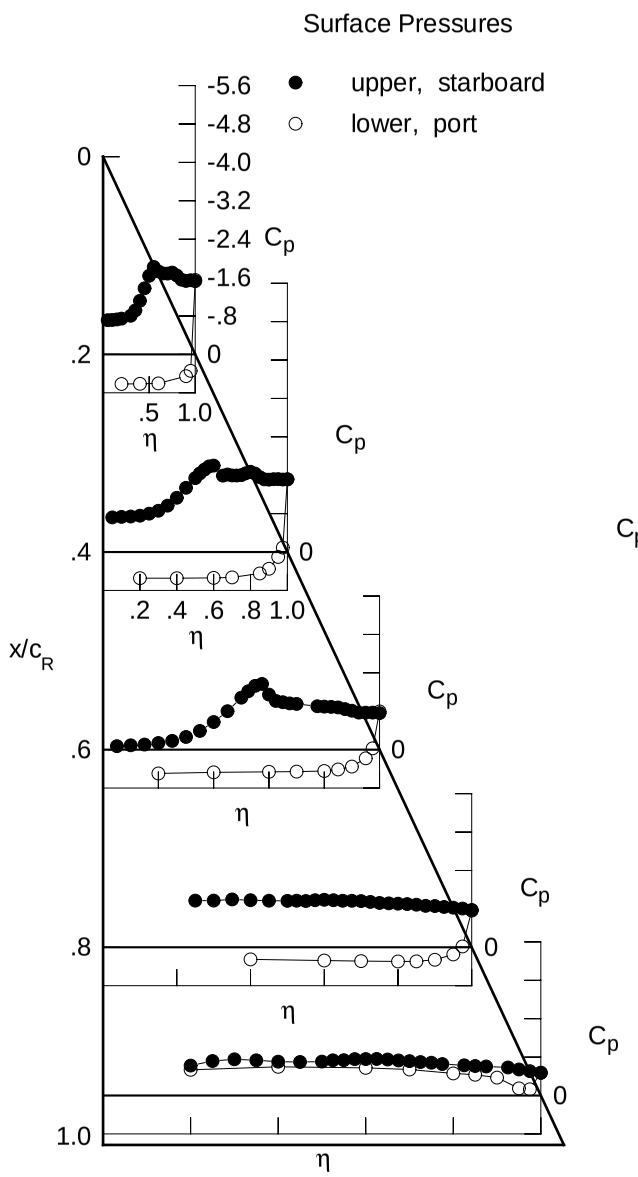
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.4459 | ******* |
| 0.20 | -1.4935 | -1.5216 |
| 0.30 | -1.4845 | ******* |
| 0.40 | -1.4794 | -1.4780 |
| 0.50 | -1.4071 | ******* |
| 0.60 | -1.1164 | -0.7773 |
| 0.70 | -1.1085 | ******* |
| 0.80 | -0.8569 | -0.7103 |
| 0.90 | -0.5469 | ******* |
| 0.95 | -0.4722 | -0.4682 |

# Table D3. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.7127 | -0.7214 | -0.0718 | ******* | ******* |
| 0.100 | -0.7175 | -0.7319 | -0.0903 | ******* | ******* |
| 0.150 | -0.7284 | -0.7403 | -0.1059 | ******* | ******* |
| 0.200 | -0.7452 | -0.7565 | -0.1383 | ******* | -0.6236 |
| 0.250 | ******* | -0.7991 | -0.1820 | -0.9719 | -0.7184 |
| 0.300 | -0.8049 | -0.8601 | -0.2640 | -0.9731 | -0.7545 |
| 0.350 | -0.9157 | -0.9667 | -0.3895 | -0.9964 | -0.7339 |
| 0.400 | -1.1169 | -1.1303 | -0.5756 | -0.9812 | -0.7048 |
| 0.450 | -1.3771 | -1.3381 | -0.8009 | -0.9701 | -0.6983 |
| 0.500 | -1.6375 | -1.5395 | -1.0822 | -0.9669 | -0.7064 |
| 0.525 | ******* | -1.6375 | -1.2157 | -0.9706 | -0.7332 |
| 0.550 | -1.8220 | -1.7164 | -1.3289 | -0.9638 | -0.7364 |
| 0.575 | ******* | -1.7840 | -1.3689 | -0.9805 | -0.7581 |
| 0.600 | -1.7285 | -1.8010 | -1.1467 | -0.9893 | -0.7596 |
| 0.625 | ******* | ******* | -1.0143 | -0.9805 | -0.7618 |
| 0.650 | -1.6861 | -1.5921 | -0.9877 | -0.9698 | -0.7504 |
| 0.675 | ******* | -1.6155 | -0.9634 | -0.9690 | -0.7304 |
| 0.700 | -1.6835 | -1.5954 | -0.9517 | -0.9628 | -0.7163 |
| 0.725 | ******* | -1.5948 | ******* | -0.9452 | -0.6972 |
| 0.750 | -1.7049 | -1.6020 | ******* | -0.9239 | -0.6832 |
| 0.775 | ******* | -1.6413 | -0.9041 | -0.9153 | -0.6553 |
| 0.800 | -1.6432 | -1.6717 | -0.8958 | -0.9085 | ******* |
| 0.825 | ******* | -1.6339 | -0.8902 | -0.9004 | -0.6286 |
| 0.850 | -1.5571 | -1.5601 | -0.8790 | -0.8868 | -0.6145 |
| 0.875 | ******* | -1.5144 | -0.8450 | -0.8629 | -0.6045 |
| 0.900 | -1.5306 | -1.5077 | -0.8112 | -0.8591 | ******* |
| 0.925 | ******* | -1.5178 | -0.7713 | -0.8400 | -0.5839 |
| 0.950 | -1.5447 | -1.5189 | -0.7704 | -0.8257 | -0.5427 |
| 0.975 | ******* | -1.5104 | -0.7715 | -0.8075 | -0.5072 |
| 1.000 | -1.5260 | -1.5126 | -0.7607 | -0.7786 | -0.4706 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.6167 | 0.5445 | 0.4959 | ******* | -0.5348 |
| -0.400 | 0.6128 | 0.5457 | 0.4732 | 0.2516 | -0.5980 |
| -0.600 | 0.6051 | 0.5383 | 0.4625 | 0.2762 | -0.5760 |
| -0.700 | ******* | 0.5285 | 0.4579 | 0.2876 | -0.5415 |
| -0.800 | ******* | ******* | 0.4455 | 0.2953 | -0.4600 |
| -0.850 | ******* | 0.4463 | 0.4129 | 0.2934 | -0.4328 |
| -0.900 | 0.4534 | 0.3490 | 0.3529 | 0.2597 | -0.3731 |
| -0.950 | 0.3421 | 0.1023 | 0.1807 | 0.1488 | -0.1478 |
| -0.975 | ******* | -0.0930 | -0.0271 | -0.0173 | -0.1300 |
| -1.000 | -1.5505 | -1.5172 | -0.7961 | -0.7636 | -0.4770 |



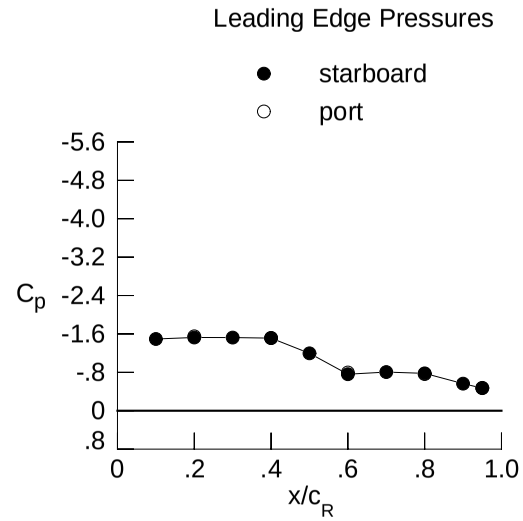

Small Radius L.E.

Run No. = 39 , Point No. = 806

$C_N$ = 1.174, $C_m$ = -0.1814

$\alpha$ = 26.7 °, $M_\infty$ = 0.800

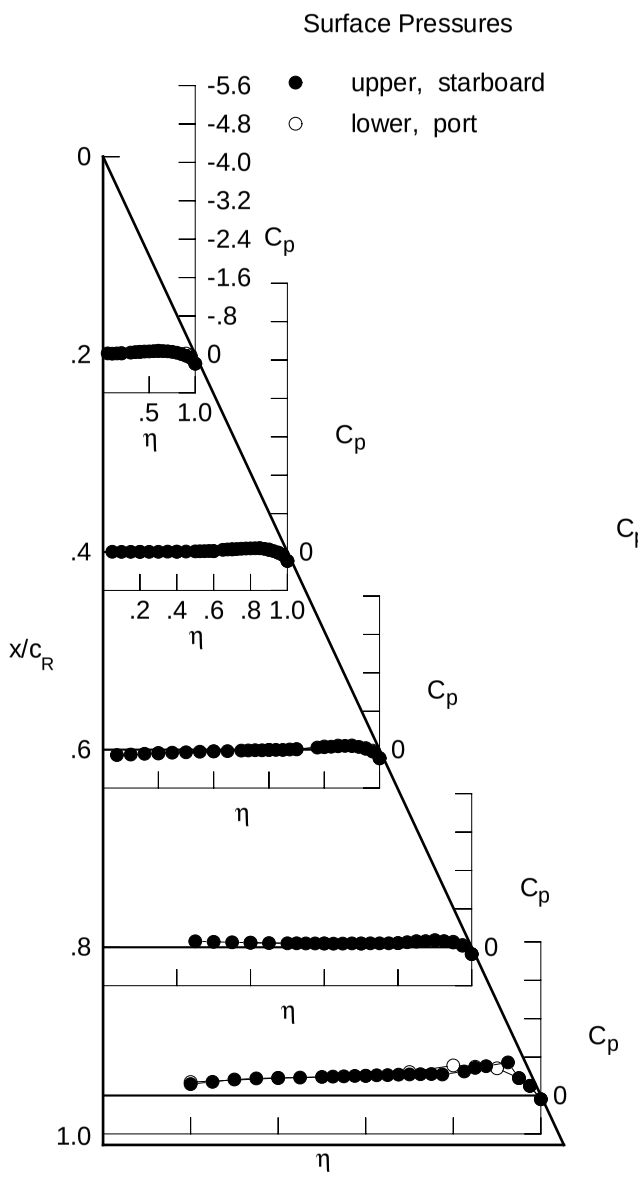
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.4946 | ******* |
| 0.20 | -1.5260 | -1.5505 |
| 0.30 | -1.5242 | ******* |
| 0.40 | -1.5126 | -1.5172 |
| 0.50 | -1.1963 | ******* |
| 0.60 | -0.7607 | -0.7961 |
| 0.70 | -0.8054 | ******* |
| 0.80 | -0.7786 | -0.7636 |
| 0.90 | -0.5643 | ******* |
| 0.95 | -0.4706 | -0.4770 |

# Table D3. Concluded.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0206 | -0.0053 | 0.1129 | ******* | ******* |
| 0.100 | -0.0148 | -0.0030 | 0.1023 | ******* | ******* |
| 0.150 | -0.0199 | -0.0037 | 0.0862 | ******* | ******* |
| 0.200 | -0.0191 | -0.0037 | 0.0796 | ******* | -0.2376 |
| 0.250 | ******* | -0.0037 | 0.0632 | -0.1247 | -0.2849 |
| 0.300 | -0.0367 | -0.0047 | 0.0554 | -0.1134 | -0.3335 |
| 0.350 | -0.0476 | -0.0089 | 0.0430 | -0.1039 | -0.3559 |
| 0.400 | -0.0508 | -0.0065 | 0.0366 | -0.0958 | -0.3677 |
| 0.450 | -0.0592 | -0.0100 | 0.0312 | -0.0879 | -0.3740 |
| 0.500 | -0.0617 | -0.0136 | 0.0200 | -0.0833 | -0.3876 |
| 0.525 | ******* | -0.0161 | 0.0170 | -0.0829 | -0.3933 |
| 0.550 | -0.0675 | -0.0179 | 0.0121 | -0.0802 | -0.3994 |
| 0.575 | ******* | -0.0219 | 0.0139 | -0.0798 | -0.4079 |
| 0.600 | -0.0704 | -0.0211 | 0.0067 | -0.0811 | -0.4132 |
| 0.625 | ******* | ******* | 0.0051 | -0.0751 | -0.4214 |
| 0.650 | -0.0689 | -0.0465 | 0.0061 | -0.0765 | -0.4252 |
| 0.675 | ******* | -0.0535 | -0.0034 | -0.0808 | -0.4341 |
| 0.700 | -0.0637 | -0.0546 | -0.0053 | -0.0756 | -0.4394 |
| 0.725 | ******* | -0.0617 | ******* | -0.0822 | -0.4440 |
| 0.750 | -0.0532 | -0.0691 | ******* | -0.0826 | -0.4471 |
| 0.775 | ******* | -0.0735 | -0.0435 | -0.0835 | -0.4384 |
| 0.800 | -0.0347 | -0.0758 | -0.0508 | -0.0853 | ******* |
| 0.825 | ******* | -0.0782 | -0.0610 | -0.1060 | -0.5010 |
| 0.850 | -0.0066 | -0.0789 | -0.0700 | -0.1187 | -0.5760 |
| 0.875 | ******* | -0.0667 | -0.0786 | -0.1277 | -0.6103 |
| 0.900 | 0.0288 | -0.0433 | -0.0742 | -0.1386 | ******* |
| 0.925 | ******* | -0.0198 | -0.0570 | -0.1292 | -0.6897 |
| 0.950 | 0.0717 | 0.0154 | -0.0176 | -0.1001 | -0.3625 |
| 0.975 | ******* | 0.0572 | 0.0399 | -0.0325 | -0.1985 |
| 1.000 | 0.1932 | 0.1865 | 0.1834 | 0.1406 | 0.0765 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0263 | -0.0042 | 0.0690 | ******* | -0.2802 |
| -0.400 | -0.0545 | -0.0077 | 0.0332 | -0.0945 | -0.3628 |
| -0.600 | -0.0763 | -0.0169 | 0.0042 | -0.0772 | -0.4072 |
| -0.700 | ******* | -0.0595 | -0.0114 | -0.0797 | -0.4884 |
| -0.800 | ******* | ******* | -0.0653 | -0.0880 | -0.6262 |
| -0.850 | ******* | -0.0798 | -0.0851 | -0.1272 | -0.5990 |
| -0.900 | -0.0167 | -0.0536 | -0.0870 | -0.1499 | -0.5675 |
| -0.950 | 0.0188 | 0.0101 | -0.0320 | -0.1143 | -0.3625 |
| -0.975 | ******* | 0.0584 | 0.0203 | -0.0475 | -0.2036 |
| -1.000 | 0.1937 | 0.1849 | 0.1739 | 0.1443 | 0.0780 |



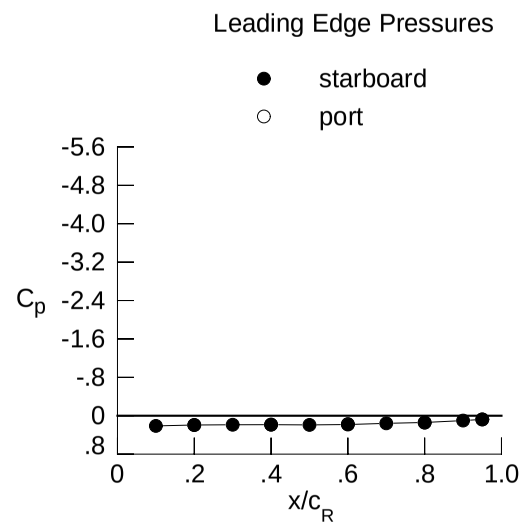

Small Radius L.E.

Run No. = 39 , Point No. = 807

$C_N$ = -0.012, $C_m$ = 0.0039

$\alpha$ = 0.1 °, $M_\infty$ = 0.801

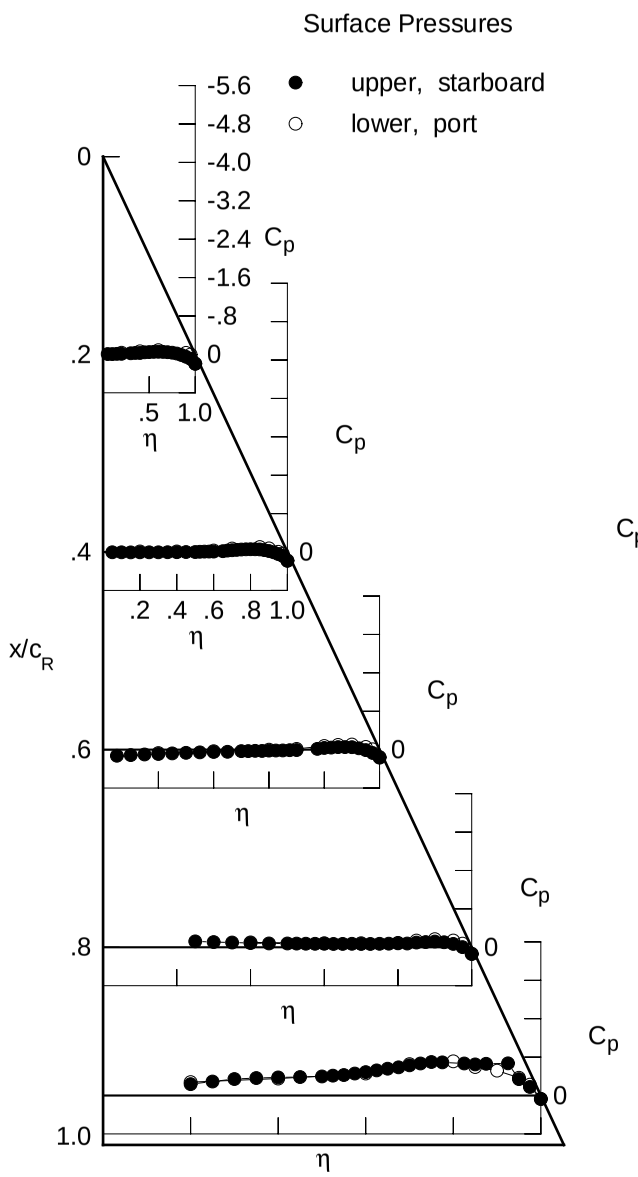
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2121 | ******* |
| 0.20 | 0.1932 | 0.1937 |
| 0.30 | 0.1882 | ******* |
| 0.40 | 0.1865 | 0.1849 |
| 0.50 | 0.1913 | ******* |
| 0.60 | 0.1834 | 0.1739 |
| 0.70 | 0.1588 | ******* |
| 0.80 | 0.1406 | 0.1443 |
| 0.90 | 0.1012 | ******* |
| 0.95 | 0.0765 | 0.0780 |

# Table D4. Tabulations and Plots of Surface Pressure Coefficients.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0071 | 0.0044 | 0.1269 | ******* | ******* |
| 0.100 | -0.0065 | 0.0056 | 0.1138 | ******* | ******* |
| 0.150 | -0.0112 | 0.0070 | 0.1009 | ******* | ******* |
| 0.200 | -0.0119 | 0.0059 | 0.0907 | ******* | -0.2370 |
| 0.250 | ******* | 0.0056 | 0.0785 | -0.1234 | -0.2915 |
| 0.300 | -0.0230 | 0.0054 | 0.0664 | -0.1087 | -0.3429 |
| 0.350 | -0.0301 | 0.0039 | 0.0567 | -0.0996 | -0.3639 |
| 0.400 | -0.0296 | 0.0033 | 0.0479 | -0.0884 | -0.3770 |
| 0.450 | -0.0431 | 0.0002 | 0.0445 | -0.0796 | -0.3851 |
| 0.500 | -0.0481 | -0.0004 | 0.0313 | -0.0789 | -0.3966 |
| 0.525 | ******* | -0.0054 | 0.0304 | -0.0764 | -0.4139 |
| 0.550 | -0.0525 | -0.0087 | 0.0249 | -0.0740 | -0.4266 |
| 0.575 | ******* | -0.0097 | 0.0271 | -0.0730 | -0.4574 |
| 0.600 | -0.0545 | -0.0094 | 0.0201 | -0.0739 | -0.4870 |
| 0.625 | ******* | ******* | 0.0181 | -0.0698 | -0.5230 |
| 0.650 | -0.0524 | -0.0176 | 0.0172 | -0.0701 | -0.5583 |
| 0.675 | ******* | -0.0303 | 0.0112 | -0.0728 | -0.5875 |
| 0.700 | -0.0456 | -0.0377 | 0.0091 | -0.0696 | -0.6288 |
| 0.725 | ******* | -0.0447 | ******* | -0.0696 | -0.6672 |
| 0.750 | -0.0354 | -0.0524 | ******* | -0.0732 | -0.6975 |
| 0.775 | ******* | -0.0570 | -0.0162 | -0.0748 | -0.6900 |
| 0.800 | -0.0178 | -0.0585 | -0.0355 | -0.0821 | ******* |
| 0.825 | ******* | -0.0573 | -0.0422 | -0.0783 | -0.6673 |
| 0.850 | 0.0128 | -0.0540 | -0.0525 | -0.0986 | -0.6478 |
| 0.875 | ******* | -0.0401 | -0.0527 | -0.1088 | -0.6606 |
| 0.900 | 0.0494 | -0.0208 | -0.0516 | -0.1198 | ******* |
| 0.925 | ******* | 0.0052 | -0.0279 | -0.1044 | -0.6703 |
| 0.950 | 0.0936 | 0.0415 | 0.0098 | -0.0703 | -0.3417 |
| 0.975 | ******* | 0.0813 | 0.0696 | -0.0028 | -0.1785 |
| 1.000 | 0.1970 | 0.1833 | 0.1670 | 0.1406 | 0.0696 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0344 | -0.0118 | 0.0712 | ******* | -0.2789 |
| -0.400 | -0.0639 | -0.0121 | 0.0327 | -0.1019 | -0.3529 |
| -0.600 | -0.0879 | -0.0309 | 0.0009 | -0.0845 | -0.4583 |
| -0.700 | ******* | -0.0727 | -0.0149 | -0.0848 | -0.6537 |
| -0.800 | ******* | ******* | -0.0762 | -0.0919 | -0.7120 |
| -0.850 | ******* | -0.1043 | -0.0985 | -0.1401 | -0.5939 |
| -0.900 | -0.0322 | -0.0759 | -0.1065 | -0.1697 | -0.5184 |
| -0.950 | 0.0016 | -0.0045 | -0.0569 | -0.1409 | -0.3699 |
| -0.975 | ******* | 0.0327 | -0.0071 | -0.0761 | -0.2268 |
| -1.000 | 0.1902 | 0.1754 | 0.1535 | 0.1325 | 0.0733 |



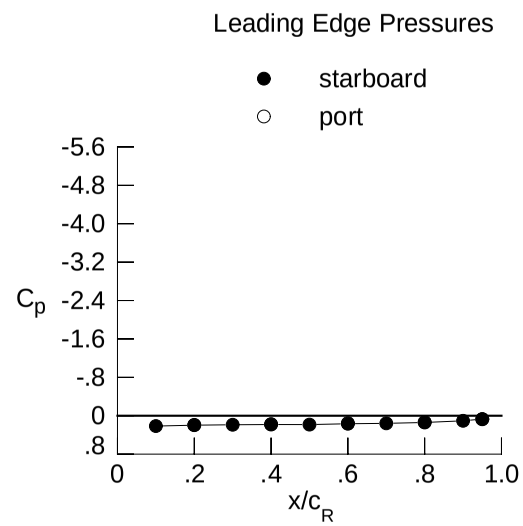

Small Radius L.E.

Run No. = 40 , Point No. = 808

$C_N$ = -0.031, $C_m$ = 0.0075

$\alpha$ = -0.4 °, $M_\infty$ = 0.829

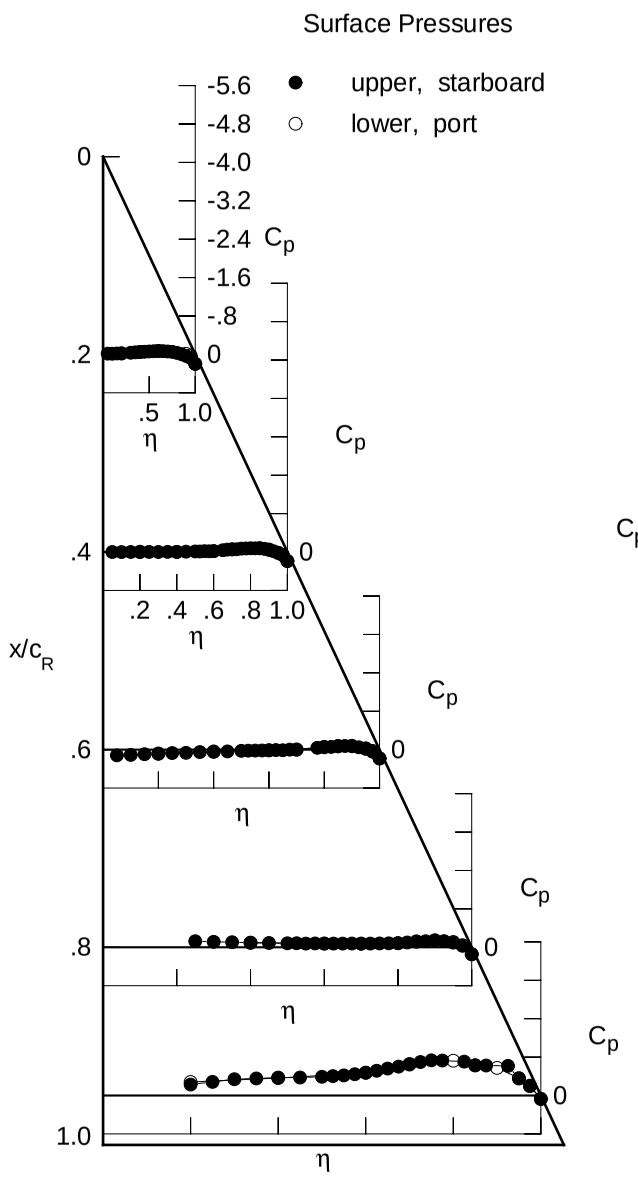
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2154 | ******* |
| 0.20 | 0.1970 | 0.1902 |
| 0.30 | 0.1881 | ******* |
| 0.40 | 0.1833 | 0.1754 |
| 0.50 | 0.1845 | ******* |
| 0.60 | 0.1670 | 0.1535 |
| 0.70 | 0.1587 | ******* |
| 0.80 | 0.1406 | 0.1325 |
| 0.90 | 0.1058 | ******* |
| 0.95 | 0.0696 | 0.0733 |

# Table D4. Continued.

| η | x/c_R .2 C_p,u | x/c_R .4 C_p,u | x/c_R .6 C_p,u | x/c_R .8 C_p,u | x/c_R .95 C_p,u |
|---|---|---|---|---|---|
| 0.050 | -0.0149 | -0.0008 | 0.1194 | ******* | ******* |
| 0.100 | -0.0138 | 0.0007 | 0.1098 | ******* | ******* |
| 0.150 | -0.0188 | -0.0011 | 0.0949 | ******* | ******* |
| 0.200 | -0.0185 | 0.0005 | 0.0861 | ******* | -0.2278 |
| 0.250 | ******* | -0.0024 | 0.0712 | -0.1260 | -0.2843 |
| 0.300 | -0.0341 | -0.0005 | 0.0661 | -0.1138 | -0.3392 |
| 0.350 | -0.0424 | -0.0034 | 0.0501 | -0.1052 | -0.3554 |
| 0.400 | -0.0482 | -0.0041 | 0.0455 | -0.0938 | -0.3733 |
| 0.450 | -0.0554 | -0.0082 | 0.0366 | -0.0892 | -0.3752 |
| 0.500 | -0.0605 | -0.0118 | 0.0247 | -0.0835 | -0.3907 |
| 0.525 | ******* | -0.0110 | 0.0218 | -0.0838 | -0.4041 |
| 0.550 | -0.0654 | -0.0179 | 0.0195 | -0.0771 | -0.4195 |
| 0.575 | ******* | -0.0155 | 0.0173 | -0.0804 | -0.4428 |
| 0.600 | -0.0680 | -0.0183 | 0.0157 | -0.0788 | -0.4770 |
| 0.625 | ******* | ******* | 0.0087 | -0.0770 | -0.5158 |
| 0.650 | -0.0671 | -0.0374 | 0.0128 | -0.0770 | -0.5609 |
| 0.675 | ******* | -0.0508 | 0.0000 | -0.0783 | -0.6013 |
| 0.700 | -0.0612 | -0.0565 | 0.0025 | -0.0749 | -0.6561 |
| 0.725 | ******* | -0.0575 | ******* | -0.0774 | -0.6979 |
| 0.750 | -0.0526 | -0.0710 | ******* | -0.0800 | -0.7330 |
| 0.775 | ******* | -0.0747 | -0.0387 | -0.0823 | -0.7288 |
| 0.800 | -0.0320 | -0.0788 | -0.0494 | -0.0866 | ******* |
| 0.825 | ******* | -0.0767 | -0.0568 | -0.1003 | -0.7053 |
| 0.850 | -0.0051 | -0.0790 | -0.0675 | -0.1180 | -0.6304 |
| 0.875 | ******* | -0.0672 | -0.0763 | -0.1266 | -0.6251 |
| 0.900 | 0.0321 | -0.0460 | -0.0705 | -0.1373 | ******* |
| 0.925 | ******* | -0.0169 | -0.0492 | -0.1284 | -0.6178 |
| 0.950 | 0.0750 | 0.0196 | -0.0166 | -0.0965 | -0.3536 |
| 0.975 | ******* | 0.0619 | 0.0442 | -0.0315 | -0.1954 |
| 1.000 | 0.1968 | 0.1863 | 0.1861 | 0.1424 | 0.0661 |
| | C_p,l | C_p,l | C_p,l | C_p,l | C_p,l |
| -0.200 | -0.0236 | -0.0072 | 0.0809 | ******* | -0.2818 |
| -0.400 | -0.0520 | -0.0007 | 0.0380 | -0.0968 | -0.3636 |
| -0.600 | -0.0735 | -0.0182 | 0.0113 | -0.0759 | -0.4720 |
| -0.700 | ******* | -0.0555 | -0.0049 | -0.0755 | -0.6445 |
| -0.800 | ******* | ******* | -0.0587 | -0.0840 | -0.7244 |
| -0.850 | ******* | -0.0787 | -0.0783 | -0.1226 | -0.6262 |
| -0.900 | -0.0120 | -0.0522 | -0.0815 | -0.1469 | -0.5752 |
| -0.950 | 0.0209 | 0.0143 | -0.0280 | -0.1100 | -0.3613 |
| -0.975 | ******* | 0.0626 | 0.0256 | -0.0438 | -0.2054 |
| -1.000 | 0.1987 | 0.1894 | 0.1797 | 0.1473 | 0.0752 |



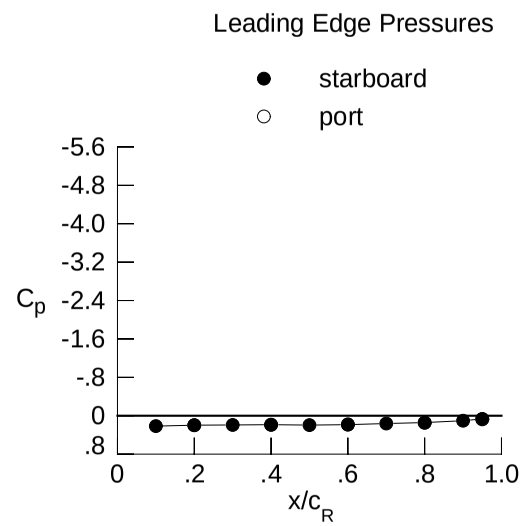

Small Radius L.E.

Run No. = 40 , Point No. = 809

$C_N$ = -0.010, $C_m$ = 0.0026

$\alpha$ = 0.1 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

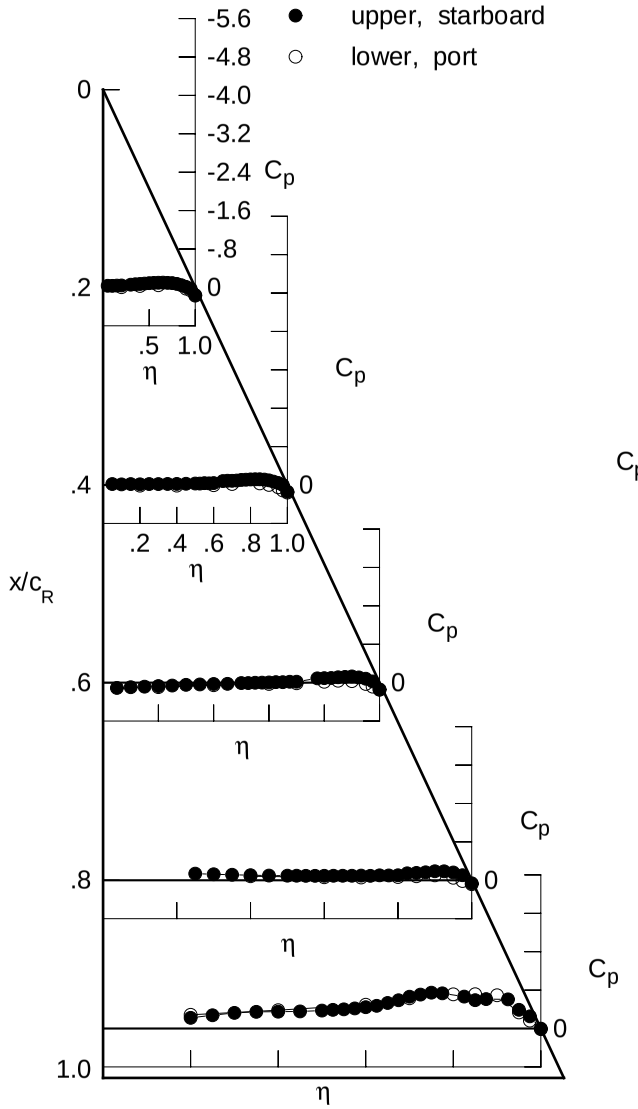



| x/c_R | starb'd C_p | port C_p |
|---|---|---|
| 0.10 | 0.2163 | ******* |
| 0.20 | 0.1968 | 0.1987 |
| 0.30 | 0.1923 | ******* |
| 0.40 | 0.1863 | 0.1894 |
| 0.50 | 0.1952 | ******* |
| 0.60 | 0.1861 | 0.1797 |
| 0.70 | 0.1627 | ******* |
| 0.80 | 0.1424 | 0.1473 |
| 0.90 | 0.1039 | ******* |
| 0.95 | 0.0661 | 0.0752 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0340 | -0.0204 | 0.1101 | ******* | ******* |
| 0.100 | -0.0318 | -0.0139 | 0.0951 | ******* | ******* |
| 0.150 | -0.0377 | -0.0201 | 0.0843 | ******* | ******* |
| 0.200 | -0.0396 | -0.0150 | 0.0709 | ******* | -0.2227 |
| 0.250 | ******* | -0.0206 | 0.0605 | -0.1382 | -0.2763 |
| 0.300 | -0.0559 | -0.0198 | 0.0459 | -0.1255 | -0.3253 |
| 0.350 | -0.0655 | -0.0226 | 0.0377 | -0.1151 | -0.3468 |
| 0.400 | -0.0715 | -0.0233 | 0.0282 | -0.1062 | -0.3506 |
| 0.450 | -0.0791 | -0.0261 | 0.0245 | -0.0984 | -0.3557 |
| 0.500 | -0.0877 | -0.0310 | 0.0088 | -0.0960 | -0.3735 |
| 0.525 | ******* | -0.0301 | 0.0084 | -0.0950 | -0.3889 |
| 0.550 | -0.0933 | -0.0391 | 0.0024 | -0.0927 | -0.3994 |
| 0.575 | ******* | -0.0349 | -0.0004 | -0.0926 | -0.4181 |
| 0.600 | -0.0971 | -0.0412 | -0.0037 | -0.0939 | -0.4442 |
| 0.625 | ******* | ******* | -0.0101 | -0.0944 | -0.4727 |
| 0.650 | -0.0994 | -0.0824 | -0.0098 | -0.0942 | -0.5321 |
| 0.675 | ******* | -0.0897 | -0.0188 | -0.0941 | -0.5889 |
| 0.700 | -0.0948 | -0.0882 | -0.0188 | -0.0973 | -0.6621 |
| 0.725 | ******* | -0.0933 | ******* | -0.0930 | -0.7060 |
| 0.750 | -0.0898 | -0.1061 | ******* | -0.1028 | -0.7461 |
| 0.775 | ******* | -0.1112 | -0.0899 | -0.1007 | -0.7329 |
| 0.800 | -0.0730 | -0.1179 | -0.0937 | -0.1050 | ******* |
| 0.825 | ******* | -0.1211 | -0.0966 | -0.1457 | -0.6645 |
| 0.850 | -0.0453 | -0.1205 | -0.1120 | -0.1536 | -0.5902 |
| 0.875 | ******* | -0.1136 | -0.1195 | -0.1663 | -0.6126 |
| 0.900 | -0.0108 | -0.0979 | -0.1294 | -0.1881 | ******* |
| 0.925 | ******* | -0.0713 | -0.1086 | -0.1874 | -0.6071 |
| 0.950 | 0.0263 | -0.0431 | -0.0813 | -0.1621 | -0.3897 |
| 0.975 | ******* | -0.0014 | -0.0257 | -0.1056 | -0.2536 |
| 1.000 | 0.1607 | 0.1388 | 0.1435 | 0.0623 | 0.0024 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0039 | 0.0124 | 0.0933 | ******* | -0.2857 |
| -0.400 | -0.0295 | 0.0119 | 0.0537 | -0.0838 | -0.3819 |
| -0.600 | -0.0452 | 0.0031 | 0.0273 | -0.0636 | -0.4955 |
| -0.700 | ******* | -0.0217 | 0.0126 | -0.0585 | -0.6295 |
| -0.800 | ******* | ******* | -0.0186 | -0.0678 | -0.7119 |
| -0.850 | ******* | -0.0346 | -0.0398 | -0.0843 | -0.7140 |
| -0.900 | 0.0256 | -0.0025 | -0.0314 | -0.1033 | -0.6929 |
| -0.950 | 0.0615 | 0.0463 | 0.0270 | -0.0528 | -0.3352 |
| -0.975 | ******* | 0.1122 | 0.0835 | 0.0154 | -0.1648 |
| -1.000 | 0.1719 | 0.1565 | 0.1462 | 0.0817 | 0.0138 |

Surface Pressures




Small Radius L.E.

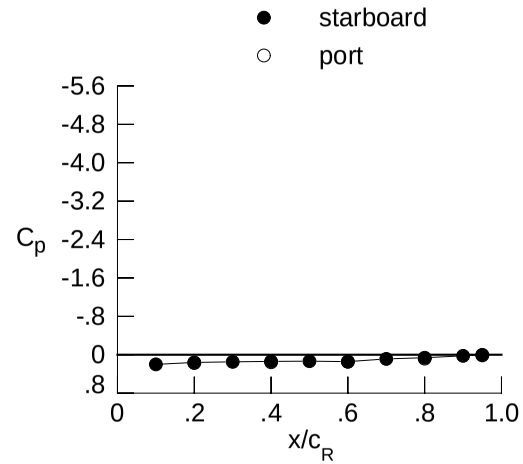
Run No. = 40 , Point No. = 810

$C_N$ = 0.032, $C_m$ = -0.0050

$\alpha$ = 1.1 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

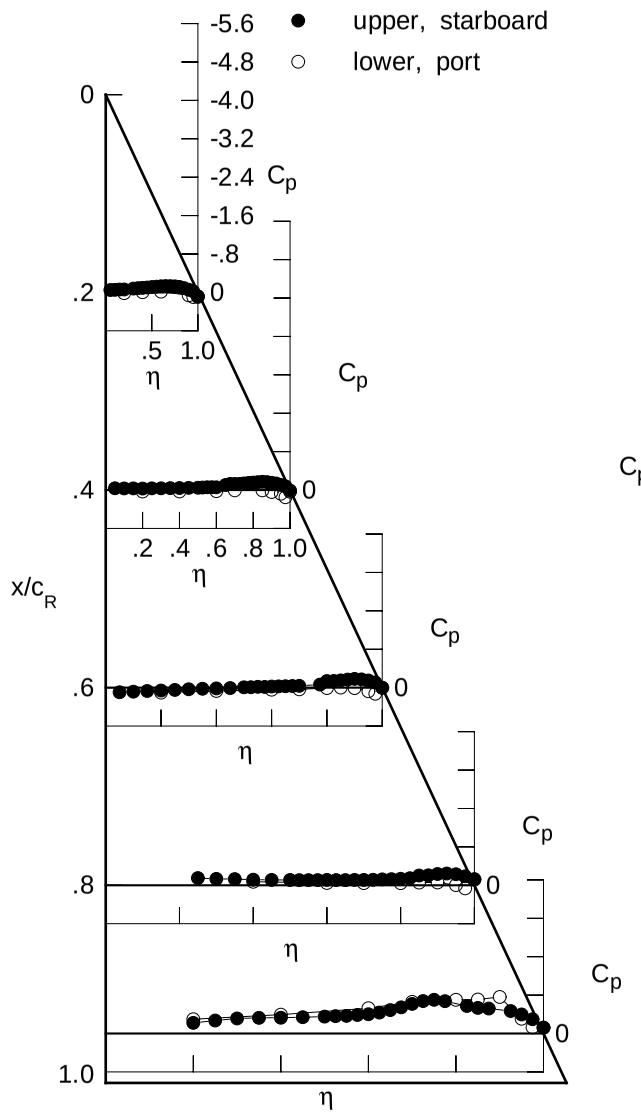



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2012 | ******* |
| 0.20 | 0.1607 | 0.1719 |
| 0.30 | 0.1481 | ******* |
| 0.40 | 0.1388 | 0.1565 |
| 0.50 | 0.1343 | ******* |
| 0.60 | 0.1435 | 0.1462 |
| 0.70 | 0.0872 | ******* |
| 0.80 | 0.0623 | 0.0817 |
| 0.90 | 0.0228 | ******* |
| 0.95 | 0.0024 | 0.0138 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0497 | -0.0370 | 0.0959 | ******* | ******* |
| 0.100 | -0.0533 | -0.0338 | 0.0838 | ******* | ******* |
| 0.150 | -0.0598 | -0.0344 | 0.0699 | ******* | ******* |
| 0.200 | -0.0609 | -0.0304 | 0.0598 | ******* | -0.2214 |
| 0.250 | ******* | -0.0352 | 0.0469 | -0.1503 | -0.2701 |
| 0.300 | -0.0795 | -0.0358 | 0.0334 | -0.1334 | -0.3134 |
| 0.350 | -0.0883 | -0.0391 | 0.0236 | -0.1289 | -0.3267 |
| 0.400 | -0.0944 | -0.0413 | 0.0160 | -0.1169 | -0.3290 |
| 0.450 | -0.1019 | -0.0460 | 0.0085 | -0.1120 | -0.3396 |
| 0.500 | -0.1108 | -0.0480 | -0.0070 | -0.1105 | -0.3521 |
| 0.525 | ******* | -0.0521 | -0.0085 | -0.1075 | -0.3618 |
| 0.550 | -0.1191 | -0.0579 | -0.0180 | -0.1071 | -0.3682 |
| 0.575 | ******* | -0.0585 | -0.0145 | -0.1079 | -0.3864 |
| 0.600 | -0.1269 | -0.0565 | -0.0231 | -0.1117 | -0.4018 |
| 0.625 | ******* | ******* | -0.0262 | -0.1092 | -0.4357 |
| 0.650 | -0.1312 | -0.1050 | -0.0293 | -0.1083 | -0.4877 |
| 0.675 | ******* | -0.1272 | -0.0345 | -0.1127 | -0.5458 |
| 0.700 | -0.1297 | -0.1258 | -0.0376 | -0.1119 | -0.6168 |
| 0.725 | ******* | -0.1276 | ******* | -0.1144 | -0.6762 |
| 0.750 | -0.1261 | -0.1373 | ******* | -0.1232 | -0.7025 |
| 0.775 | ******* | -0.1483 | -0.0641 | -0.1271 | -0.6733 |
| 0.800 | -0.1136 | -0.1555 | -0.1368 | -0.1362 | ******* |
| 0.825 | ******* | -0.1631 | -0.1393 | -0.1469 | -0.5736 |
| 0.850 | -0.0884 | -0.1722 | -0.1513 | -0.2032 | -0.5334 |
| 0.875 | ******* | -0.1655 | -0.1682 | -0.2081 | -0.5199 |
| 0.900 | -0.0561 | -0.1506 | -0.1820 | -0.2354 | ******* |
| 0.925 | ******* | -0.1359 | -0.1723 | -0.2447 | -0.4682 |
| 0.950 | -0.0217 | -0.1058 | -0.1496 | -0.2307 | -0.3968 |
| 0.975 | ******* | -0.0775 | -0.1099 | -0.1879 | -0.2980 |
| 1.000 | 0.0813 | 0.0093 | 0.0026 | -0.1286 | -0.1204 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0162 | 0.0300 | 0.1028 | ******* | -0.2979 |
| -0.400 | -0.0037 | 0.0294 | 0.0686 | -0.0738 | -0.3929 |
| -0.600 | -0.0162 | 0.0231 | 0.0427 | -0.0477 | -0.5265 |
| -0.700 | ******* | 0.0060 | 0.0350 | -0.0453 | -0.6596 |
| -0.800 | ******* | ******* | 0.0087 | -0.0441 | -0.7026 |
| -0.850 | ******* | 0.0063 | -0.0014 | -0.0560 | -0.7077 |
| -0.900 | 0.0612 | 0.0418 | 0.0100 | -0.0595 | -0.7616 |
| -0.950 | 0.0967 | 0.0769 | 0.0750 | -0.0040 | -0.3079 |
| -0.975 | ******* | 0.1507 | 0.1275 | 0.0641 | -0.1285 |
| -1.000 | 0.0947 | 0.0344 | 0.0015 | -0.1157 | -0.1235 |

Surface Pressures




Small Radius L.E.

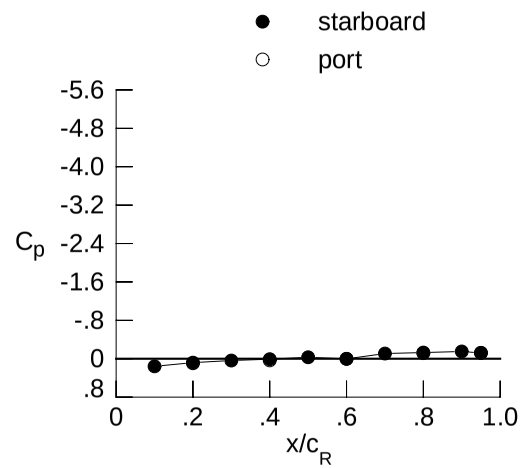
Run No. = 40 , Point No. = 811

$C_N$ = 0.071, $C_m$ = -0.0108

$\alpha$ = 2.2 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

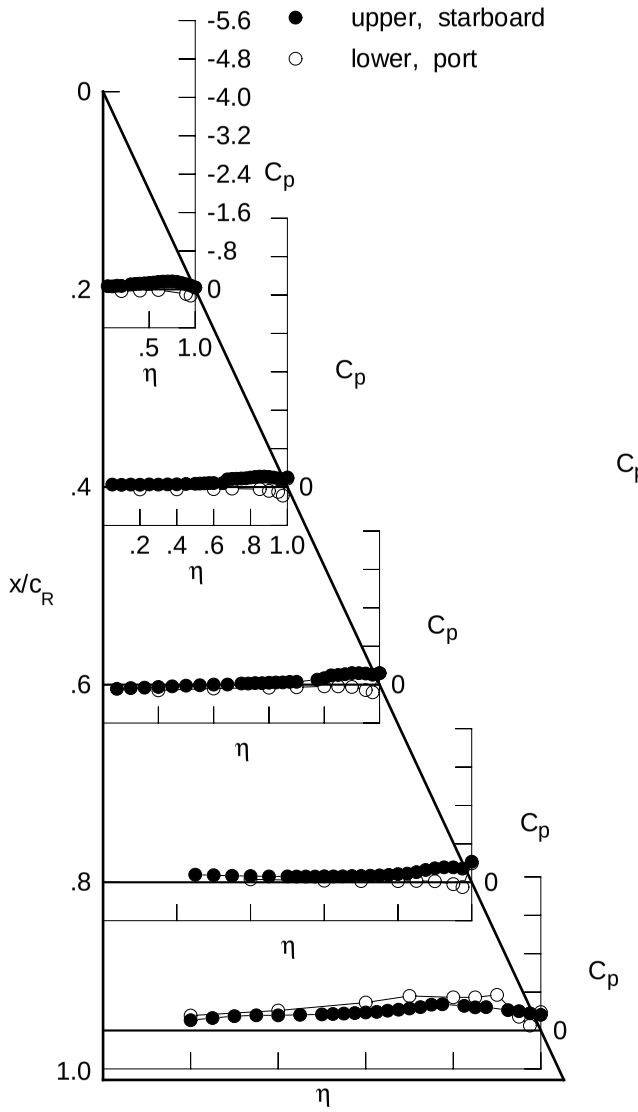



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.1581 | ******* |
| 0.20 | 0.0813 | 0.0947 |
| 0.30 | 0.0373 | ******* |
| 0.40 | 0.0093 | 0.0344 |
| 0.50 | -0.0304 | ******* |
| 0.60 | 0.0026 | 0.0015 |
| 0.70 | -0.1083 | ******* |
| 0.80 | -0.1286 | -0.1157 |
| 0.90 | -0.1509 | ******* |
| 0.95 | -0.1204 | -0.1235 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0670 | -0.0511 | 0.0872 | ******* | ******* |
| 0.100 | -0.0622 | -0.0455 | 0.0724 | ******* | ******* |
| 0.150 | -0.0766 | -0.0510 | 0.0624 | ******* | ******* |
| 0.200 | -0.0723 | -0.0479 | 0.0478 | ******* | -0.2143 |
| 0.250 | ******* | -0.0543 | 0.0356 | -0.1582 | -0.2601 |
| 0.300 | -0.1057 | -0.0501 | 0.0208 | -0.1468 | -0.2993 |
| 0.350 | -0.1137 | -0.0555 | 0.0126 | -0.1350 | -0.3164 |
| 0.400 | -0.1181 | -0.0571 | -0.0013 | -0.1300 | -0.3163 |
| 0.450 | -0.1254 | -0.0643 | -0.0027 | -0.1217 | -0.3271 |
| 0.500 | -0.1338 | -0.0682 | -0.0242 | -0.1226 | -0.3349 |
| 0.525 | ******* | -0.0720 | -0.0221 | -0.1198 | -0.3442 |
| 0.550 | -0.1427 | -0.0769 | -0.0323 | -0.1198 | -0.3531 |
| 0.575 | ******* | -0.0821 | -0.0308 | -0.1194 | -0.3635 |
| 0.600 | -0.1551 | -0.0822 | -0.0397 | -0.1252 | -0.3763 |
| 0.625 | ******* | ******* | -0.0446 | -0.1227 | -0.3881 |
| 0.650 | -0.1624 | -0.0833 | -0.0467 | -0.1242 | -0.4126 |
| 0.675 | ******* | -0.1596 | -0.0579 | -0.1306 | -0.4338 |
| 0.700 | -0.1650 | -0.1697 | -0.0594 | -0.1317 | -0.4593 |
| 0.725 | ******* | -0.1732 | ******* | -0.1365 | -0.4875 |
| 0.750 | -0.1663 | -0.1782 | ******* | -0.1439 | -0.5381 |
| 0.775 | ******* | -0.1822 | -0.1039 | -0.1534 | -0.5461 |
| 0.800 | -0.1576 | -0.1974 | -0.1343 | -0.1706 | ******* |
| 0.825 | ******* | -0.2099 | -0.1936 | -0.1804 | -0.5136 |
| 0.850 | -0.1332 | -0.2179 | -0.2014 | -0.2115 | -0.4824 |
| 0.875 | ******* | -0.2183 | -0.2171 | -0.2571 | -0.4862 |
| 0.900 | -0.1071 | -0.2110 | -0.2410 | -0.2908 | ******* |
| 0.925 | ******* | -0.1977 | -0.2389 | -0.3124 | -0.4250 |
| 0.950 | -0.0794 | -0.1806 | -0.2310 | -0.3114 | -0.4022 |
| 0.975 | ******* | -0.1643 | -0.2070 | -0.2848 | -0.3586 |
| 1.000 | -0.0410 | -0.1992 | -0.2392 | -0.4284 | -0.3266 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0350 | 0.0493 | 0.1182 | ******* | -0.3119 |
| -0.400 | 0.0251 | 0.0476 | 0.0810 | -0.0606 | -0.4162 |
| -0.600 | 0.0129 | 0.0437 | 0.0628 | -0.0338 | -0.5826 |
| -0.700 | ******* | 0.0326 | 0.0545 | -0.0250 | -0.7201 |
| -0.800 | ******* | ******* | 0.0359 | -0.0241 | -0.6911 |
| -0.850 | ******* | 0.0442 | 0.0353 | -0.0284 | -0.6906 |
| -0.900 | 0.0946 | 0.0804 | 0.0484 | -0.0228 | -0.7425 |
| -0.950 | 0.1298 | 0.1000 | 0.1129 | 0.0382 | -0.2861 |
| -0.975 | ******* | 0.1782 | 0.1600 | 0.0996 | -0.1020 |
| -1.000 | -0.0377 | -0.1736 | -0.2387 | -0.3941 | -0.3831 |

Surface Pressures




Small Radius L.E.

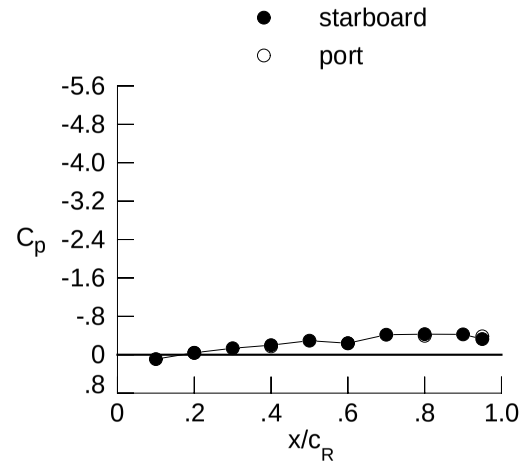
Run No. = 40 , Point No. = 812

$C_N$ = 0.115, $C_m$ = -0.0212

$\alpha$ = 3.2 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

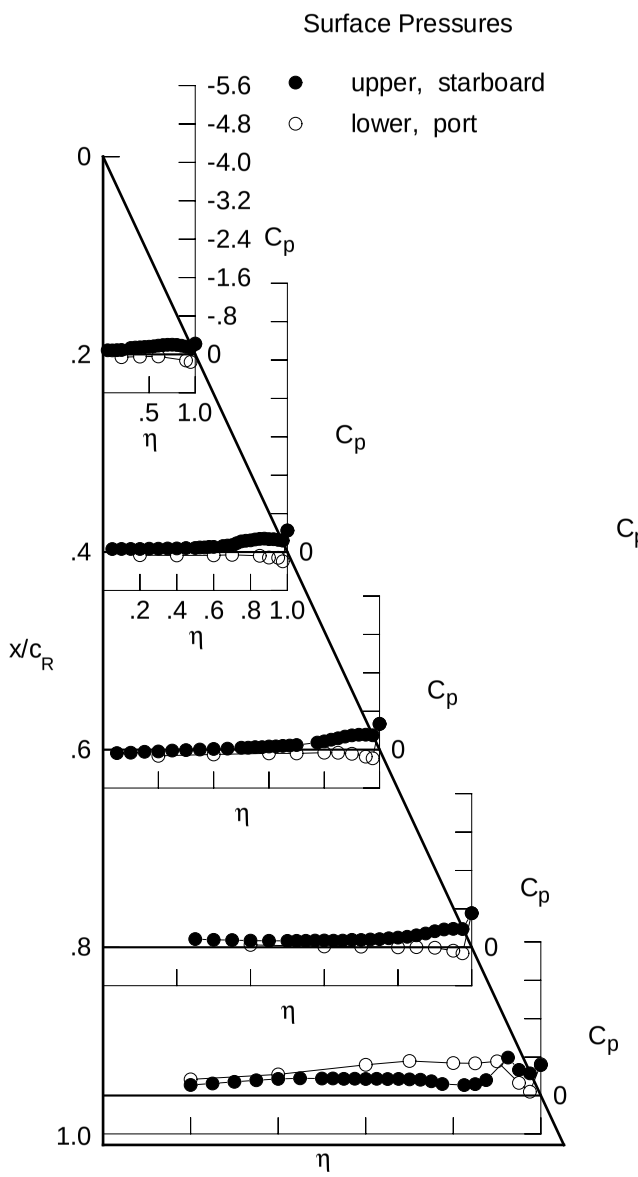
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.0912 | ******* |
| 0.20 | -0.0410 | -0.0377 |
| 0.30 | -0.1348 | ******* |
| 0.40 | -0.1992 | -0.1736 |
| 0.50 | -0.2927 | ******* |
| 0.60 | -0.2392 | -0.2387 |
| 0.70 | -0.4167 | ******* |
| 0.80 | -0.4284 | -0.3941 |
| 0.90 | -0.4241 | ******* |
| 0.95 | -0.3266 | -0.3831 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0853 | -0.0624 | 0.0718 | ******* | ******* |
| 0.100 | -0.0834 | -0.0644 | 0.0638 | ******* | ******* |
| 0.150 | -0.0881 | -0.0639 | 0.0451 | ******* | ******* |
| 0.200 | -0.0924 | -0.0638 | 0.0376 | ******* | -0.2191 |
| 0.250 | ******* | -0.0693 | 0.0190 | -0.1709 | -0.2508 |
| 0.300 | -0.1328 | -0.0693 | 0.0100 | -0.1550 | -0.2851 |
| 0.350 | -0.1424 | -0.0741 | -0.0024 | -0.1503 | -0.3173 |
| 0.400 | -0.1469 | -0.0753 | -0.0143 | -0.1381 | -0.3454 |
| 0.450 | -0.1538 | -0.0834 | -0.0207 | -0.1349 | -0.3581 |
| 0.500 | -0.1599 | -0.0841 | -0.0404 | -0.1340 | -0.3540 |
| 0.525 | ******* | -0.0951 | -0.0407 | -0.1343 | -0.3549 |
| 0.550 | -0.1686 | -0.0963 | -0.0518 | -0.1355 | -0.3471 |
| 0.575 | ******* | -0.1074 | -0.0524 | -0.1404 | -0.3494 |
| 0.600 | -0.1827 | -0.1075 | -0.0655 | -0.1414 | -0.3442 |
| 0.625 | ******* | ******* | -0.0681 | -0.1380 | -0.3481 |
| 0.650 | -0.1938 | -0.1238 | -0.0785 | -0.1393 | -0.3435 |
| 0.675 | ******* | -0.1350 | -0.0849 | -0.1550 | -0.3459 |
| 0.700 | -0.2001 | -0.1443 | -0.0959 | -0.1523 | -0.3359 |
| 0.725 | ******* | -0.1844 | ******* | -0.1622 | -0.3286 |
| 0.750 | -0.2013 | -0.2213 | ******* | -0.1693 | -0.2964 |
| 0.775 | ******* | -0.2349 | -0.1470 | -0.1880 | -0.2388 |
| 0.800 | -0.1966 | -0.2435 | -0.1725 | -0.2017 | ******* |
| 0.825 | ******* | -0.2617 | -0.2073 | -0.2191 | -0.2178 |
| 0.850 | -0.1805 | -0.2745 | -0.2370 | -0.2495 | -0.2371 |
| 0.875 | ******* | -0.2795 | -0.2722 | -0.2870 | -0.3210 |
| 0.900 | -0.1613 | -0.2685 | -0.2977 | -0.3344 | ******* |
| 0.925 | ******* | -0.2672 | -0.3108 | -0.3711 | -0.7904 |
| 0.950 | -0.1442 | -0.2533 | -0.3112 | -0.3838 | -0.5337 |
| 0.975 | ******* | -0.2376 | -0.2995 | -0.3796 | -0.4619 |
| 1.000 | -0.2134 | -0.4500 | -0.5393 | -0.7092 | -0.6337 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0586 | 0.0656 | 0.1290 | ******* | -0.3362 |
| -0.400 | 0.0463 | 0.0705 | 0.1002 | -0.0495 | -0.4395 |
| -0.600 | 0.0423 | 0.0687 | 0.0777 | -0.0178 | -0.6398 |
| -0.700 | ******* | 0.0584 | 0.0787 | -0.0134 | -0.7193 |
| -0.800 | ******* | ******* | 0.0635 | 0.0008 | -0.6760 |
| -0.850 | ******* | 0.0782 | 0.0649 | -0.0030 | -0.6707 |
| -0.900 | 0.1264 | 0.1152 | 0.0860 | 0.0096 | -0.7120 |
| -0.950 | 0.1578 | 0.1202 | 0.1456 | 0.0716 | -0.2629 |
| -0.975 | ******* | 0.1939 | 0.1797 | 0.1247 | -0.0796 |
| -1.000 | -0.2259 | -0.4460 | -0.5331 | -0.7108 | -0.6524 |



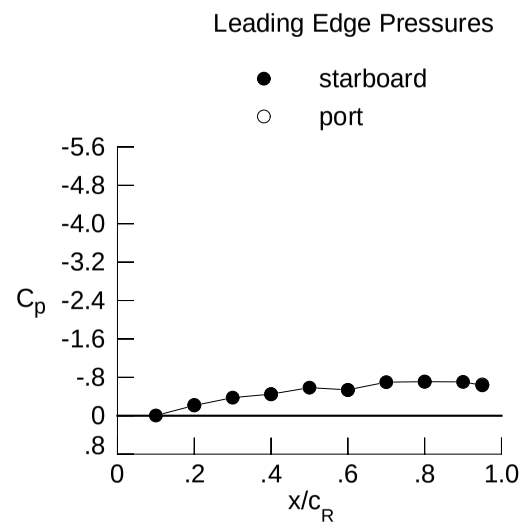

Small Radius L.E.

Run No. = 40 , Point No. = 813

$C_N$ = 0.152, $C_m$ = -0.0240

$\alpha$ = 4.2 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

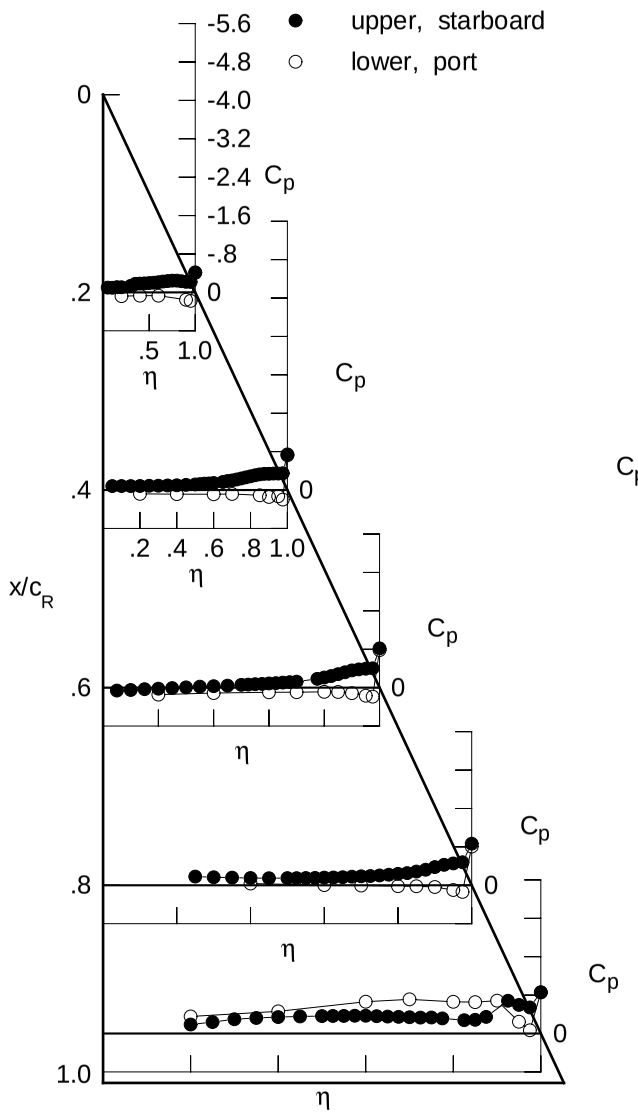



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.0051 | ******* |
| 0.20 | -0.2134 | -0.2259 |
| 0.30 | -0.3770 | ******* |
| 0.40 | -0.4500 | -0.4460 |
| 0.50 | -0.5848 | ******* |
| 0.60 | -0.5393 | -0.5331 |
| 0.70 | -0.6995 | ******* |
| 0.80 | -0.7092 | -0.7108 |
| 0.90 | -0.7050 | ******* |
| 0.95 | -0.6337 | -0.6524 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0992 | -0.0820 | 0.0610 | ******* | ******* |
| 0.100 | -0.0963 | -0.0829 | 0.0489 | ******* | ******* |
| 0.150 | -0.1085 | -0.0821 | 0.0323 | ******* | ******* |
| 0.200 | -0.1072 | -0.0838 | 0.0218 | ******* | -0.1871 |
| 0.250 | ******* | -0.0885 | 0.0091 | -0.1815 | -0.2380 |
| 0.300 | -0.1370 | -0.0905 | -0.0056 | -0.1676 | -0.2977 |
| 0.350 | -0.1787 | -0.0955 | -0.0205 | -0.1598 | -0.3237 |
| 0.400 | -0.1828 | -0.0994 | -0.0301 | -0.1517 | -0.3428 |
| 0.450 | -0.1880 | -0.1080 | -0.0416 | -0.1471 | -0.3555 |
| 0.500 | -0.1942 | -0.1159 | -0.0584 | -0.1499 | -0.3630 |
| 0.525 | ******* | -0.1234 | -0.0631 | -0.1480 | -0.3660 |
| 0.550 | -0.2019 | -0.1335 | -0.0722 | -0.1511 | -0.3667 |
| 0.575 | ******* | -0.1378 | -0.0773 | -0.1535 | -0.3703 |
| 0.600 | -0.2117 | -0.1464 | -0.0875 | -0.1601 | -0.3701 |
| 0.625 | ******* | ******* | -0.0940 | -0.1624 | -0.3605 |
| 0.650 | -0.2264 | -0.1681 | -0.1045 | -0.1677 | -0.3528 |
| 0.675 | ******* | -0.1877 | -0.1147 | -0.1793 | -0.3473 |
| 0.700 | -0.2359 | -0.1997 | -0.1252 | -0.1870 | -0.3390 |
| 0.725 | ******* | -0.2199 | ******* | -0.1927 | -0.3309 |
| 0.750 | -0.2446 | -0.2416 | ******* | -0.2045 | -0.3335 |
| 0.775 | ******* | -0.2644 | -0.1829 | -0.2204 | -0.3145 |
| 0.800 | -0.2451 | -0.2856 | -0.2116 | -0.2386 | ******* |
| 0.825 | ******* | -0.3077 | -0.2420 | -0.2534 | -0.2778 |
| 0.850 | -0.2330 | -0.3267 | -0.2809 | -0.2864 | -0.2854 |
| 0.875 | ******* | -0.3375 | -0.3198 | -0.3237 | -0.3461 |
| 0.900 | -0.2197 | -0.3387 | -0.3596 | -0.3793 | ******* |
| 0.925 | ******* | -0.3430 | -0.3804 | -0.4262 | -0.6828 |
| 0.950 | -0.2176 | -0.3431 | -0.3941 | -0.4548 | -0.5963 |
| 0.975 | ******* | -0.3493 | -0.4035 | -0.4803 | -0.5429 |
| 1.000 | -0.4177 | -0.7425 | -0.8181 | -0.8665 | -0.8594 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0788 | 0.0799 | 0.1455 | ******* | -0.3552 |
| -0.400 | 0.0679 | 0.0860 | 0.1125 | -0.0365 | -0.4615 |
| -0.600 | 0.0678 | 0.0879 | 0.0965 | -0.0037 | -0.6624 |
| -0.700 | ******* | 0.0824 | 0.0953 | 0.0048 | -0.7119 |
| -0.800 | ******* | ******* | 0.0875 | 0.0183 | -0.6606 |
| -0.850 | ******* | 0.1094 | 0.0905 | 0.0197 | -0.6536 |
| -0.900 | 0.1529 | 0.1441 | 0.1155 | 0.0363 | -0.6840 |
| -0.950 | 0.1767 | 0.1308 | 0.1681 | 0.0988 | -0.2453 |
| -0.975 | ******* | 0.1987 | 0.1875 | 0.1373 | -0.0671 |
| -1.000 | -0.4070 | -0.7234 | -0.7813 | -0.8068 | -0.8564 |

Surface Pressures




Small Radius L.E.

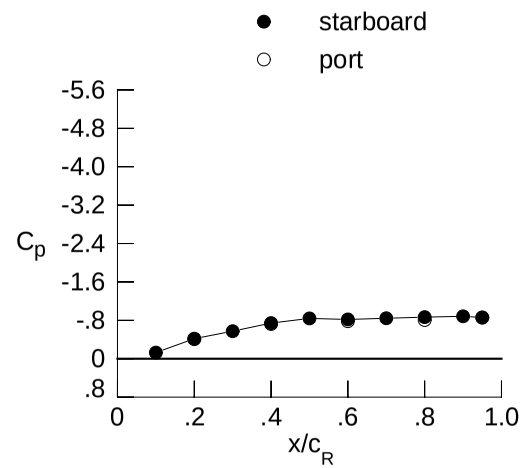
Run No. = 40 , Point No. = 814

$C_N$ = 0.197, $C_m$ = -0.0329

$\alpha$ = 5.2 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

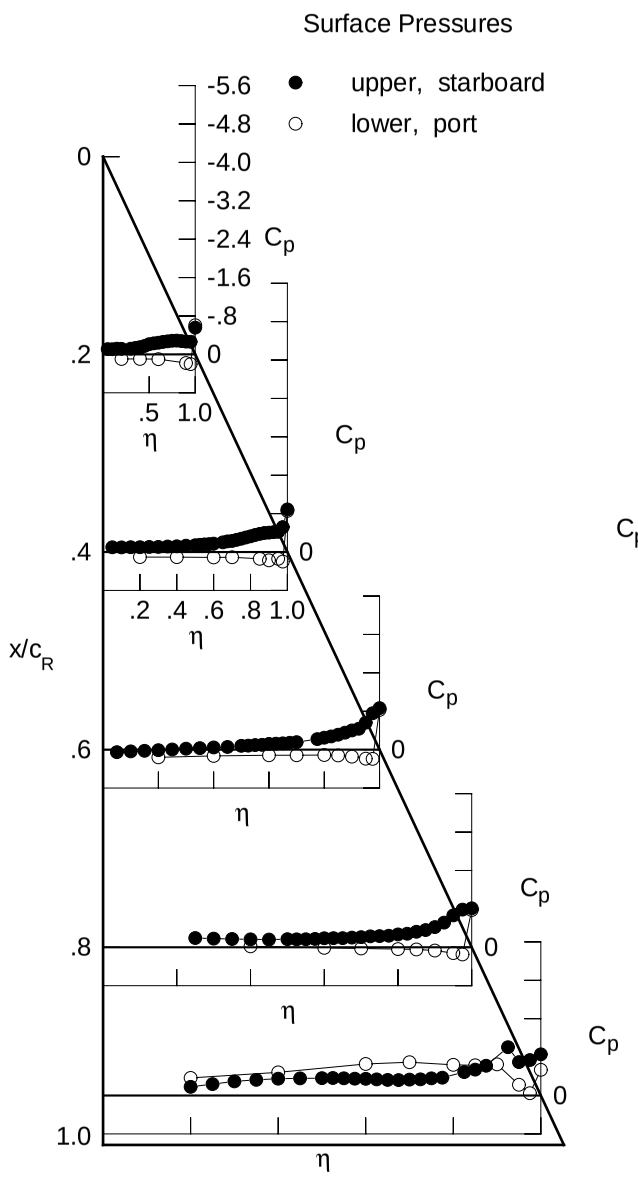
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.1281 | ******* |
| 0.20 | -0.4177 | -0.4070 |
| 0.30 | -0.5739 | ******* |
| 0.40 | -0.7425 | -0.7234 |
| 0.50 | -0.8402 | ******* |
| 0.60 | -0.8181 | -0.7813 |
| 0.70 | -0.8430 | ******* |
| 0.80 | -0.8665 | -0.8068 |
| 0.90 | -0.8838 | ******* |
| 0.95 | -0.8594 | -0.8564 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1097 | -0.0989 | 0.0526 | ******* | ******* |
| 0.100 | -0.1074 | -0.0969 | 0.0360 | ******* | ******* |
| 0.150 | -0.1195 | -0.1004 | 0.0236 | ******* | ******* |
| 0.200 | -0.1159 | -0.1005 | 0.0109 | ******* | -0.1805 |
| 0.250 | ******* | -0.1066 | -0.0035 | -0.1925 | -0.2376 |
| 0.300 | -0.1186 | -0.1074 | -0.0197 | -0.1811 | -0.2947 |
| 0.350 | -0.1339 | -0.1148 | -0.0313 | -0.1730 | -0.3266 |
| 0.400 | -0.1505 | -0.1203 | -0.0454 | -0.1658 | -0.3505 |
| 0.450 | -0.1750 | -0.1327 | -0.0559 | -0.1610 | -0.3569 |
| 0.500 | -0.2126 | -0.1414 | -0.0796 | -0.1689 | -0.3614 |
| 0.525 | ******* | -0.1503 | -0.0829 | -0.1653 | -0.3651 |
| 0.550 | -0.2303 | -0.1592 | -0.0955 | -0.1675 | -0.3583 |
| 0.575 | ******* | -0.1646 | -0.1004 | -0.1742 | -0.3508 |
| 0.600 | -0.2434 | -0.1755 | -0.1195 | -0.1884 | -0.3476 |
| 0.625 | ******* | ******* | -0.1240 | -0.1901 | -0.3359 |
| 0.650 | -0.2597 | -0.2013 | -0.1308 | -0.1905 | -0.3246 |
| 0.675 | ******* | -0.2221 | -0.1429 | -0.2013 | -0.3215 |
| 0.700 | -0.2719 | -0.2311 | -0.1560 | -0.2113 | -0.3309 |
| 0.725 | ******* | -0.2542 | ******* | -0.2282 | -0.3368 |
| 0.750 | -0.2838 | -0.2778 | ******* | -0.2328 | -0.3575 |
| 0.775 | ******* | -0.3029 | -0.2195 | -0.2404 | -0.3711 |
| 0.800 | -0.2870 | -0.3269 | -0.2485 | -0.2680 | ******* |
| 0.825 | ******* | -0.3553 | -0.2751 | -0.2826 | -0.4882 |
| 0.850 | -0.2778 | -0.3788 | -0.3112 | -0.3229 | -0.5391 |
| 0.875 | ******* | -0.3965 | -0.3536 | -0.3594 | -0.6204 |
| 0.900 | -0.2661 | -0.4043 | -0.3998 | -0.4207 | ******* |
| 0.925 | ******* | -0.4144 | -0.4354 | -0.5140 | -1.0067 |
| 0.950 | -0.2622 | -0.4212 | -0.5626 | -0.6642 | -0.6962 |
| 0.975 | ******* | -0.5197 | -0.7583 | -0.7851 | -0.7389 |
| 1.000 | -0.5578 | -0.8870 | -0.8651 | -0.8118 | -0.8574 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0949 | 0.1050 | 0.1604 | ******* | -0.3667 |
| -0.400 | 0.0947 | 0.1062 | 0.1304 | -0.0203 | -0.4824 |
| -0.600 | 0.0989 | 0.1123 | 0.1169 | 0.0112 | -0.6570 |
| -0.700 | ******* | 0.1089 | 0.1165 | 0.0250 | -0.6937 |
| -0.800 | ******* | ******* | 0.1123 | 0.0379 | -0.6390 |
| -0.850 | ******* | 0.1410 | 0.1205 | 0.0452 | -0.6292 |
| -0.900 | 0.1799 | 0.1729 | 0.1454 | 0.0677 | -0.6485 |
| -0.950 | 0.2027 | 0.1409 | 0.1879 | 0.1210 | -0.2237 |
| -0.975 | ******* | 0.1984 | 0.1921 | 0.1490 | -0.0478 |
| -1.000 | -0.6074 | -0.8575 | -0.8283 | -0.7757 | -0.5350 |



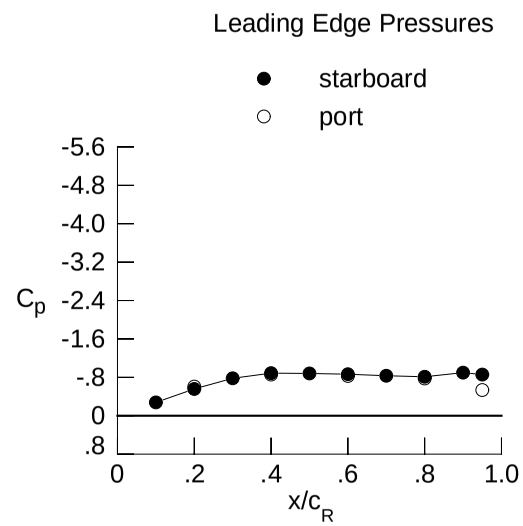

Small Radius L.E.

Run No. = 40 , Point No. = 815

$C_N$ = 0.245, $C_m$ = -0.0417

$\alpha$ = 6.3 °, $M_\infty$ = 0.829

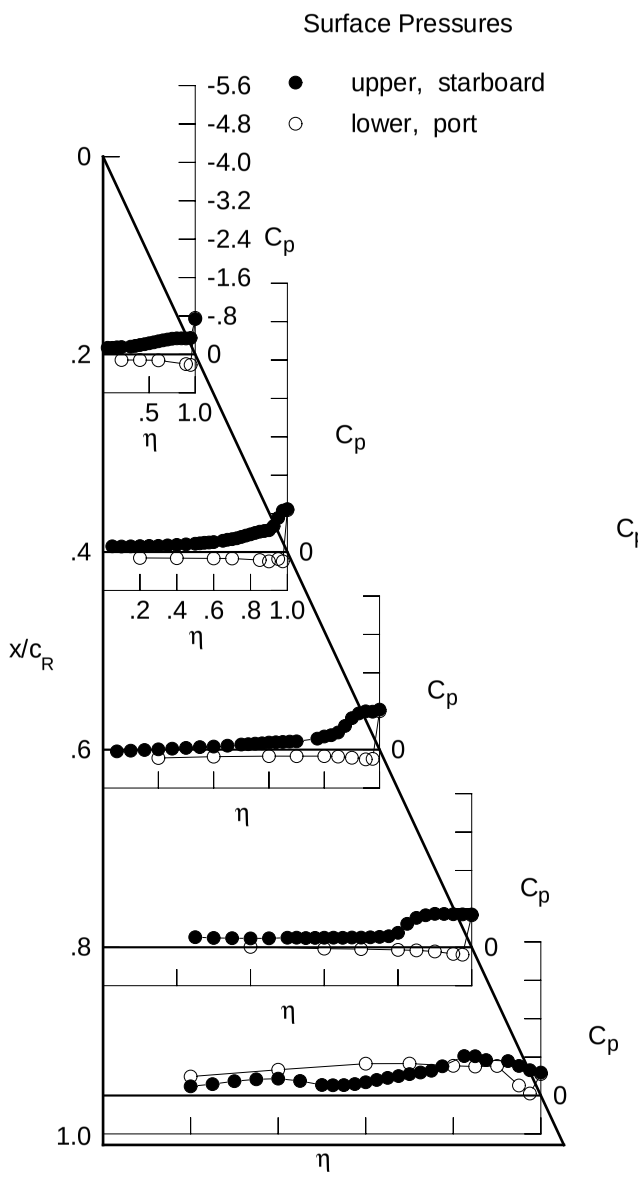
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.2778 | ******* |
| 0.20 | -0.5578 | -0.6074 |
| 0.30 | -0.7800 | ******* |
| 0.40 | -0.8870 | -0.8575 |
| 0.50 | -0.8807 | ******* |
| 0.60 | -0.8651 | -0.8283 |
| 0.70 | -0.8330 | ******* |
| 0.80 | -0.8118 | -0.7757 |
| 0.90 | -0.8979 | ******* |
| 0.95 | -0.8574 | -0.5350 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1379 | -0.1194 | 0.0361 | ******* | ******* |
| 0.100 | -0.1357 | -0.1156 | 0.0216 | ******* | ******* |
| 0.150 | -0.1473 | -0.1183 | 0.0076 | ******* | ******* |
| 0.200 | -0.1531 | -0.1235 | -0.0064 | ******* | -0.1915 |
| 0.250 | ******* | -0.1269 | -0.0202 | -0.2107 | -0.2371 |
| 0.300 | -0.1609 | -0.1286 | -0.0357 | -0.1946 | -0.2982 |
| 0.350 | -0.1767 | -0.1381 | -0.0524 | -0.1896 | -0.3374 |
| 0.400 | -0.1953 | -0.1484 | -0.0640 | -0.1847 | -0.3509 |
| 0.450 | -0.2120 | -0.1595 | -0.0827 | -0.1872 | -0.3033 |
| 0.500 | -0.2323 | -0.1731 | -0.1061 | -0.1989 | -0.2188 |
| 0.525 | ******* | -0.1819 | -0.1136 | -0.1997 | -0.2136 |
| 0.550 | -0.2515 | -0.1926 | -0.1248 | -0.1918 | -0.2167 |
| 0.575 | ******* | -0.1981 | -0.1317 | -0.1962 | -0.2383 |
| 0.600 | -0.2728 | -0.2076 | -0.1469 | -0.1992 | -0.2763 |
| 0.625 | ******* | ******* | -0.1538 | -0.2003 | -0.3241 |
| 0.650 | -0.2927 | -0.2348 | -0.1603 | -0.1973 | -0.3675 |
| 0.675 | ******* | -0.2562 | -0.1675 | -0.2029 | -0.4044 |
| 0.700 | -0.3094 | -0.2684 | -0.1727 | -0.2016 | -0.4454 |
| 0.725 | ******* | -0.2864 | ******* | -0.2080 | -0.4794 |
| 0.750 | -0.3263 | -0.3142 | ******* | -0.2169 | -0.5161 |
| 0.775 | ******* | -0.3426 | -0.2292 | -0.2302 | -0.6089 |
| 0.800 | -0.3341 | -0.3686 | -0.2734 | -0.3018 | ******* |
| 0.825 | ******* | -0.3974 | -0.3008 | -0.4887 | -0.8213 |
| 0.850 | -0.3342 | -0.4239 | -0.3576 | -0.6131 | -0.8188 |
| 0.875 | ******* | -0.4388 | -0.4937 | -0.6668 | -0.7381 |
| 0.900 | -0.3324 | -0.4546 | -0.6557 | -0.6968 | ******* |
| 0.925 | ******* | -0.5392 | -0.7546 | -0.6946 | -0.7179 |
| 0.950 | -0.3426 | -0.7113 | -0.7980 | -0.6887 | -0.6157 |
| 0.975 | ******* | -0.8617 | -0.7906 | -0.6859 | -0.5275 |
| 1.000 | -0.7359 | -0.8939 | -0.8334 | -0.6834 | -0.4778 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1168 | 0.1230 | 0.1744 | ******* | -0.3948 |
| -0.400 | 0.1182 | 0.1276 | 0.1464 | -0.0079 | -0.5365 |
| -0.600 | 0.1239 | 0.1329 | 0.1352 | 0.0283 | -0.6631 |
| -0.700 | ******* | 0.1343 | 0.1361 | 0.0379 | -0.6651 |
| -0.800 | ******* | ******* | 0.1351 | 0.0540 | -0.6187 |
| -0.850 | ******* | 0.1673 | 0.1450 | 0.0651 | -0.6039 |
| -0.900 | 0.2025 | 0.1950 | 0.1688 | 0.0873 | -0.6152 |
| -0.950 | 0.2194 | 0.1446 | 0.2021 | 0.1378 | -0.2087 |
| -0.975 | ******* | 0.1932 | 0.1923 | 0.1537 | -0.0416 |
| -1.000 | -0.7606 | -0.8728 | -0.8002 | -0.6668 | -0.4472 |



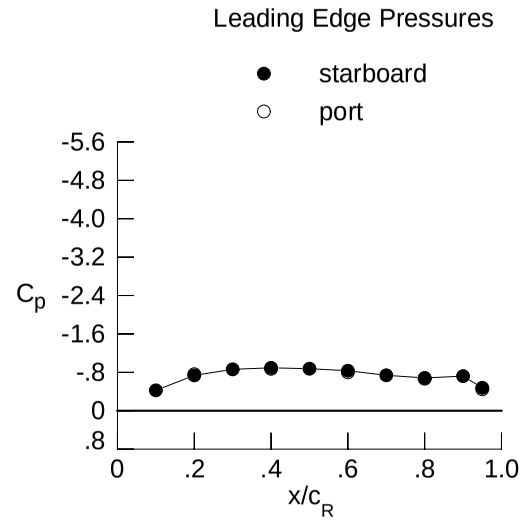

Small Radius L.E.

Run No. = 40 , Point No. = 816

$C_N$ = 0.304, $C_m$ = -0.0559

$\alpha$ = 7.3 °, $M_\infty$ = 0.829

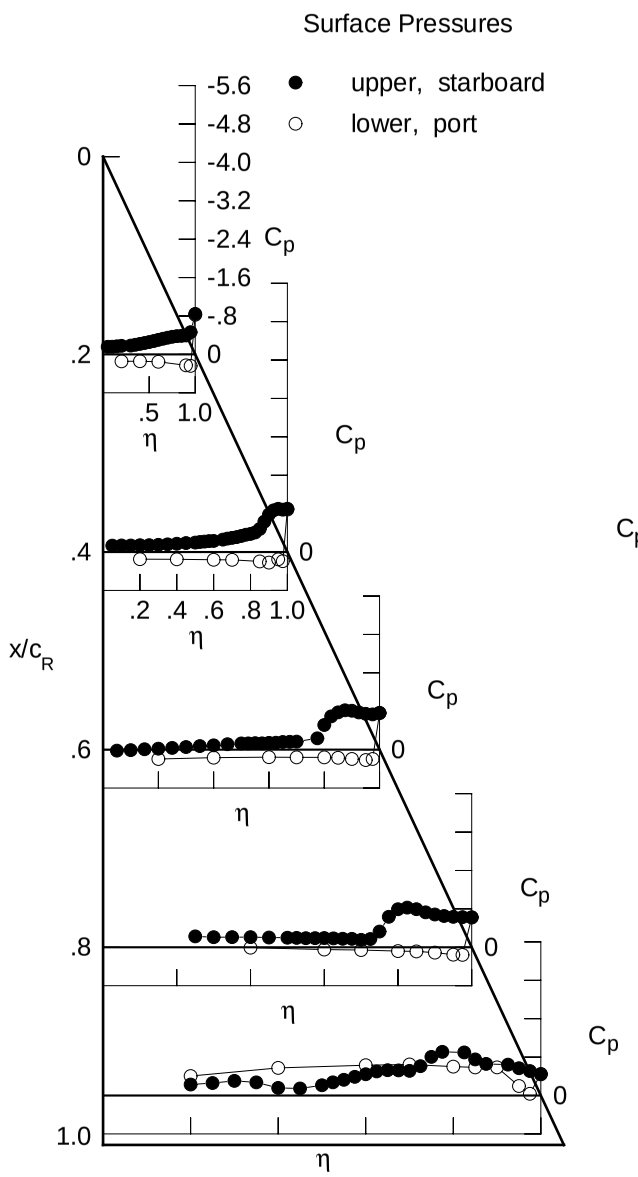
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.4249 | ******* |
| 0.20 | -0.7359 | -0.7606 |
| 0.30 | -0.8626 | ******* |
| 0.40 | -0.8939 | -0.8728 |
| 0.50 | -0.8754 | ******* |
| 0.60 | -0.8334 | -0.8002 |
| 0.70 | -0.7380 | ******* |
| 0.80 | -0.6834 | -0.6668 |
| 0.90 | -0.7204 | ******* |
| 0.95 | -0.4778 | -0.4472 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1582 | -0.1336 | 0.0207 | ******* | ******* |
| 0.100 | -0.1600 | -0.1372 | 0.0104 | ******* | ******* |
| 0.150 | -0.1685 | -0.1360 | -0.0080 | ******* | ******* |
| 0.200 | -0.1787 | -0.1423 | -0.0200 | ******* | -0.2286 |
| 0.250 | ******* | -0.1435 | -0.0357 | -0.2271 | -0.2599 |
| 0.300 | -0.1831 | -0.1502 | -0.0543 | -0.2102 | -0.3049 |
| 0.350 | -0.1997 | -0.1603 | -0.0741 | -0.2109 | -0.2735 |
| 0.400 | -0.2184 | -0.1727 | -0.0898 | -0.2116 | -0.1584 |
| 0.450 | -0.2368 | -0.1872 | -0.1125 | -0.2032 | -0.1462 |
| 0.500 | -0.2567 | -0.1969 | -0.1296 | -0.1994 | -0.2134 |
| 0.525 | ******* | -0.2089 | -0.1301 | -0.1963 | -0.2742 |
| 0.550 | -0.2781 | -0.2172 | -0.1352 | -0.1899 | -0.3269 |
| 0.575 | ******* | -0.2280 | -0.1311 | -0.1907 | -0.3890 |
| 0.600 | -0.3035 | -0.2311 | -0.1415 | -0.1925 | -0.4430 |
| 0.625 | ******* | ******* | -0.1436 | -0.1856 | -0.5012 |
| 0.650 | -0.3259 | -0.2587 | -0.1594 | -0.1775 | -0.5269 |
| 0.675 | ******* | -0.2802 | -0.1631 | -0.1763 | -0.5234 |
| 0.700 | -0.3468 | -0.2949 | -0.1672 | -0.1546 | -0.5138 |
| 0.725 | ******* | -0.3113 | ******* | -0.1719 | -0.6110 |
| 0.750 | -0.3668 | -0.3349 | ******* | -0.3278 | -0.8049 |
| 0.775 | ******* | -0.3606 | -0.2363 | -0.6356 | -0.9098 |
| 0.800 | -0.3801 | -0.3773 | -0.5138 | -0.7928 | ******* |
| 0.825 | ******* | -0.4069 | -0.6924 | -0.8264 | -0.8973 |
| 0.850 | -0.3859 | -0.4810 | -0.7770 | -0.7934 | -0.7517 |
| 0.875 | ******* | -0.6333 | -0.8197 | -0.7282 | -0.6582 |
| 0.900 | -0.3937 | -0.7821 | -0.8104 | -0.6833 | ******* |
| 0.925 | ******* | -0.8688 | -0.7753 | -0.6519 | -0.6432 |
| 0.950 | -0.4631 | -0.9005 | -0.7467 | -0.6344 | -0.5685 |
| 0.975 | ******* | -0.8825 | -0.7345 | -0.6279 | -0.5092 |
| 1.000 | -0.8443 | -0.9014 | -0.7669 | -0.6257 | -0.4405 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1445 | 0.1490 | 0.1951 | ******* | -0.4055 |
| -0.400 | 0.1421 | 0.1515 | 0.1670 | 0.0077 | -0.5749 |
| -0.600 | 0.1539 | 0.1608 | 0.1567 | 0.0475 | -0.6309 |
| -0.700 | ******* | 0.1626 | 0.1608 | 0.0573 | -0.6467 |
| -0.800 | ******* | ******* | 0.1612 | 0.0789 | -0.6019 |
| -0.850 | ******* | 0.1956 | 0.1697 | 0.0861 | -0.5860 |
| -0.900 | 0.2281 | 0.2197 | 0.1941 | 0.1111 | -0.5865 |
| -0.950 | 0.2391 | 0.1517 | 0.2172 | 0.1534 | -0.1972 |
| -0.975 | ******* | 0.1901 | 0.1943 | 0.1579 | -0.0359 |
| -1.000 | -0.8258 | -0.8848 | -0.7589 | -0.6206 | -0.4498 |



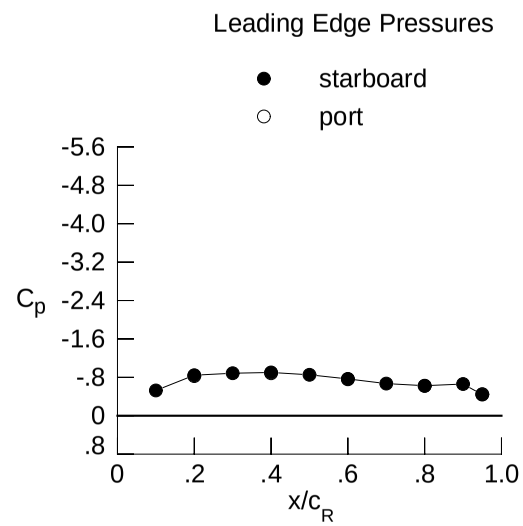

Small Radius L.E.

Run No. = 40 , Point No. = 817

$C_N$ = 0.358, $C_m$ = -0.0650

$\alpha$ = 8.3 °, $M_\infty$ = 0.828

$R_{mac}$ = $6.0 \times 10^6$

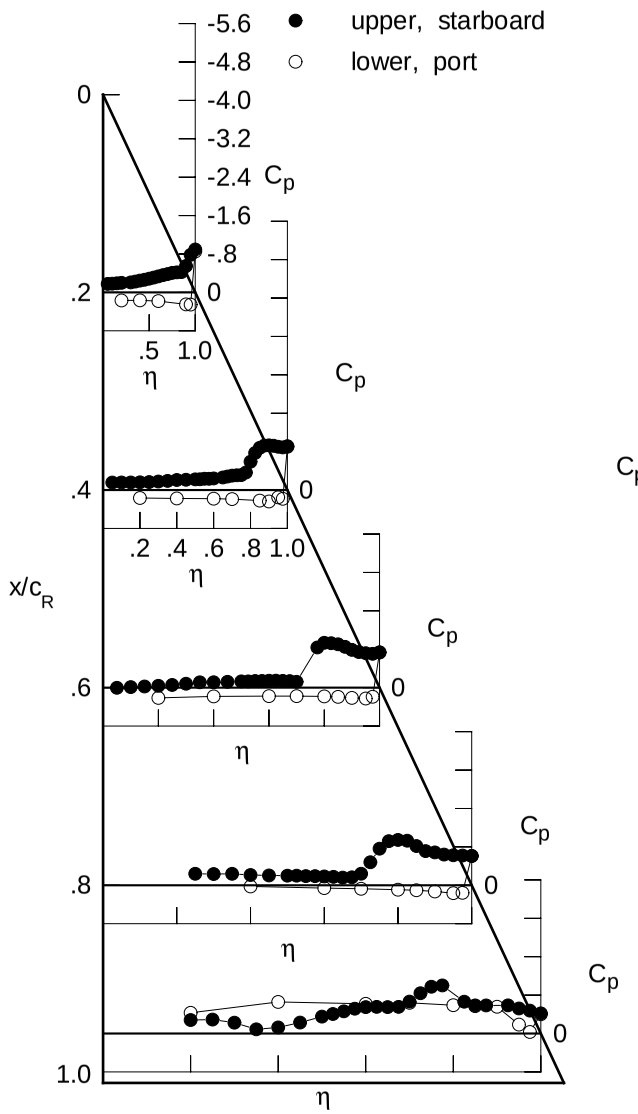



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.5264 | ******* |
| 0.20 | -0.8443 | -0.8258 |
| 0.30 | -0.8853 | ******* |
| 0.40 | -0.9014 | -0.8848 |
| 0.50 | -0.8527 | ******* |
| 0.60 | -0.7669 | -0.7589 |
| 0.70 | -0.6694 | ******* |
| 0.80 | -0.6257 | -0.6206 |
| 0.90 | -0.6604 | ******* |
| 0.95 | -0.4405 | -0.4498 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1769 | -0.1563 | 0.0032 | ******* | ******* |
| 0.100 | -0.1818 | -0.1579 | -0.0113 | ******* | ******* |
| 0.150 | -0.1897 | -0.1574 | -0.0239 | ******* | ******* |
| 0.200 | -0.1989 | -0.1610 | -0.0382 | ******* | -0.2807 |
| 0.250 | ******* | -0.1662 | -0.0564 | -0.2397 | -0.2902 |
| 0.300 | -0.2081 | -0.1773 | -0.0818 | -0.2344 | -0.2255 |
| 0.350 | -0.2255 | -0.1905 | -0.1114 | -0.2389 | -0.0874 |
| 0.400 | -0.2460 | -0.2092 | -0.1118 | -0.2146 | -0.1265 |
| 0.450 | -0.2631 | -0.2148 | -0.1213 | -0.2049 | -0.2281 |
| 0.500 | -0.2857 | -0.2223 | -0.1303 | -0.2003 | -0.3517 |
| 0.525 | ******* | -0.2243 | -0.1306 | -0.1996 | -0.4061 |
| 0.550 | -0.3091 | -0.2350 | -0.1381 | -0.1915 | -0.4619 |
| 0.575 | ******* | -0.2348 | -0.1388 | -0.1903 | -0.5166 |
| 0.600 | -0.3339 | -0.2418 | -0.1440 | -0.1838 | -0.5495 |
| 0.625 | ******* | ******* | -0.1452 | -0.1757 | -0.5556 |
| 0.650 | -0.3595 | -0.2614 | -0.1411 | -0.1600 | -0.5500 |
| 0.675 | ******* | -0.2816 | -0.1360 | -0.1662 | -0.5552 |
| 0.700 | -0.3819 | -0.3002 | -0.1214 | -0.2409 | -0.6651 |
| 0.725 | ******* | -0.3073 | ******* | -0.4804 | -0.8388 |
| 0.750 | -0.4062 | -0.3118 | ******* | -0.7627 | -0.9747 |
| 0.775 | ******* | -0.3652 | -0.8368 | -0.9191 | -1.0018 |
| 0.800 | -0.4175 | -0.5907 | -0.9346 | -0.9452 | ******* |
| 0.825 | ******* | -0.7732 | -0.9257 | -0.9287 | -0.6626 |
| 0.850 | -0.4227 | -0.8802 | -0.9033 | -0.8174 | -0.5858 |
| 0.875 | ******* | -0.9261 | -0.8502 | -0.7123 | -0.5847 |
| 0.900 | -0.5505 | -0.9309 | -0.7874 | -0.6845 | ******* |
| 0.925 | ******* | -0.9235 | -0.7414 | -0.6396 | -0.5863 |
| 0.950 | -0.7815 | -0.9019 | -0.7180 | -0.6255 | -0.5212 |
| 0.975 | ******* | -0.8878 | -0.7047 | -0.6197 | -0.4766 |
| 1.000 | -0.8939 | -0.9139 | -0.7352 | -0.6123 | -0.4199 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1678 | 0.1659 | 0.2138 | ******* | -0.4314 |
| -0.400 | 0.1652 | 0.1755 | 0.1827 | 0.0239 | -0.6574 |
| -0.600 | 0.1811 | 0.1801 | 0.1764 | 0.0584 | -0.6188 |
| -0.700 | ******* | 0.1888 | 0.1768 | 0.0725 | -0.6393 |
| -0.800 | ******* | ******* | 0.1826 | 0.0922 | -0.5893 |
| -0.850 | ******* | 0.2202 | 0.1923 | 0.1031 | -0.5697 |
| -0.900 | 0.2496 | 0.2381 | 0.2133 | 0.1290 | -0.5579 |
| -0.950 | 0.2537 | 0.1522 | 0.2266 | 0.1641 | -0.1855 |
| -0.975 | ******* | 0.1825 | 0.1898 | 0.1569 | -0.0317 |
| -1.000 | -0.8521 | -0.9011 | -0.7326 | -0.6096 | -0.4007 |

Surface Pressures




Small Radius L.E.

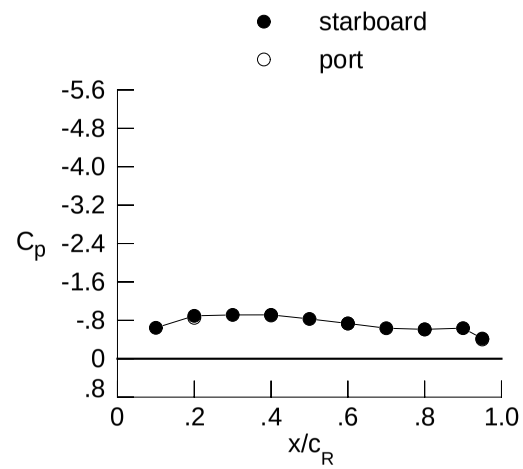
Run No. = 40 , Point No. = 818

$C_N$ = 0.409, $C_m$ = -0.0720

$\alpha$ = 9.3 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

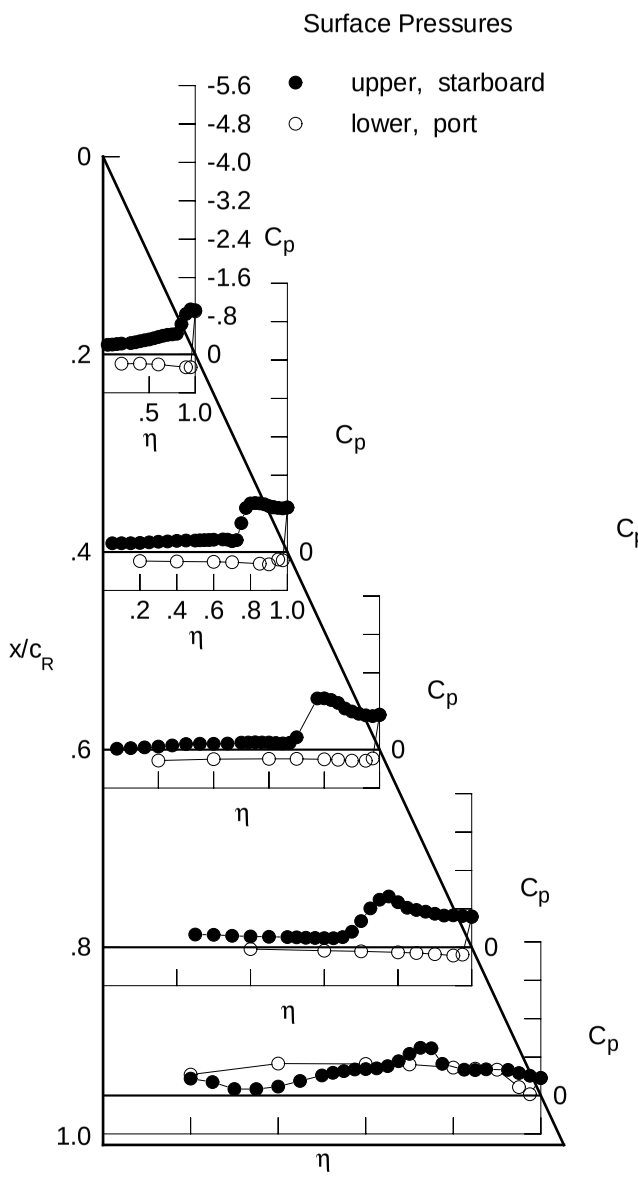
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.6440 | ******* |
| 0.20 | -0.8939 | -0.8521 |
| 0.30 | -0.9125 | ******* |
| 0.40 | -0.9139 | -0.9011 |
| 0.50 | -0.8290 | ******* |
| 0.60 | -0.7352 | -0.7326 |
| 0.70 | -0.6356 | ******* |
| 0.80 | -0.6123 | -0.6096 |
| 0.90 | -0.6371 | ******* |
| 0.95 | -0.4199 | -0.4007 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2001 | -0.1821 | -0.0189 | ******* | ******* |
| 0.100 | -0.2049 | -0.1830 | -0.0315 | ******* | ******* |
| 0.150 | -0.2156 | -0.1835 | -0.0469 | ******* | ******* |
| 0.200 | -0.2250 | -0.1895 | -0.0638 | ******* | -0.3517 |
| 0.250 | ******* | -0.2015 | -0.0870 | -0.2654 | -0.2797 |
| 0.300 | -0.2353 | -0.2143 | -0.1169 | -0.2602 | -0.1351 |
| 0.350 | -0.2522 | -0.2208 | -0.1231 | -0.2394 | -0.1334 |
| 0.400 | -0.2739 | -0.2326 | -0.1219 | -0.2254 | -0.1852 |
| 0.450 | -0.2935 | -0.2403 | -0.1276 | -0.2186 | -0.3028 |
| 0.500 | -0.3110 | -0.2396 | -0.1453 | -0.2124 | -0.4176 |
| 0.525 | ******* | -0.2451 | -0.1490 | -0.2075 | -0.4730 |
| 0.550 | -0.3352 | -0.2483 | -0.1535 | -0.1983 | -0.5079 |
| 0.575 | ******* | -0.2501 | -0.1490 | -0.1947 | -0.5423 |
| 0.600 | -0.3627 | -0.2565 | -0.1492 | -0.1902 | -0.5501 |
| 0.625 | ******* | ******* | -0.1383 | -0.1884 | -0.5653 |
| 0.650 | -0.3883 | -0.2623 | -0.1296 | -0.2118 | -0.6121 |
| 0.675 | ******* | -0.2585 | -0.1427 | -0.3242 | -0.7140 |
| 0.700 | -0.4080 | -0.2263 | -0.2579 | -0.5460 | -0.8672 |
| 0.725 | ******* | -0.2483 | ******* | -0.8103 | -0.9937 |
| 0.750 | -0.4169 | -0.6012 | ******* | -0.9911 | -0.9837 |
| 0.775 | ******* | -0.9174 | -1.0667 | -1.0583 | -0.6596 |
| 0.800 | -0.4296 | -1.0118 | -1.0689 | -0.9392 | ******* |
| 0.825 | ******* | -1.0210 | -1.0347 | -0.8230 | -0.5377 |
| 0.850 | -0.6282 | -1.0136 | -0.9730 | -0.7779 | -0.5297 |
| 0.875 | ******* | -0.9953 | -0.8570 | -0.7417 | -0.5459 |
| 0.900 | -0.8433 | -0.9566 | -0.7941 | -0.6984 | ******* |
| 0.925 | ******* | -0.9376 | -0.7474 | -0.6611 | -0.5333 |
| 0.950 | -0.9377 | -0.9206 | -0.7147 | -0.6653 | -0.4680 |
| 0.975 | ******* | -0.9095 | -0.6986 | -0.6518 | -0.4117 |
| 1.000 | -0.9196 | -0.9270 | -0.7197 | -0.6447 | -0.3656 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1939 | 0.1876 | 0.2271 | ******* | -0.4357 |
| -0.400 | 0.1931 | 0.1969 | 0.1980 | 0.0373 | -0.6655 |
| -0.600 | 0.2092 | 0.2041 | 0.1919 | 0.0712 | -0.6570 |
| -0.700 | ******* | 0.2118 | 0.1921 | 0.0845 | -0.6476 |
| -0.800 | ******* | ******* | 0.2015 | 0.1058 | -0.5815 |
| -0.850 | ******* | 0.2433 | 0.2104 | 0.1193 | -0.5594 |
| -0.900 | 0.2689 | 0.2566 | 0.2293 | 0.1431 | -0.5374 |
| -0.950 | 0.2680 | 0.1549 | 0.2311 | 0.1721 | -0.1753 |
| -0.975 | ******* | 0.1724 | 0.1831 | 0.1524 | -0.0261 |
| -1.000 | -0.8972 | -0.9279 | -0.7303 | -0.6320 | -0.3646 |



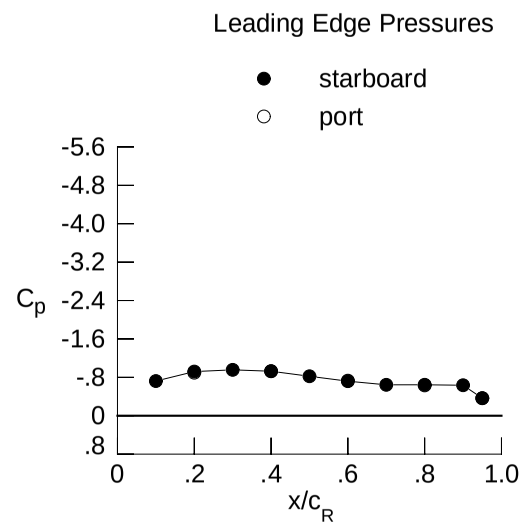

Small Radius L.E.

Run No. = 40 , Point No. = 819

$C_N$ = 0.468, $C_m$ = -0.0832

$\alpha$ = 10.4 °, $M_\infty$ = 0.830

$R_{mac}$ = $6.0 \times 10^6$

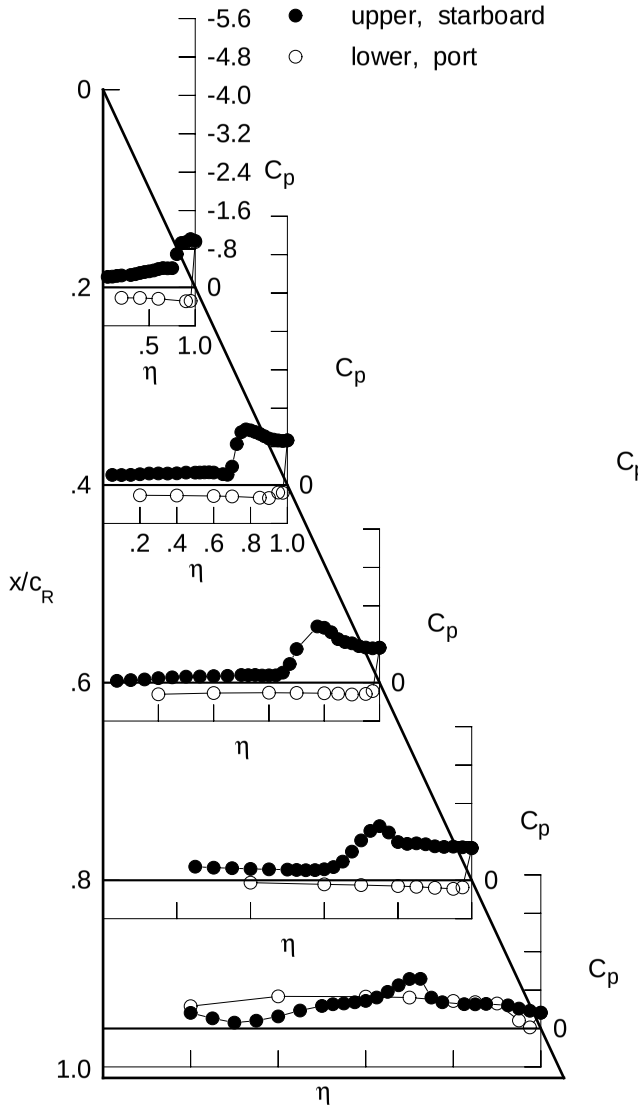



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.7225 | ******* |
| 0.20 | -0.9196 | -0.8972 |
| 0.30 | -0.9559 | ******* |
| 0.40 | -0.9270 | -0.9279 |
| 0.50 | -0.8222 | ******* |
| 0.60 | -0.7197 | -0.7303 |
| 0.70 | -0.6441 | ******* |
| 0.80 | -0.6447 | -0.6320 |
| 0.90 | -0.6351 | ******* |
| 0.95 | -0.3656 | -0.3646 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2193 | -0.2102 | -0.0373 | ******* | ******* |
| 0.100 | -0.2237 | -0.2077 | -0.0528 | ******* | ******* |
| 0.150 | -0.2392 | -0.2114 | -0.0665 | ******* | ******* |
| 0.200 | -0.2480 | -0.2250 | -0.0937 | ******* | -0.3255 |
| 0.250 | ******* | -0.2398 | -0.1107 | -0.2834 | -0.2118 |
| 0.300 | -0.2579 | -0.2415 | -0.1252 | -0.2622 | -0.1223 |
| 0.350 | -0.2748 | -0.2390 | -0.1282 | -0.2517 | -0.1623 |
| 0.400 | -0.3002 | -0.2443 | -0.1361 | -0.2371 | -0.2516 |
| 0.450 | -0.3197 | -0.2592 | -0.1416 | -0.2279 | -0.3745 |
| 0.500 | -0.3344 | -0.2581 | -0.1592 | -0.2227 | -0.4693 |
| 0.525 | ******* | -0.2600 | -0.1563 | -0.2155 | -0.5054 |
| 0.550 | -0.3525 | -0.2637 | -0.1603 | -0.2094 | -0.5220 |
| 0.575 | ******* | -0.2653 | -0.1477 | -0.2118 | -0.5468 |
| 0.600 | -0.3827 | -0.2598 | -0.1521 | -0.2298 | -0.5753 |
| 0.625 | ******* | ******* | -0.1522 | -0.2756 | -0.6457 |
| 0.650 | -0.4024 | -0.2265 | -0.2082 | -0.3889 | -0.7634 |
| 0.675 | ******* | -0.2144 | -0.3879 | -0.5972 | -0.9005 |
| 0.700 | -0.3979 | -0.3839 | -0.7000 | -0.8306 | -1.0322 |
| 0.725 | ******* | -0.8537 | ******* | -1.0284 | -1.0342 |
| 0.750 | -0.4011 | -1.1016 | ******* | -1.1282 | -0.6443 |
| 0.775 | ******* | -1.1595 | -1.1701 | -0.9950 | -0.5469 |
| 0.800 | -0.6924 | -1.1389 | -1.1431 | -0.7967 | ******* |
| 0.825 | ******* | -1.1046 | -1.0497 | -0.7581 | -0.5071 |
| 0.850 | -0.9246 | -1.0668 | -0.9068 | -0.7693 | -0.5042 |
| 0.875 | ******* | -1.0180 | -0.8453 | -0.7504 | -0.5127 |
| 0.900 | -0.9432 | -0.9686 | -0.8191 | -0.7082 | ******* |
| 0.925 | ******* | -0.9461 | -0.7609 | -0.6954 | -0.4824 |
| 0.950 | -1.0065 | -0.9303 | -0.7313 | -0.7007 | -0.4155 |
| 0.975 | ******* | -0.9188 | -0.7148 | -0.6877 | -0.3698 |
| 1.000 | -0.9674 | -0.9305 | -0.7278 | -0.6760 | -0.3315 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2178 | 0.2135 | 0.2426 | ******* | -0.4647 |
| -0.400 | 0.2203 | 0.2186 | 0.2169 | 0.0496 | -0.6693 |
| -0.600 | 0.2378 | 0.2288 | 0.2099 | 0.0848 | -0.6637 |
| -0.700 | ******* | 0.2374 | 0.2144 | 0.1000 | -0.6448 |
| -0.800 | ******* | ******* | 0.2206 | 0.1197 | -0.5734 |
| -0.850 | ******* | 0.2641 | 0.2289 | 0.1353 | -0.5485 |
| -0.900 | 0.2885 | 0.2714 | 0.2471 | 0.1564 | -0.5208 |
| -0.950 | 0.2805 | 0.1564 | 0.2349 | 0.1783 | -0.1671 |
| -0.975 | ******* | 0.1619 | 0.1749 | 0.1484 | -0.0229 |
| -1.000 | -0.9437 | -0.9315 | -0.7258 | -0.6667 | -0.3269 |

Surface Pressures




Small Radius L.E.

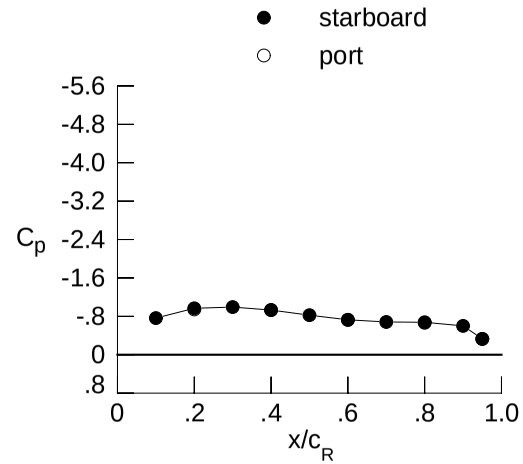
Run No. = 40 , Point No. = 820

$C_N$ = 0.516, $C_m$ = -0.0869

$\alpha$ = 11.4 °, $M_\infty$ = 0.828

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

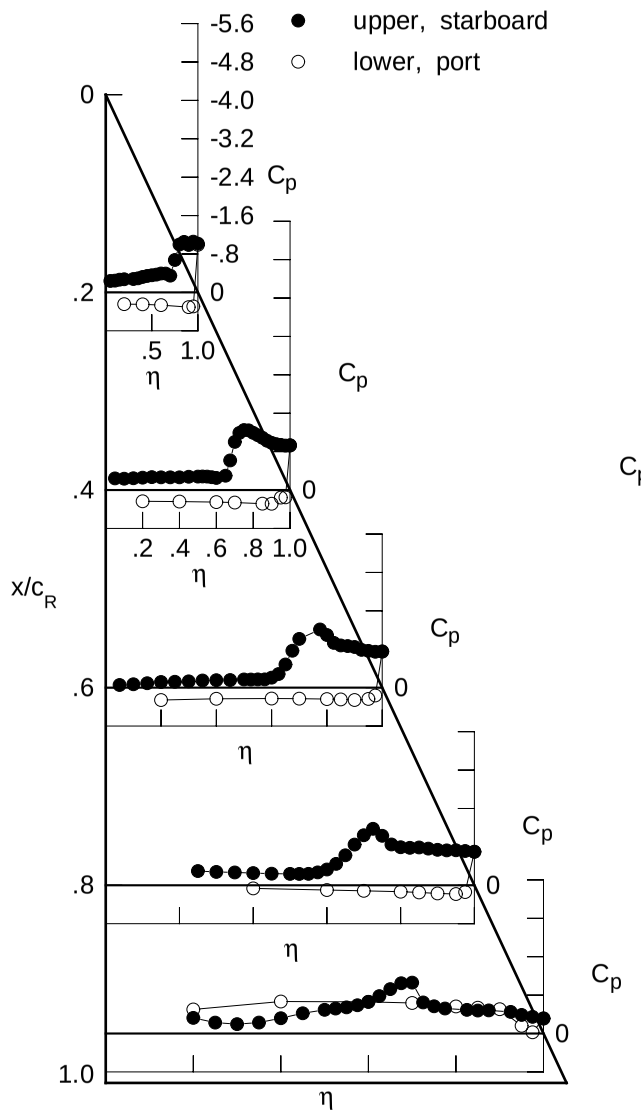



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.7636 | ******* |
| 0.20 | -0.9674 | -0.9437 |
| 0.30 | -0.9928 | ******* |
| 0.40 | -0.9305 | -0.9315 |
| 0.50 | -0.8240 | ******* |
| 0.60 | -0.7278 | -0.7258 |
| 0.70 | -0.6824 | ******* |
| 0.80 | -0.6760 | -0.6667 |
| 0.90 | -0.6012 | ******* |
| 0.95 | -0.3315 | -0.3269 |

# Table D4. Continued.

| η | x/c_R .2 C_p,u | x/c_R .4 C_p,u | x/c_R .6 C_p,u | x/c_R .8 C_p,u | x/c_R .95 C_p,u |
|---|---|---|---|---|---|
| 0.050 | -0.2388 | -0.2424 | -0.0553 | ******* | ******* |
| 0.100 | -0.2445 | -0.2357 | -0.0707 | ******* | ******* |
| 0.150 | -0.2650 | -0.2455 | -0.0922 | ******* | ******* |
| 0.200 | -0.2735 | -0.2573 | -0.1175 | ******* | -0.3258 |
| 0.250 | ******* | -0.2688 | -0.1224 | -0.2966 | -0.2272 |
| 0.300 | -0.2784 | -0.2649 | -0.1313 | -0.2780 | -0.1951 |
| 0.350 | -0.2926 | -0.2651 | -0.1486 | -0.2676 | -0.2280 |
| 0.400 | -0.3219 | -0.2647 | -0.1548 | -0.2548 | -0.3186 |
| 0.450 | -0.3426 | -0.2770 | -0.1583 | -0.2420 | -0.4216 |
| 0.500 | -0.3567 | -0.2800 | -0.1707 | -0.2377 | -0.4935 |
| 0.525 | ******* | -0.2822 | -0.1690 | -0.2368 | -0.5201 |
| 0.550 | -0.3700 | -0.2800 | -0.1717 | -0.2386 | -0.5447 |
| 0.575 | ******* | -0.2669 | -0.1720 | -0.2686 | -0.5885 |
| 0.600 | -0.3936 | -0.2519 | -0.2077 | -0.3289 | -0.6608 |
| 0.625 | ******* | ******* | -0.2829 | -0.4460 | -0.7791 |
| 0.650 | -0.3923 | -0.2987 | -0.4827 | -0.6248 | -0.9249 |
| 0.675 | ******* | -0.6167 | -0.7691 | -0.8482 | -1.0472 |
| 0.700 | -0.3489 | -1.0028 | -1.0154 | -1.0422 | -1.0599 |
| 0.725 | ******* | -1.1895 | ******* | -1.1767 | -0.6468 |
| 0.750 | -0.6751 | -1.2493 | ******* | -1.0314 | -0.5669 |
| 0.775 | ******* | -1.2443 | -1.2117 | -0.8506 | -0.5212 |
| 0.800 | -0.9976 | -1.1920 | -1.0965 | -0.7929 | ******* |
| 0.825 | ******* | -1.1421 | -0.9332 | -0.7811 | -0.4930 |
| 0.850 | -1.0517 | -1.0884 | -0.8794 | -0.7879 | -0.4787 |
| 0.875 | ******* | -1.0275 | -0.8665 | -0.7642 | -0.4816 |
| 0.900 | -0.9881 | -0.9828 | -0.8471 | -0.7396 | ******* |
| 0.925 | ******* | -0.9560 | -0.7875 | -0.7268 | -0.4505 |
| 0.950 | -1.0571 | -0.9405 | -0.7662 | -0.7293 | -0.3870 |
| 0.975 | ******* | -0.9262 | -0.7476 | -0.7143 | -0.3470 |
| 1.000 | -1.0152 | -0.9340 | -0.7563 | -0.6995 | -0.3158 |
| | C_p,l | C_p,l | C_p,l | C_p,l | C_p,l |
| -0.200 | 0.2450 | 0.2346 | 0.2584 | ******* | -0.5012 |
| -0.400 | 0.2486 | 0.2403 | 0.2321 | 0.0644 | -0.6666 |
| -0.600 | 0.2649 | 0.2513 | 0.2269 | 0.0991 | -0.6589 |
| -0.700 | ******* | 0.2606 | 0.2297 | 0.1154 | -0.6361 |
| -0.800 | ******* | ******* | 0.2380 | 0.1337 | -0.5641 |
| -0.850 | ******* | 0.2842 | 0.2456 | 0.1491 | -0.5373 |
| -0.900 | 0.3070 | 0.2854 | 0.2574 | 0.1697 | -0.5063 |
| -0.950 | 0.2923 | 0.1569 | 0.2353 | 0.1822 | -0.1604 |
| -0.975 | ******* | 0.1518 | 0.1635 | 0.1412 | -0.0255 |
| -1.000 | -0.9913 | -0.9262 | -0.7499 | -0.6972 | -0.3101 |

Surface Pressures




Small Radius L.E.

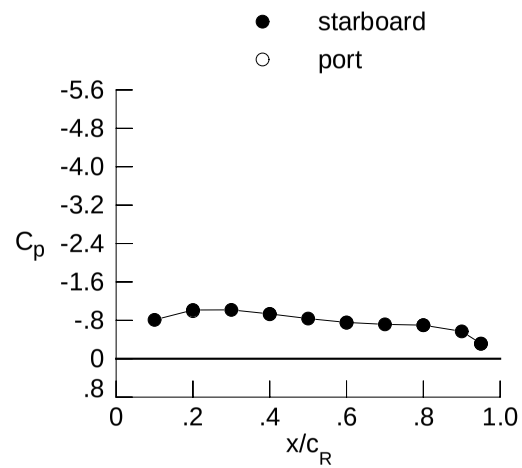
Run No. = 40 , Point No. = 821

$C_N$ = 0.569, $C_m$ = -0.0936

$\alpha$ = 12.4 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

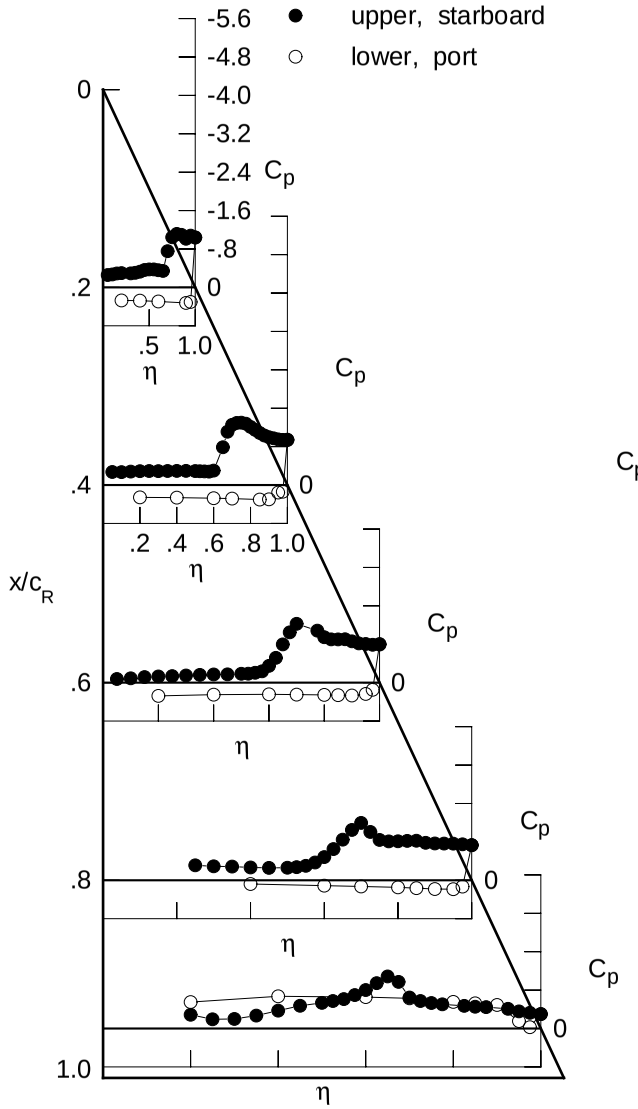



| x/c_R | starb'd C_p | port C_p |
|---|---|---|
| 0.10 | -0.8096 | ******* |
| 0.20 | -1.0152 | -0.9913 |
| 0.30 | -1.0179 | ******* |
| 0.40 | -0.9340 | -0.9262 |
| 0.50 | -0.8366 | ******* |
| 0.60 | -0.7563 | -0.7499 |
| 0.70 | -0.7158 | ******* |
| 0.80 | -0.6995 | -0.6972 |
| 0.90 | -0.5698 | ******* |
| 0.95 | -0.3158 | -0.3101 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2575 | -0.2718 | -0.0762 | ******* | ******* |
| 0.100 | -0.2696 | -0.2692 | -0.0907 | ******* | ******* |
| 0.150 | -0.2900 | -0.2800 | -0.1156 | ******* | ******* |
| 0.200 | -0.2976 | -0.2891 | -0.1290 | ******* | -0.2865 |
| 0.250 | ******* | -0.2921 | -0.1358 | -0.3118 | -0.1923 |
| 0.300 | -0.2924 | -0.2897 | -0.1491 | -0.2910 | -0.1992 |
| 0.350 | -0.3043 | -0.2926 | -0.1614 | -0.2856 | -0.2690 |
| 0.400 | -0.3276 | -0.2945 | -0.1705 | -0.2674 | -0.3721 |
| 0.450 | -0.3623 | -0.2955 | -0.1729 | -0.2581 | -0.4735 |
| 0.500 | -0.3745 | -0.2908 | -0.1846 | -0.2619 | -0.5343 |
| 0.525 | ******* | -0.2876 | -0.1861 | -0.2737 | -0.5728 |
| 0.550 | -0.3742 | -0.2840 | -0.2054 | -0.3015 | -0.6131 |
| 0.575 | ******* | -0.2790 | -0.2361 | -0.3704 | -0.6970 |
| 0.600 | -0.3576 | -0.3007 | -0.3498 | -0.4830 | -0.8015 |
| 0.625 | ******* | ******* | -0.5165 | -0.6508 | -0.9448 |
| 0.650 | -0.3429 | -0.7873 | -0.7969 | -0.8462 | -1.0849 |
| 0.675 | ******* | -1.1102 | -1.0481 | -1.0492 | -0.9710 |
| 0.700 | -0.7547 | -1.2542 | -1.2256 | -1.1955 | -0.6455 |
| 0.725 | ******* | -1.2936 | ******* | -1.0072 | -0.5730 |
| 0.750 | -1.0438 | -1.2989 | ******* | -0.8409 | -0.5310 |
| 0.775 | ******* | -1.2779 | -1.0835 | -0.8106 | -0.5036 |
| 0.800 | -1.1145 | -1.2108 | -0.9462 | -0.8126 | ******* |
| 0.825 | ******* | -1.1492 | -0.9020 | -0.8210 | -0.4718 |
| 0.850 | -1.0953 | -1.0850 | -0.9009 | -0.8240 | -0.4533 |
| 0.875 | ******* | -1.0321 | -0.9044 | -0.7810 | -0.4453 |
| 0.900 | -1.0127 | -0.9959 | -0.8604 | -0.7674 | ******* |
| 0.925 | ******* | -0.9733 | -0.8175 | -0.7645 | -0.4103 |
| 0.950 | -1.0781 | -0.9511 | -0.8054 | -0.7631 | -0.3567 |
| 0.975 | ******* | -0.9412 | -0.7884 | -0.7497 | -0.3272 |
| 1.000 | -1.0426 | -0.9447 | -0.7938 | -0.7337 | -0.2989 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2720 | 0.2572 | 0.2763 | ******* | -0.5505 |
| -0.400 | 0.2761 | 0.2624 | 0.2504 | 0.0775 | -0.6711 |
| -0.600 | 0.2938 | 0.2743 | 0.2433 | 0.1116 | -0.6542 |
| -0.700 | ******* | 0.2826 | 0.2492 | 0.1286 | -0.6286 |
| -0.800 | ******* | ******* | 0.2555 | 0.1473 | -0.5545 |
| -0.850 | ******* | 0.3023 | 0.2610 | 0.1641 | -0.5247 |
| -0.900 | 0.3239 | 0.2976 | 0.2680 | 0.1820 | -0.4901 |
| -0.950 | 0.3030 | 0.1556 | 0.2351 | 0.1857 | -0.1545 |
| -0.975 | ******* | 0.1395 | 0.1486 | 0.1316 | -0.0274 |
| -1.000 | -1.0373 | -0.9371 | -0.8041 | -0.7295 | -0.3024 |

Surface Pressures




Small Radius L.E.

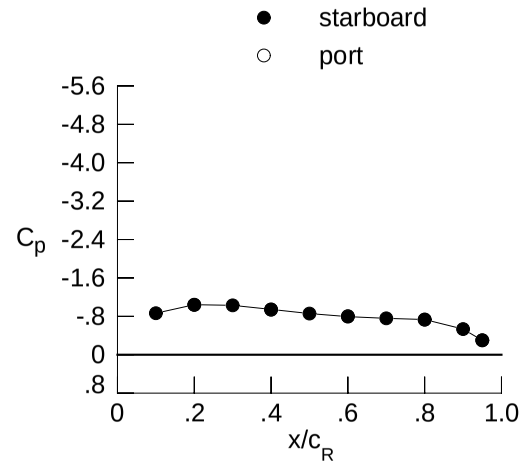
Run No. = 40 , Point No. = 822

$C_N$ = 0.619, $C_m$ = -0.0998

$\alpha$ = 13.4 °, $M_\infty$ = 0.830

$R_{mac}$ = $6.0 \times 10^6$

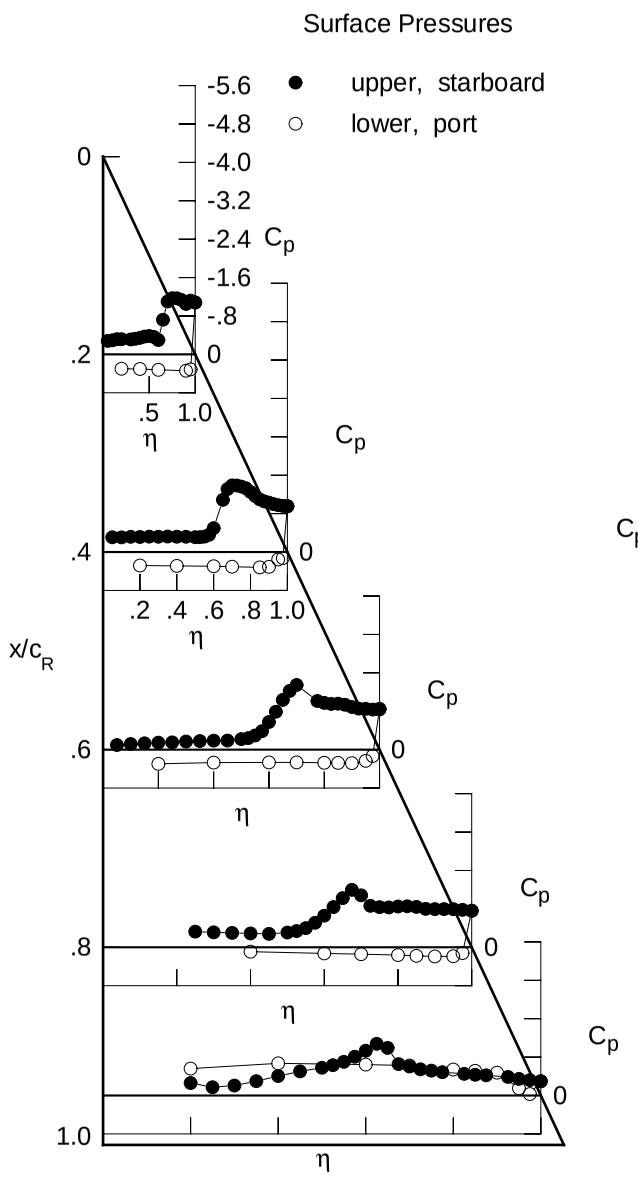
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.8646 | ******* |
| 0.20 | -1.0426 | -1.0373 |
| 0.30 | -1.0291 | ******* |
| 0.40 | -0.9447 | -0.9371 |
| 0.50 | -0.8577 | ******* |
| 0.60 | -0.7938 | -0.8041 |
| 0.70 | -0.7581 | ******* |
| 0.80 | -0.7337 | -0.7295 |
| 0.90 | -0.5348 | ******* |
| 0.95 | -0.2989 | -0.3024 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2807 | -0.3068 | -0.0961 | ******* | ******* |
| 0.100 | -0.2925 | -0.3053 | -0.1169 | ******* | ******* |
| 0.150 | -0.3169 | -0.3178 | -0.1322 | ******* | ******* |
| 0.200 | -0.3159 | -0.3136 | -0.1454 | ******* | -0.2604 |
| 0.250 | ******* | -0.3206 | -0.1510 | -0.3262 | -0.1732 |
| 0.300 | -0.3110 | -0.3182 | -0.1690 | -0.3114 | -0.2075 |
| 0.350 | -0.3247 | -0.3235 | -0.1791 | -0.2999 | -0.2980 |
| 0.400 | -0.3450 | -0.3195 | -0.1878 | -0.2882 | -0.4052 |
| 0.450 | -0.3718 | -0.3186 | -0.1896 | -0.2800 | -0.5026 |
| 0.500 | -0.3829 | -0.3086 | -0.2193 | -0.3073 | -0.5782 |
| 0.525 | ******* | -0.3088 | -0.2398 | -0.3382 | -0.6310 |
| 0.550 | -0.3629 | -0.3207 | -0.2956 | -0.3988 | -0.7018 |
| 0.575 | ******* | -0.3595 | -0.3849 | -0.5104 | -0.8080 |
| 0.600 | -0.2991 | -0.4976 | -0.5763 | -0.6585 | -0.9329 |
| 0.625 | ******* | ******* | -0.7895 | -0.8387 | -1.0770 |
| 0.650 | -0.7212 | -1.0870 | -1.0360 | -1.0243 | -0.9916 |
| 0.675 | ******* | -1.3111 | -1.2242 | -1.1970 | -0.6543 |
| 0.700 | -1.1017 | -1.3892 | -1.3471 | -1.0822 | -0.6049 |
| 0.725 | ******* | -1.3866 | ******* | -0.8637 | -0.5456 |
| 0.750 | -1.1703 | -1.3632 | ******* | -0.8359 | -0.5180 |
| 0.775 | ******* | -1.3284 | -1.0139 | -0.8306 | -0.4860 |
| 0.800 | -1.1688 | -1.2515 | -0.9742 | -0.8499 | ******* |
| 0.825 | ******* | -1.1683 | -0.9532 | -0.8541 | -0.4514 |
| 0.850 | -1.1332 | -1.0966 | -0.9575 | -0.8417 | -0.4316 |
| 0.875 | ******* | -1.0554 | -0.9350 | -0.8008 | -0.4207 |
| 0.900 | -1.0511 | -1.0286 | -0.8877 | -0.7956 | ******* |
| 0.925 | ******* | -0.9987 | -0.8543 | -0.7955 | -0.3869 |
| 0.950 | -1.1202 | -0.9749 | -0.8515 | -0.7945 | -0.3453 |
| 0.975 | ******* | -0.9613 | -0.8346 | -0.7801 | -0.3208 |
| 1.000 | -1.0803 | -0.9588 | -0.8371 | -0.7624 | -0.2963 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2996 | 0.2812 | 0.2958 | ******* | -0.5605 |
| -0.400 | 0.3038 | 0.2884 | 0.2698 | 0.0917 | -0.6701 |
| -0.600 | 0.3214 | 0.2963 | 0.2661 | 0.1273 | -0.6441 |
| -0.700 | ******* | 0.3056 | 0.2657 | 0.1438 | -0.6237 |
| -0.800 | ******* | ******* | 0.2733 | 0.1613 | -0.5407 |
| -0.850 | ******* | 0.3199 | 0.2758 | 0.1785 | -0.5148 |
| -0.900 | 0.3403 | 0.3079 | 0.2817 | 0.1912 | -0.4758 |
| -0.950 | 0.3127 | 0.1545 | 0.2338 | 0.1861 | -0.1498 |
| -0.975 | ******* | 0.1260 | 0.1326 | 0.1211 | -0.0307 |
| -1.000 | -1.0820 | -0.9492 | -0.8517 | -0.7605 | -0.2985 |



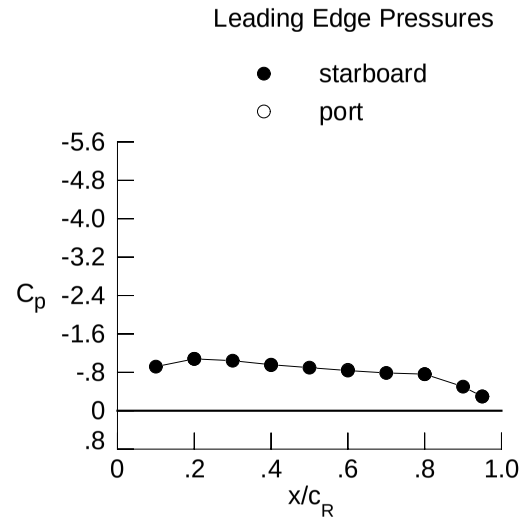

Small Radius L.E.

Run No. = 40 , Point No. = 823

$C_N$ = 0.669, $C_m$ = -0.1053

$\alpha$ = 14.5 °, $M_\infty$ = 0.828

$R_{mac}$ = $6.0 \times 10^6$

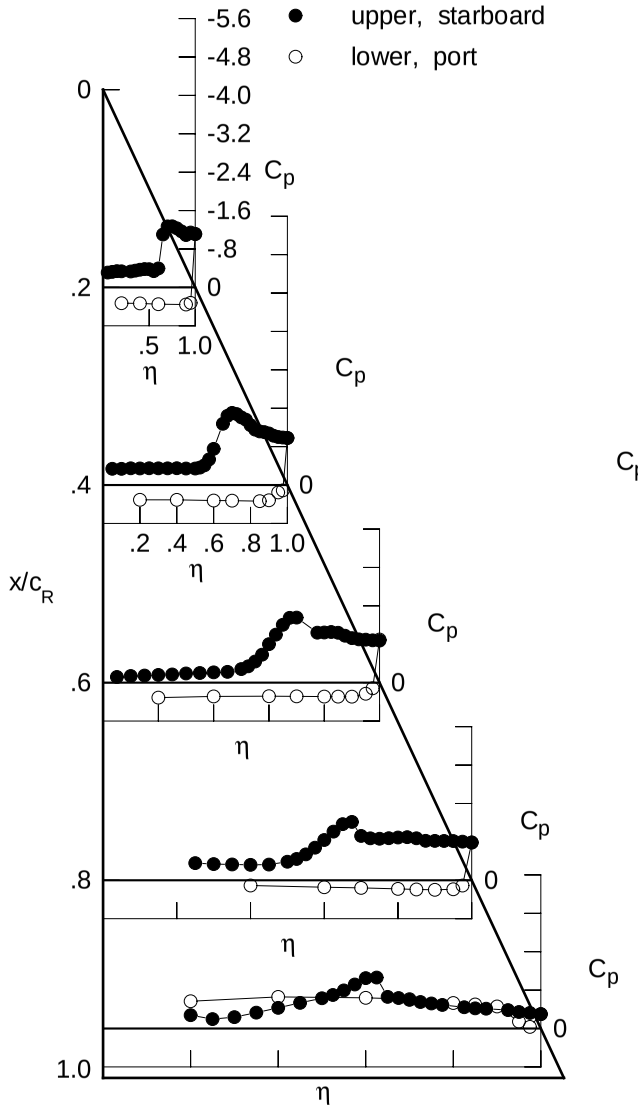



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.9187 | ******* |
| 0.20 | -1.0803 | -1.0820 |
| 0.30 | -1.0427 | ******* |
| 0.40 | -0.9588 | -0.9492 |
| 0.50 | -0.8974 | ******* |
| 0.60 | -0.8371 | -0.8517 |
| 0.70 | -0.7870 | ******* |
| 0.80 | -0.7624 | -0.7605 |
| 0.90 | -0.5014 | ******* |
| 0.95 | -0.2963 | -0.2985 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3085 | -0.3382 | -0.1187 | ******* | ******* |
| 0.100 | -0.3234 | -0.3377 | -0.1381 | ******* | ******* |
| 0.150 | -0.3380 | -0.3485 | -0.1482 | ******* | ******* |
| 0.200 | -0.3355 | -0.3457 | -0.1607 | ******* | -0.2777 |
| 0.250 | ******* | -0.3498 | -0.1703 | -0.3576 | -0.1959 |
| 0.300 | -0.3308 | -0.3484 | -0.1909 | -0.3379 | -0.2371 |
| 0.350 | -0.3490 | -0.3483 | -0.2006 | -0.3297 | -0.3306 |
| 0.400 | -0.3683 | -0.3503 | -0.2142 | -0.3219 | -0.4308 |
| 0.450 | -0.3816 | -0.3442 | -0.2245 | -0.3269 | -0.5348 |
| 0.500 | -0.3788 | -0.3443 | -0.2823 | -0.3865 | -0.6306 |
| 0.525 | ******* | -0.3630 | -0.3399 | -0.4439 | -0.6988 |
| 0.550 | -0.3383 | -0.4104 | -0.4402 | -0.5401 | -0.7937 |
| 0.575 | ******* | -0.5338 | -0.5827 | -0.6792 | -0.9170 |
| 0.600 | -0.3949 | -0.7532 | -0.8015 | -0.8392 | -1.0494 |
| 0.625 | ******* | ******* | -0.9999 | -1.0132 | -1.0612 |
| 0.650 | -1.1024 | -1.2760 | -1.2048 | -1.1696 | -0.6590 |
| 0.675 | ******* | -1.4421 | -1.3505 | -1.2161 | -0.6348 |
| 0.700 | -1.2712 | -1.5035 | -1.3556 | -0.9238 | -0.5971 |
| 0.725 | ******* | -1.4787 | ******* | -0.8744 | -0.5520 |
| 0.750 | -1.2731 | -1.4099 | ******* | -0.8653 | -0.5217 |
| 0.775 | ******* | -1.3617 | -1.0405 | -0.8764 | -0.4912 |
| 0.800 | -1.2310 | -1.2468 | -1.0448 | -0.8916 | ******* |
| 0.825 | ******* | -1.1541 | -1.0554 | -0.8983 | -0.4429 |
| 0.850 | -1.1673 | -1.1169 | -1.0395 | -0.8749 | -0.4197 |
| 0.875 | ******* | -1.1025 | -0.9773 | -0.8228 | -0.4124 |
| 0.900 | -1.0905 | -1.0747 | -0.9270 | -0.8209 | ******* |
| 0.925 | ******* | -1.0270 | -0.9018 | -0.8194 | -0.3842 |
| 0.950 | -1.1431 | -1.0004 | -0.8955 | -0.8173 | -0.3436 |
| 0.975 | ******* | -0.9899 | -0.8818 | -0.8047 | -0.3249 |
| 1.000 | -1.1086 | -0.9809 | -0.8763 | -0.7861 | -0.3020 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3295 | 0.3080 | 0.3122 | ******* | -0.5681 |
| -0.400 | 0.3335 | 0.3086 | 0.2872 | 0.1088 | -0.6583 |
| -0.600 | 0.3502 | 0.3229 | 0.2823 | 0.1446 | -0.6392 |
| -0.700 | ******* | 0.3253 | 0.2860 | 0.1583 | -0.6109 |
| -0.800 | ******* | ******* | 0.2901 | 0.1791 | -0.5315 |
| -0.850 | ******* | 0.3360 | 0.2915 | 0.1915 | -0.5010 |
| -0.900 | 0.3571 | 0.3174 | 0.2918 | 0.1982 | -0.4594 |
| -0.950 | 0.3227 | 0.1539 | 0.2315 | 0.1872 | -0.1439 |
| -0.975 | ******* | 0.1117 | 0.1175 | 0.1096 | -0.0338 |
| -1.000 | -1.1153 | -0.9794 | -0.8988 | -0.7878 | -0.2981 |

Surface Pressures




Small Radius L.E.

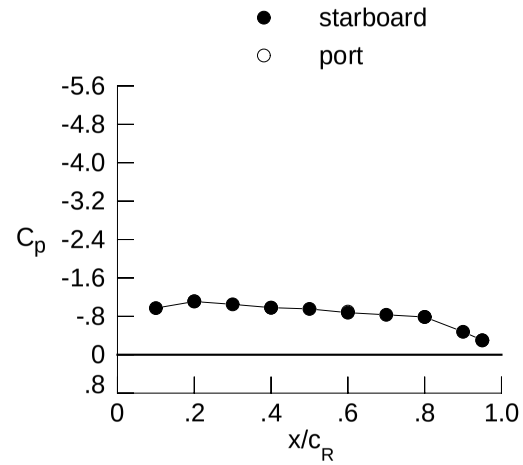
Run No. = 40 , Point No. = 824

$C_N$ = 0.722, $C_m$ = -0.1125

$\alpha$ = 15.5 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

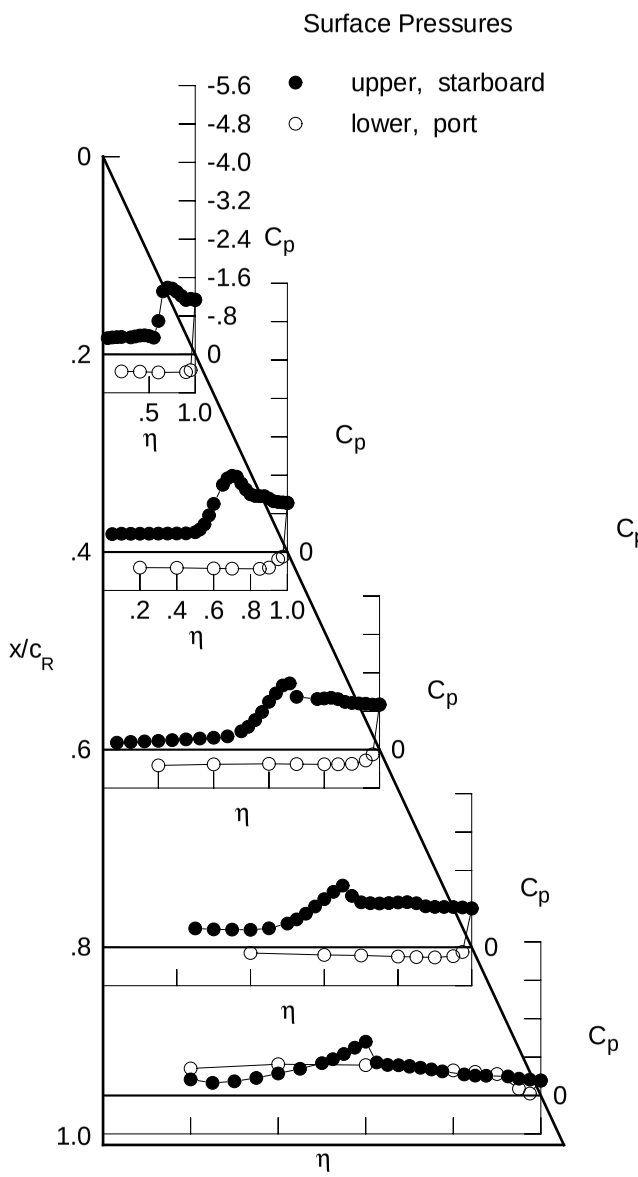
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.9715 | ******* |
| 0.20 | -1.1086 | -1.1153 |
| 0.30 | -1.0496 | ******* |
| 0.40 | -0.9809 | -0.9794 |
| 0.50 | -0.9542 | ******* |
| 0.60 | -0.8763 | -0.8988 |
| 0.70 | -0.8320 | ******* |
| 0.80 | -0.7861 | -0.7878 |
| 0.90 | -0.4780 | ******* |
| 0.95 | -0.3020 | -0.2981 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3382 | -0.3739 | -0.1445 | ******* | ******* |
| 0.100 | -0.3532 | -0.3816 | -0.1598 | ******* | ******* |
| 0.150 | -0.3590 | -0.3804 | -0.1711 | ******* | ******* |
| 0.200 | -0.3634 | -0.3819 | -0.1830 | ******* | -0.3354 |
| 0.250 | ******* | -0.3825 | -0.1982 | -0.3929 | -0.2630 |
| 0.300 | -0.3542 | -0.3843 | -0.2138 | -0.3726 | -0.2952 |
| 0.350 | -0.3740 | -0.3851 | -0.2317 | -0.3691 | -0.3659 |
| 0.400 | -0.3927 | -0.3860 | -0.2492 | -0.3641 | -0.4586 |
| 0.450 | -0.3975 | -0.3892 | -0.2772 | -0.3948 | -0.5568 |
| 0.500 | -0.3817 | -0.4118 | -0.3818 | -0.4939 | -0.6736 |
| 0.525 | ******* | -0.4693 | -0.4761 | -0.5807 | -0.7566 |
| 0.550 | -0.3491 | -0.5768 | -0.6163 | -0.7003 | -0.8644 |
| 0.575 | ******* | -0.7647 | -0.7850 | -0.8494 | -0.9964 |
| 0.600 | -0.6963 | -1.0028 | -0.9968 | -1.0023 | -1.1207 |
| 0.625 | ******* | ******* | -1.1711 | -1.1552 | -0.6884 |
| 0.650 | -1.3130 | -1.4006 | -1.3366 | -1.2858 | -0.6369 |
| 0.675 | ******* | -1.5349 | -1.3799 | -1.0709 | -0.6304 |
| 0.700 | -1.3915 | -1.5876 | -1.0996 | -0.9370 | -0.6154 |
| 0.725 | ******* | -1.5693 | ******* | -0.9180 | -0.5785 |
| 0.750 | -1.3708 | -1.4281 | ******* | -0.9132 | -0.5434 |
| 0.775 | ******* | -1.3020 | -1.0543 | -0.9207 | -0.5025 |
| 0.800 | -1.3039 | -1.2017 | -1.0665 | -0.9335 | ******* |
| 0.825 | ******* | -1.1679 | -1.0799 | -0.9402 | -0.4393 |
| 0.850 | -1.2190 | -1.1631 | -1.0518 | -0.9179 | -0.4141 |
| 0.875 | ******* | -1.1642 | -0.9940 | -0.8537 | -0.4119 |
| 0.900 | -1.1326 | -1.1130 | -0.9717 | -0.8411 | ******* |
| 0.925 | ******* | -1.0576 | -0.9623 | -0.8399 | -0.3973 |
| 0.950 | -1.1578 | -1.0425 | -0.9570 | -0.8387 | -0.3501 |
| 0.975 | ******* | -1.0347 | -0.9386 | -0.8292 | -0.3314 |
| 1.000 | -1.1294 | -1.0278 | -0.9323 | -0.8121 | -0.3146 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3553 | 0.3246 | 0.3291 | ******* | -0.5636 |
| -0.400 | 0.3604 | 0.3288 | 0.3061 | 0.1195 | -0.6516 |
| -0.600 | 0.3758 | 0.3419 | 0.2957 | 0.1595 | -0.6330 |
| -0.700 | ******* | 0.3464 | 0.3020 | 0.1703 | -0.6010 |
| -0.800 | ******* | ******* | 0.3059 | 0.1926 | -0.5235 |
| -0.850 | ******* | 0.3501 | 0.3045 | 0.2038 | -0.4911 |
| -0.900 | 0.3699 | 0.3243 | 0.2962 | 0.2112 | -0.4469 |
| -0.950 | 0.3291 | 0.1498 | 0.2258 | 0.1857 | -0.1405 |
| -0.975 | ******* | 0.0958 | 0.0988 | 0.0972 | -0.0408 |
| -1.000 | -1.1430 | -1.0158 | -0.9452 | -0.8063 | -0.3086 |



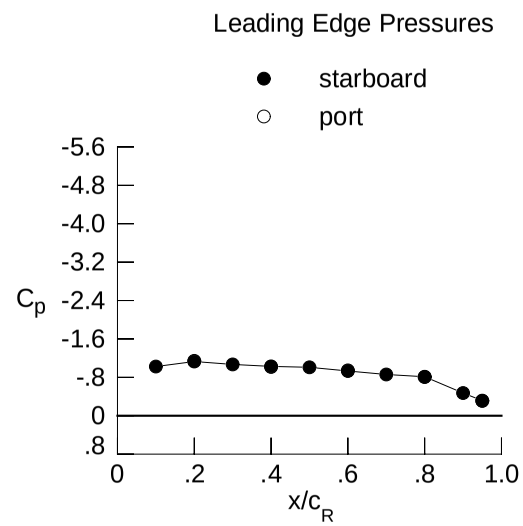

Small Radius L.E.

Run No. = 40 , Point No. = 825

$C_N$ = 0.776, $C_m$ = -0.1192

$\alpha$ = 16.5 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

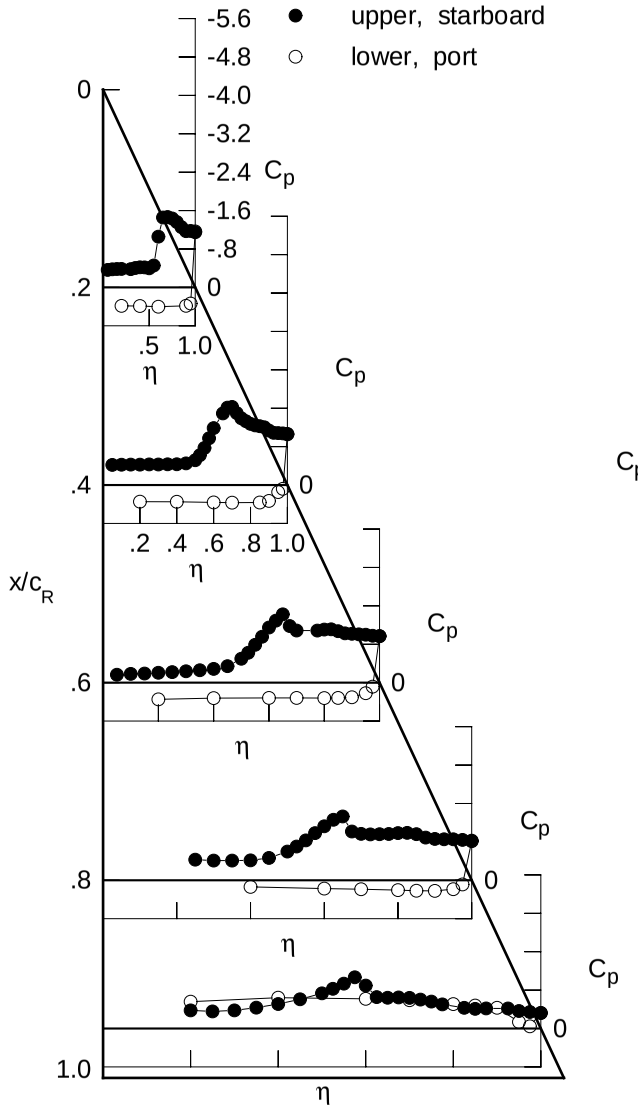



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0247 | ******* |
| 0.20 | -1.1294 | -1.1430 |
| 0.30 | -1.0688 | ******* |
| 0.40 | -1.0278 | -1.0158 |
| 0.50 | -1.0090 | ******* |
| 0.60 | -0.9323 | -0.9452 |
| 0.70 | -0.8593 | ******* |
| 0.80 | -0.8121 | -0.8063 |
| 0.90 | -0.4729 | ******* |
| 0.95 | -0.3146 | -0.3086 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3637 | -0.4196 | -0.1646 | ******* | ******* |
| 0.100 | -0.3771 | -0.4235 | -0.1822 | ******* | ******* |
| 0.150 | -0.3834 | -0.4256 | -0.1897 | ******* | ******* |
| 0.200 | -0.3847 | -0.4248 | -0.2057 | ******* | -0.3774 |
| 0.250 | ******* | -0.4297 | -0.2192 | -0.4300 | -0.3563 |
| 0.300 | -0.3803 | -0.4279 | -0.2368 | -0.4103 | -0.3780 |
| 0.350 | -0.4041 | -0.4322 | -0.2580 | -0.4106 | -0.4343 |
| 0.400 | -0.4186 | -0.4327 | -0.2865 | -0.4154 | -0.5101 |
| 0.450 | -0.4169 | -0.4509 | -0.3429 | -0.4653 | -0.6089 |
| 0.500 | -0.3976 | -0.5169 | -0.4979 | -0.5988 | -0.7331 |
| 0.525 | ******* | -0.6212 | -0.6221 | -0.7030 | -0.8270 |
| 0.550 | -0.4558 | -0.7727 | -0.7880 | -0.8314 | -0.9341 |
| 0.575 | ******* | -0.9744 | -0.9557 | -0.9824 | -1.0671 |
| 0.600 | -1.0567 | -1.1863 | -1.1484 | -1.1249 | -0.8943 |
| 0.625 | ******* | ******* | -1.2910 | -1.2606 | -0.6543 |
| 0.650 | -1.4563 | -1.4921 | -1.4235 | -1.3295 | -0.6409 |
| 0.675 | ******* | -1.6129 | -1.1789 | -1.0161 | -0.6469 |
| 0.700 | -1.4668 | -1.6273 | -1.0854 | -0.9676 | -0.6387 |
| 0.725 | ******* | -1.4988 | ******* | -0.9558 | -0.6027 |
| 0.750 | -1.4363 | -1.3904 | ******* | -0.9598 | -0.5606 |
| 0.775 | ******* | -1.3296 | -1.0847 | -0.9651 | -0.5028 |
| 0.800 | -1.3615 | -1.2740 | -1.1054 | -0.9829 | ******* |
| 0.825 | ******* | -1.2428 | -1.1110 | -0.9877 | -0.4309 |
| 0.850 | -1.2553 | -1.2258 | -1.0720 | -0.9609 | -0.4097 |
| 0.875 | ******* | -1.2033 | -1.0274 | -0.8893 | -0.4187 |
| 0.900 | -1.1708 | -1.1350 | -1.0177 | -0.8612 | ******* |
| 0.925 | ******* | -1.0880 | -1.0060 | -0.8543 | -0.4177 |
| 0.950 | -1.1758 | -1.0823 | -0.9985 | -0.8546 | -0.3645 |
| 0.975 | ******* | -1.0757 | -0.9768 | -0.8418 | -0.3440 |
| 1.000 | -1.1484 | -1.0650 | -0.9672 | -0.8254 | -0.3240 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3849 | 0.3468 | 0.3478 | ******* | -0.5588 |
| -0.400 | 0.3881 | 0.3492 | 0.3224 | 0.1374 | -0.6420 |
| -0.600 | 0.4024 | 0.3621 | 0.3186 | 0.1728 | -0.6184 |
| -0.700 | ******* | 0.3674 | 0.3183 | 0.1863 | -0.5898 |
| -0.800 | ******* | ******* | 0.3215 | 0.2048 | -0.5086 |
| -0.850 | ******* | 0.3641 | 0.3183 | 0.2177 | -0.4786 |
| -0.900 | 0.3837 | 0.3313 | 0.3045 | 0.2208 | -0.4323 |
| -0.950 | 0.3358 | 0.1465 | 0.2200 | 0.1855 | -0.1371 |
| -0.975 | ******* | 0.0796 | 0.0828 | 0.0861 | -0.0459 |
| -1.000 | -1.1661 | -1.0561 | -0.9700 | -0.8146 | -0.3238 |

Surface Pressures




Small Radius L.E.

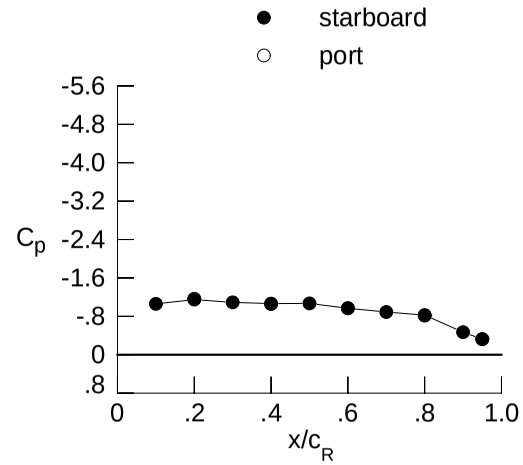
Run No. = 40 , Point No. = 826

$C_N$ = 0.836, $C_m$ = -0.1313

$\alpha$ = 17.5 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

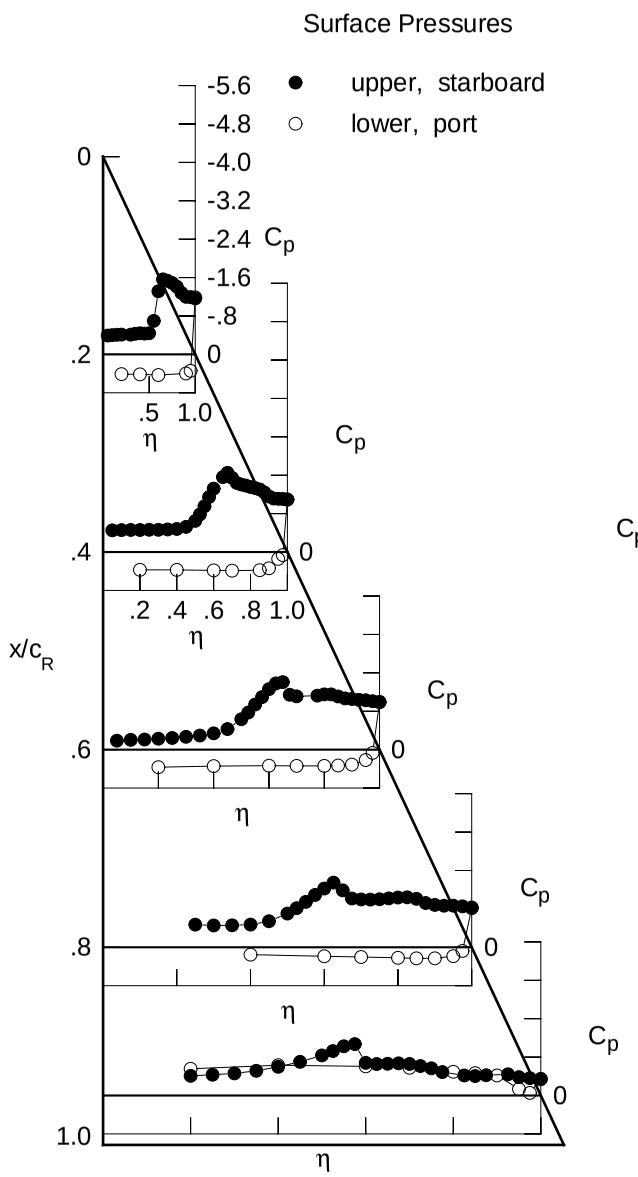
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0600 | ******* |
| 0.20 | -1.1484 | -1.1661 |
| 0.30 | -1.0912 | ******* |
| 0.40 | -1.0650 | -1.0561 |
| 0.50 | -1.0695 | ******* |
| 0.60 | -0.9672 | -0.9700 |
| 0.70 | -0.8902 | ******* |
| 0.80 | -0.8254 | -0.8146 |
| 0.90 | -0.4695 | ******* |
| 0.95 | -0.3240 | -0.3238 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3930 | -0.4517 | -0.1875 | ******* | ******* |
| 0.100 | -0.4011 | -0.4567 | -0.2041 | ******* | ******* |
| 0.150 | -0.4088 | -0.4601 | -0.2110 | ******* | ******* |
| 0.200 | -0.4123 | -0.4595 | -0.2281 | ******* | -0.4099 |
| 0.250 | ******* | -0.4642 | -0.2430 | -0.4717 | -0.4326 |
| 0.300 | -0.4109 | -0.4629 | -0.2670 | -0.4544 | -0.4605 |
| 0.350 | -0.4306 | -0.4704 | -0.2934 | -0.4576 | -0.5147 |
| 0.400 | -0.4398 | -0.4810 | -0.3394 | -0.4728 | -0.5983 |
| 0.450 | -0.4339 | -0.5242 | -0.4286 | -0.5422 | -0.7020 |
| 0.500 | -0.4405 | -0.6485 | -0.6336 | -0.7023 | -0.8350 |
| 0.525 | ******* | -0.7816 | -0.7730 | -0.8142 | -0.9267 |
| 0.550 | -0.6981 | -0.9527 | -0.9402 | -0.9468 | -1.0254 |
| 0.575 | ******* | -1.1454 | -1.0947 | -1.0901 | -1.0714 |
| 0.600 | -1.3151 | -1.3204 | -1.2597 | -1.2239 | -0.6812 |
| 0.625 | ******* | ******* | -1.3803 | -1.3472 | -0.6557 |
| 0.650 | -1.5634 | -1.5605 | -1.4064 | -1.1862 | -0.6615 |
| 0.675 | ******* | -1.6504 | -1.1429 | -1.0171 | -0.6703 |
| 0.700 | -1.5331 | -1.5448 | -1.1108 | -0.9966 | -0.6574 |
| 0.725 | ******* | -1.4400 | ******* | -0.9934 | -0.6138 |
| 0.750 | -1.4874 | -1.4063 | ******* | -1.0008 | -0.5660 |
| 0.775 | ******* | -1.3837 | -1.1250 | -1.0182 | -0.4891 |
| 0.800 | -1.4108 | -1.3545 | -1.1512 | -1.0371 | ******* |
| 0.825 | ******* | -1.3329 | -1.1514 | -1.0407 | -0.4173 |
| 0.850 | -1.2811 | -1.3029 | -1.1078 | -1.0093 | -0.4057 |
| 0.875 | ******* | -1.2427 | -1.0675 | -0.9226 | -0.4224 |
| 0.900 | -1.1989 | -1.1574 | -1.0550 | -0.8826 | ******* |
| 0.925 | ******* | -1.1153 | -1.0373 | -0.8661 | -0.4424 |
| 0.950 | -1.1926 | -1.1092 | -1.0285 | -0.8671 | -0.3826 |
| 0.975 | ******* | -1.1059 | -1.0086 | -0.8526 | -0.3613 |
| 1.000 | -1.1657 | -1.0953 | -0.9943 | -0.8301 | -0.3404 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4113 | 0.3708 | 0.3658 | ******* | -0.5571 |
| -0.400 | 0.4160 | 0.3721 | 0.3428 | 0.1532 | -0.6309 |
| -0.600 | 0.4295 | 0.3828 | 0.3344 | 0.1875 | -0.6072 |
| -0.700 | ******* | 0.3880 | 0.3386 | 0.2021 | -0.5779 |
| -0.800 | ******* | ******* | 0.3387 | 0.2195 | -0.4945 |
| -0.850 | ******* | 0.3780 | 0.3306 | 0.2303 | -0.4656 |
| -0.900 | 0.3977 | 0.3387 | 0.3118 | 0.2297 | -0.4178 |
| -0.950 | 0.3428 | 0.1430 | 0.2171 | 0.1850 | -0.1338 |
| -0.975 | ******* | 0.0642 | 0.0676 | 0.0760 | -0.0547 |
| -1.000 | -1.1879 | -1.0926 | -0.9876 | -0.8135 | -0.3478 |



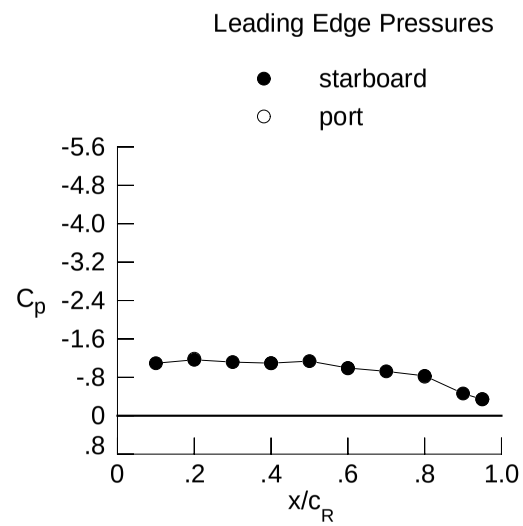

Small Radius L.E.

Run No. = 40 , Point No. = 827

$C_N$ = 0.895, $C_m$ = -0.1428

$\alpha$ = 18.6 °, $M_\infty$ = 0.828

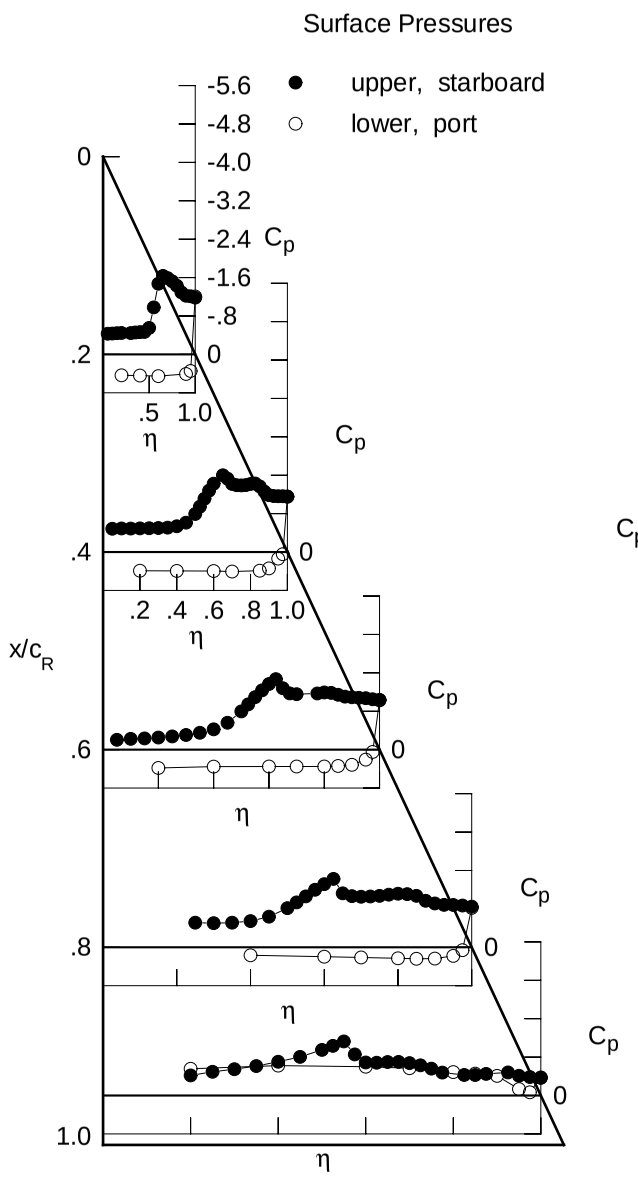
$R_{mac}$ = $6.0 \times 10^6$




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0935 | ******* |
| 0.20 | -1.1657 | -1.1879 |
| 0.30 | -1.1173 | ******* |
| 0.40 | -1.0953 | -1.0926 |
| 0.50 | -1.1379 | ******* |
| 0.60 | -0.9943 | -0.9876 |
| 0.70 | -0.9244 | ******* |
| 0.80 | -0.8301 | -0.8135 |
| 0.90 | -0.4630 | ******* |
| 0.95 | -0.3404 | -0.3478 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4300 | -0.4849 | -0.2050 | ******* | ******* |
| 0.100 | -0.4346 | -0.4912 | -0.2247 | ******* | ******* |
| 0.150 | -0.4413 | -0.4889 | -0.2339 | ******* | ******* |
| 0.200 | -0.4467 | -0.4928 | -0.2520 | ******* | -0.4181 |
| 0.250 | ******* | -0.4960 | -0.2752 | -0.5129 | -0.4945 |
| 0.300 | -0.4436 | -0.5008 | -0.3055 | -0.5022 | -0.5478 |
| 0.350 | -0.4567 | -0.5081 | -0.3511 | -0.5124 | -0.6136 |
| 0.400 | -0.4641 | -0.5364 | -0.4230 | -0.5457 | -0.7031 |
| 0.450 | -0.4677 | -0.6118 | -0.5603 | -0.6373 | -0.8046 |
| 0.500 | -0.5522 | -0.7931 | -0.7965 | -0.8149 | -0.9500 |
| 0.525 | ******* | -0.9438 | -0.9440 | -0.9351 | -1.0342 |
| 0.550 | -0.9793 | -1.1104 | -1.0937 | -1.0604 | -1.1265 |
| 0.575 | ******* | -1.2787 | -1.2355 | -1.1986 | -0.8561 |
| 0.600 | -1.4718 | -1.4242 | -1.3674 | -1.3152 | -0.6880 |
| 0.625 | ******* | ******* | -1.4685 | -1.4250 | -0.6828 |
| 0.650 | -1.6352 | -1.5993 | -1.2796 | -1.1243 | -0.6975 |
| 0.675 | ******* | -1.5286 | -1.1719 | -1.0655 | -0.7001 |
| 0.700 | -1.5895 | -1.4182 | -1.1554 | -1.0532 | -0.6749 |
| 0.725 | ******* | -1.3923 | ******* | -1.0586 | -0.6292 |
| 0.750 | -1.5220 | -1.3879 | ******* | -1.0713 | -0.5599 |
| 0.775 | ******* | -1.3950 | -1.1707 | -1.0961 | -0.4774 |
| 0.800 | -1.4311 | -1.4181 | -1.1910 | -1.1162 | ******* |
| 0.825 | ******* | -1.4277 | -1.1828 | -1.1070 | -0.4282 |
| 0.850 | -1.2916 | -1.3671 | -1.1436 | -1.0717 | -0.4270 |
| 0.875 | ******* | -1.2607 | -1.1042 | -0.9692 | -0.4507 |
| 0.900 | -1.2220 | -1.1856 | -1.0910 | -0.9127 | ******* |
| 0.925 | ******* | -1.1661 | -1.0800 | -0.8837 | -0.4806 |
| 0.950 | -1.2103 | -1.1628 | -1.0718 | -0.8816 | -0.4113 |
| 0.975 | ******* | -1.1621 | -1.0500 | -0.8699 | -0.3851 |
| 1.000 | -1.1822 | -1.1576 | -1.0375 | -0.8467 | -0.3675 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4360 | 0.3895 | 0.3819 | ******* | -0.5568 |
| -0.400 | 0.4408 | 0.3935 | 0.3538 | 0.1661 | -0.6228 |
| -0.600 | 0.4524 | 0.3962 | 0.3515 | 0.1960 | -0.5998 |
| -0.700 | ******* | 0.4063 | 0.3513 | 0.2123 | -0.5691 |
| -0.800 | ******* | ******* | 0.3514 | 0.2296 | -0.4882 |
| -0.850 | ******* | 0.3887 | 0.3399 | 0.2395 | -0.4556 |
| -0.900 | 0.4082 | 0.3411 | 0.3160 | 0.2356 | -0.4091 |
| -0.950 | 0.3456 | 0.1364 | 0.2082 | 0.1792 | -0.1342 |
| -0.975 | ******* | 0.0460 | 0.0482 | 0.0598 | -0.0669 |
| -1.000 | -1.2063 | -1.1516 | -1.0271 | -0.8200 | -0.3774 |



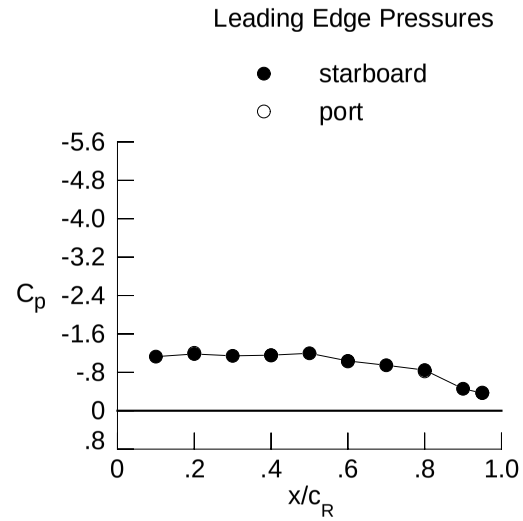

Small Radius L.E.

Run No. = 40 , Point No. = 828

$C_N$ = 0.955, $C_m$ = -0.1554

$\alpha$ = 19.6 °, $M_\infty$ = 0.829

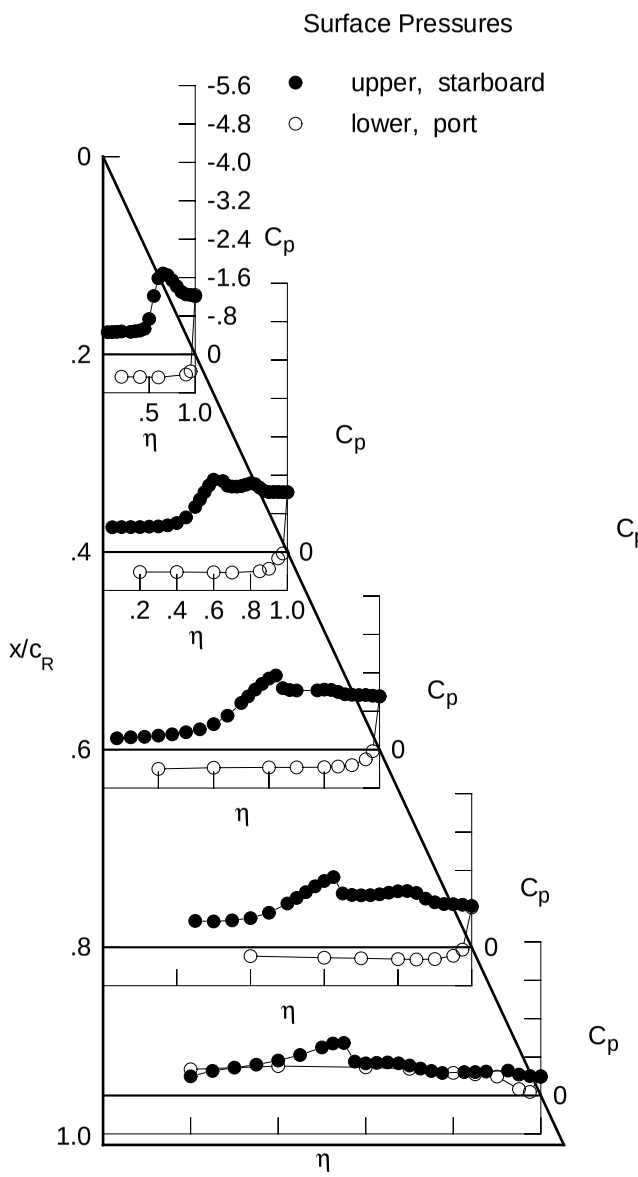
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1269 | ******* |
| 0.20 | -1.1822 | -1.2063 |
| 0.30 | -1.1435 | ******* |
| 0.40 | -1.1576 | -1.1516 |
| 0.50 | -1.1968 | ******* |
| 0.60 | -1.0375 | -1.0271 |
| 0.70 | -0.9471 | ******* |
| 0.80 | -0.8467 | -0.8200 |
| 0.90 | -0.4577 | ******* |
| 0.95 | -0.3675 | -0.3774 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4621 | -0.5156 | -0.2359 | ******* | ******* |
| 0.100 | -0.4658 | -0.5193 | -0.2573 | ******* | ******* |
| 0.150 | -0.4697 | -0.5192 | -0.2676 | ******* | ******* |
| 0.200 | -0.4773 | -0.5204 | -0.2921 | ******* | -0.3994 |
| 0.250 | ******* | -0.5289 | -0.3195 | -0.5485 | -0.5129 |
| 0.300 | -0.4697 | -0.5336 | -0.3621 | -0.5384 | -0.5809 |
| 0.350 | -0.4826 | -0.5562 | -0.4237 | -0.5611 | -0.6422 |
| 0.400 | -0.4957 | -0.6040 | -0.5312 | -0.6072 | -0.7291 |
| 0.450 | -0.5340 | -0.7212 | -0.7070 | -0.7190 | -0.8439 |
| 0.500 | -0.7376 | -0.9390 | -0.9718 | -0.9118 | -1.0009 |
| 0.525 | ******* | -1.0929 | -1.1105 | -1.0277 | -1.0835 |
| 0.550 | -1.2166 | -1.2458 | -1.2514 | -1.1478 | -1.0943 |
| 0.575 | ******* | -1.3876 | -1.3697 | -1.2707 | -0.7062 |
| 0.600 | -1.5856 | -1.5075 | -1.4808 | -1.3817 | -0.6699 |
| 0.625 | ******* | ******* | -1.5449 | -1.4620 | -0.6804 |
| 0.650 | -1.6846 | -1.4777 | -1.2805 | -1.1198 | -0.6886 |
| 0.675 | ******* | -1.3817 | -1.2415 | -1.0901 | -0.6714 |
| 0.700 | -1.6488 | -1.3640 | -1.2327 | -1.0823 | -0.6250 |
| 0.725 | ******* | -1.3624 | ******* | -1.0855 | -0.5605 |
| 0.750 | -1.5425 | -1.3737 | ******* | -1.1037 | -0.5116 |
| 0.775 | ******* | -1.4030 | -1.2346 | -1.1373 | -0.4692 |
| 0.800 | -1.4174 | -1.4329 | -1.2504 | -1.1670 | ******* |
| 0.825 | ******* | -1.4133 | -1.2443 | -1.1717 | -0.4877 |
| 0.850 | -1.3016 | -1.3400 | -1.2024 | -1.1318 | -0.4881 |
| 0.875 | ******* | -1.2734 | -1.1539 | -1.0139 | -0.4994 |
| 0.900 | -1.2497 | -1.2481 | -1.1435 | -0.9374 | ******* |
| 0.925 | ******* | -1.2520 | -1.1361 | -0.9009 | -0.5196 |
| 0.950 | -1.2372 | -1.2516 | -1.1382 | -0.8977 | -0.4358 |
| 0.975 | ******* | -1.2471 | -1.1233 | -0.8856 | -0.4057 |
| 1.000 | -1.2121 | -1.2431 | -1.1108 | -0.8608 | -0.3881 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4665 | 0.4172 | 0.4015 | ******* | -0.5459 |
| -0.400 | 0.4709 | 0.4168 | 0.3769 | 0.1844 | -0.6127 |
| -0.600 | 0.4789 | 0.4221 | 0.3701 | 0.2179 | -0.5870 |
| -0.700 | ******* | 0.4284 | 0.3704 | 0.2294 | -0.5560 |
| -0.800 | ******* | ******* | 0.3657 | 0.2462 | -0.4721 |
| -0.850 | ******* | 0.4003 | 0.3523 | 0.2541 | -0.4427 |
| -0.900 | 0.4203 | 0.3482 | 0.3234 | 0.2455 | -0.3952 |
| -0.950 | 0.3528 | 0.1321 | 0.2027 | 0.1773 | -0.1325 |
| -0.975 | ******* | 0.0287 | 0.0312 | 0.0484 | -0.0747 |
| -1.000 | -1.2378 | -1.2484 | -1.1069 | -0.8305 | -0.4029 |



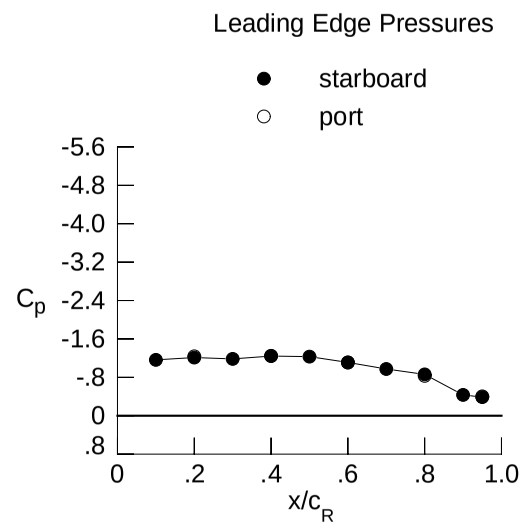

Small Radius L.E.

Run No. = 40 , Point No. = 829

$C_N$ = 1.005, $C_m$ = -0.1619

$\alpha$ = 20.6 °, $M_\infty$ = 0.828

$R_{mac}$ = $6.0 \times 10^6$

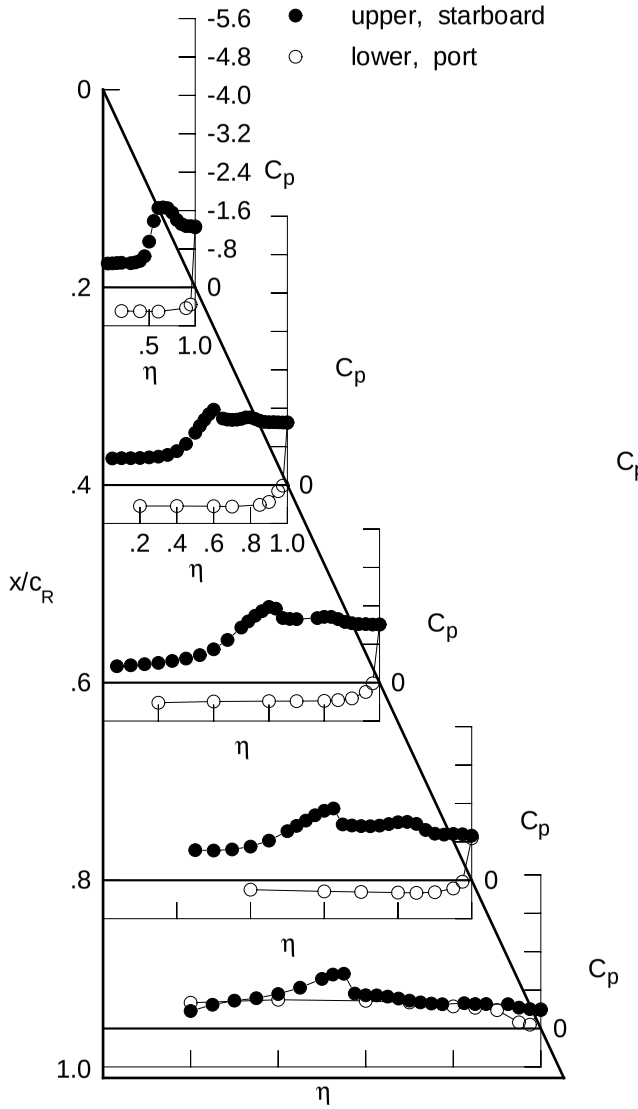



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1642 | ******* |
| 0.20 | -1.2121 | -1.2378 |
| 0.30 | -1.1839 | ******* |
| 0.40 | -1.2431 | -1.2484 |
| 0.50 | -1.2312 | ******* |
| 0.60 | -1.1108 | -1.1069 |
| 0.70 | -0.9739 | ******* |
| 0.80 | -0.8608 | -0.8305 |
| 0.90 | -0.4335 | ******* |
| 0.95 | -0.3881 | -0.4029 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4970 | -0.5534 | -0.3418 | ******* | ******* |
| 0.100 | -0.5002 | -0.5596 | -0.3614 | ******* | ******* |
| 0.150 | -0.5071 | -0.5596 | -0.3845 | ******* | ******* |
| 0.200 | -0.5129 | -0.5631 | -0.4111 | ******* | -0.3644 |
| 0.250 | ******* | -0.5761 | -0.4517 | -0.6278 | -0.4955 |
| 0.300 | -0.5041 | -0.5916 | -0.5015 | -0.6203 | -0.5807 |
| 0.350 | -0.5200 | -0.6271 | -0.5735 | -0.6426 | -0.6313 |
| 0.400 | -0.5513 | -0.7068 | -0.6944 | -0.7018 | -0.7182 |
| 0.450 | -0.6497 | -0.8577 | -0.8897 | -0.8263 | -0.8507 |
| 0.500 | -0.9540 | -1.0886 | -1.1484 | -1.0233 | -1.0333 |
| 0.525 | ******* | -1.2308 | -1.2763 | -1.1332 | -1.1243 |
| 0.550 | -1.3821 | -1.3590 | -1.3936 | -1.2429 | -1.1409 |
| 0.575 | ******* | -1.4762 | -1.4892 | -1.3542 | -0.7278 |
| 0.600 | -1.6535 | -1.5706 | -1.5778 | -1.4483 | -0.6931 |
| 0.625 | ******* | ******* | -1.5413 | -1.4959 | -0.6906 |
| 0.650 | -1.6663 | -1.3853 | -1.3464 | -1.1631 | -0.6649 |
| 0.675 | ******* | -1.3641 | -1.3271 | -1.1415 | -0.6238 |
| 0.700 | -1.6504 | -1.3575 | -1.3236 | -1.1285 | -0.5804 |
| 0.725 | ******* | -1.3623 | ******* | -1.1253 | -0.5437 |
| 0.750 | -1.5586 | -1.3794 | ******* | -1.1389 | -0.5200 |
| 0.775 | ******* | -1.4089 | -1.3450 | -1.1712 | -0.5058 |
| 0.800 | -1.4064 | -1.4108 | -1.3705 | -1.2089 | ******* |
| 0.825 | ******* | -1.3776 | -1.3697 | -1.2161 | -0.5271 |
| 0.850 | -1.3204 | -1.3396 | -1.3244 | -1.1744 | -0.5099 |
| 0.875 | ******* | -1.3158 | -1.2638 | -1.0477 | -0.5098 |
| 0.900 | -1.2773 | -1.3089 | -1.2375 | -0.9706 | ******* |
| 0.925 | ******* | -1.3107 | -1.2208 | -0.9522 | -0.5061 |
| 0.950 | -1.2751 | -1.3066 | -1.2193 | -0.9652 | -0.4340 |
| 0.975 | ******* | -1.3027 | -1.2097 | -0.9586 | -0.4038 |
| 1.000 | -1.2508 | -1.2960 | -1.2094 | -0.9296 | -0.3847 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4929 | 0.4371 | 0.4183 | ******* | -0.5368 |
| -0.400 | 0.4966 | 0.4374 | 0.3933 | 0.1955 | -0.5989 |
| -0.600 | 0.5040 | 0.4416 | 0.3852 | 0.2316 | -0.5760 |
| -0.700 | ******* | 0.4489 | 0.3859 | 0.2434 | -0.5431 |
| -0.800 | ******* | ******* | 0.3797 | 0.2557 | -0.4610 |
| -0.850 | ******* | 0.4132 | 0.3638 | 0.2628 | -0.4321 |
| -0.900 | 0.4317 | 0.3524 | 0.3282 | 0.2487 | -0.3826 |
| -0.950 | 0.3575 | 0.1276 | 0.1942 | 0.1706 | -0.1281 |
| -0.975 | ******* | 0.0125 | 0.0134 | 0.0300 | -0.0799 |
| -1.000 | -1.2717 | -1.3064 | -1.2125 | -0.8763 | -0.4007 |

Surface Pressures




Small Radius L.E.

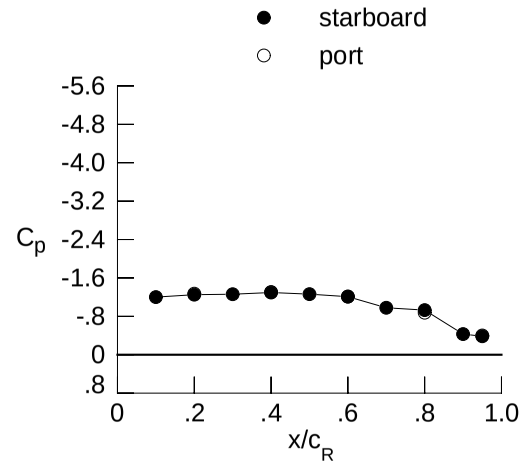
Run No. = 40 , Point No. = 830

$C_N$ = 1.063, $C_m$ = -0.1725

$\alpha$ = 21.6 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

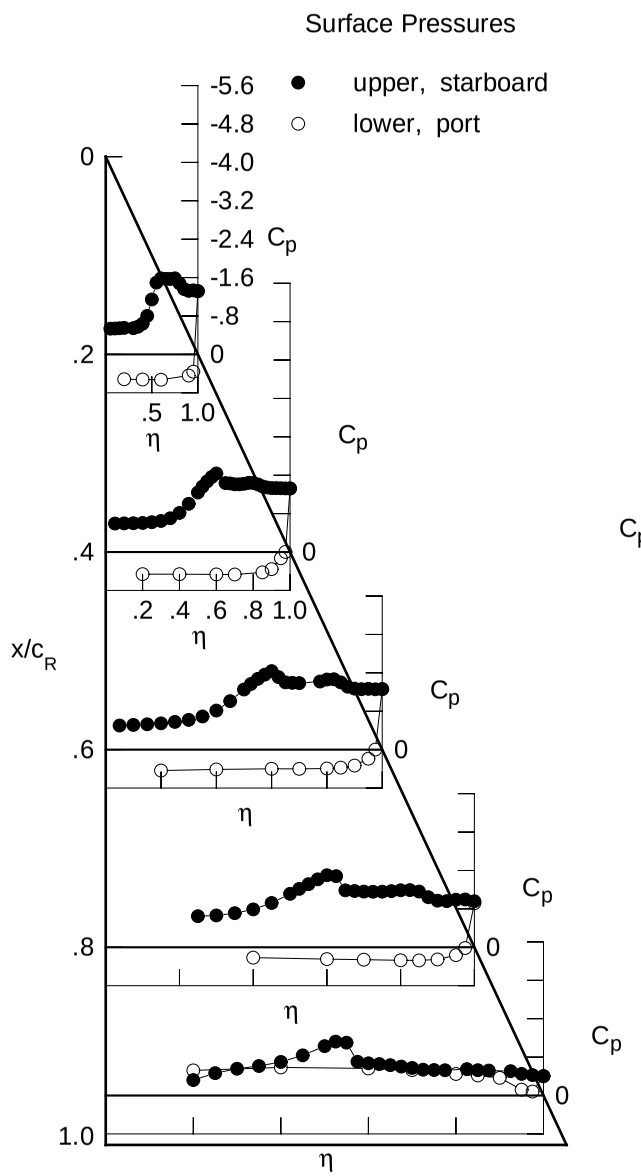
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.2005 | ******* |
| 0.20 | -1.2508 | -1.2717 |
| 0.30 | -1.2607 | ******* |
| 0.40 | -1.2960 | -1.3064 |
| 0.50 | -1.2622 | ******* |
| 0.60 | -1.2094 | -1.2125 |
| 0.70 | -0.9783 | ******* |
| 0.80 | -0.9296 | -0.8763 |
| 0.90 | -0.4301 | ******* |
| 0.95 | -0.3847 | -0.4007 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5361 | -0.5933 | -0.5021 | ******* | ******* |
| 0.100 | -0.5394 | -0.5967 | -0.5148 | ******* | ******* |
| 0.150 | -0.5451 | -0.6001 | -0.5280 | ******* | ******* |
| 0.200 | -0.5529 | -0.6059 | -0.5483 | ******* | -0.3218 |
| 0.250 | ******* | -0.6215 | -0.5786 | -0.6478 | -0.4654 |
| 0.300 | -0.5468 | -0.6471 | -0.6204 | -0.6628 | -0.5577 |
| 0.350 | -0.5771 | -0.7031 | -0.6909 | -0.7107 | -0.6147 |
| 0.400 | -0.6392 | -0.8143 | -0.8147 | -0.7884 | -0.6996 |
| 0.450 | -0.8026 | -1.0045 | -1.0108 | -0.9234 | -0.8367 |
| 0.500 | -1.1439 | -1.2399 | -1.2532 | -1.1135 | -1.0292 |
| 0.525 | ******* | -1.3635 | -1.3673 | -1.2170 | -1.1229 |
| 0.550 | -1.4951 | -1.4714 | -1.4740 | -1.3156 | -1.1008 |
| 0.575 | ******* | -1.5633 | -1.5614 | -1.4154 | -0.7038 |
| 0.600 | -1.5841 | -1.6369 | -1.6358 | -1.5006 | -0.6711 |
| 0.625 | ******* | ******* | -1.5112 | -1.4817 | -0.6549 |
| 0.650 | -1.5739 | -1.4368 | -1.4014 | -1.1861 | -0.6319 |
| 0.675 | ******* | -1.4288 | -1.3919 | -1.1729 | -0.6029 |
| 0.700 | -1.5710 | -1.4108 | -1.3861 | -1.1598 | -0.5741 |
| 0.725 | ******* | -1.4102 | ******* | -1.1565 | -0.5377 |
| 0.750 | -1.5851 | -1.4223 | ******* | -1.1581 | -0.5309 |
| 0.775 | ******* | -1.4417 | -1.4196 | -1.1703 | -0.5261 |
| 0.800 | -1.4796 | -1.4404 | -1.4608 | -1.1881 | ******* |
| 0.825 | ******* | -1.4085 | -1.4660 | -1.1910 | -0.5491 |
| 0.850 | -1.3609 | -1.3681 | -1.4014 | -1.1619 | -0.5268 |
| 0.875 | ******* | -1.3448 | -1.3111 | -1.0433 | -0.5197 |
| 0.900 | -1.3237 | -1.3318 | -1.2711 | -0.9710 | ******* |
| 0.925 | ******* | -1.3324 | -1.2591 | -0.9608 | -0.5076 |
| 0.950 | -1.3347 | -1.3285 | -1.2668 | -0.9909 | -0.4507 |
| 0.975 | ******* | -1.3257 | -1.2564 | -0.9958 | -0.4249 |
| 1.000 | -1.3153 | -1.3244 | -1.2617 | -0.9590 | -0.4066 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5178 | 0.4611 | 0.4353 | ******* | -0.5229 |
| -0.400 | 0.5231 | 0.4618 | 0.4125 | 0.2158 | -0.5850 |
| -0.600 | 0.5278 | 0.4666 | 0.3990 | 0.2466 | -0.5640 |
| -0.700 | ******* | 0.4679 | 0.4008 | 0.2581 | -0.5298 |
| -0.800 | ******* | ******* | 0.3931 | 0.2714 | -0.4486 |
| -0.850 | ******* | 0.4240 | 0.3754 | 0.2734 | -0.4175 |
| -0.900 | 0.4410 | 0.3569 | 0.3320 | 0.2536 | -0.3679 |
| -0.950 | 0.3602 | 0.1299 | 0.1890 | 0.1642 | -0.1214 |
| -0.975 | ******* | -0.0027 | -0.0018 | 0.0151 | -0.0823 |
| -1.000 | -1.3195 | -1.3260 | -1.2610 | -0.9172 | -0.3998 |



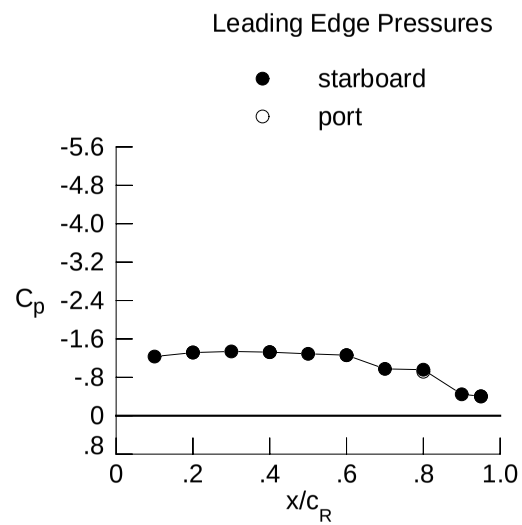

Small Radius L.E.

Run No. = 40 , Point No. = 831

$C_N$ = 1.111, $C_m$ = -0.1771

$\alpha$ = 22.6 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

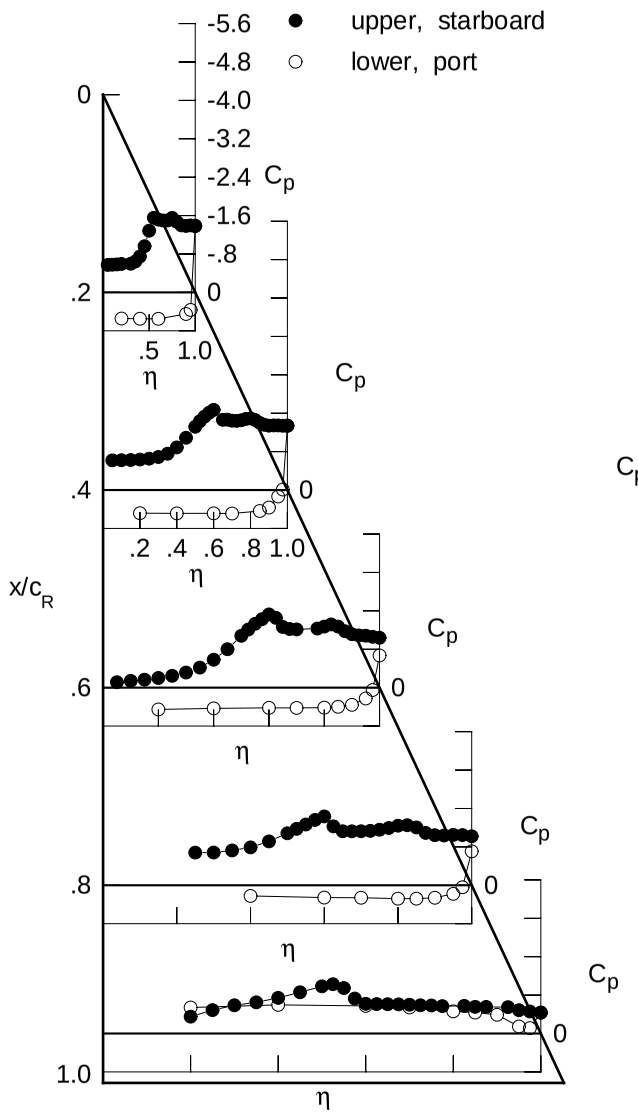



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.2330 | ******* |
| 0.20 | -1.3153 | -1.3195 |
| 0.30 | -1.3394 | ******* |
| 0.40 | -1.3244 | -1.3260 |
| 0.50 | -1.2898 | ******* |
| 0.60 | -1.2617 | -1.2610 |
| 0.70 | -0.9758 | ******* |
| 0.80 | -0.9590 | -0.9172 |
| 0.90 | -0.4466 | ******* |
| 0.95 | -0.4066 | -0.3998 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5722 | -0.6185 | -0.1129 | ******* | ******* |
| 0.100 | -0.5765 | -0.6215 | -0.1416 | ******* | ******* |
| 0.150 | -0.5824 | -0.6259 | -0.1660 | ******* | ******* |
| 0.200 | -0.5931 | -0.6348 | -0.2018 | ******* | -0.3512 |
| 0.250 | ******* | -0.6538 | -0.2467 | -0.6808 | -0.4869 |
| 0.300 | -0.5970 | -0.6881 | -0.3148 | -0.6821 | -0.5878 |
| 0.350 | -0.6439 | -0.7564 | -0.4177 | -0.7254 | -0.6496 |
| 0.400 | -0.7488 | -0.8882 | -0.5813 | -0.7900 | -0.7422 |
| 0.450 | -0.9618 | -1.0884 | -0.7999 | -0.9145 | -0.8588 |
| 0.500 | -1.2860 | -1.3184 | -1.0801 | -1.0834 | -0.9827 |
| 0.525 | ******* | -1.4327 | -1.2097 | -1.1757 | -1.0274 |
| 0.550 | -1.5545 | -1.5279 | -1.3303 | -1.2664 | -0.9474 |
| 0.575 | ******* | -1.6103 | -1.4263 | -1.3617 | -0.7290 |
| 0.600 | -1.5160 | -1.6701 | -1.5257 | -1.4342 | -0.6194 |
| 0.625 | ******* | ******* | -1.4541 | -1.2273 | -0.6127 |
| 0.650 | -1.4981 | -1.4631 | -1.2639 | -1.1254 | -0.6107 |
| 0.675 | ******* | -1.4664 | -1.2210 | -1.1245 | -0.6072 |
| 0.700 | -1.4977 | -1.4450 | -1.2129 | -1.1255 | -0.5999 |
| 0.725 | ******* | -1.4418 | ******* | -1.1347 | -0.5882 |
| 0.750 | -1.5532 | -1.4534 | ******* | -1.1575 | -0.5840 |
| 0.775 | ******* | -1.4821 | -1.2315 | -1.1935 | -0.5700 |
| 0.800 | -1.4705 | -1.4924 | -1.2718 | -1.2413 | ******* |
| 0.825 | ******* | -1.4603 | -1.3165 | -1.2509 | -0.5761 |
| 0.850 | -1.3956 | -1.3992 | -1.2726 | -1.2050 | -0.5556 |
| 0.875 | ******* | -1.3593 | -1.1753 | -1.0908 | -0.5545 |
| 0.900 | -1.3850 | -1.3411 | -1.1124 | -1.0437 | ******* |
| 0.925 | ******* | -1.3462 | -1.0878 | -1.0372 | -0.5486 |
| 0.950 | -1.3955 | -1.3452 | -1.0820 | -1.0501 | -0.4856 |
| 0.975 | ******* | -1.3391 | -1.0595 | -1.0461 | -0.4592 |
| 1.000 | -1.3789 | -1.3371 | -1.0382 | -1.0211 | -0.4372 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5447 | 0.4823 | 0.4542 | ******* | -0.5415 |
| -0.400 | 0.5489 | 0.4862 | 0.4321 | 0.2220 | -0.5965 |
| -0.600 | 0.5508 | 0.4853 | 0.4211 | 0.2560 | -0.5749 |
| -0.700 | ******* | 0.4886 | 0.4222 | 0.2596 | -0.5423 |
| -0.800 | ******* | ******* | 0.4170 | 0.2783 | -0.4612 |
| -0.850 | ******* | 0.4367 | 0.3988 | 0.2781 | -0.4368 |
| -0.900 | 0.4501 | 0.3648 | 0.3587 | 0.2597 | -0.3901 |
| -0.950 | 0.3646 | 0.1342 | 0.2253 | 0.1786 | -0.1460 |
| -0.975 | ******* | -0.0103 | 0.0497 | 0.0410 | -0.1119 |
| -1.000 | -1.3896 | -1.3439 | -0.6705 | -0.7069 | -0.4339 |

Surface Pressures




Small Radius L.E.

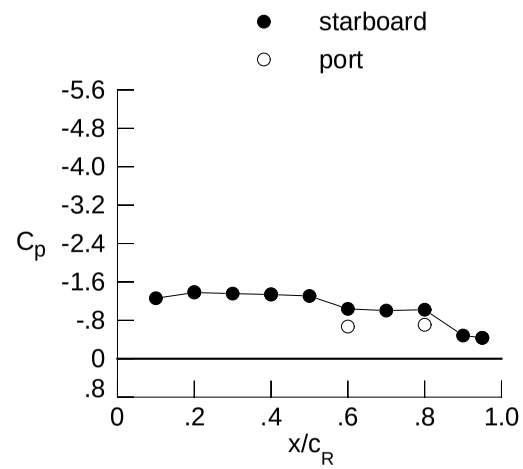
Run No. = 40 , Point No. = 832

$C_N$ = 1.107, $C_m$ = -0.1839

$\alpha$ = 23.6 °, $M_\infty$ = 0.830

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

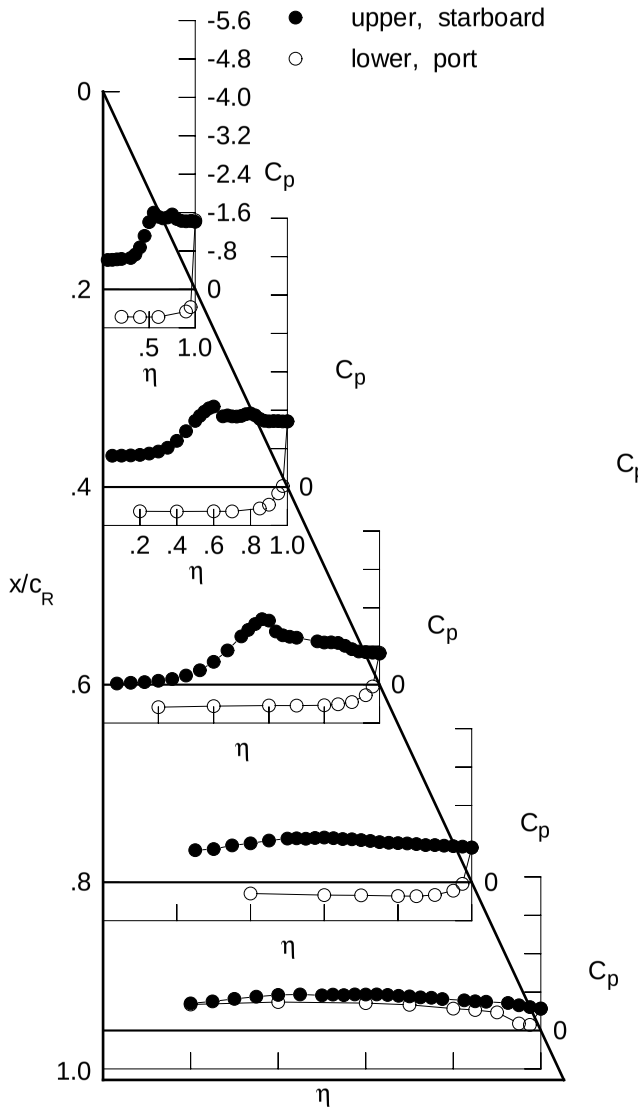



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.2600 | ******* |
| 0.20 | -1.3789 | -1.3896 |
| 0.30 | -1.3570 | ******* |
| 0.40 | -1.3371 | -1.3439 |
| 0.50 | -1.3076 | ******* |
| 0.60 | -1.0382 | -0.6705 |
| 0.70 | -1.0031 | ******* |
| 0.80 | -1.0211 | -0.7069 |
| 0.90 | -0.4832 | ******* |
| 0.95 | -0.4372 | -0.4339 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6130 | -0.6521 | -0.0230 | ******* | ******* |
| 0.100 | -0.6159 | -0.6534 | -0.0383 | ******* | ******* |
| 0.150 | -0.6259 | -0.6586 | -0.0529 | ******* | ******* |
| 0.200 | -0.6341 | -0.6698 | -0.0808 | ******* | -0.5650 |
| 0.250 | ******* | -0.6965 | -0.1174 | -0.6685 | -0.6062 |
| 0.300 | -0.6546 | -0.7393 | -0.1895 | -0.6921 | -0.6591 |
| 0.350 | -0.7263 | -0.8187 | -0.2989 | -0.7677 | -0.7045 |
| 0.400 | -0.8752 | -0.9623 | -0.4752 | -0.8114 | -0.7414 |
| 0.450 | -1.1146 | -1.1635 | -0.7131 | -0.8694 | -0.7516 |
| 0.500 | -1.4018 | -1.3779 | -1.0046 | -0.9103 | -0.7324 |
| 0.525 | ******* | -1.4820 | -1.1398 | -0.9163 | -0.7476 |
| 0.550 | -1.5982 | -1.5697 | -1.2626 | -0.9069 | -0.7366 |
| 0.575 | ******* | -1.6408 | -1.3643 | -0.9233 | -0.7521 |
| 0.600 | -1.5131 | -1.6765 | -1.3338 | -0.9321 | -0.7495 |
| 0.625 | ******* | ******* | -1.1071 | -0.9192 | -0.7524 |
| 0.650 | -1.4791 | -1.4731 | -1.0283 | -0.9012 | -0.7409 |
| 0.675 | ******* | -1.4917 | -0.9975 | -0.8961 | -0.7230 |
| 0.700 | -1.4988 | -1.4720 | -0.9775 | -0.8791 | -0.7110 |
| 0.725 | ******* | -1.4680 | ******* | -0.8610 | -0.6906 |
| 0.750 | -1.5610 | -1.4815 | ******* | -0.8371 | -0.6827 |
| 0.775 | ******* | -1.5175 | -0.9015 | -0.8234 | -0.6551 |
| 0.800 | -1.4667 | -1.5340 | -0.8777 | -0.8164 | ******* |
| 0.825 | ******* | -1.4934 | -0.8807 | -0.8091 | -0.6285 |
| 0.850 | -1.4274 | -1.4211 | -0.8687 | -0.7960 | -0.6090 |
| 0.875 | ******* | -1.3798 | -0.8090 | -0.7756 | -0.5990 |
| 0.900 | -1.4183 | -1.3685 | -0.7393 | -0.7753 | ******* |
| 0.925 | ******* | -1.3744 | -0.6902 | -0.7623 | -0.5734 |
| 0.950 | -1.4255 | -1.3735 | -0.6767 | -0.7531 | -0.5259 |
| 0.975 | ******* | -1.3673 | -0.6658 | -0.7424 | -0.4876 |
| 1.000 | -1.4080 | -1.3694 | -0.6467 | -0.7226 | -0.4596 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5711 | 0.5058 | 0.4697 | ******* | -0.5419 |
| -0.400 | 0.5762 | 0.5093 | 0.4479 | 0.2336 | -0.5930 |
| -0.600 | 0.5749 | 0.5057 | 0.4354 | 0.2670 | -0.5707 |
| -0.700 | ******* | 0.5078 | 0.4368 | 0.2723 | -0.5354 |
| -0.800 | ******* | ******* | 0.4299 | 0.2861 | -0.4563 |
| -0.850 | ******* | 0.4471 | 0.4087 | 0.2892 | -0.4271 |
| -0.900 | 0.4610 | 0.3679 | 0.3630 | 0.2647 | -0.3777 |
| -0.950 | 0.3692 | 0.1310 | 0.2204 | 0.1754 | -0.1453 |
| -0.975 | ******* | -0.0219 | 0.0382 | 0.0327 | -0.1173 |
| -1.000 | -1.4404 | -1.3648 | -0.6652 | -0.7235 | -0.4514 |

Surface Pressures




Small Radius L.E.

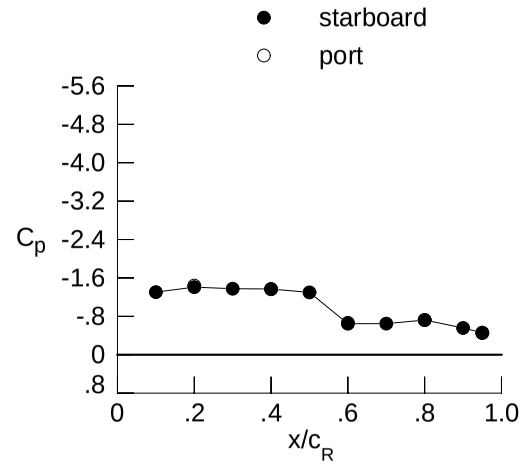
Run No. = 40 , Point No. = 833

$C_N$ = 1.088, $C_m$ = -0.1762

$\alpha$ = 24.6 °, $M_\infty$ = 0.830

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

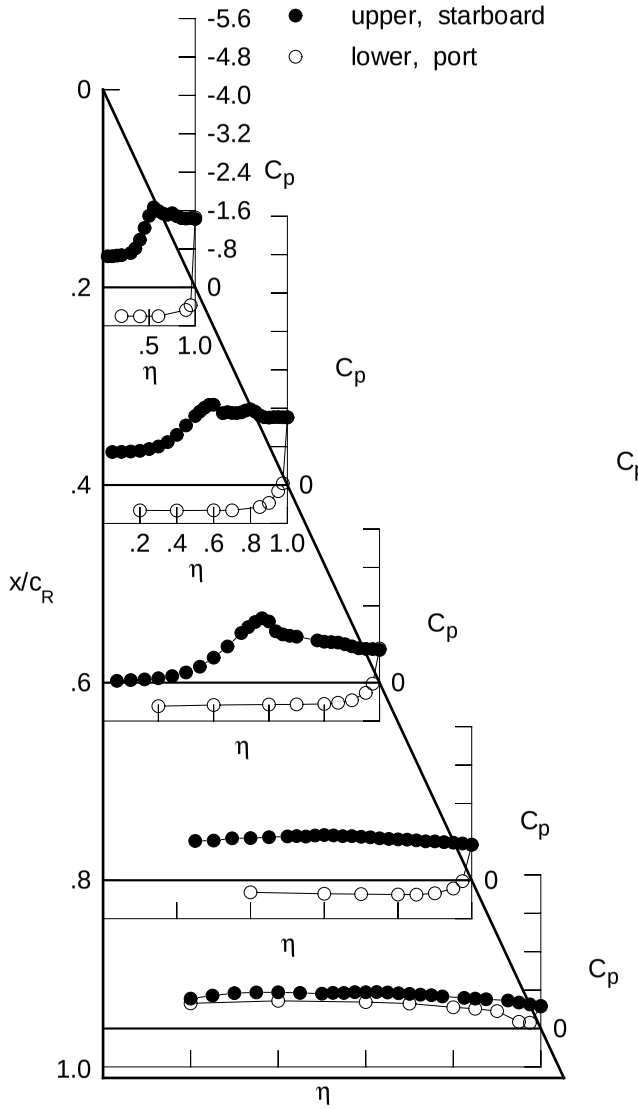



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.3039 | ******* |
| 0.20 | -1.4080 | -1.4404 |
| 0.30 | -1.3754 | ******* |
| 0.40 | -1.3694 | -1.3648 |
| 0.50 | -1.2987 | ******* |
| 0.60 | -0.6467 | -0.6652 |
| 0.70 | -0.6478 | ******* |
| 0.80 | -0.7226 | -0.7235 |
| 0.90 | -0.5575 | ******* |
| 0.95 | -0.4596 | -0.4514 |

# Table D4. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6476 | -0.6882 | -0.0380 | ******* | ******* |
| 0.100 | -0.6497 | -0.6906 | -0.0538 | ******* | ******* |
| 0.150 | -0.6625 | -0.6983 | -0.0670 | ******* | ******* |
| 0.200 | -0.6714 | -0.7131 | -0.0919 | ******* | -0.6234 |
| 0.250 | ******* | -0.7492 | -0.1361 | -0.8194 | -0.6861 |
| 0.300 | -0.7148 | -0.8021 | -0.2121 | -0.8271 | -0.7368 |
| 0.350 | -0.8117 | -0.8941 | -0.3323 | -0.8741 | -0.7524 |
| 0.400 | -0.9928 | -1.0459 | -0.5211 | -0.8789 | -0.7542 |
| 0.450 | -1.2388 | -1.2414 | -0.7538 | -0.8971 | -0.7414 |
| 0.500 | -1.4918 | -1.4382 | -1.0329 | -0.9137 | -0.7259 |
| 0.525 | ******* | -1.5295 | -1.1559 | -0.9207 | -0.7421 |
| 0.550 | -1.6674 | -1.6080 | -1.2626 | -0.9114 | -0.7410 |
| 0.575 | ******* | -1.6707 | -1.3419 | -0.9328 | -0.7565 |
| 0.600 | -1.5921 | -1.6727 | -1.2738 | -0.9434 | -0.7560 |
| 0.625 | ******* | ******* | -1.0685 | -0.9345 | -0.7599 |
| 0.650 | -1.5395 | -1.4968 | -1.0038 | -0.9193 | -0.7506 |
| 0.675 | ******* | -1.5184 | -0.9760 | -0.9201 | -0.7342 |
| 0.700 | -1.5125 | -1.5013 | -0.9576 | -0.9064 | -0.7219 |
| 0.725 | ******* | -1.4992 | ******* | -0.8952 | -0.7051 |
| 0.750 | -1.5451 | -1.5139 | ******* | -0.8745 | -0.6933 |
| 0.775 | ******* | -1.5532 | -0.8795 | -0.8618 | -0.6678 |
| 0.800 | -1.4834 | -1.5764 | -0.8529 | -0.8517 | ******* |
| 0.825 | ******* | -1.5284 | -0.8439 | -0.8468 | -0.6384 |
| 0.850 | -1.4441 | -1.4522 | -0.8349 | -0.8320 | -0.6229 |
| 0.875 | ******* | -1.4120 | -0.8003 | -0.8112 | -0.6092 |
| 0.900 | -1.4339 | -1.4037 | -0.7561 | -0.8107 | ******* |
| 0.925 | ******* | -1.4138 | -0.7154 | -0.7945 | -0.5840 |
| 0.950 | -1.4424 | -1.4161 | -0.7045 | -0.7833 | -0.5409 |
| 0.975 | ******* | -1.4122 | -0.6991 | -0.7663 | -0.5025 |
| 1.000 | -1.4237 | -1.4146 | -0.6818 | -0.7429 | -0.4710 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5979 | 0.5282 | 0.4902 | ******* | -0.5241 |
| -0.400 | 0.6020 | 0.5315 | 0.4665 | 0.2512 | -0.5767 |
| -0.600 | 0.5984 | 0.5269 | 0.4559 | 0.2808 | -0.5501 |
| -0.700 | ******* | 0.5281 | 0.4537 | 0.2882 | -0.5199 |
| -0.800 | ******* | ******* | 0.4442 | 0.2966 | -0.4413 |
| -0.850 | ******* | 0.4579 | 0.4188 | 0.2993 | -0.4120 |
| -0.900 | 0.4703 | 0.3727 | 0.3674 | 0.2715 | -0.3624 |
| -0.950 | 0.3720 | 0.1273 | 0.2129 | 0.1721 | -0.1390 |
| -0.975 | ******* | -0.0361 | 0.0216 | 0.0178 | -0.1199 |
| -1.000 | -1.4558 | -1.4063 | -0.7119 | -0.7392 | -0.4590 |

Surface Pressures




Small Radius L.E.

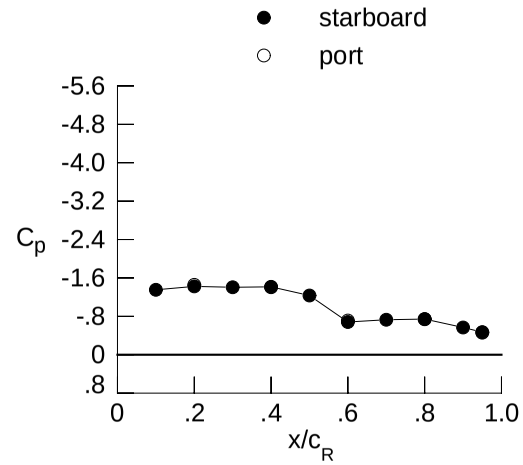
Run No. = 40 , Point No. = 834

$C_N$ = 1.138, $C_m$ = -0.1822

$\alpha$ = 25.6 °, $M_\infty$ = 0.829

$R_{mac}$ = $6.0 \times 10^6$

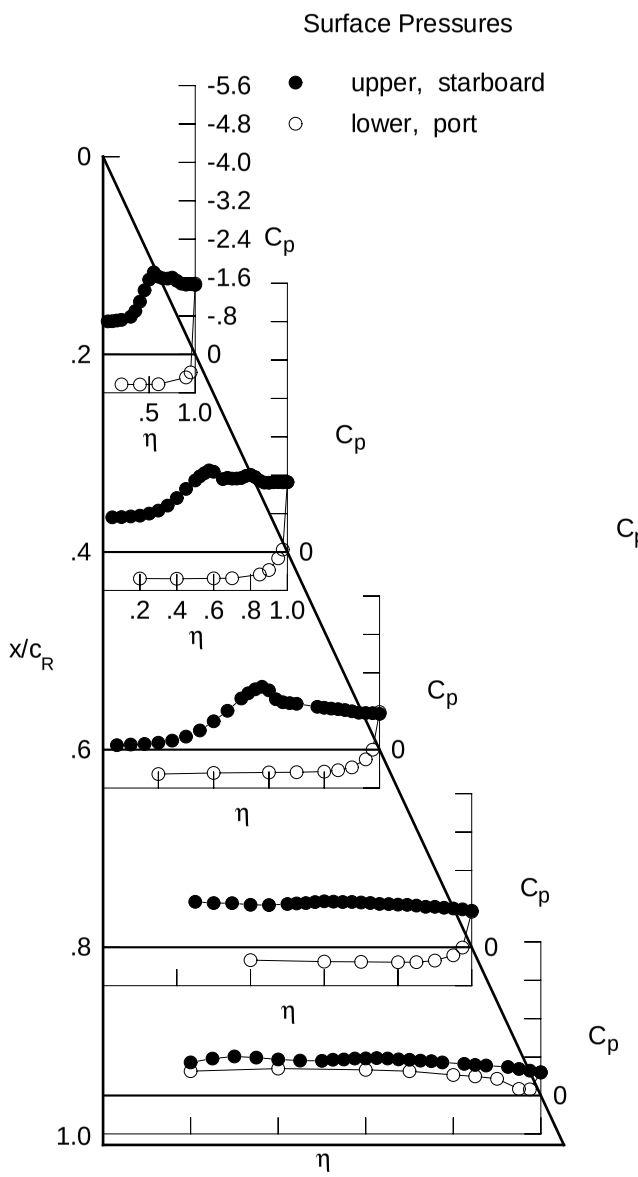
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.3527 | ******* |
| 0.20 | -1.4237 | -1.4558 |
| 0.30 | -1.4054 | ******* |
| 0.40 | -1.4146 | -1.4063 |
| 0.50 | -1.2338 | ******* |
| 0.60 | -0.6818 | -0.7119 |
| 0.70 | -0.7290 | ******* |
| 0.80 | -0.7429 | -0.7392 |
| 0.90 | -0.5676 | ******* |
| 0.95 | -0.4710 | -0.4590 |

# Table D4. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6884 | -0.7236 | -0.0924 | ******* | ******* |
| 0.100 | -0.6909 | -0.7278 | -0.1065 | ******* | ******* |
| 0.150 | -0.7055 | -0.7413 | -0.1180 | ******* | ******* |
| 0.200 | -0.7191 | -0.7577 | -0.1441 | ******* | -0.6895 |
| 0.250 | ******* | -0.8008 | -0.1880 | -0.9471 | -0.7699 |
| 0.300 | -0.7841 | -0.8634 | -0.2711 | -0.9205 | -0.8133 |
| 0.350 | -0.9028 | -0.9672 | -0.3994 | -0.9189 | -0.7894 |
| 0.400 | -1.0995 | -1.1247 | -0.5907 | -0.8851 | -0.7512 |
| 0.450 | -1.3361 | -1.3150 | -0.8096 | -0.8791 | -0.7269 |
| 0.500 | -1.5580 | -1.4909 | -1.0658 | -0.9016 | -0.7221 |
| 0.525 | ******* | -1.5768 | -1.1744 | -0.9130 | -0.7453 |
| 0.550 | -1.7092 | -1.6419 | -1.2570 | -0.9208 | -0.7500 |
| 0.575 | ******* | -1.7007 | -1.3099 | -0.9420 | -0.7707 |
| 0.600 | -1.6182 | -1.6721 | -1.2340 | -0.9575 | -0.7730 |
| 0.625 | ******* | ******* | -1.0502 | -0.9503 | -0.7798 |
| 0.650 | -1.5843 | -1.5194 | -0.9870 | -0.9434 | -0.7715 |
| 0.675 | ******* | -1.5457 | -0.9690 | -0.9443 | -0.7530 |
| 0.700 | -1.5784 | -1.5296 | -0.9551 | -0.9324 | -0.7450 |
| 0.725 | ******* | -1.5309 | ******* | -0.9220 | -0.7265 |
| 0.750 | -1.5996 | -1.5425 | ******* | -0.9034 | -0.7156 |
| 0.775 | ******* | -1.5853 | -0.8932 | -0.8997 | -0.6888 |
| 0.800 | -1.5337 | -1.6086 | -0.8716 | -0.8892 | ******* |
| 0.825 | ******* | -1.5611 | -0.8552 | -0.8838 | -0.6595 |
| 0.850 | -1.4732 | -1.4854 | -0.8433 | -0.8692 | -0.6367 |
| 0.875 | ******* | -1.4467 | -0.8246 | -0.8428 | -0.6245 |
| 0.900 | -1.4533 | -1.4432 | -0.7995 | -0.8431 | ******* |
| 0.925 | ******* | -1.4548 | -0.7687 | -0.8243 | -0.5943 |
| 0.950 | -1.4626 | -1.4549 | -0.7620 | -0.8087 | -0.5530 |
| 0.975 | ******* | -1.4527 | -0.7597 | -0.7907 | -0.5175 |
| 1.000 | -1.4481 | -1.4582 | -0.7444 | -0.7607 | -0.4846 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.6253 | 0.5519 | 0.5089 | ******* | -0.5071 |
| -0.400 | 0.6282 | 0.5570 | 0.4859 | 0.2681 | -0.5610 |
| -0.600 | 0.6226 | 0.5489 | 0.4753 | 0.2988 | -0.5344 |
| -0.700 | ******* | 0.5462 | 0.4707 | 0.3038 | -0.5061 |
| -0.800 | ******* | ******* | 0.4582 | 0.3113 | -0.4274 |
| -0.850 | ******* | 0.4681 | 0.4285 | 0.3102 | -0.3992 |
| -0.900 | 0.4796 | 0.3753 | 0.3693 | 0.2769 | -0.3483 |
| -0.950 | 0.3749 | 0.1311 | 0.2026 | 0.1673 | -0.1367 |
| -0.975 | ******* | -0.0509 | 0.0010 | 0.0059 | -0.1276 |
| -1.000 | -1.4739 | -1.4533 | -0.7835 | -0.7398 | -0.4777 |



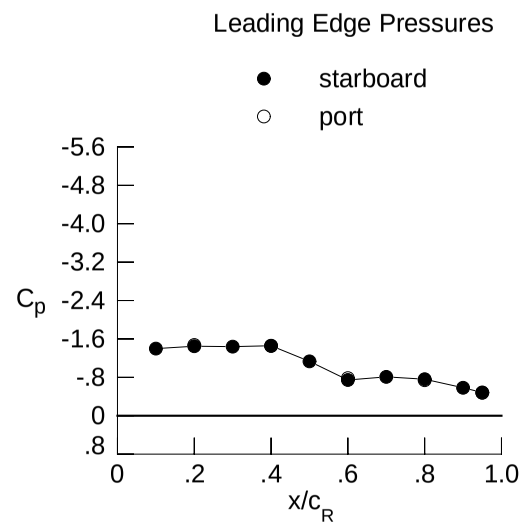

Small Radius L.E.

Run No. = 40 , Point No. = 835

$C_N$ = 1.183, $C_m$ = -0.1870

$\alpha$ = 26.7 °, $M_\infty$ = 0.829

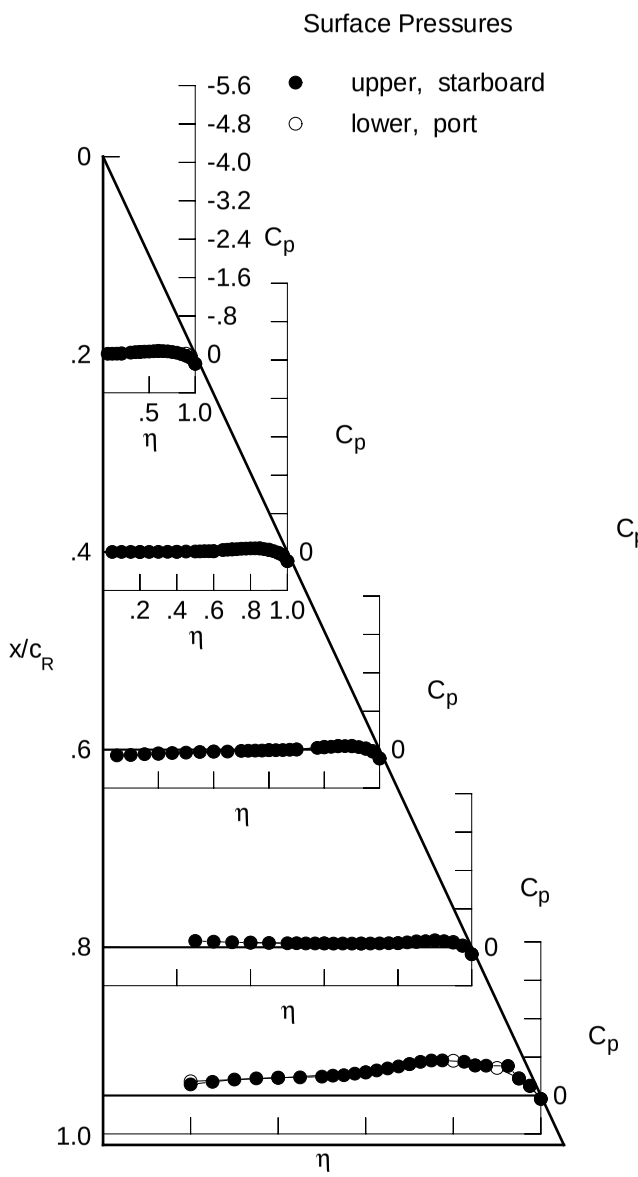
$R_{mac}$ = $6.0 \times 10^6$




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.3981 | ******* |
| 0.20 | -1.4481 | -1.4739 |
| 0.30 | -1.4394 | ******* |
| 0.40 | -1.4582 | -1.4533 |
| 0.50 | -1.1327 | ******* |
| 0.60 | -0.7444 | -0.7835 |
| 0.70 | -0.8100 | ******* |
| 0.80 | -0.7607 | -0.7398 |
| 0.90 | -0.5827 | ******* |
| 0.95 | -0.4846 | -0.4777 |

# Table D4. Concluded.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0130 | -0.0020 | 0.1200 | ******* | ******* |
| 0.100 | -0.0135 | -0.0023 | 0.1119 | ******* | ******* |
| 0.150 | -0.0151 | -0.0021 | 0.0946 | ******* | ******* |
| 0.200 | -0.0154 | -0.0004 | 0.0870 | ******* | -0.2311 |
| 0.250 | ******* | -0.0022 | 0.0705 | -0.1321 | -0.2847 |
| 0.300 | -0.0365 | -0.0030 | 0.0625 | -0.1168 | -0.3324 |
| 0.350 | -0.0467 | -0.0051 | 0.0486 | -0.1046 | -0.3567 |
| 0.400 | -0.0495 | -0.0050 | 0.0416 | -0.0963 | -0.3735 |
| 0.450 | -0.0569 | -0.0104 | 0.0404 | -0.0901 | -0.3777 |
| 0.500 | -0.0596 | -0.0113 | 0.0261 | -0.0837 | -0.3932 |
| 0.525 | ******* | -0.0136 | 0.0234 | -0.0848 | -0.4138 |
| 0.550 | -0.0658 | -0.0174 | 0.0201 | -0.0796 | -0.4235 |
| 0.575 | ******* | -0.0178 | 0.0195 | -0.0801 | -0.4551 |
| 0.600 | -0.0689 | -0.0192 | 0.0122 | -0.0815 | -0.4853 |
| 0.625 | ******* | ******* | 0.0108 | -0.0769 | -0.5224 |
| 0.650 | -0.0683 | -0.0417 | 0.0092 | -0.0786 | -0.5639 |
| 0.675 | ******* | -0.0489 | 0.0025 | -0.0769 | -0.6054 |
| 0.700 | -0.0632 | -0.0547 | -0.0032 | -0.0777 | -0.6554 |
| 0.725 | ******* | -0.0591 | ******* | -0.0784 | -0.7009 |
| 0.750 | -0.0496 | -0.0692 | ******* | -0.0811 | -0.7300 |
| 0.775 | ******* | -0.0714 | -0.0370 | -0.0847 | -0.7313 |
| 0.800 | -0.0340 | -0.0759 | -0.0466 | -0.0854 | ******* |
| 0.825 | ******* | -0.0766 | -0.0594 | -0.1026 | -0.7033 |
| 0.850 | -0.0055 | -0.0739 | -0.0699 | -0.1121 | -0.6287 |
| 0.875 | ******* | -0.0597 | -0.0734 | -0.1269 | -0.6216 |
| 0.900 | 0.0294 | -0.0395 | -0.0699 | -0.1372 | ******* |
| 0.925 | ******* | -0.0186 | -0.0537 | -0.1276 | -0.6160 |
| 0.950 | 0.0742 | 0.0178 | -0.0170 | -0.0965 | -0.3503 |
| 0.975 | ******* | 0.0620 | 0.0416 | -0.0306 | -0.1967 |
| 1.000 | 0.1954 | 0.1893 | 0.1866 | 0.1434 | 0.0698 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0218 | -0.0009 | 0.0768 | ******* | -0.2959 |
| -0.400 | -0.0530 | -0.0050 | 0.0383 | -0.0969 | -0.3656 |
| -0.600 | -0.0742 | -0.0143 | 0.0086 | -0.0804 | -0.4784 |
| -0.700 | ******* | -0.0579 | -0.0041 | -0.0777 | -0.6530 |
| -0.800 | ******* | ******* | -0.0595 | -0.0868 | -0.7241 |
| -0.850 | ******* | -0.0789 | -0.0792 | -0.1242 | -0.6251 |
| -0.900 | -0.0146 | -0.0508 | -0.0802 | -0.1467 | -0.5741 |
| -0.950 | 0.0203 | 0.0134 | -0.0281 | -0.1112 | -0.3610 |
| -0.975 | ******* | 0.0621 | 0.0265 | -0.0386 | -0.2062 |
| -1.000 | 0.1957 | 0.1872 | 0.1799 | 0.1458 | 0.0722 |



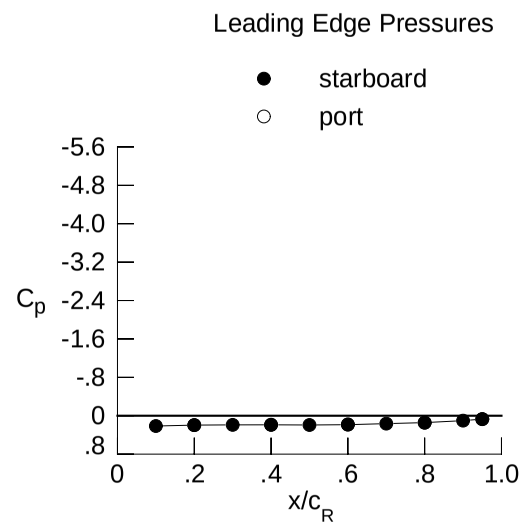

Small Radius L.E.

Run No. = 40 , Point No. = 836

$C_N$ = -0.011, $C_m$ = 0.0032

$\alpha$ = 0.1 °, $M_\infty$ = 0.829

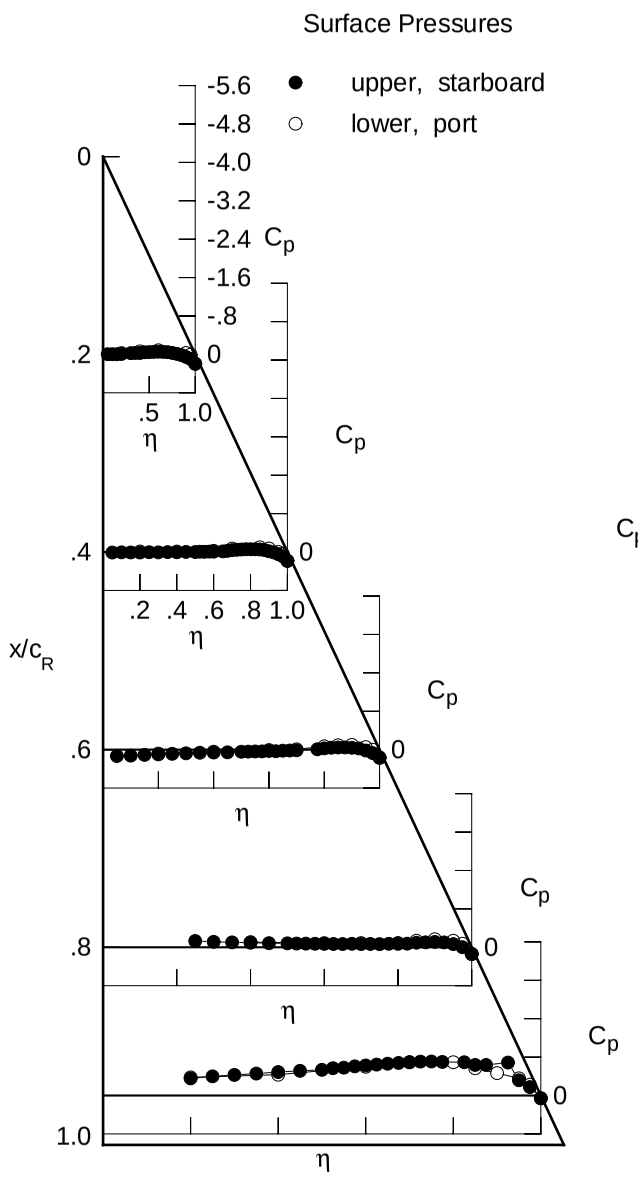
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2145 | ******* |
| 0.20 | 0.1954 | 0.1957 |
| 0.30 | 0.1905 | ******* |
| 0.40 | 0.1893 | 0.1872 |
| 0.50 | 0.1929 | ******* |
| 0.60 | 0.1866 | 0.1799 |
| 0.70 | 0.1646 | ******* |
| 0.80 | 0.1434 | 0.1458 |
| 0.90 | 0.1025 | ******* |
| 0.95 | 0.0698 | 0.0722 |

# Table D5. Tabulations and Plots of Surface Pressure Coefficients.

| | $x/c_R$ .2 | $x/c_R$ .4 | $x/c_R$ .6 | $x/c_R$ .8 | $x/c_R$ .95 |
|---|---|---|---|---|---|
| η | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ | $C_{p,u}$ |
| 0.050 | -0.0038 | 0.0101 | 0.1335 | ******* | ******* |
| 0.100 | -0.0041 | 0.0062 | 0.1247 | ******* | ******* |
| 0.150 | -0.0032 | 0.0089 | 0.1099 | ******* | ******* |
| 0.200 | -0.0084 | 0.0097 | 0.0982 | ******* | -0.3567 |
| 0.250 | ******* | 0.0043 | 0.0876 | -0.1312 | -0.3991 |
| 0.300 | -0.0253 | 0.0072 | 0.0764 | -0.1139 | -0.4289 |
| 0.350 | -0.0306 | 0.0016 | 0.0648 | -0.1021 | -0.4565 |
| 0.400 | -0.0298 | 0.0050 | 0.0597 | -0.0951 | -0.4886 |
| 0.450 | -0.0437 | -0.0022 | 0.0559 | -0.0854 | -0.5146 |
| 0.500 | -0.0475 | -0.0002 | 0.0439 | -0.0823 | -0.5349 |
| 0.525 | ******* | -0.0060 | 0.0420 | -0.0779 | -0.5684 |
| 0.550 | -0.0518 | -0.0051 | 0.0374 | -0.0763 | -0.5798 |
| 0.575 | ******* | -0.0092 | 0.0367 | -0.0733 | -0.6076 |
| 0.600 | -0.0556 | -0.0080 | 0.0276 | -0.0717 | -0.6253 |
| 0.625 | ******* | ******* | 0.0324 | -0.0685 | -0.6443 |
| 0.650 | -0.0521 | -0.0140 | 0.0215 | -0.0684 | -0.6623 |
| 0.675 | ******* | -0.0250 | 0.0186 | -0.0731 | -0.6787 |
| 0.700 | -0.0466 | -0.0396 | 0.0138 | -0.0671 | -0.6945 |
| 0.725 | ******* | -0.0472 | ******* | -0.0697 | -0.7054 |
| 0.750 | -0.0305 | -0.0524 | ******* | -0.0654 | -0.7085 |
| 0.775 | ******* | -0.0587 | -0.0068 | -0.0728 | -0.6991 |
| 0.800 | -0.0109 | -0.0578 | -0.0264 | -0.0724 | ******* |
| 0.825 | ******* | -0.0572 | -0.0403 | -0.0749 | -0.6930 |
| 0.850 | 0.0143 | -0.0534 | -0.0448 | -0.0952 | -0.6372 |
| 0.875 | ******* | -0.0415 | -0.0459 | -0.1028 | -0.6363 |
| 0.900 | 0.0535 | -0.0162 | -0.0391 | -0.1116 | ******* |
| 0.925 | ******* | 0.0076 | -0.0253 | -0.1019 | -0.6863 |
| 0.950 | 0.0962 | 0.0438 | 0.0184 | -0.0666 | -0.3173 |
| 0.975 | ******* | 0.0884 | 0.0723 | -0.0018 | -0.1761 |
| 1.000 | 0.1988 | 0.1873 | 0.1721 | 0.1441 | 0.0555 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0266 | -0.0114 | 0.0828 | ******* | -0.3774 |
| -0.400 | -0.0625 | -0.0106 | 0.0429 | -0.1075 | -0.4338 |
| -0.600 | -0.0856 | -0.0258 | 0.0077 | -0.0866 | -0.5990 |
| -0.700 | ******* | -0.0724 | -0.0067 | -0.0882 | -0.6923 |
| -0.800 | ******* | ******* | -0.0690 | -0.0892 | -0.6931 |
| -0.850 | ******* | -0.0982 | -0.0909 | -0.1365 | -0.5680 |
| -0.900 | -0.0300 | -0.0742 | -0.0985 | -0.1681 | -0.4674 |
| -0.950 | 0.0036 | -0.0026 | -0.0528 | -0.1369 | -0.3578 |
| -0.975 | ******* | 0.0359 | 0.0009 | -0.0733 | -0.2267 |
| -1.000 | 0.1911 | 0.1777 | 0.1605 | 0.1337 | 0.0597 |



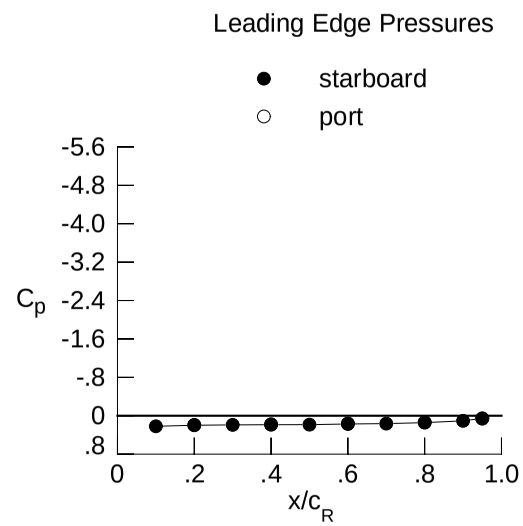

Small Radius L.E.

Run No. = 42 , Point No. = 866

$C_N$ = -0.029, $C_m$ = 0.0061

$\alpha$ = -0.4 °, $M_\infty$ = 0.870

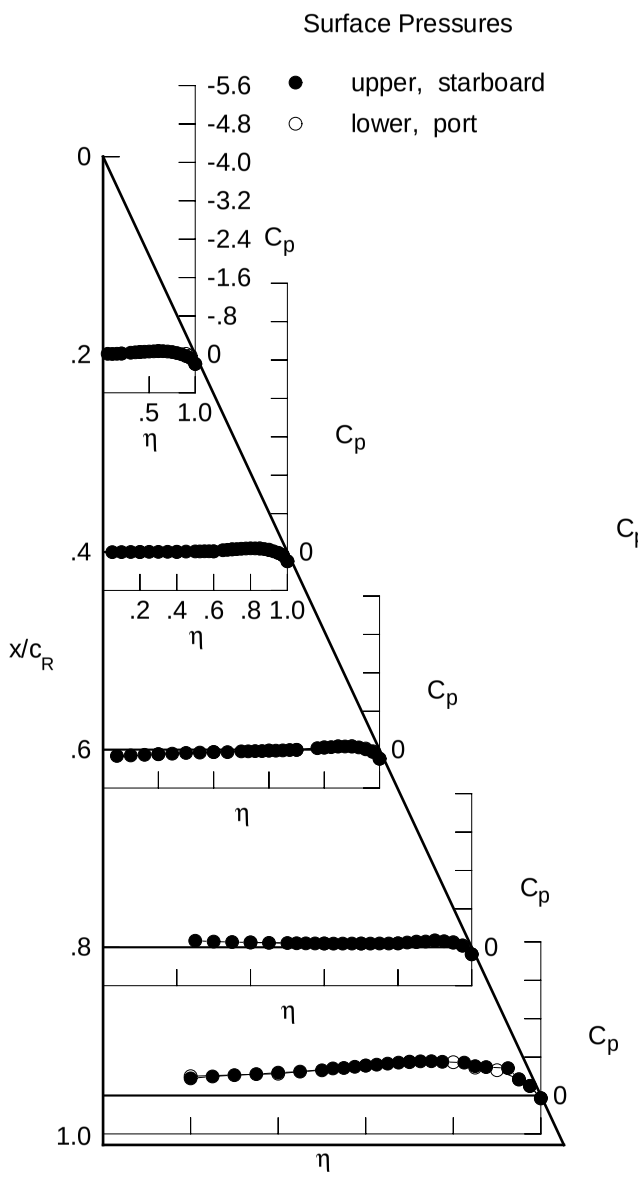
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2199 | ******* |
| 0.20 | 0.1988 | 0.1911 |
| 0.30 | 0.1906 | ******* |
| 0.40 | 0.1873 | 0.1777 |
| 0.50 | 0.1860 | ******* |
| 0.60 | 0.1721 | 0.1605 |
| 0.70 | 0.1642 | ******* |
| 0.80 | 0.1441 | 0.1337 |
| 0.90 | 0.1062 | ******* |
| 0.95 | 0.0555 | 0.0597 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0121 | 0.0021 | 0.1310 | ******* | ******* |
| 0.100 | -0.0089 | 0.0013 | 0.1211 | ******* | ******* |
| 0.150 | -0.0126 | -0.0007 | 0.1079 | ******* | ******* |
| 0.200 | -0.0167 | 0.0018 | 0.0962 | ******* | -0.3565 |
| 0.250 | ******* | -0.0037 | 0.0836 | -0.1362 | -0.3972 |
| 0.300 | -0.0345 | -0.0030 | 0.0690 | -0.1183 | -0.4244 |
| 0.350 | -0.0429 | -0.0050 | 0.0613 | -0.1095 | -0.4457 |
| 0.400 | -0.0486 | -0.0060 | 0.0518 | -0.0995 | -0.4761 |
| 0.450 | -0.0547 | -0.0094 | 0.0521 | -0.0920 | -0.4974 |
| 0.500 | -0.0592 | -0.0127 | 0.0364 | -0.0890 | -0.5250 |
| 0.525 | ******* | -0.0129 | 0.0356 | -0.0839 | -0.5637 |
| 0.550 | -0.0642 | -0.0161 | 0.0303 | -0.0817 | -0.5737 |
| 0.575 | ******* | -0.0161 | 0.0295 | -0.0797 | -0.5984 |
| 0.600 | -0.0673 | -0.0144 | 0.0214 | -0.0794 | -0.6220 |
| 0.625 | ******* | ******* | 0.0216 | -0.0764 | -0.6424 |
| 0.650 | -0.0669 | -0.0377 | 0.0158 | -0.0772 | -0.6638 |
| 0.675 | ******* | -0.0459 | 0.0077 | -0.0776 | -0.6849 |
| 0.700 | -0.0600 | -0.0550 | 0.0053 | -0.0766 | -0.7057 |
| 0.725 | ******* | -0.0611 | ******* | -0.0766 | -0.7119 |
| 0.750 | -0.0491 | -0.0681 | ******* | -0.0791 | -0.7148 |
| 0.775 | ******* | -0.0739 | -0.0305 | -0.0786 | -0.7020 |
| 0.800 | -0.0281 | -0.0773 | -0.0394 | -0.0802 | ******* |
| 0.825 | ******* | -0.0757 | -0.0518 | -0.0989 | -0.6846 |
| 0.850 | -0.0029 | -0.0705 | -0.0629 | -0.1091 | -0.6114 |
| 0.875 | ******* | -0.0614 | -0.0657 | -0.1201 | -0.5918 |
| 0.900 | 0.0351 | -0.0401 | -0.0626 | -0.1353 | ******* |
| 0.925 | ******* | -0.0149 | -0.0468 | -0.1265 | -0.5702 |
| 0.950 | 0.0780 | 0.0195 | -0.0073 | -0.0942 | -0.3315 |
| 0.975 | ******* | 0.0660 | 0.0473 | -0.0320 | -0.1958 |
| 1.000 | 0.1996 | 0.1918 | 0.1903 | 0.1447 | 0.0519 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0181 | -0.0028 | 0.0929 | ******* | -0.4021 |
| -0.400 | -0.0507 | 0.0001 | 0.0489 | -0.1022 | -0.4537 |
| -0.600 | -0.0723 | -0.0132 | 0.0174 | -0.0781 | -0.6257 |
| -0.700 | ******* | -0.0566 | 0.0032 | -0.0783 | -0.6943 |
| -0.800 | ******* | ******* | -0.0507 | -0.0837 | -0.6935 |
| -0.850 | ******* | -0.0773 | -0.0715 | -0.1181 | -0.5809 |
| -0.900 | -0.0106 | -0.0493 | -0.0737 | -0.1446 | -0.5274 |
| -0.950 | 0.0234 | 0.0162 | -0.0228 | -0.1062 | -0.3410 |
| -0.975 | ******* | 0.0647 | 0.0331 | -0.0402 | -0.2027 |
| -1.000 | 0.1992 | 0.1921 | 0.1873 | 0.1474 | 0.0613 |



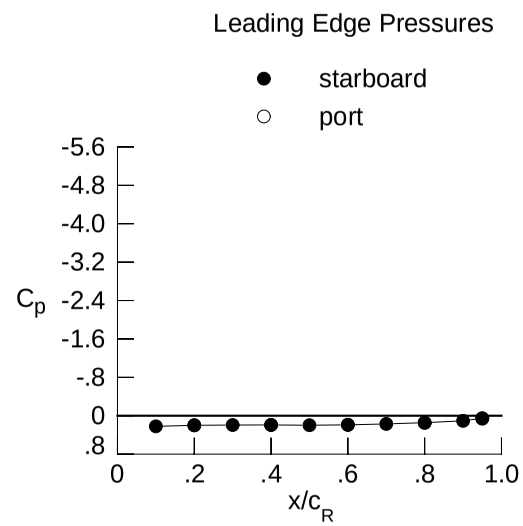

Small Radius L.E.

Run No. = 42 , Point No. = 867

$C_N$ = -0.014, $C_m$ = 0.0061

$\alpha$ = 0.1 °, $M_\infty$ = 0.871

$R_{mac}$ = $6.0 \times 10^6$

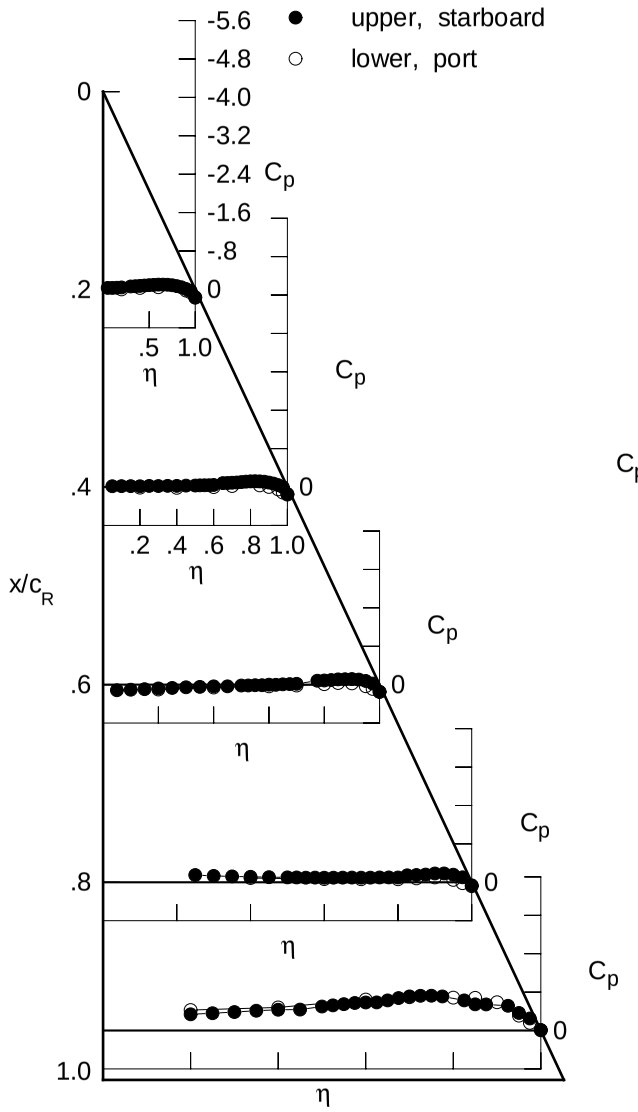



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2211 | ******* |
| 0.20 | 0.1996 | 0.1992 |
| 0.30 | 0.1937 | ******* |
| 0.40 | 0.1918 | 0.1921 |
| 0.50 | 0.1978 | ******* |
| 0.60 | 0.1903 | 0.1873 |
| 0.70 | 0.1706 | ******* |
| 0.80 | 0.1447 | 0.1474 |
| 0.90 | 0.1062 | ******* |
| 0.95 | 0.0519 | 0.0613 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0312 | -0.0166 | 0.1164 | ******* | ******* |
| 0.100 | -0.0305 | -0.0187 | 0.1054 | ******* | ******* |
| 0.150 | -0.0344 | -0.0181 | 0.0941 | ******* | ******* |
| 0.200 | -0.0405 | -0.0163 | 0.0791 | ******* | -0.3378 |
| 0.250 | ******* | -0.0230 | 0.0690 | -0.1508 | -0.3598 |
| 0.300 | -0.0604 | -0.0207 | 0.0549 | -0.1324 | -0.3847 |
| 0.350 | -0.0668 | -0.0251 | 0.0460 | -0.1222 | -0.4120 |
| 0.400 | -0.0730 | -0.0239 | 0.0360 | -0.1141 | -0.4324 |
| 0.450 | -0.0805 | -0.0295 | 0.0354 | -0.1061 | -0.4358 |
| 0.500 | -0.0878 | -0.0314 | 0.0187 | -0.1025 | -0.4999 |
| 0.525 | ******* | -0.0351 | 0.0178 | -0.1011 | -0.5244 |
| 0.550 | -0.0936 | -0.0368 | 0.0119 | -0.0957 | -0.5491 |
| 0.575 | ******* | -0.0378 | 0.0117 | -0.0972 | -0.5732 |
| 0.600 | -0.0989 | -0.0432 | 0.0010 | -0.0948 | -0.5837 |
| 0.625 | ******* | ******* | 0.0034 | -0.0963 | -0.5858 |
| 0.650 | -0.0994 | -0.0813 | -0.0065 | -0.0971 | -0.6271 |
| 0.675 | ******* | -0.0838 | -0.0110 | -0.0985 | -0.6758 |
| 0.700 | -0.0966 | -0.0895 | -0.0176 | -0.0958 | -0.7106 |
| 0.725 | ******* | -0.0947 | ******* | -0.0972 | -0.7233 |
| 0.750 | -0.0861 | -0.1035 | ******* | -0.1006 | -0.7245 |
| 0.775 | ******* | -0.1131 | -0.0812 | -0.1015 | -0.7098 |
| 0.800 | -0.0683 | -0.1191 | -0.0868 | -0.0999 | ******* |
| 0.825 | ******* | -0.1217 | -0.0960 | -0.1453 | -0.6275 |
| 0.850 | -0.0448 | -0.1187 | -0.1094 | -0.1520 | -0.5458 |
| 0.875 | ******* | -0.1112 | -0.1128 | -0.1609 | -0.5435 |
| 0.900 | -0.0087 | -0.0928 | -0.1171 | -0.1831 | ******* |
| 0.925 | ******* | -0.0722 | -0.1053 | -0.1840 | -0.5149 |
| 0.950 | 0.0298 | -0.0401 | -0.0764 | -0.1586 | -0.3655 |
| 0.975 | ******* | -0.0003 | -0.0234 | -0.1036 | -0.2504 |
| 1.000 | 0.1634 | 0.1448 | 0.1481 | 0.0632 | -0.0107 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0003 | 0.0126 | 0.1016 | ******* | -0.4261 |
| -0.400 | -0.0307 | 0.0164 | 0.0600 | -0.0890 | -0.4808 |
| -0.600 | -0.0449 | 0.0012 | 0.0354 | -0.0663 | -0.6450 |
| -0.700 | ******* | -0.0204 | 0.0186 | -0.0632 | -0.6936 |
| -0.800 | ******* | ******* | -0.0092 | -0.0636 | -0.6847 |
| -0.850 | ******* | -0.0348 | -0.0334 | -0.0816 | -0.6810 |
| -0.900 | 0.0251 | -0.0014 | -0.0261 | -0.1007 | -0.5887 |
| -0.950 | 0.0613 | 0.0491 | 0.0327 | -0.0496 | -0.3099 |
| -0.975 | ******* | 0.1140 | 0.0894 | 0.0185 | -0.1590 |
| -1.000 | 0.1736 | 0.1578 | 0.1519 | 0.0816 | -0.0047 |

Surface Pressures




Small Radius L.E.

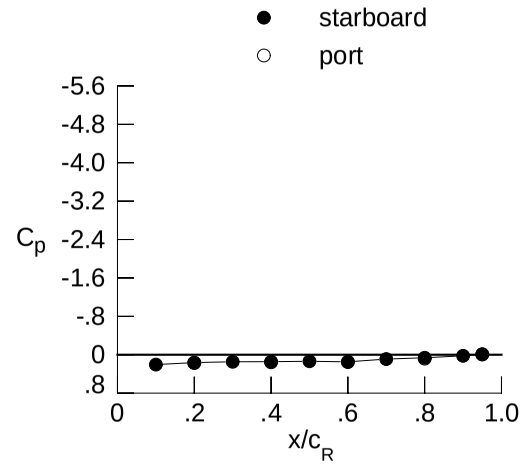
Run No. = 42 , Point No. = 868

$C_N$ = 0.030, $C_m$ = -0.0028

$\alpha$ = 1.1 °, $M_\infty$ = 0.870

$R_{mac}$ = $6.0 \times 10^6$

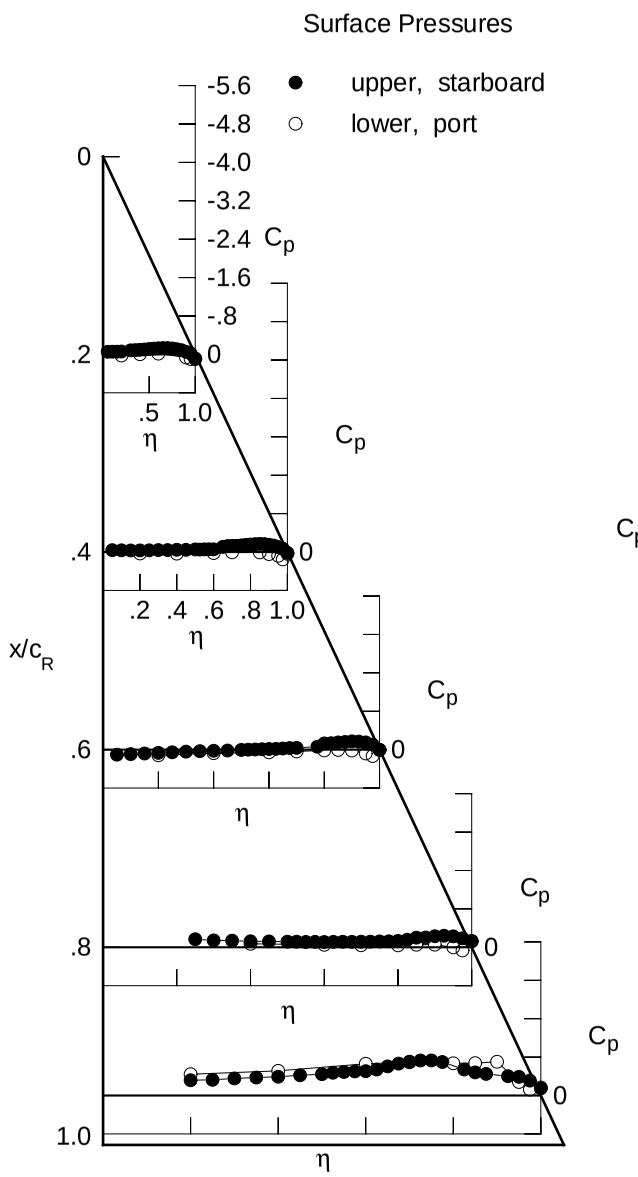
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2054 | ******* |
| 0.20 | 0.1634 | 0.1736 |
| 0.30 | 0.1467 | ******* |
| 0.40 | 0.1448 | 0.1578 |
| 0.50 | 0.1364 | ******* |
| 0.60 | 0.1481 | 0.1519 |
| 0.70 | 0.0905 | ******* |
| 0.80 | 0.0632 | 0.0816 |
| 0.90 | 0.0223 | ******* |
| 0.95 | -0.0107 | -0.0047 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0533 | -0.0389 | 0.1044 | ******* | ******* |
| 0.100 | -0.0562 | -0.0361 | 0.0936 | ******* | ******* |
| 0.150 | -0.0572 | -0.0331 | 0.0811 | ******* | ******* |
| 0.200 | -0.0603 | -0.0335 | 0.0670 | ******* | -0.3184 |
| 0.250 | ******* | -0.0362 | 0.0552 | -0.1670 | -0.3274 |
| 0.300 | -0.0845 | -0.0410 | 0.0412 | -0.1429 | -0.3559 |
| 0.350 | -0.0890 | -0.0406 | 0.0317 | -0.1382 | -0.3747 |
| 0.400 | -0.0953 | -0.0471 | 0.0230 | -0.1252 | -0.3908 |
| 0.450 | -0.1016 | -0.0464 | 0.0186 | -0.1222 | -0.4215 |
| 0.500 | -0.1118 | -0.0542 | 0.0054 | -0.1170 | -0.4448 |
| 0.525 | ******* | -0.0515 | 0.0007 | -0.1168 | -0.4742 |
| 0.550 | -0.1200 | -0.0558 | -0.0027 | -0.1110 | -0.4901 |
| 0.575 | ******* | -0.0579 | -0.0080 | -0.1136 | -0.5020 |
| 0.600 | -0.1272 | -0.0563 | -0.0136 | -0.1093 | -0.5075 |
| 0.625 | ******* | ******* | -0.0161 | -0.1132 | -0.5411 |
| 0.650 | -0.1310 | -0.1090 | -0.0230 | -0.1151 | -0.6062 |
| 0.675 | ******* | -0.1241 | -0.0328 | -0.1139 | -0.6638 |
| 0.700 | -0.1312 | -0.1293 | -0.0379 | -0.1165 | -0.7046 |
| 0.725 | ******* | -0.1298 | ******* | -0.1172 | -0.7300 |
| 0.750 | -0.1234 | -0.1390 | ******* | -0.1226 | -0.7307 |
| 0.775 | ******* | -0.1496 | -0.0607 | -0.1250 | -0.6979 |
| 0.800 | -0.1070 | -0.1568 | -0.1296 | -0.1322 | ******* |
| 0.825 | ******* | -0.1642 | -0.1334 | -0.1577 | -0.5427 |
| 0.850 | -0.0881 | -0.1690 | -0.1500 | -0.2008 | -0.4820 |
| 0.875 | ******* | -0.1655 | -0.1597 | -0.2038 | -0.4502 |
| 0.900 | -0.0547 | -0.1519 | -0.1725 | -0.2303 | ******* |
| 0.925 | ******* | -0.1348 | -0.1683 | -0.2406 | -0.4025 |
| 0.950 | -0.0195 | -0.1043 | -0.1503 | -0.2280 | -0.3890 |
| 0.975 | ******* | -0.0701 | -0.1045 | -0.1877 | -0.3102 |
| 1.000 | 0.0851 | 0.0150 | 0.0018 | -0.1332 | -0.1493 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0232 | 0.0300 | 0.1176 | ******* | -0.4432 |
| -0.400 | -0.0038 | 0.0328 | 0.0735 | -0.0730 | -0.5138 |
| -0.600 | -0.0161 | 0.0219 | 0.0561 | -0.0517 | -0.6610 |
| -0.700 | ******* | 0.0054 | 0.0372 | -0.0425 | -0.6930 |
| -0.800 | ******* | ******* | 0.0167 | -0.0409 | -0.6713 |
| -0.850 | ******* | 0.0072 | 0.0061 | -0.0533 | -0.6742 |
| -0.900 | 0.0622 | 0.0424 | 0.0186 | -0.0550 | -0.7029 |
| -0.950 | 0.0969 | 0.0787 | 0.0794 | 0.0011 | -0.2820 |
| -0.975 | ******* | 0.1539 | 0.1326 | 0.0649 | -0.1236 |
| -1.000 | 0.0973 | 0.0370 | 0.0068 | -0.1213 | -0.1664 |



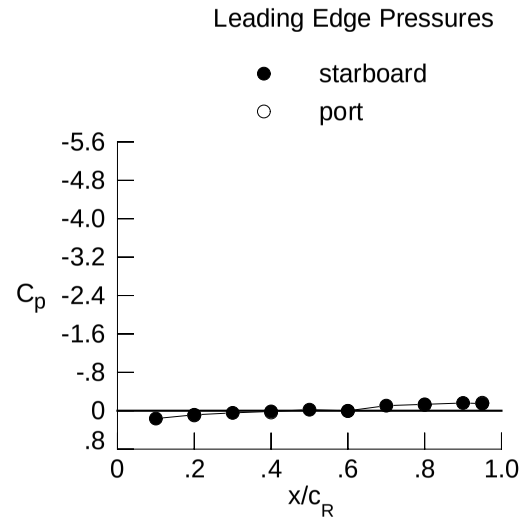

Small Radius L.E.

Run No. = 42 , Point No. = 869

$C_N$ = 0.071, $C_m$ = -0.0099

$\alpha$ = 2.2 °, $M_\infty$ = 0.870

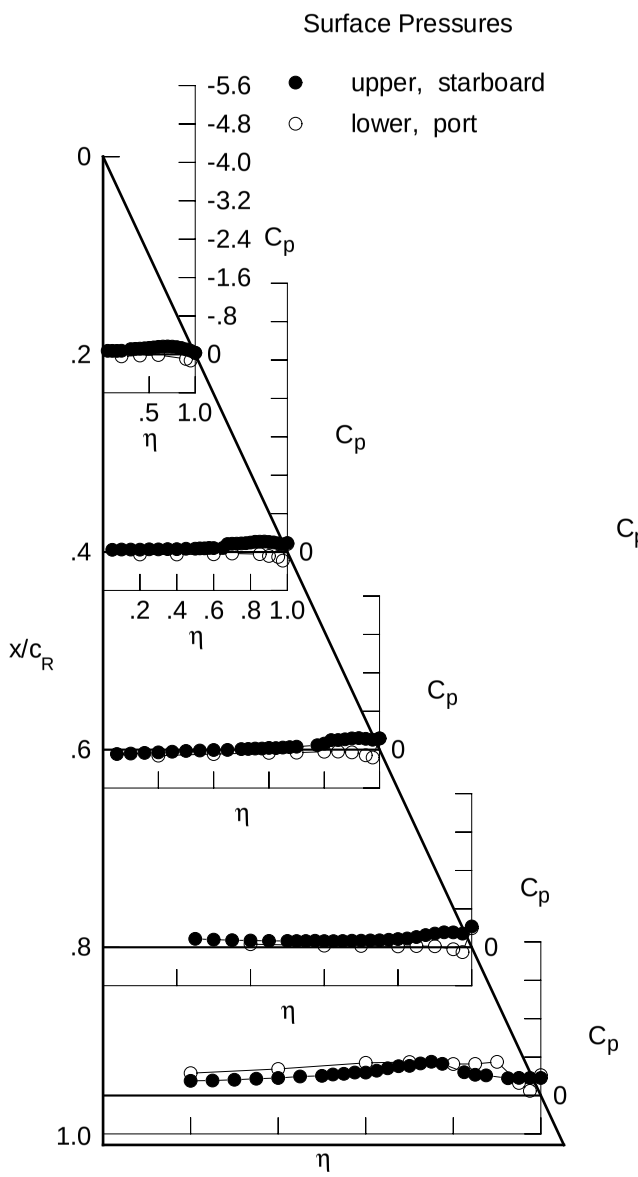
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.1633 | ******* |
| 0.20 | 0.0851 | 0.0973 |
| 0.30 | 0.0449 | ******* |
| 0.40 | 0.0150 | 0.0370 |
| 0.50 | -0.0214 | ******* |
| 0.60 | 0.0018 | 0.0068 |
| 0.70 | -0.1058 | ******* |
| 0.80 | -0.1332 | -0.1213 |
| 0.90 | -0.1613 | ******* |
| 0.95 | -0.1493 | -0.1664 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0746 | -0.0463 | 0.0910 | ******* | ******* |
| 0.100 | -0.0733 | -0.0523 | 0.0819 | ******* | ******* |
| 0.150 | -0.0732 | -0.0510 | 0.0676 | ******* | ******* |
| 0.200 | -0.0761 | -0.0494 | 0.0571 | ******* | -0.3058 |
| 0.250 | ******* | -0.0570 | 0.0431 | -0.1759 | -0.3120 |
| 0.300 | -0.1093 | -0.0551 | 0.0275 | -0.1591 | -0.3278 |
| 0.350 | -0.1150 | -0.0611 | 0.0185 | -0.1480 | -0.3493 |
| 0.400 | -0.1197 | -0.0603 | 0.0074 | -0.1411 | -0.3650 |
| 0.450 | -0.1269 | -0.0684 | 0.0053 | -0.1331 | -0.3960 |
| 0.500 | -0.1358 | -0.0693 | -0.0113 | -0.1319 | -0.4100 |
| 0.525 | ******* | -0.0758 | -0.0141 | -0.1293 | -0.4379 |
| 0.550 | -0.1457 | -0.0768 | -0.0220 | -0.1306 | -0.4521 |
| 0.575 | ******* | -0.0857 | -0.0225 | -0.1360 | -0.4784 |
| 0.600 | -0.1566 | -0.0823 | -0.0362 | -0.1287 | -0.4776 |
| 0.625 | ******* | ******* | -0.0322 | -0.1282 | -0.5166 |
| 0.650 | -0.1631 | -0.0862 | -0.0434 | -0.1304 | -0.5671 |
| 0.675 | ******* | -0.1661 | -0.0522 | -0.1365 | -0.6104 |
| 0.700 | -0.1659 | -0.1730 | -0.0618 | -0.1375 | -0.6176 |
| 0.725 | ******* | -0.1748 | ******* | -0.1430 | -0.6676 |
| 0.750 | -0.1619 | -0.1790 | ******* | -0.1458 | -0.7031 |
| 0.775 | ******* | -0.1850 | -0.0916 | -0.1568 | -0.6597 |
| 0.800 | -0.1511 | -0.1967 | -0.1259 | -0.1709 | ******* |
| 0.825 | ******* | -0.2133 | -0.1988 | -0.1841 | -0.4852 |
| 0.850 | -0.1325 | -0.2163 | -0.2002 | -0.2137 | -0.4321 |
| 0.875 | ******* | -0.2182 | -0.2149 | -0.2546 | -0.4193 |
| 0.900 | -0.1049 | -0.2096 | -0.2347 | -0.2856 | ******* |
| 0.925 | ******* | -0.2004 | -0.2408 | -0.3122 | -0.3598 |
| 0.950 | -0.0766 | -0.1815 | -0.2258 | -0.3102 | -0.3675 |
| 0.975 | ******* | -0.1596 | -0.2064 | -0.2850 | -0.3661 |
| 1.000 | -0.0345 | -0.1879 | -0.2349 | -0.4338 | -0.3654 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0408 | 0.0506 | 0.1251 | ******* | -0.4653 |
| -0.400 | 0.0233 | 0.0504 | 0.0918 | -0.0644 | -0.5531 |
| -0.600 | 0.0129 | 0.0465 | 0.0670 | -0.0344 | -0.6805 |
| -0.700 | ******* | 0.0307 | 0.0625 | -0.0283 | -0.6966 |
| -0.800 | ******* | ******* | 0.0432 | -0.0189 | -0.6558 |
| -0.850 | ******* | 0.0435 | 0.0397 | -0.0256 | -0.6574 |
| -0.900 | 0.0940 | 0.0814 | 0.0572 | -0.0214 | -0.7007 |
| -0.950 | 0.1280 | 0.1016 | 0.1178 | 0.0406 | -0.2617 |
| -0.975 | ******* | 0.1789 | 0.1640 | 0.1009 | -0.0970 |
| -1.000 | -0.0299 | -0.1670 | -0.2320 | -0.3966 | -0.4241 |



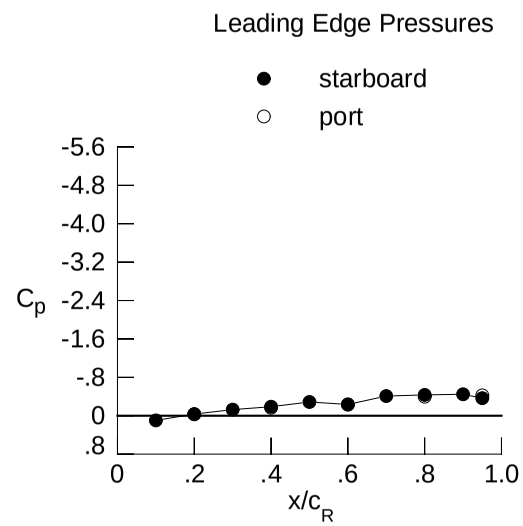

Small Radius L.E.

Run No. = 42 , Point No. = 870

$C_N$ = 0.117, $C_m$ = -0.0200

$\alpha$ = 3.2 °, $M_\infty$ = 0.870

$R_{mac}$ = $6.0 \times 10^6$

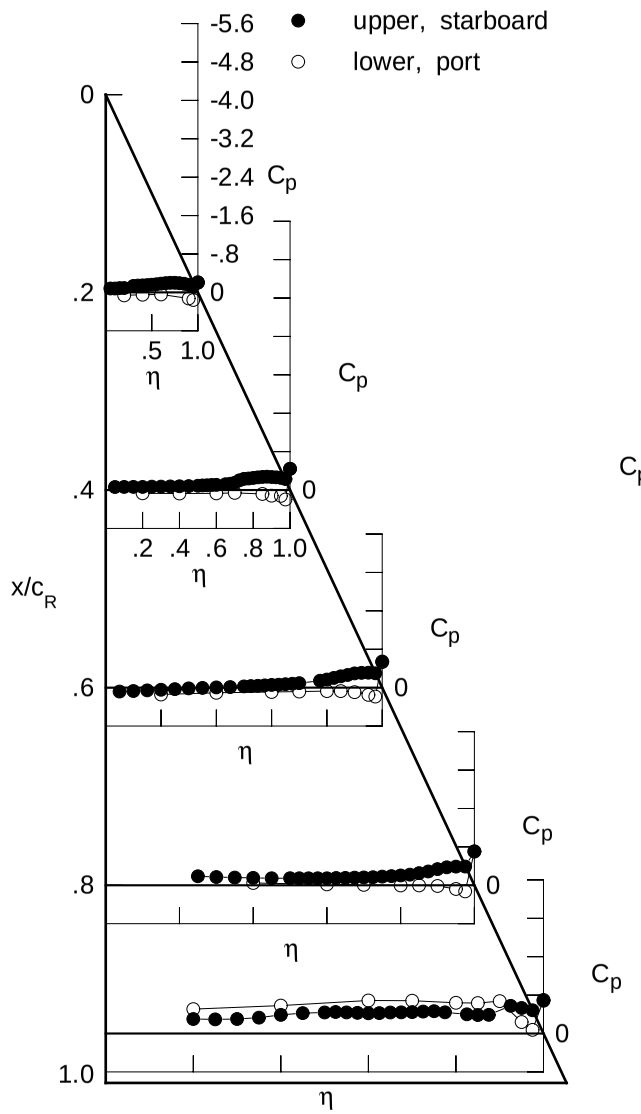



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.0979 | ******* |
| 0.20 | -0.0345 | -0.0299 |
| 0.30 | -0.1273 | ******* |
| 0.40 | -0.1879 | -0.1670 |
| 0.50 | -0.2863 | ******* |
| 0.60 | -0.2349 | -0.2320 |
| 0.70 | -0.4097 | ******* |
| 0.80 | -0.4338 | -0.3966 |
| 0.90 | -0.4474 | ******* |
| 0.95 | -0.3654 | -0.4241 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0813 | -0.0634 | 0.0819 | ******* | ******* |
| 0.100 | -0.0811 | -0.0644 | 0.0707 | ******* | ******* |
| 0.150 | -0.0897 | -0.0653 | 0.0571 | ******* | ******* |
| 0.200 | -0.0901 | -0.0644 | 0.0438 | ******* | -0.3016 |
| 0.250 | ******* | -0.0705 | 0.0310 | -0.1882 | -0.2941 |
| 0.300 | -0.1348 | -0.0715 | 0.0156 | -0.1720 | -0.3022 |
| 0.350 | -0.1421 | -0.0754 | 0.0053 | -0.1611 | -0.3301 |
| 0.400 | -0.1462 | -0.0780 | -0.0049 | -0.1545 | -0.3884 |
| 0.450 | -0.1519 | -0.0826 | -0.0118 | -0.1466 | -0.4244 |
| 0.500 | -0.1604 | -0.0894 | -0.0257 | -0.1471 | -0.4383 |
| 0.525 | ******* | -0.0963 | -0.0331 | -0.1466 | -0.4479 |
| 0.550 | -0.1697 | -0.0990 | -0.0384 | -0.1460 | -0.4391 |
| 0.575 | ******* | -0.1056 | -0.0468 | -0.1467 | -0.4304 |
| 0.600 | -0.1825 | -0.1080 | -0.0564 | -0.1454 | -0.4214 |
| 0.625 | ******* | ******* | -0.0608 | -0.1517 | -0.4248 |
| 0.650 | -0.1925 | -0.1206 | -0.0715 | -0.1537 | -0.4372 |
| 0.675 | ******* | -0.1304 | -0.0811 | -0.1592 | -0.4410 |
| 0.700 | -0.2003 | -0.1512 | -0.0933 | -0.1633 | -0.4467 |
| 0.725 | ******* | -0.2027 | ******* | -0.1683 | -0.4572 |
| 0.750 | -0.2002 | -0.2326 | ******* | -0.1807 | -0.4646 |
| 0.775 | ******* | -0.2399 | -0.1439 | -0.1914 | -0.4413 |
| 0.800 | -0.1921 | -0.2518 | -0.1688 | -0.2052 | ******* |
| 0.825 | ******* | -0.2643 | -0.2024 | -0.2220 | -0.3997 |
| 0.850 | -0.1800 | -0.2729 | -0.2357 | -0.2538 | -0.3848 |
| 0.875 | ******* | -0.2776 | -0.2640 | -0.2877 | -0.3885 |
| 0.900 | -0.1582 | -0.2708 | -0.2967 | -0.3370 | ******* |
| 0.925 | ******* | -0.2645 | -0.3082 | -0.3743 | -0.5767 |
| 0.950 | -0.1406 | -0.2533 | -0.3110 | -0.3888 | -0.5320 |
| 0.975 | ******* | -0.2290 | -0.2993 | -0.3904 | -0.4841 |
| 1.000 | -0.2008 | -0.4432 | -0.5442 | -0.7077 | -0.6825 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0621 | 0.0683 | 0.1430 | ******* | -0.5084 |
| -0.400 | 0.0478 | 0.0724 | 0.1072 | -0.0479 | -0.5817 |
| -0.600 | 0.0422 | 0.0694 | 0.0904 | -0.0189 | -0.6878 |
| -0.700 | ******* | 0.0596 | 0.0818 | -0.0089 | -0.6835 |
| -0.800 | ******* | ******* | 0.0719 | 0.0031 | -0.6399 |
| -0.850 | ******* | 0.0814 | 0.0723 | 0.0023 | -0.6346 |
| -0.900 | 0.1267 | 0.1177 | 0.0944 | 0.0142 | -0.6742 |
| -0.950 | 0.1584 | 0.1215 | 0.1508 | 0.0770 | -0.2388 |
| -0.975 | ******* | 0.1971 | 0.1853 | 0.1268 | -0.0761 |
| -1.000 | -0.2120 | -0.4405 | -0.5330 | -0.7016 | -0.6998 |

Surface Pressures




Small Radius L.E.

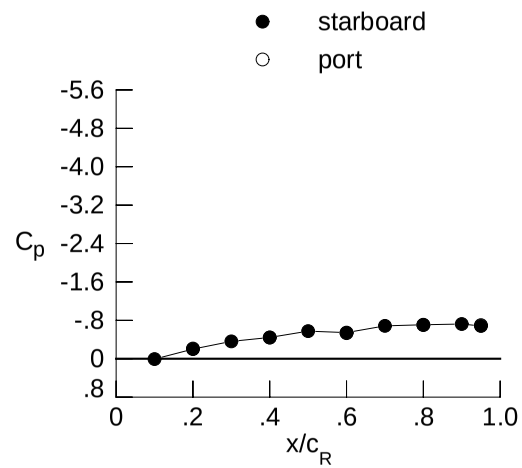
Run No. = 42 , Point No. = 871

$C_N$ = 0.160, $C_m$ = -0.0284

$\alpha$ = 4.2 °, $M_\infty$ = 0.870

$R_{mac}$ = $6.0 \times 10^6$

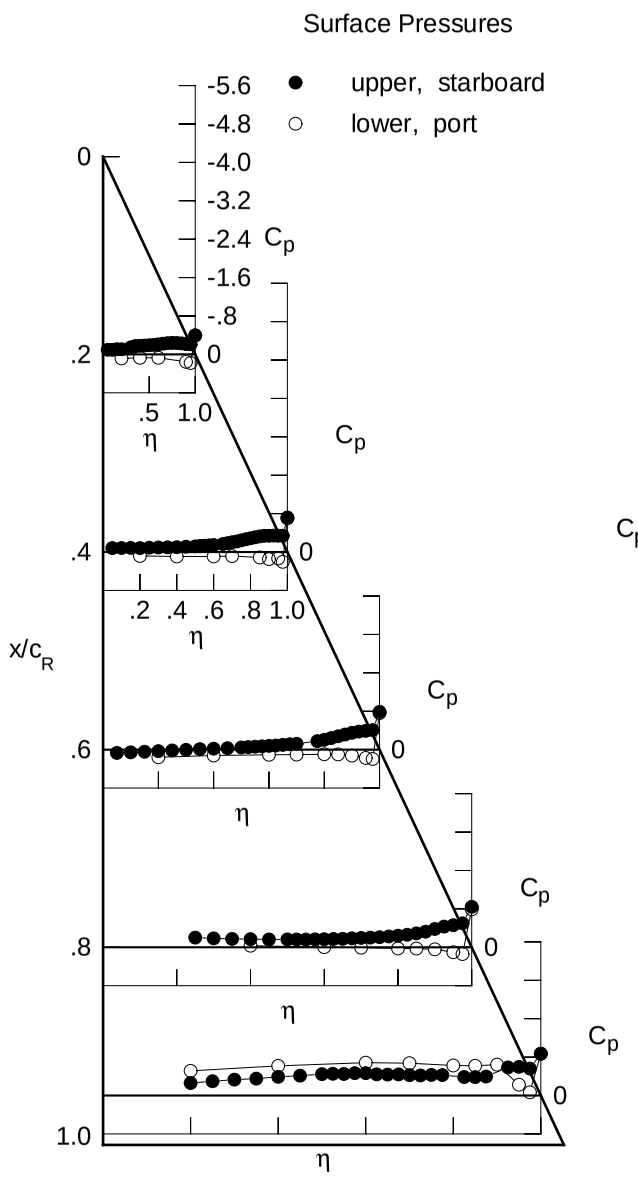
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.0074 | ******* |
| 0.20 | -0.2008 | -0.2120 |
| 0.30 | -0.3616 | ******* |
| 0.40 | -0.4432 | -0.4405 |
| 0.50 | -0.5749 | ******* |
| 0.60 | -0.5442 | -0.5330 |
| 0.70 | -0.6845 | ******* |
| 0.80 | -0.7077 | -0.7016 |
| 0.90 | -0.7231 | ******* |
| 0.95 | -0.6825 | -0.6998 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0959 | -0.0823 | 0.0691 | ******* | ******* |
| 0.100 | -0.0955 | -0.0841 | 0.0571 | ******* | ******* |
| 0.150 | -0.1078 | -0.0863 | 0.0437 | ******* | ******* |
| 0.200 | -0.1065 | -0.0824 | 0.0313 | ******* | -0.2603 |
| 0.250 | ******* | -0.0906 | 0.0169 | -0.2018 | -0.2969 |
| 0.300 | -0.1464 | -0.0952 | 0.0043 | -0.1859 | -0.3302 |
| 0.350 | -0.1747 | -0.0982 | -0.0111 | -0.1746 | -0.3521 |
| 0.400 | -0.1788 | -0.1008 | -0.0203 | -0.1694 | -0.3892 |
| 0.450 | -0.1845 | -0.1108 | -0.0299 | -0.1636 | -0.4135 |
| 0.500 | -0.1906 | -0.1178 | -0.0455 | -0.1637 | -0.4451 |
| 0.525 | ******* | -0.1263 | -0.0535 | -0.1621 | -0.4527 |
| 0.550 | -0.1987 | -0.1320 | -0.0616 | -0.1606 | -0.4484 |
| 0.575 | ******* | -0.1392 | -0.0690 | -0.1657 | -0.4659 |
| 0.600 | -0.2093 | -0.1464 | -0.0787 | -0.1672 | -0.4652 |
| 0.625 | ******* | ******* | -0.0864 | -0.1728 | -0.4409 |
| 0.650 | -0.2234 | -0.1667 | -0.0989 | -0.1770 | -0.4357 |
| 0.675 | ******* | -0.1845 | -0.1119 | -0.1870 | -0.4395 |
| 0.700 | -0.2344 | -0.2039 | -0.1220 | -0.1953 | -0.4238 |
| 0.725 | ******* | -0.2198 | ******* | -0.2018 | -0.4175 |
| 0.750 | -0.2393 | -0.2428 | ******* | -0.2103 | -0.4288 |
| 0.775 | ******* | -0.2652 | -0.1777 | -0.2252 | -0.4255 |
| 0.800 | -0.2366 | -0.2868 | -0.2048 | -0.2416 | ******* |
| 0.825 | ******* | -0.3062 | -0.2398 | -0.2611 | -0.3844 |
| 0.850 | -0.2298 | -0.3259 | -0.2782 | -0.2899 | -0.3834 |
| 0.875 | ******* | -0.3381 | -0.3144 | -0.3244 | -0.3951 |
| 0.900 | -0.2142 | -0.3396 | -0.3505 | -0.3820 | ******* |
| 0.925 | ******* | -0.3420 | -0.3758 | -0.4310 | -0.5859 |
| 0.950 | -0.2096 | -0.3400 | -0.3919 | -0.4599 | -0.5971 |
| 0.975 | ******* | -0.3404 | -0.4076 | -0.4992 | -0.5611 |
| 1.000 | -0.3996 | -0.7198 | -0.7876 | -0.8436 | -0.8709 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0843 | 0.0818 | 0.1587 | ******* | -0.5134 |
| -0.400 | 0.0701 | 0.0926 | 0.1221 | -0.0334 | -0.6177 |
| -0.600 | 0.0702 | 0.0921 | 0.1069 | -0.0023 | -0.6842 |
| -0.700 | ******* | 0.0848 | 0.1032 | 0.0080 | -0.6734 |
| -0.800 | ******* | ******* | 0.0964 | 0.0248 | -0.6253 |
| -0.850 | ******* | 0.1127 | 0.0996 | 0.0268 | -0.6187 |
| -0.900 | 0.1551 | 0.1472 | 0.1239 | 0.0423 | -0.6432 |
| -0.950 | 0.1791 | 0.1340 | 0.1729 | 0.1029 | -0.2246 |
| -0.975 | ******* | 0.2038 | 0.1941 | 0.1404 | -0.0666 |
| -1.000 | -0.3920 | -0.7024 | -0.7609 | -0.7914 | -0.8694 |



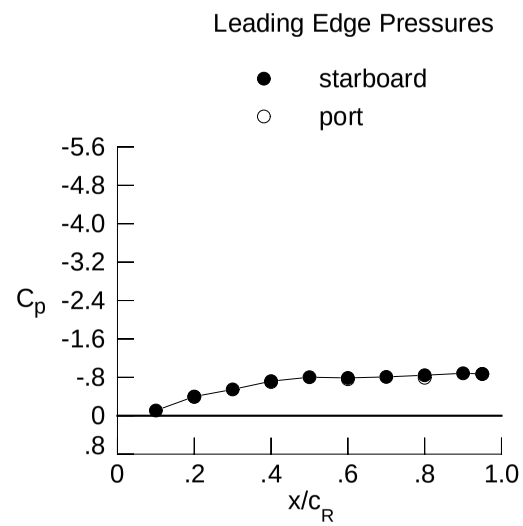

Small Radius L.E.

Run No. = 42 , Point No. = 872

$C_N$ = 0.209, $C_m$ = -0.0401

$\alpha$ = 5.3 °, $M_\infty$ = 0.870

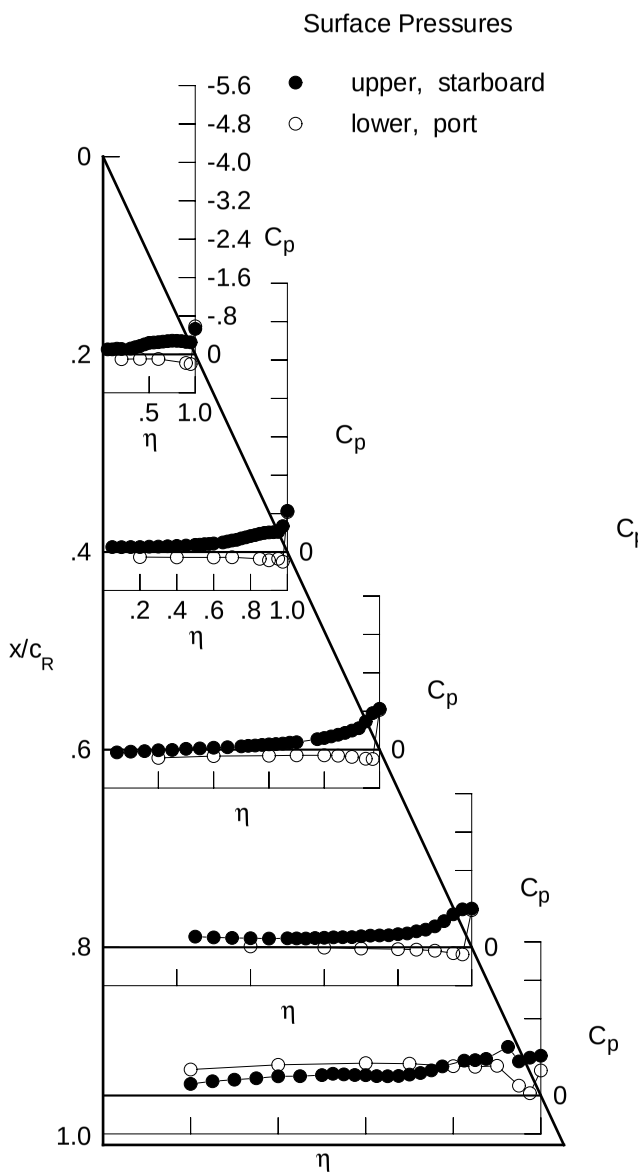
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.1085 | ******* |
| 0.20 | -0.3996 | -0.3920 |
| 0.30 | -0.5477 | ******* |
| 0.40 | -0.7198 | -0.7024 |
| 0.50 | -0.8026 | ******* |
| 0.60 | -0.7876 | -0.7609 |
| 0.70 | -0.8089 | ******* |
| 0.80 | -0.8436 | -0.7914 |
| 0.90 | -0.8842 | ******* |
| 0.95 | -0.8709 | -0.8694 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1047 | -0.1041 | 0.0576 | ******* | ******* |
| 0.100 | -0.1051 | -0.1019 | 0.0426 | ******* | ******* |
| 0.150 | -0.1193 | -0.1042 | 0.0313 | ******* | ******* |
| 0.200 | -0.1126 | -0.1039 | 0.0130 | ******* | -0.2414 |
| 0.250 | ******* | -0.1120 | 0.0061 | -0.2215 | -0.2969 |
| 0.300 | -0.1228 | -0.1138 | -0.0168 | -0.2059 | -0.3293 |
| 0.350 | -0.1496 | -0.1210 | -0.0257 | -0.1954 | -0.3593 |
| 0.400 | -0.1756 | -0.1277 | -0.0400 | -0.1889 | -0.3999 |
| 0.450 | -0.2084 | -0.1356 | -0.0505 | -0.1817 | -0.4025 |
| 0.500 | -0.2404 | -0.1497 | -0.0677 | -0.1871 | -0.4247 |
| 0.525 | ******* | -0.1530 | -0.0793 | -0.1847 | -0.4529 |
| 0.550 | -0.2469 | -0.1640 | -0.0853 | -0.1822 | -0.4404 |
| 0.575 | ******* | -0.1682 | -0.0985 | -0.1931 | -0.4275 |
| 0.600 | -0.2541 | -0.1786 | -0.1098 | -0.1986 | -0.4232 |
| 0.625 | ******* | ******* | -0.1171 | -0.2072 | -0.4043 |
| 0.650 | -0.2653 | -0.1992 | -0.1262 | -0.2096 | -0.4015 |
| 0.675 | ******* | -0.2200 | -0.1446 | -0.2114 | -0.4072 |
| 0.700 | -0.2760 | -0.2403 | -0.1543 | -0.2297 | -0.4360 |
| 0.725 | ******* | -0.2546 | ******* | -0.2423 | -0.4690 |
| 0.750 | -0.2852 | -0.2836 | ******* | -0.2467 | -0.5230 |
| 0.775 | ******* | -0.3067 | -0.2174 | -0.2504 | -0.6066 |
| 0.800 | -0.2824 | -0.3328 | -0.2423 | -0.2726 | ******* |
| 0.825 | ******* | -0.3539 | -0.2756 | -0.2880 | -0.7265 |
| 0.850 | -0.2770 | -0.3804 | -0.3107 | -0.3329 | -0.7372 |
| 0.875 | ******* | -0.3987 | -0.3486 | -0.3668 | -0.7622 |
| 0.900 | -0.2604 | -0.4088 | -0.3965 | -0.4360 | ******* |
| 0.925 | ******* | -0.4134 | -0.4468 | -0.5444 | -1.0137 |
| 0.950 | -0.2520 | -0.4190 | -0.5858 | -0.6876 | -0.7104 |
| 0.975 | ******* | -0.5390 | -0.7611 | -0.7906 | -0.7882 |
| 1.000 | -0.5313 | -0.8574 | -0.8510 | -0.8054 | -0.8289 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1002 | 0.1048 | 0.1723 | ******* | -0.5414 |
| -0.400 | 0.0934 | 0.1116 | 0.1345 | -0.0180 | -0.6395 |
| -0.600 | 0.0956 | 0.1125 | 0.1261 | 0.0073 | -0.6742 |
| -0.700 | ******* | 0.1092 | 0.1182 | 0.0267 | -0.6629 |
| -0.800 | ******* | ******* | 0.1184 | 0.0394 | -0.6115 |
| -0.850 | ******* | 0.1416 | 0.1258 | 0.0497 | -0.5984 |
| -0.900 | 0.1792 | 0.1719 | 0.1510 | 0.0713 | -0.6182 |
| -0.950 | 0.2008 | 0.1403 | 0.1899 | 0.1224 | -0.2047 |
| -0.975 | ******* | 0.2026 | 0.1952 | 0.1482 | -0.0478 |
| -1.000 | -0.5841 | -0.8332 | -0.8269 | -0.7747 | -0.5218 |



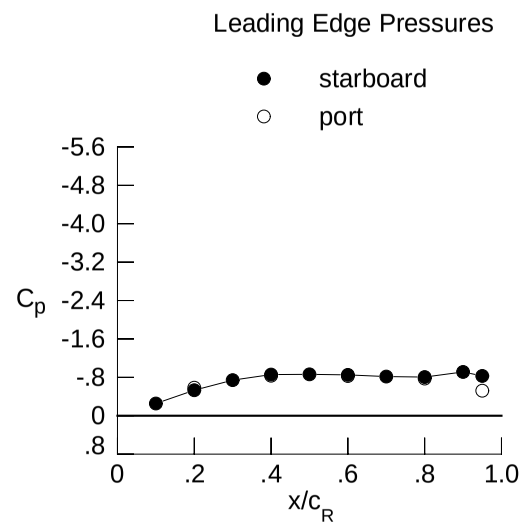

Small Radius L.E.

Run No. = 42 , Point No. = 873

$C_N$ = 0.254, $C_m$ = -0.0453

$\alpha$ = 6.3 °, $M_\infty$ = 0.870

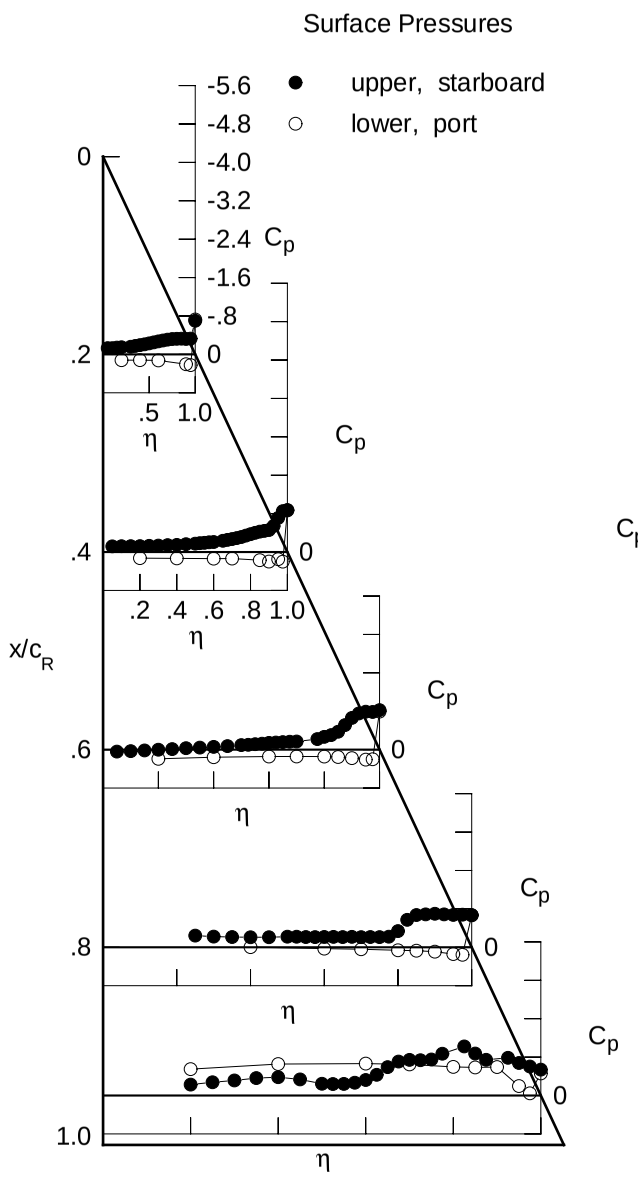
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.2547 | ******* |
| 0.20 | -0.5313 | -0.5841 |
| 0.30 | -0.7415 | ******* |
| 0.40 | -0.8574 | -0.8332 |
| 0.50 | -0.8624 | ******* |
| 0.60 | -0.8510 | -0.8269 |
| 0.70 | -0.8159 | ******* |
| 0.80 | -0.8054 | -0.7747 |
| 0.90 | -0.9121 | ******* |
| 0.95 | -0.8289 | -0.5218 |

# Table D5. Continued.

| η | x/c_R .2 C_p,u | x/c_R .4 C_p,u | x/c_R .6 C_p,u | x/c_R .8 C_p,u | x/c_R .95 C_p,u |
|---|---|---|---|---|---|
| 0.050 | -0.1304 | -0.1181 | 0.0411 | ******* | ******* |
| 0.100 | -0.1296 | -0.1215 | 0.0309 | ******* | ******* |
| 0.150 | -0.1413 | -0.1222 | 0.0171 | ******* | ******* |
| 0.200 | -0.1489 | -0.1228 | 0.0018 | ******* | -0.2273 |
| 0.250 | ******* | -0.1299 | -0.0112 | -0.2429 | -0.2760 |
| 0.300 | -0.1596 | -0.1342 | -0.0301 | -0.2227 | -0.3133 |
| 0.350 | -0.1757 | -0.1438 | -0.0428 | -0.2139 | -0.3628 |
| 0.400 | -0.1924 | -0.1486 | -0.0580 | -0.2092 | -0.3816 |
| 0.450 | -0.2100 | -0.1636 | -0.0738 | -0.2094 | -0.3351 |
| 0.500 | -0.2293 | -0.1742 | -0.0943 | -0.2205 | -0.2451 |
| 0.525 | ******* | -0.1851 | -0.1007 | -0.2201 | -0.2393 |
| 0.550 | -0.2502 | -0.1920 | -0.1133 | -0.2139 | -0.2415 |
| 0.575 | ******* | -0.2030 | -0.1241 | -0.2118 | -0.2661 |
| 0.600 | -0.2715 | -0.2084 | -0.1407 | -0.2150 | -0.3236 |
| 0.625 | ******* | ******* | -0.1479 | -0.2169 | -0.4315 |
| 0.650 | -0.2900 | -0.2348 | -0.1566 | -0.2127 | -0.5913 |
| 0.675 | ******* | -0.2535 | -0.1647 | -0.2178 | -0.7072 |
| 0.700 | -0.3073 | -0.2702 | -0.1695 | -0.2108 | -0.7421 |
| 0.725 | ******* | -0.2902 | ******* | -0.2137 | -0.7351 |
| 0.750 | -0.3199 | -0.3128 | ******* | -0.2120 | -0.7505 |
| 0.775 | ******* | -0.3425 | -0.2200 | -0.2208 | -0.8701 |
| 0.800 | -0.3248 | -0.3719 | -0.2665 | -0.3375 | ******* |
| 0.825 | ******* | -0.4002 | -0.3029 | -0.5720 | -1.0223 |
| 0.850 | -0.3269 | -0.4244 | -0.3726 | -0.6721 | -0.8744 |
| 0.875 | ******* | -0.4411 | -0.5109 | -0.6859 | -0.7440 |
| 0.900 | -0.3219 | -0.4586 | -0.6607 | -0.6981 | ******* |
| 0.925 | ******* | -0.5419 | -0.7539 | -0.6858 | -0.7856 |
| 0.950 | -0.3286 | -0.7107 | -0.7901 | -0.6745 | -0.6775 |
| 0.975 | ******* | -0.8519 | -0.7849 | -0.6795 | -0.6039 |
| 1.000 | -0.6997 | -0.8754 | -0.8234 | -0.6716 | -0.5391 |
| | C_p,l | C_p,l | C_p,l | C_p,l | C_p,l |
| -0.200 | 0.1206 | 0.1274 | 0.1911 | ******* | -0.5494 |
| -0.400 | 0.1199 | 0.1324 | 0.1578 | -0.0034 | -0.6554 |
| -0.600 | 0.1255 | 0.1373 | 0.1432 | 0.0277 | -0.6646 |
| -0.700 | ******* | 0.1359 | 0.1423 | 0.0408 | -0.6480 |
| -0.800 | ******* | ******* | 0.1440 | 0.0625 | -0.5957 |
| -0.850 | ******* | 0.1694 | 0.1533 | 0.0712 | -0.5849 |
| -0.900 | 0.2051 | 0.1982 | 0.1767 | 0.0916 | -0.5931 |
| -0.950 | 0.2231 | 0.1488 | 0.2079 | 0.1411 | -0.1970 |
| -0.975 | ******* | 0.2003 | 0.1998 | 0.1560 | -0.0458 |
| -1.000 | -0.7261 | -0.8672 | -0.7930 | -0.6659 | -0.4603 |



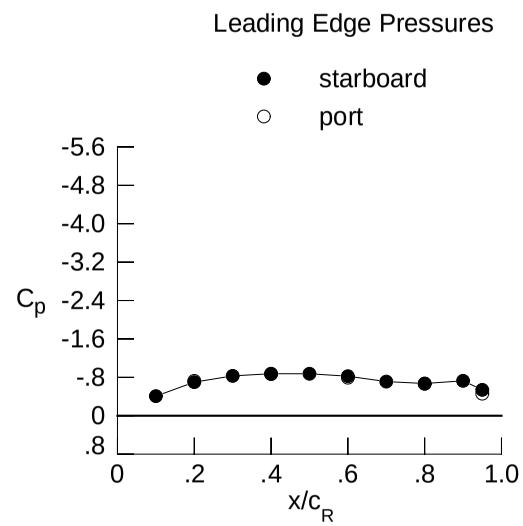

Small Radius L.E.

Run No. = 42 , Point No. = 874

$C_N$ = 0.315, $C_m$ = -0.0608

$\alpha$ = 7.3 °, $M_\infty$ = 0.869

$R_{mac}$ = $6.0 \times 10^6$

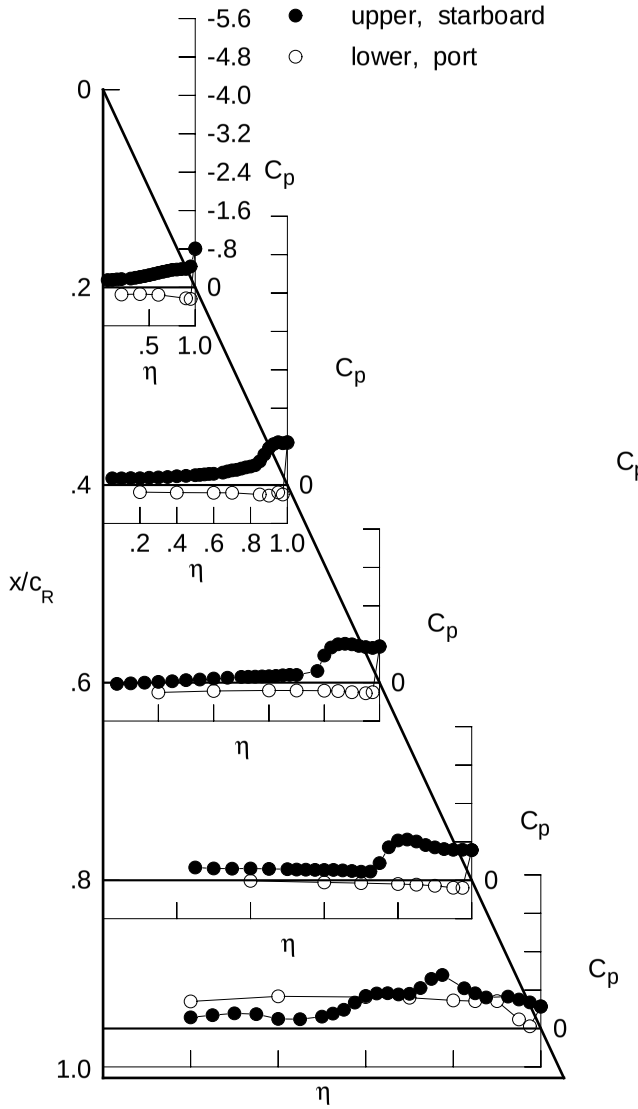



| x/c_R | starb'd C_p | port C_p |
|---|---|---|
| 0.10 | -0.4081 | ******* |
| 0.20 | -0.6997 | -0.7261 |
| 0.30 | -0.8301 | ******* |
| 0.40 | -0.8754 | -0.8672 |
| 0.50 | -0.8742 | ******* |
| 0.60 | -0.8234 | -0.7930 |
| 0.70 | -0.7112 | ******* |
| 0.80 | -0.6716 | -0.6659 |
| 0.90 | -0.7274 | ******* |
| 0.95 | -0.5391 | -0.4603 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1532 | -0.1397 | 0.0257 | ******* | ******* |
| 0.100 | -0.1561 | -0.1391 | 0.0154 | ******* | ******* |
| 0.150 | -0.1668 | -0.1442 | 0.0010 | ******* | ******* |
| 0.200 | -0.1727 | -0.1413 | -0.0157 | ******* | -0.2318 |
| 0.250 | ******* | -0.1520 | -0.0286 | -0.2661 | -0.2779 |
| 0.300 | -0.1835 | -0.1587 | -0.0524 | -0.2465 | -0.3159 |
| 0.350 | -0.2003 | -0.1672 | -0.0652 | -0.2420 | -0.2990 |
| 0.400 | -0.2179 | -0.1832 | -0.0853 | -0.2456 | -0.2000 |
| 0.450 | -0.2352 | -0.1908 | -0.1026 | -0.2368 | -0.1935 |
| 0.500 | -0.2558 | -0.2046 | -0.1200 | -0.2316 | -0.2472 |
| 0.525 | ******* | -0.2122 | -0.1220 | -0.2234 | -0.3103 |
| 0.550 | -0.2788 | -0.2214 | -0.1248 | -0.2207 | -0.3904 |
| 0.575 | ******* | -0.2314 | -0.1292 | -0.2168 | -0.5403 |
| 0.600 | -0.3020 | -0.2341 | -0.1334 | -0.2153 | -0.6780 |
| 0.625 | ******* | ******* | -0.1399 | -0.2156 | -0.7296 |
| 0.650 | -0.3237 | -0.2581 | -0.1532 | -0.2053 | -0.7353 |
| 0.675 | ******* | -0.2841 | -0.1619 | -0.1938 | -0.7093 |
| 0.700 | -0.3438 | -0.3052 | -0.1602 | -0.1787 | -0.7228 |
| 0.725 | ******* | -0.3166 | ******* | -0.1817 | -0.8434 |
| 0.750 | -0.3646 | -0.3422 | ******* | -0.3579 | -1.0331 |
| 0.775 | ******* | -0.3683 | -0.2422 | -0.6878 | -1.1149 |
| 0.800 | -0.3710 | -0.3858 | -0.5651 | -0.8298 | ******* |
| 0.825 | ******* | -0.4133 | -0.7308 | -0.8484 | -0.8386 |
| 0.850 | -0.3814 | -0.4932 | -0.7989 | -0.8080 | -0.7338 |
| 0.875 | ******* | -0.6364 | -0.8096 | -0.7340 | -0.6466 |
| 0.900 | -0.3847 | -0.7700 | -0.7986 | -0.6857 | ******* |
| 0.925 | ******* | -0.8519 | -0.7653 | -0.6501 | -0.6651 |
| 0.950 | -0.4377 | -0.8919 | -0.7405 | -0.6352 | -0.6043 |
| 0.975 | ******* | -0.8708 | -0.7231 | -0.6359 | -0.5441 |
| 1.000 | -0.8125 | -0.8945 | -0.7592 | -0.6308 | -0.4636 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1477 | 0.1479 | 0.2047 | ******* | -0.5638 |
| -0.400 | 0.1391 | 0.1573 | 0.1737 | 0.0120 | -0.6703 |
| -0.600 | 0.1535 | 0.1614 | 0.1626 | 0.0443 | -0.6552 |
| -0.700 | ******* | 0.1618 | 0.1643 | 0.0590 | -0.6413 |
| -0.800 | ******* | ******* | 0.1678 | 0.0775 | -0.5850 |
| -0.850 | ******* | 0.1973 | 0.1753 | 0.0914 | -0.5705 |
| -0.900 | 0.2281 | 0.2211 | 0.1993 | 0.1141 | -0.5706 |
| -0.950 | 0.2402 | 0.1532 | 0.2208 | 0.1552 | -0.1893 |
| -0.975 | ******* | 0.1966 | 0.1990 | 0.1580 | -0.0460 |
| -1.000 | -0.7980 | -0.8767 | -0.7448 | -0.6260 | -0.4527 |

Surface Pressures




Small Radius L.E.

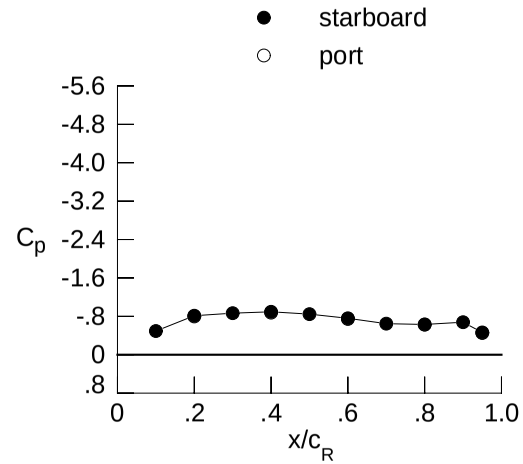
Run No. = 42 , Point No. = 875

$C_N$ = 0.370, $C_m$ = -0.0710

$\alpha$ = 8.3 °, $M_\infty$ = 0.869

$R_{mac}$ = $6.0 \times 10^6$

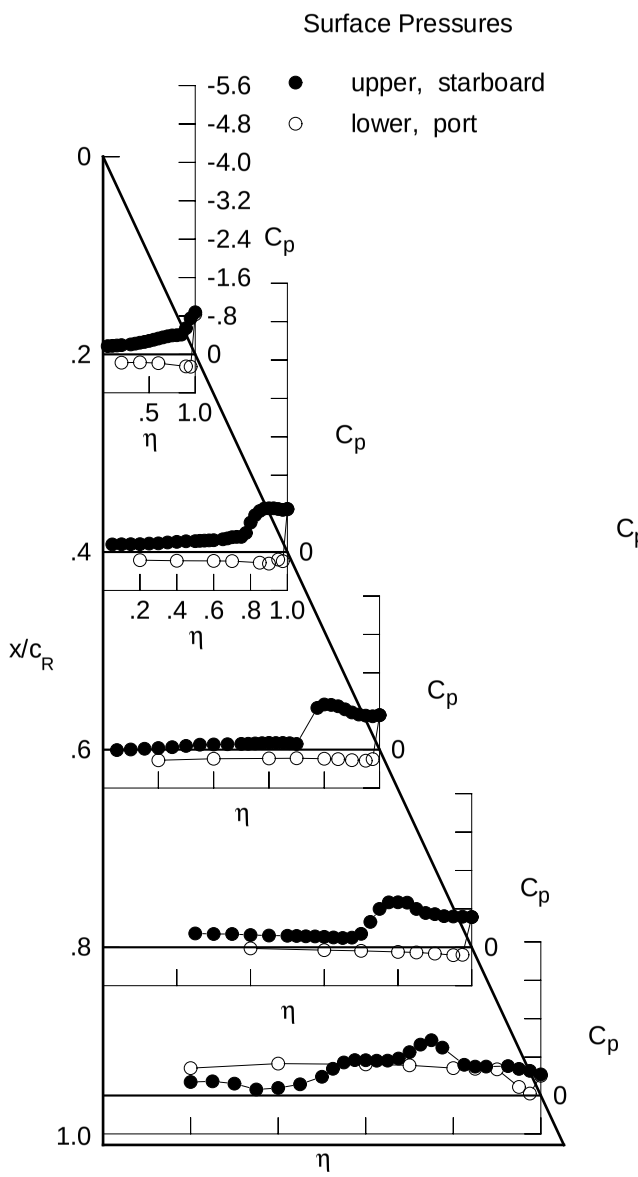
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.4932 | ******* |
| 0.20 | -0.8125 | -0.7980 |
| 0.30 | -0.8659 | ******* |
| 0.40 | -0.8945 | -0.8767 |
| 0.50 | -0.8459 | ******* |
| 0.60 | -0.7592 | -0.7448 |
| 0.70 | -0.6470 | ******* |
| 0.80 | -0.6308 | -0.6260 |
| 0.90 | -0.6777 | ******* |
| 0.95 | -0.4636 | -0.4527 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1723 | -0.1587 | 0.0086 | ******* | ******* |
| 0.100 | -0.1772 | -0.1618 | -0.0028 | ******* | ******* |
| 0.150 | -0.1845 | -0.1636 | -0.0184 | ******* | ******* |
| 0.200 | -0.1925 | -0.1640 | -0.0332 | ******* | -0.2816 |
| 0.250 | ******* | -0.1757 | -0.0509 | -0.2883 | -0.2949 |
| 0.300 | -0.2075 | -0.1812 | -0.0778 | -0.2771 | -0.2474 |
| 0.350 | -0.2238 | -0.1989 | -0.1031 | -0.2766 | -0.1252 |
| 0.400 | -0.2434 | -0.2117 | -0.1083 | -0.2553 | -0.1566 |
| 0.450 | -0.2600 | -0.2236 | -0.1129 | -0.2452 | -0.2339 |
| 0.500 | -0.2820 | -0.2260 | -0.1198 | -0.2397 | -0.3908 |
| 0.525 | ******* | -0.2335 | -0.1224 | -0.2363 | -0.5567 |
| 0.550 | -0.3053 | -0.2375 | -0.1287 | -0.2289 | -0.6881 |
| 0.575 | ******* | -0.2422 | -0.1342 | -0.2262 | -0.7379 |
| 0.600 | -0.3306 | -0.2463 | -0.1405 | -0.2174 | -0.7351 |
| 0.625 | ******* | ******* | -0.1374 | -0.2046 | -0.7246 |
| 0.650 | -0.3543 | -0.2657 | -0.1395 | -0.1936 | -0.7261 |
| 0.675 | ******* | -0.2844 | -0.1333 | -0.2007 | -0.7707 |
| 0.700 | -0.3766 | -0.3092 | -0.1180 | -0.2796 | -0.9033 |
| 0.725 | ******* | -0.3157 | ******* | -0.5285 | -1.0599 |
| 0.750 | -0.3956 | -0.3160 | ******* | -0.7990 | -1.1519 |
| 0.775 | ******* | -0.3976 | -0.8697 | -0.9360 | -0.9973 |
| 0.800 | -0.3996 | -0.6127 | -0.9406 | -0.9374 | ******* |
| 0.825 | ******* | -0.7669 | -0.9322 | -0.9299 | -0.6404 |
| 0.850 | -0.4121 | -0.8554 | -0.9044 | -0.7988 | -0.6015 |
| 0.875 | ******* | -0.9066 | -0.8398 | -0.7146 | -0.6023 |
| 0.900 | -0.5462 | -0.9114 | -0.7744 | -0.6908 | ******* |
| 0.925 | ******* | -0.9110 | -0.7315 | -0.6486 | -0.6128 |
| 0.950 | -0.7508 | -0.8971 | -0.7083 | -0.6413 | -0.5546 |
| 0.975 | ******* | -0.8788 | -0.6951 | -0.6365 | -0.5136 |
| 1.000 | -0.8776 | -0.8990 | -0.7201 | -0.6307 | -0.4392 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1726 | 0.1698 | 0.2214 | ******* | -0.5701 |
| -0.400 | 0.1662 | 0.1813 | 0.1896 | 0.0235 | -0.6646 |
| -0.600 | 0.1822 | 0.1849 | 0.1833 | 0.0598 | -0.6485 |
| -0.700 | ******* | 0.1888 | 0.1789 | 0.0745 | -0.6292 |
| -0.800 | ******* | ******* | 0.1893 | 0.0968 | -0.5707 |
| -0.850 | ******* | 0.2223 | 0.1979 | 0.1079 | -0.5565 |
| -0.900 | 0.2503 | 0.2418 | 0.2195 | 0.1310 | -0.5454 |
| -0.950 | 0.2570 | 0.1571 | 0.2301 | 0.1641 | -0.1783 |
| -0.975 | ******* | 0.1905 | 0.1979 | 0.1559 | -0.0407 |
| -1.000 | -0.8347 | -0.8895 | -0.7166 | -0.6290 | -0.4115 |



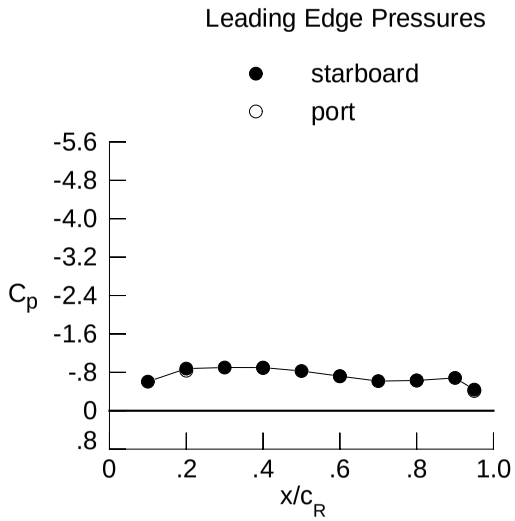

Small Radius L.E.

Run No. = 42 , Point No. = 876

$C_N$ = 0.426, $C_m$ = -0.0797

$\alpha$ = 9.4 °, $M_\infty$ = 0.869

$R_{mac}$ = $6.0 \times 10^6$

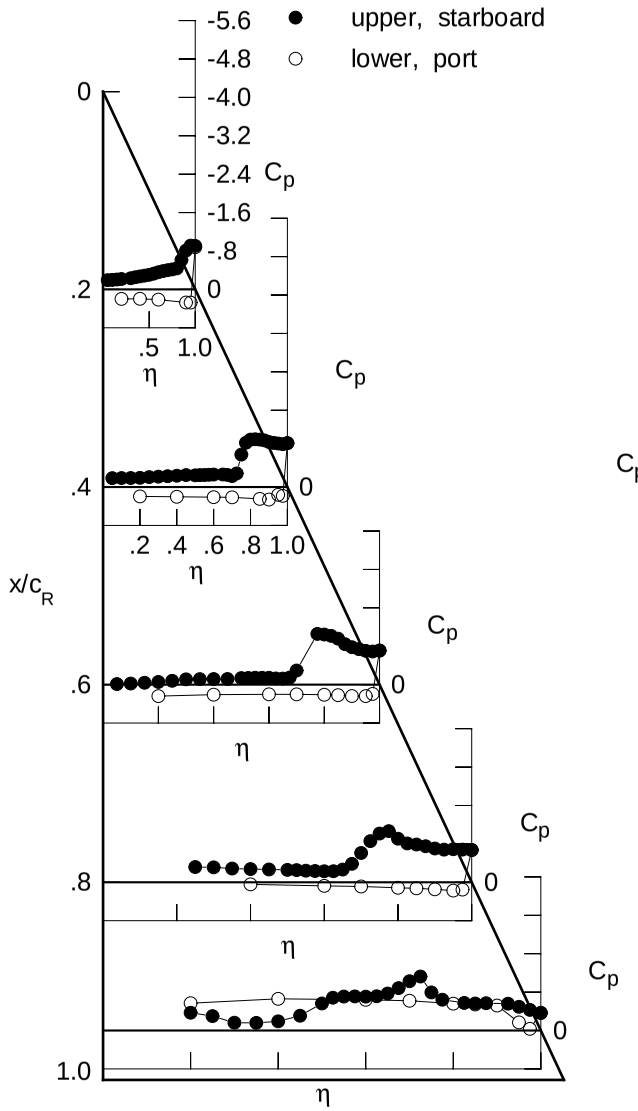



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.6056 | ******* |
| 0.20 | -0.8776 | -0.8347 |
| 0.30 | -0.9003 | ******* |
| 0.40 | -0.8990 | -0.8895 |
| 0.50 | -0.8275 | ******* |
| 0.60 | -0.7201 | -0.7166 |
| 0.70 | -0.6171 | ******* |
| 0.80 | -0.6307 | -0.6290 |
| 0.90 | -0.6834 | ******* |
| 0.95 | -0.4392 | -0.4115 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1928 | -0.1852 | -0.0120 | ******* | ******* |
| 0.100 | -0.1976 | -0.1873 | -0.0235 | ******* | ******* |
| 0.150 | -0.2066 | -0.1881 | -0.0389 | ******* | ******* |
| 0.200 | -0.2169 | -0.1918 | -0.0557 | ******* | -0.3701 |
| 0.250 | ******* | -0.2072 | -0.0799 | -0.3175 | -0.3001 |
| 0.300 | -0.2321 | -0.2161 | -0.1106 | -0.3114 | -0.1620 |
| 0.350 | -0.2524 | -0.2255 | -0.1153 | -0.2865 | -0.1592 |
| 0.400 | -0.2703 | -0.2362 | -0.1170 | -0.2750 | -0.1911 |
| 0.450 | -0.2862 | -0.2494 | -0.1175 | -0.2674 | -0.3082 |
| 0.500 | -0.3040 | -0.2443 | -0.1371 | -0.2588 | -0.5634 |
| 0.525 | ******* | -0.2485 | -0.1393 | -0.2537 | -0.6833 |
| 0.550 | -0.3280 | -0.2503 | -0.1438 | -0.2415 | -0.7069 |
| 0.575 | ******* | -0.2551 | -0.1431 | -0.2351 | -0.7104 |
| 0.600 | -0.3573 | -0.2597 | -0.1434 | -0.2296 | -0.7054 |
| 0.625 | ******* | ******* | -0.1289 | -0.2307 | -0.7134 |
| 0.650 | -0.3804 | -0.2609 | -0.1263 | -0.2648 | -0.7705 |
| 0.675 | ******* | -0.2522 | -0.1484 | -0.3852 | -0.8836 |
| 0.700 | -0.3996 | -0.2282 | -0.2943 | -0.6101 | -1.0268 |
| 0.725 | ******* | -0.2839 | ******* | -0.8580 | -1.1245 |
| 0.750 | -0.4162 | -0.6757 | ******* | -1.0150 | -0.7938 |
| 0.775 | ******* | -0.9222 | -1.0569 | -1.0654 | -0.6419 |
| 0.800 | -0.4368 | -0.9886 | -1.0440 | -0.9082 | ******* |
| 0.825 | ******* | -0.9951 | -1.0162 | -0.8092 | -0.5742 |
| 0.850 | -0.6114 | -0.9881 | -0.9573 | -0.7872 | -0.5626 |
| 0.875 | ******* | -0.9728 | -0.8423 | -0.7509 | -0.5692 |
| 0.900 | -0.8095 | -0.9387 | -0.7798 | -0.7041 | ******* |
| 0.925 | ******* | -0.9218 | -0.7399 | -0.6802 | -0.5582 |
| 0.950 | -0.9120 | -0.9069 | -0.7040 | -0.6891 | -0.4941 |
| 0.975 | ******* | -0.8939 | -0.6907 | -0.6811 | -0.4292 |
| 1.000 | -0.9056 | -0.9130 | -0.7082 | -0.6720 | -0.3706 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1986 | 0.1954 | 0.2390 | ******* | -0.5687 |
| -0.400 | 0.1963 | 0.2032 | 0.2084 | 0.0434 | -0.6602 |
| -0.600 | 0.2131 | 0.2111 | 0.2017 | 0.0747 | -0.6401 |
| -0.700 | ******* | 0.2142 | 0.2023 | 0.0875 | -0.6201 |
| -0.800 | ******* | ******* | 0.2101 | 0.1146 | -0.5596 |
| -0.850 | ******* | 0.2471 | 0.2189 | 0.1257 | -0.5424 |
| -0.900 | 0.2735 | 0.2609 | 0.2378 | 0.1466 | -0.5197 |
| -0.950 | 0.2740 | 0.1616 | 0.2380 | 0.1728 | -0.1691 |
| -0.975 | ******* | 0.1837 | 0.1927 | 0.1516 | -0.0343 |
| -1.000 | -0.8776 | -0.9156 | -0.7128 | -0.6717 | -0.3629 |

Surface Pressures




Small Radius L.E.

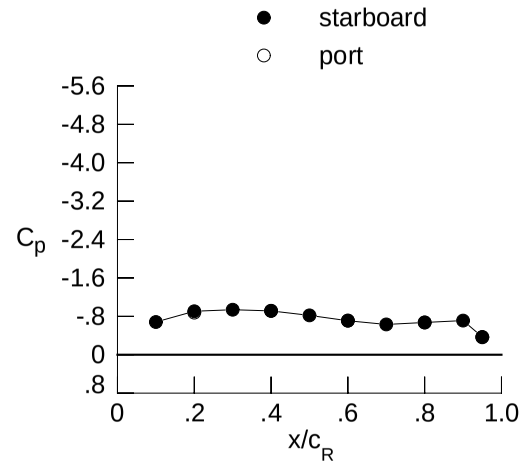
Run No. = 42 , Point No. = 877

$C_N$ = 0.484, $C_m$ = -0.0908

$\alpha$ = 10.4 °, $M_\infty$ = 0.869

$R_{mac}$ = $6.0 \times 10^6$

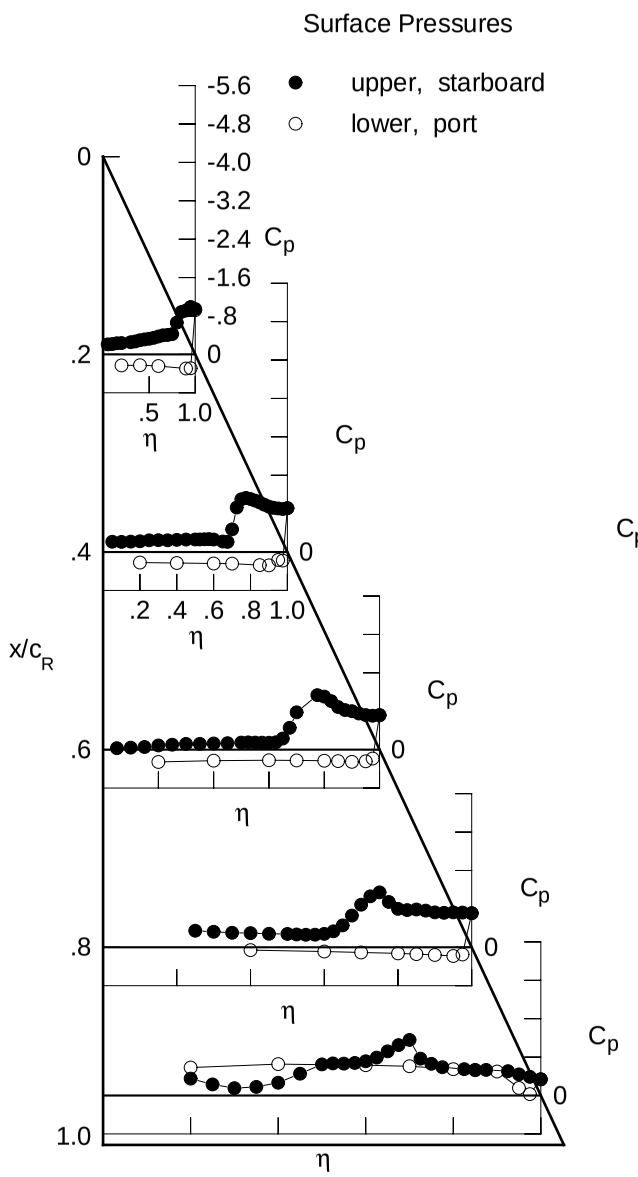
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.6820 | ******* |
| 0.20 | -0.9056 | -0.8776 |
| 0.30 | -0.9377 | ******* |
| 0.40 | -0.9130 | -0.9156 |
| 0.50 | -0.8196 | ******* |
| 0.60 | -0.7082 | -0.7128 |
| 0.70 | -0.6309 | ******* |
| 0.80 | -0.6720 | -0.6717 |
| 0.90 | -0.7116 | ******* |
| 0.95 | -0.3706 | -0.3629 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2090 | -0.2142 | -0.0307 | ******* | ******* |
| 0.100 | -0.2154 | -0.2115 | -0.0417 | ******* | ******* |
| 0.150 | -0.2323 | -0.2172 | -0.0549 | ******* | ******* |
| 0.200 | -0.2363 | -0.2244 | -0.0872 | ******* | -0.3516 |
| 0.250 | ******* | -0.2443 | -0.1028 | -0.3451 | -0.2313 |
| 0.300 | -0.2538 | -0.2470 | -0.1202 | -0.3229 | -0.1529 |
| 0.350 | -0.2699 | -0.2449 | -0.1196 | -0.3027 | -0.1795 |
| 0.400 | -0.2953 | -0.2534 | -0.1277 | -0.2950 | -0.2666 |
| 0.450 | -0.3123 | -0.2597 | -0.1346 | -0.2813 | -0.4545 |
| 0.500 | -0.3254 | -0.2616 | -0.1471 | -0.2778 | -0.6483 |
| 0.525 | ******* | -0.2628 | -0.1523 | -0.2673 | -0.6687 |
| 0.550 | -0.3458 | -0.2657 | -0.1471 | -0.2604 | -0.6637 |
| 0.575 | ******* | -0.2684 | -0.1459 | -0.2622 | -0.6783 |
| 0.600 | -0.3724 | -0.2611 | -0.1443 | -0.2791 | -0.7139 |
| 0.625 | ******* | ******* | -0.1535 | -0.3329 | -0.7893 |
| 0.650 | -0.3973 | -0.2190 | -0.2318 | -0.4557 | -0.9196 |
| 0.675 | ******* | -0.2113 | -0.4553 | -0.6610 | -1.0502 |
| 0.700 | -0.4049 | -0.4727 | -0.7773 | -0.8868 | -1.1575 |
| 0.725 | ******* | -0.9273 | ******* | -1.0619 | -0.7681 |
| 0.750 | -0.4212 | -1.0988 | ******* | -1.1441 | -0.6611 |
| 0.775 | ******* | -1.1283 | -1.1349 | -0.9438 | -0.5898 |
| 0.800 | -0.6615 | -1.1043 | -1.1045 | -0.8008 | ******* |
| 0.825 | ******* | -1.0715 | -1.0112 | -0.7754 | -0.5490 |
| 0.850 | -0.8840 | -1.0327 | -0.8879 | -0.7870 | -0.5339 |
| 0.875 | ******* | -0.9868 | -0.8250 | -0.7642 | -0.5339 |
| 0.900 | -0.9146 | -0.9454 | -0.8015 | -0.7270 | ******* |
| 0.925 | ******* | -0.9226 | -0.7524 | -0.7181 | -0.5076 |
| 0.950 | -0.9883 | -0.9077 | -0.7204 | -0.7269 | -0.4398 |
| 0.975 | ******* | -0.8956 | -0.7064 | -0.7232 | -0.3887 |
| 1.000 | -0.9455 | -0.9138 | -0.7212 | -0.7103 | -0.3402 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2299 | 0.2191 | 0.2565 | ******* | -0.5823 |
| -0.400 | 0.2257 | 0.2284 | 0.2298 | 0.0590 | -0.6540 |
| -0.600 | 0.2420 | 0.2390 | 0.2206 | 0.0883 | -0.6308 |
| -0.700 | ******* | 0.2419 | 0.2247 | 0.1080 | -0.6095 |
| -0.800 | ******* | ******* | 0.2310 | 0.1269 | -0.5485 |
| -0.850 | ******* | 0.2718 | 0.2381 | 0.1422 | -0.5268 |
| -0.900 | 0.2946 | 0.2776 | 0.2546 | 0.1603 | -0.5003 |
| -0.950 | 0.2888 | 0.1644 | 0.2435 | 0.1814 | -0.1574 |
| -0.975 | ******* | 0.1775 | 0.1850 | 0.1495 | -0.0291 |
| -1.000 | -0.9215 | -0.9133 | -0.7141 | -0.7084 | -0.3355 |



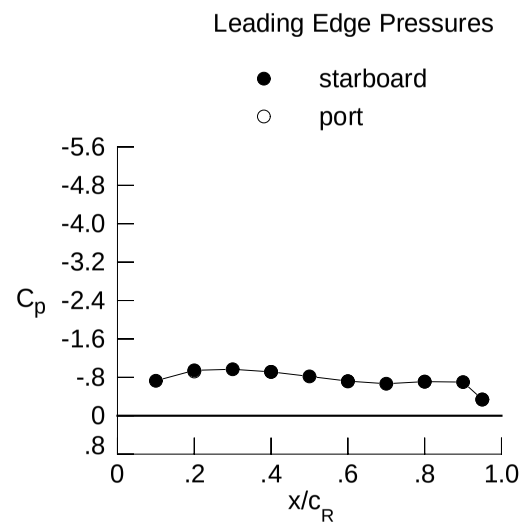

Small Radius L.E.

Run No. = 42 , Point No. = 878

$C_N$ = 0.535, $C_m$ = -0.0959

$\alpha$ = 11.4 °, $M_\infty$ = 0.867

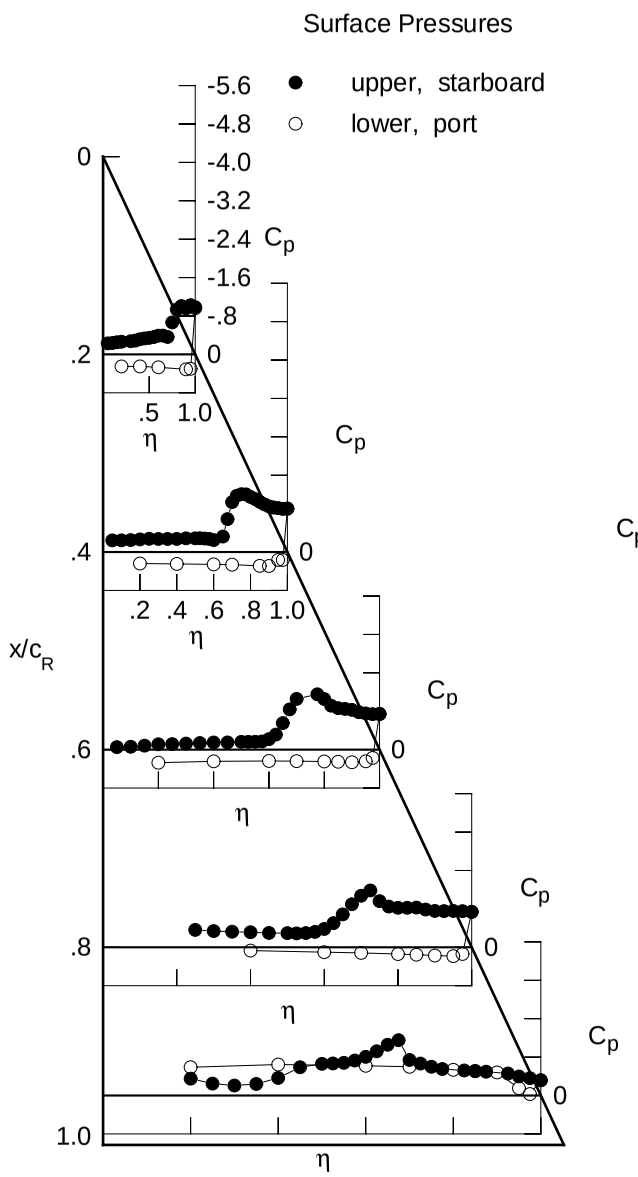
$R_{mac}$ = $6.0 \times 10^6$




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.7283 | ******* |
| 0.20 | -0.9455 | -0.9215 |
| 0.30 | -0.9678 | ******* |
| 0.40 | -0.9138 | -0.9133 |
| 0.50 | -0.8190 | ******* |
| 0.60 | -0.7212 | -0.7141 |
| 0.70 | -0.6666 | ******* |
| 0.80 | -0.7103 | -0.7084 |
| 0.90 | -0.7010 | ******* |
| 0.95 | -0.3402 | -0.3355 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2296 | -0.2428 | -0.0522 | ******* | ******* |
| 0.100 | -0.2369 | -0.2438 | -0.0603 | ******* | ******* |
| 0.150 | -0.2528 | -0.2487 | -0.0829 | ******* | ******* |
| 0.200 | -0.2635 | -0.2631 | -0.1121 | ******* | -0.3513 |
| 0.250 | ******* | -0.2758 | -0.1155 | -0.3627 | -0.2483 |
| 0.300 | -0.2741 | -0.2717 | -0.1265 | -0.3374 | -0.2080 |
| 0.350 | -0.2870 | -0.2718 | -0.1380 | -0.3246 | -0.2406 |
| 0.400 | -0.3160 | -0.2733 | -0.1485 | -0.3134 | -0.3652 |
| 0.450 | -0.3327 | -0.2856 | -0.1503 | -0.2982 | -0.5886 |
| 0.500 | -0.3439 | -0.2859 | -0.1621 | -0.2949 | -0.6597 |
| 0.525 | ******* | -0.2871 | -0.1623 | -0.2897 | -0.6676 |
| 0.550 | -0.3616 | -0.2818 | -0.1638 | -0.2970 | -0.6807 |
| 0.575 | ******* | -0.2736 | -0.1701 | -0.3206 | -0.7288 |
| 0.600 | -0.3906 | -0.2499 | -0.2183 | -0.3813 | -0.8054 |
| 0.625 | ******* | ******* | -0.3139 | -0.5035 | -0.9215 |
| 0.650 | -0.3918 | -0.3225 | -0.5529 | -0.6849 | -1.0579 |
| 0.675 | ******* | -0.6861 | -0.8392 | -0.8971 | -1.1527 |
| 0.700 | -0.3632 | -1.0399 | -1.0569 | -1.0736 | -0.7405 |
| 0.725 | ******* | -1.1723 | ******* | -1.1837 | -0.6657 |
| 0.750 | -0.6655 | -1.2049 | ******* | -0.9617 | -0.5991 |
| 0.775 | ******* | -1.2016 | -1.1532 | -0.8491 | -0.5518 |
| 0.800 | -0.9348 | -1.1476 | -1.0542 | -0.8229 | ******* |
| 0.825 | ******* | -1.1030 | -0.9161 | -0.8230 | -0.5219 |
| 0.850 | -1.0071 | -1.0466 | -0.8640 | -0.8272 | -0.5048 |
| 0.875 | ******* | -0.9932 | -0.8487 | -0.7867 | -0.4960 |
| 0.900 | -0.9578 | -0.9511 | -0.8289 | -0.7578 | ******* |
| 0.925 | ******* | -0.9299 | -0.7802 | -0.7539 | -0.4586 |
| 0.950 | -1.0257 | -0.9152 | -0.7544 | -0.7578 | -0.3969 |
| 0.975 | ******* | -0.8987 | -0.7390 | -0.7526 | -0.3614 |
| 1.000 | -0.9841 | -0.9063 | -0.7468 | -0.7379 | -0.3188 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2514 | 0.2393 | 0.2719 | ******* | -0.5887 |
| -0.400 | 0.2508 | 0.2473 | 0.2436 | 0.0687 | -0.6455 |
| -0.600 | 0.2690 | 0.2579 | 0.2362 | 0.1019 | -0.6193 |
| -0.700 | ******* | 0.2628 | 0.2403 | 0.1170 | -0.5984 |
| -0.800 | ******* | ******* | 0.2467 | 0.1409 | -0.5352 |
| -0.850 | ******* | 0.2880 | 0.2523 | 0.1542 | -0.5130 |
| -0.900 | 0.3109 | 0.2905 | 0.2634 | 0.1718 | -0.4809 |
| -0.950 | 0.2998 | 0.1651 | 0.2430 | 0.1839 | -0.1511 |
| -0.975 | ******* | 0.1659 | 0.1723 | 0.1392 | -0.0305 |
| -1.000 | -0.9623 | -0.9026 | -0.7389 | -0.7386 | -0.3164 |



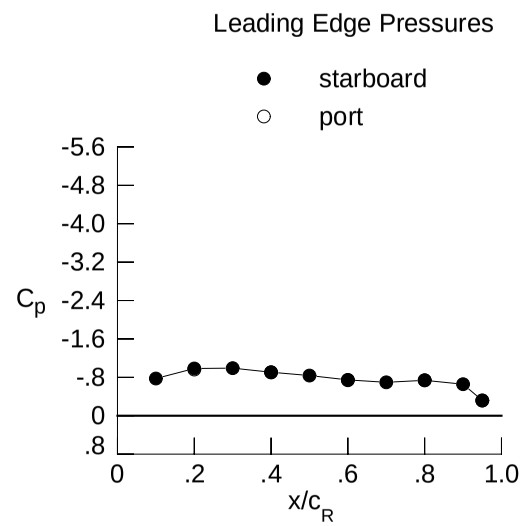

Small Radius L.E.

Run No. = 42 , Point No. = 879

$C_N$ = 0.592, $C_m$ = -0.1062

$\alpha$ = 12.4 °, $M_\infty$ = 0.870

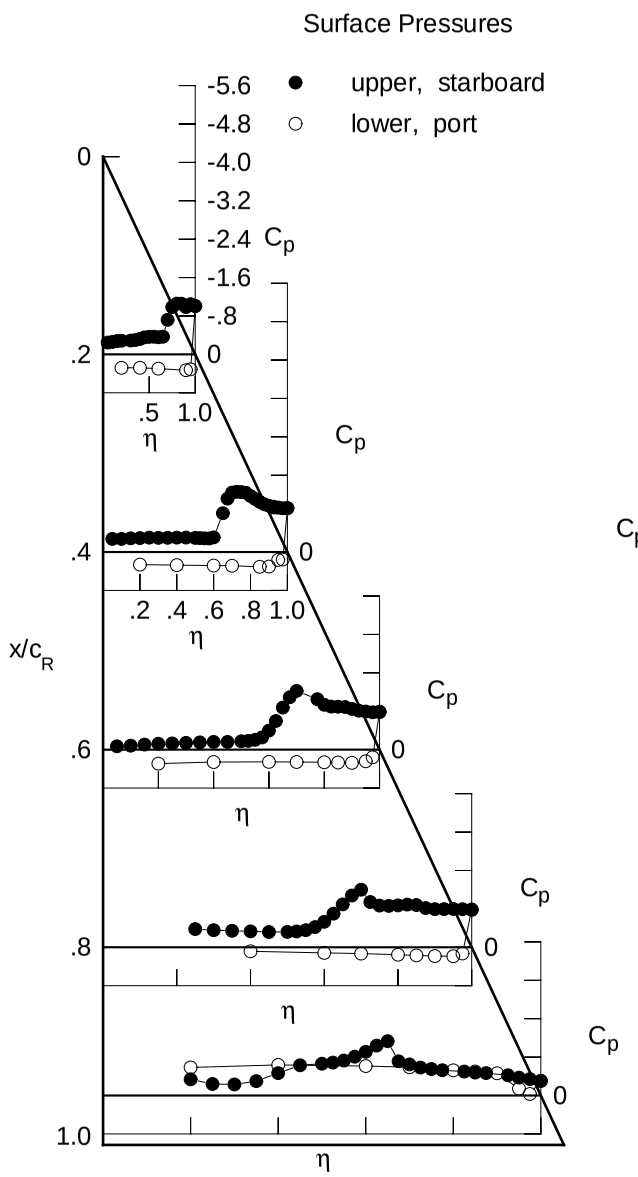
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.7749 | ******* |
| 0.20 | -0.9841 | -0.9623 |
| 0.30 | -0.9916 | ******* |
| 0.40 | -0.9063 | -0.9026 |
| 0.50 | -0.8371 | ******* |
| 0.60 | -0.7468 | -0.7389 |
| 0.70 | -0.6962 | ******* |
| 0.80 | -0.7379 | -0.7386 |
| 0.90 | -0.6564 | ******* |
| 0.95 | -0.3188 | -0.3164 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2476 | -0.2739 | -0.0697 | ******* | ******* |
| 0.100 | -0.2587 | -0.2735 | -0.0827 | ******* | ******* |
| 0.150 | -0.2776 | -0.2855 | -0.1053 | ******* | ******* |
| 0.200 | -0.2845 | -0.2907 | -0.1234 | ******* | -0.3364 |
| 0.250 | ******* | -0.2990 | -0.1298 | -0.3789 | -0.2401 |
| 0.300 | -0.2886 | -0.2957 | -0.1404 | -0.3557 | -0.2305 |
| 0.350 | -0.2981 | -0.2969 | -0.1509 | -0.3440 | -0.2994 |
| 0.400 | -0.3207 | -0.3001 | -0.1612 | -0.3320 | -0.4666 |
| 0.450 | -0.3548 | -0.3018 | -0.1611 | -0.3188 | -0.6296 |
| 0.500 | -0.3656 | -0.2946 | -0.1741 | -0.3200 | -0.6628 |
| 0.525 | ******* | -0.2901 | -0.1823 | -0.3300 | -0.6854 |
| 0.550 | -0.3682 | -0.2850 | -0.2049 | -0.3566 | -0.7278 |
| 0.575 | ******* | -0.2823 | -0.2544 | -0.4205 | -0.8086 |
| 0.600 | -0.3574 | -0.3046 | -0.3978 | -0.5313 | -0.9114 |
| 0.625 | ******* | ******* | -0.5969 | -0.7010 | -1.0404 |
| 0.650 | -0.3683 | -0.8083 | -0.8763 | -0.8935 | -1.1310 |
| 0.675 | ******* | -1.1123 | -1.0913 | -1.0788 | -0.7128 |
| 0.700 | -0.7195 | -1.2392 | -1.2240 | -1.2004 | -0.6481 |
| 0.725 | ******* | -1.2548 | ******* | -0.9435 | -0.5821 |
| 0.750 | -0.9846 | -1.2488 | ******* | -0.8685 | -0.5514 |
| 0.775 | ******* | -1.2353 | -1.0515 | -0.8627 | -0.5267 |
| 0.800 | -1.0583 | -1.1673 | -0.9348 | -0.8724 | ******* |
| 0.825 | ******* | -1.1056 | -0.8972 | -0.8892 | -0.4990 |
| 0.850 | -1.0568 | -1.0445 | -0.8942 | -0.8798 | -0.4775 |
| 0.875 | ******* | -0.9952 | -0.8887 | -0.8175 | -0.4668 |
| 0.900 | -0.9840 | -0.9628 | -0.8491 | -0.7941 | ******* |
| 0.925 | ******* | -0.9440 | -0.8117 | -0.7953 | -0.4218 |
| 0.950 | -1.0462 | -0.9269 | -0.7942 | -0.7986 | -0.3727 |
| 0.975 | ******* | -0.9121 | -0.7777 | -0.7926 | -0.3424 |
| 1.000 | -1.0091 | -0.9177 | -0.7813 | -0.7795 | -0.3028 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2796 | 0.2618 | 0.2910 | ******* | -0.5849 |
| -0.400 | 0.2793 | 0.2730 | 0.2582 | 0.0837 | -0.6372 |
| -0.600 | 0.2965 | 0.2812 | 0.2551 | 0.1168 | -0.6135 |
| -0.700 | ******* | 0.2854 | 0.2575 | 0.1310 | -0.5894 |
| -0.800 | ******* | ******* | 0.2629 | 0.1545 | -0.5248 |
| -0.850 | ******* | 0.3075 | 0.2682 | 0.1688 | -0.5001 |
| -0.900 | 0.3300 | 0.3024 | 0.2748 | 0.1835 | -0.4636 |
| -0.950 | 0.3108 | 0.1644 | 0.2425 | 0.1854 | -0.1436 |
| -0.975 | ******* | 0.1559 | 0.1592 | 0.1292 | -0.0318 |
| -1.000 | -1.0041 | -0.9097 | -0.7914 | -0.7880 | -0.3068 |



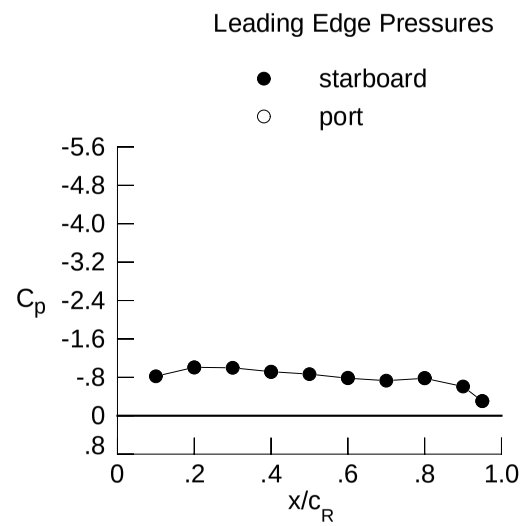

Small Radius L.E.

Run No. = 42 , Point No. = 880

$C_N$ = 0.647, $C_m$ = -0.1153

$\alpha$ = 13.5 °, $M_\infty$ = 0.870

$R_{mac}$ = $6.0 \times 10^6$

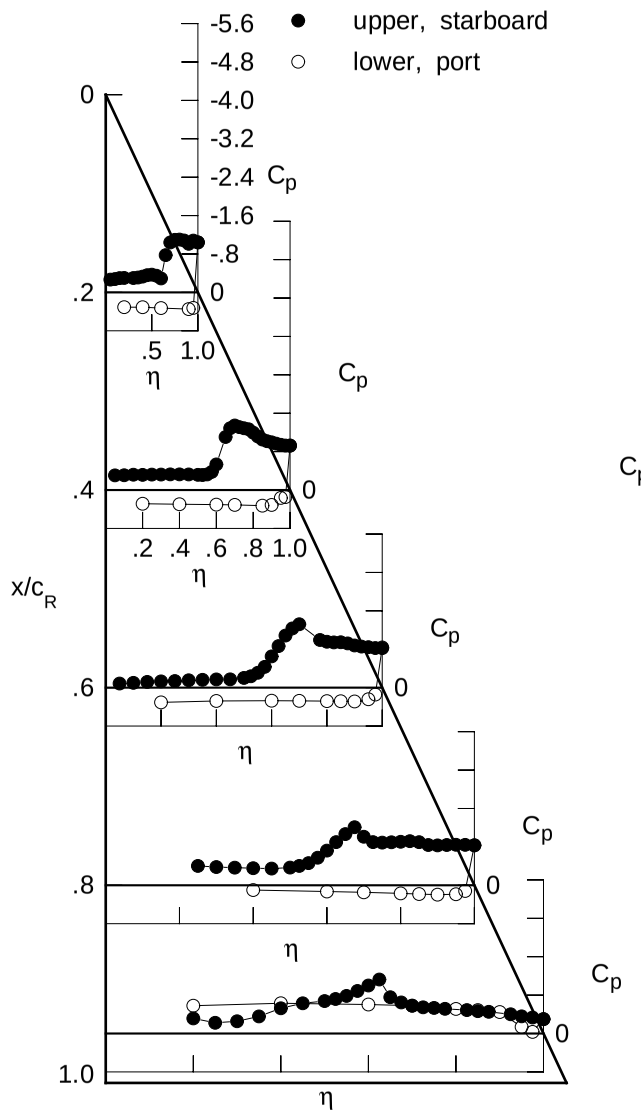



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.8218 | ******* |
| 0.20 | -1.0091 | -1.0041 |
| 0.30 | -0.9982 | ******* |
| 0.40 | -0.9177 | -0.9097 |
| 0.50 | -0.8664 | ******* |
| 0.60 | -0.7813 | -0.7914 |
| 0.70 | -0.7308 | ******* |
| 0.80 | -0.7795 | -0.7880 |
| 0.90 | -0.6085 | ******* |
| 0.95 | -0.3028 | -0.3068 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2667 | -0.3052 | -0.0855 | ******* | ******* |
| 0.100 | -0.2779 | -0.3078 | -0.1002 | ******* | ******* |
| 0.150 | -0.2972 | -0.3191 | -0.1190 | ******* | ******* |
| 0.200 | -0.3005 | -0.3161 | -0.1306 | ******* | -0.3148 |
| 0.250 | ******* | -0.3212 | -0.1376 | -0.4036 | -0.2232 |
| 0.300 | -0.2993 | -0.3222 | -0.1534 | -0.3802 | -0.2550 |
| 0.350 | -0.3097 | -0.3260 | -0.1632 | -0.3671 | -0.3560 |
| 0.400 | -0.3290 | -0.3262 | -0.1710 | -0.3559 | -0.5259 |
| 0.450 | -0.3586 | -0.3244 | -0.1725 | -0.3480 | -0.6298 |
| 0.500 | -0.3695 | -0.3165 | -0.2028 | -0.3688 | -0.6763 |
| 0.525 | ******* | -0.3126 | -0.2371 | -0.4030 | -0.7192 |
| 0.550 | -0.3469 | -0.3246 | -0.3093 | -0.4619 | -0.7832 |
| 0.575 | ******* | -0.3774 | -0.4324 | -0.5740 | -0.8865 |
| 0.600 | -0.2908 | -0.5332 | -0.6511 | -0.7225 | -1.0000 |
| 0.625 | ******* | ******* | -0.8659 | -0.8991 | -1.1252 |
| 0.650 | -0.7761 | -1.1049 | -1.0845 | -1.0665 | -0.7558 |
| 0.675 | ******* | -1.2872 | -1.2333 | -1.2098 | -0.6473 |
| 0.700 | -1.0403 | -1.3447 | -1.3211 | -1.0111 | -0.5796 |
| 0.725 | ******* | -1.3102 | ******* | -0.8990 | -0.5455 |
| 0.750 | -1.0949 | -1.2876 | ******* | -0.8887 | -0.5330 |
| 0.775 | ******* | -1.2667 | -0.9925 | -0.8957 | -0.5145 |
| 0.800 | -1.1007 | -1.1964 | -0.9562 | -0.9067 | ******* |
| 0.825 | ******* | -1.1168 | -0.9424 | -0.9195 | -0.4877 |
| 0.850 | -1.0818 | -1.0520 | -0.9454 | -0.8984 | -0.4653 |
| 0.875 | ******* | -1.0174 | -0.9217 | -0.8394 | -0.4517 |
| 0.900 | -1.0121 | -0.9942 | -0.8781 | -0.8311 | ******* |
| 0.925 | ******* | -0.9664 | -0.8551 | -0.8389 | -0.4006 |
| 0.950 | -1.0792 | -0.9425 | -0.8431 | -0.8441 | -0.3578 |
| 0.975 | ******* | -0.9275 | -0.8245 | -0.8424 | -0.3337 |
| 1.000 | -1.0399 | -0.9280 | -0.8236 | -0.8308 | -0.2979 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3080 | 0.2853 | 0.3069 | ******* | -0.5793 |
| -0.400 | 0.3091 | 0.2960 | 0.2778 | 0.0995 | -0.6302 |
| -0.600 | 0.3265 | 0.3036 | 0.2721 | 0.1299 | -0.6038 |
| -0.700 | ******* | 0.3095 | 0.2755 | 0.1466 | -0.5799 |
| -0.800 | ******* | ******* | 0.2810 | 0.1687 | -0.5117 |
| -0.850 | ******* | 0.3257 | 0.2834 | 0.1828 | -0.4876 |
| -0.900 | 0.3484 | 0.3101 | 0.2879 | 0.1952 | -0.4475 |
| -0.950 | 0.3230 | 0.1643 | 0.2412 | 0.1866 | -0.1371 |
| -0.975 | ******* | 0.1462 | 0.1442 | 0.1184 | -0.0339 |
| -1.000 | -1.0434 | -0.9235 | -0.8373 | -0.8344 | -0.3017 |

Surface Pressures




Small Radius L.E.

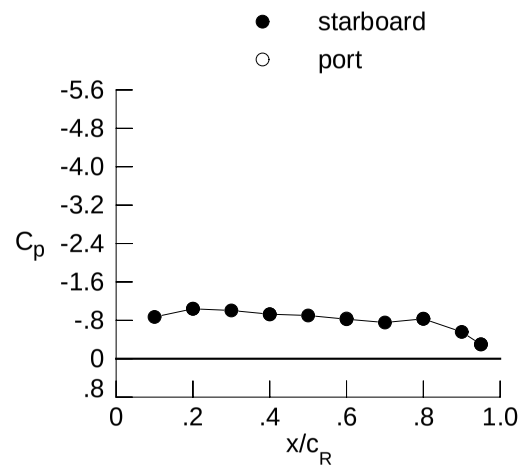
Run No. = 42 , Point No. = 881

$C_N$ = 0.699, $C_m$ = -0.1223

$\alpha$ = 14.5 °, $M_\infty$ = 0.870

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

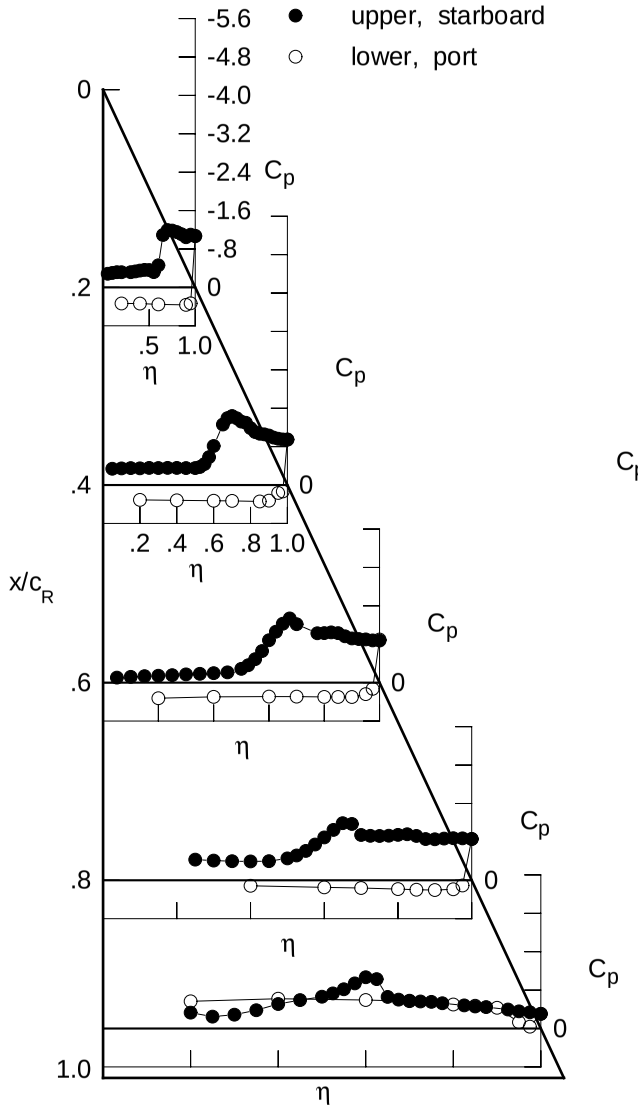



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.8700 | ******* |
| 0.20 | -1.0399 | -1.0434 |
| 0.30 | -1.0054 | ******* |
| 0.40 | -0.9280 | -0.9235 |
| 0.50 | -0.9008 | ******* |
| 0.60 | -0.8236 | -0.8373 |
| 0.70 | -0.7544 | ******* |
| 0.80 | -0.8308 | -0.8344 |
| 0.90 | -0.5582 | ******* |
| 0.95 | -0.2979 | -0.3017 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2844 | -0.3388 | -0.1045 | ******* | ******* |
| 0.100 | -0.3009 | -0.3467 | -0.1208 | ******* | ******* |
| 0.150 | -0.3165 | -0.3524 | -0.1353 | ******* | ******* |
| 0.200 | -0.3157 | -0.3483 | -0.1442 | ******* | -0.3305 |
| 0.250 | ******* | -0.3569 | -0.1559 | -0.4304 | -0.2473 |
| 0.300 | -0.3167 | -0.3542 | -0.1724 | -0.4105 | -0.2879 |
| 0.350 | -0.3327 | -0.3578 | -0.1840 | -0.3975 | -0.3812 |
| 0.400 | -0.3504 | -0.3568 | -0.1978 | -0.3926 | -0.5106 |
| 0.450 | -0.3644 | -0.3537 | -0.2147 | -0.3986 | -0.5916 |
| 0.500 | -0.3614 | -0.3539 | -0.2875 | -0.4559 | -0.6628 |
| 0.525 | ******* | -0.3763 | -0.3630 | -0.5170 | -0.7313 |
| 0.550 | -0.3186 | -0.4368 | -0.4886 | -0.6120 | -0.8173 |
| 0.575 | ******* | -0.5814 | -0.6585 | -0.7445 | -0.9397 |
| 0.600 | -0.4610 | -0.8136 | -0.8833 | -0.8931 | -1.0679 |
| 0.625 | ******* | ******* | -1.0608 | -1.0497 | -1.0284 |
| 0.650 | -1.0921 | -1.2608 | -1.2275 | -1.1892 | -0.6586 |
| 0.675 | ******* | -1.3944 | -1.3376 | -1.1737 | -0.6020 |
| 0.700 | -1.1947 | -1.4376 | -1.2176 | -0.9437 | -0.5791 |
| 0.725 | ******* | -1.3910 | ******* | -0.9266 | -0.5629 |
| 0.750 | -1.1836 | -1.3217 | ******* | -0.9229 | -0.5554 |
| 0.775 | ******* | -1.2967 | -1.0289 | -0.9291 | -0.5264 |
| 0.800 | -1.1530 | -1.1859 | -1.0322 | -0.9461 | ******* |
| 0.825 | ******* | -1.1041 | -1.0472 | -0.9592 | -0.4815 |
| 0.850 | -1.1092 | -1.0684 | -1.0313 | -0.9242 | -0.4592 |
| 0.875 | ******* | -1.0558 | -0.9655 | -0.8590 | -0.4462 |
| 0.900 | -1.0447 | -1.0309 | -0.9208 | -0.8548 | ******* |
| 0.925 | ******* | -0.9892 | -0.9079 | -0.8685 | -0.3962 |
| 0.950 | -1.0986 | -0.9650 | -0.9008 | -0.8766 | -0.3578 |
| 0.975 | ******* | -0.9500 | -0.8802 | -0.8735 | -0.3387 |
| 1.000 | -1.0653 | -0.9495 | -0.8766 | -0.8616 | -0.3065 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3350 | 0.3097 | 0.3244 | ******* | -0.5666 |
| -0.400 | 0.3365 | 0.3187 | 0.2959 | 0.1147 | -0.6205 |
| -0.600 | 0.3544 | 0.3270 | 0.2906 | 0.1475 | -0.5935 |
| -0.700 | ******* | 0.3303 | 0.2912 | 0.1611 | -0.5694 |
| -0.800 | ******* | ******* | 0.2976 | 0.1832 | -0.4999 |
| -0.850 | ******* | 0.3422 | 0.2988 | 0.1968 | -0.4742 |
| -0.900 | 0.3643 | 0.3254 | 0.2995 | 0.2036 | -0.4321 |
| -0.950 | 0.3321 | 0.1652 | 0.2390 | 0.1871 | -0.1322 |
| -0.975 | ******* | 0.1335 | 0.1292 | 0.1078 | -0.0384 |
| -1.000 | -1.0756 | -0.9450 | -0.8984 | -0.8592 | -0.3057 |

Surface Pressures




Small Radius L.E.

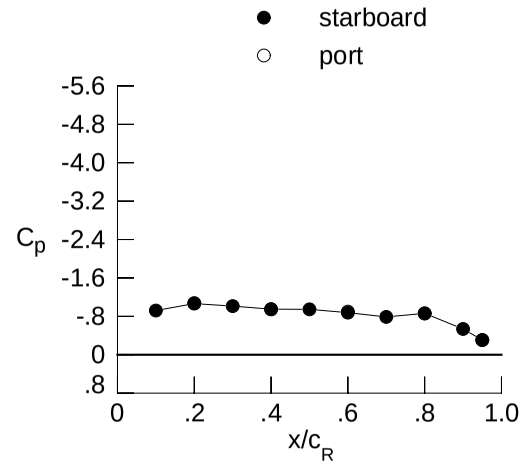
Run No. = 42 , Point No. = 882

$C_N$ = 0.752, $C_m$ = -0.1294

$\alpha$ = 15.5 °, $M_\infty$ = 0.870

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

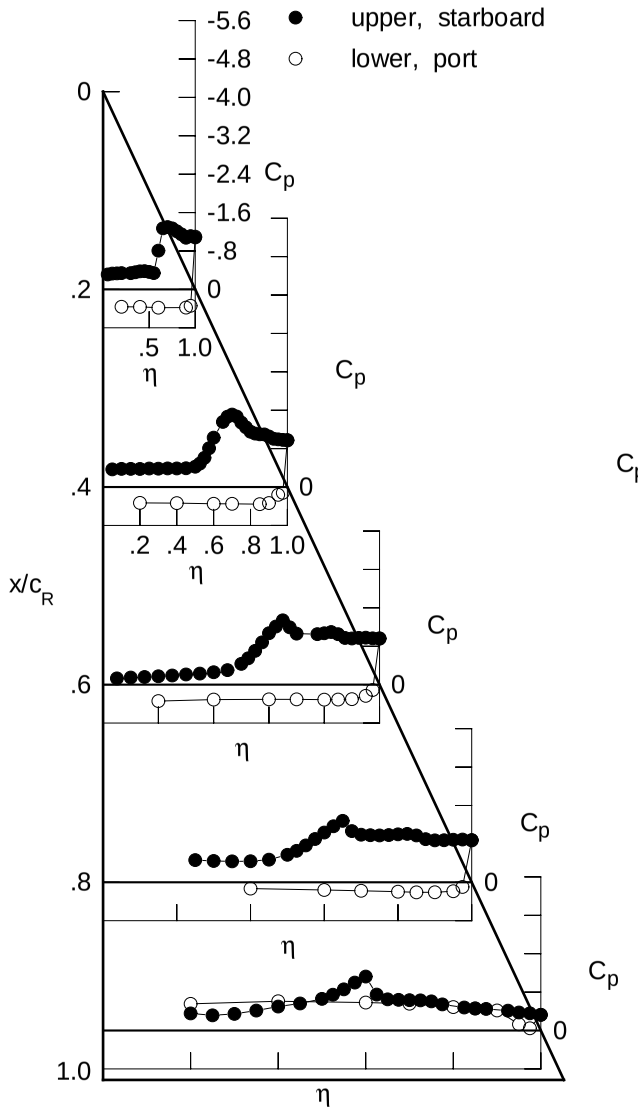



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.9208 | ******* |
| 0.20 | -1.0653 | -1.0756 |
| 0.30 | -1.0132 | ******* |
| 0.40 | -0.9495 | -0.9450 |
| 0.50 | -0.9457 | ******* |
| 0.60 | -0.8766 | -0.8984 |
| 0.70 | -0.7879 | ******* |
| 0.80 | -0.8616 | -0.8592 |
| 0.90 | -0.5369 | ******* |
| 0.95 | -0.3065 | -0.3057 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3116 | -0.3679 | -0.1301 | ******* | ******* |
| 0.100 | -0.3293 | -0.3786 | -0.1478 | ******* | ******* |
| 0.150 | -0.3338 | -0.3785 | -0.1592 | ******* | ******* |
| 0.200 | -0.3392 | -0.3770 | -0.1741 | ******* | -0.3564 |
| 0.250 | ******* | -0.3858 | -0.1903 | -0.4624 | -0.3164 |
| 0.300 | -0.3385 | -0.3823 | -0.2119 | -0.4436 | -0.3465 |
| 0.350 | -0.3570 | -0.3876 | -0.2301 | -0.4357 | -0.4156 |
| 0.400 | -0.3758 | -0.3869 | -0.2585 | -0.4386 | -0.4990 |
| 0.450 | -0.3802 | -0.3913 | -0.3025 | -0.4715 | -0.5633 |
| 0.500 | -0.3642 | -0.4229 | -0.4332 | -0.5725 | -0.6594 |
| 0.525 | ******* | -0.4891 | -0.5489 | -0.6549 | -0.7455 |
| 0.550 | -0.3403 | -0.6088 | -0.7040 | -0.7682 | -0.8580 |
| 0.575 | ******* | -0.8083 | -0.8808 | -0.9015 | -0.9980 |
| 0.600 | -0.8069 | -1.0288 | -1.0715 | -1.0359 | -1.1238 |
| 0.625 | ******* | ******* | -1.2102 | -1.1672 | -0.7486 |
| 0.650 | -1.2717 | -1.3567 | -1.3404 | -1.2800 | -0.6500 |
| 0.675 | ******* | -1.4658 | -1.1943 | -1.0667 | -0.6391 |
| 0.700 | -1.2984 | -1.5094 | -1.0625 | -0.9909 | -0.6319 |
| 0.725 | ******* | -1.4684 | ******* | -0.9811 | -0.6280 |
| 0.750 | -1.2710 | -1.3429 | ******* | -0.9761 | -0.6074 |
| 0.775 | ******* | -1.2448 | -1.0519 | -0.9842 | -0.5437 |
| 0.800 | -1.2102 | -1.1520 | -1.0704 | -0.9994 | ******* |
| 0.825 | ******* | -1.1136 | -1.0957 | -1.0079 | -0.4792 |
| 0.850 | -1.1474 | -1.0987 | -1.0513 | -0.9762 | -0.4563 |
| 0.875 | ******* | -1.0956 | -0.9726 | -0.8980 | -0.4494 |
| 0.900 | -1.0761 | -1.0531 | -0.9619 | -0.8738 | ******* |
| 0.925 | ******* | -1.0057 | -0.9744 | -0.8759 | -0.4137 |
| 0.950 | -1.1098 | -0.9932 | -0.9785 | -0.8861 | -0.3749 |
| 0.975 | ******* | -0.9825 | -0.9650 | -0.8908 | -0.3586 |
| 1.000 | -1.0824 | -0.9787 | -0.9573 | -0.8800 | -0.3261 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3622 | 0.3304 | 0.3424 | ******* | -0.5555 |
| -0.400 | 0.3646 | 0.3353 | 0.3114 | 0.1311 | -0.6093 |
| -0.600 | 0.3812 | 0.3486 | 0.3066 | 0.1604 | -0.5826 |
| -0.700 | ******* | 0.3497 | 0.3068 | 0.1770 | -0.5586 |
| -0.800 | ******* | ******* | 0.3127 | 0.1956 | -0.4877 |
| -0.850 | ******* | 0.3570 | 0.3105 | 0.2092 | -0.4621 |
| -0.900 | 0.3790 | 0.3340 | 0.3026 | 0.2083 | -0.4180 |
| -0.950 | 0.3412 | 0.1625 | 0.2333 | 0.1865 | -0.1298 |
| -0.975 | ******* | 0.1205 | 0.1119 | 0.0965 | -0.0467 |
| -1.000 | -1.0983 | -0.9698 | -0.9645 | -0.8721 | -0.3269 |

Surface Pressures




Small Radius L.E.

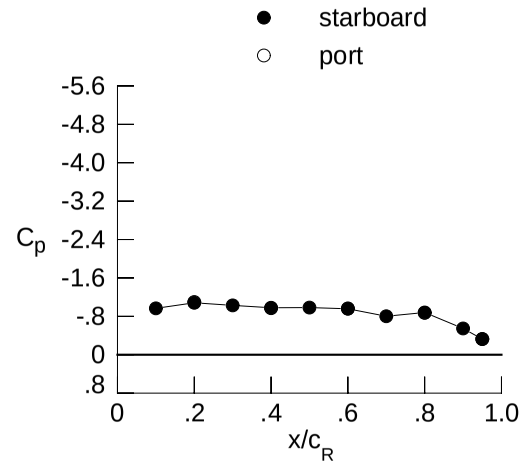
Run No. = 42 , Point No. = 883

$C_N$ = 0.820, $C_m$ = -0.1471

$\alpha$ = 16.5 °, $M_\infty$ = 0.870

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

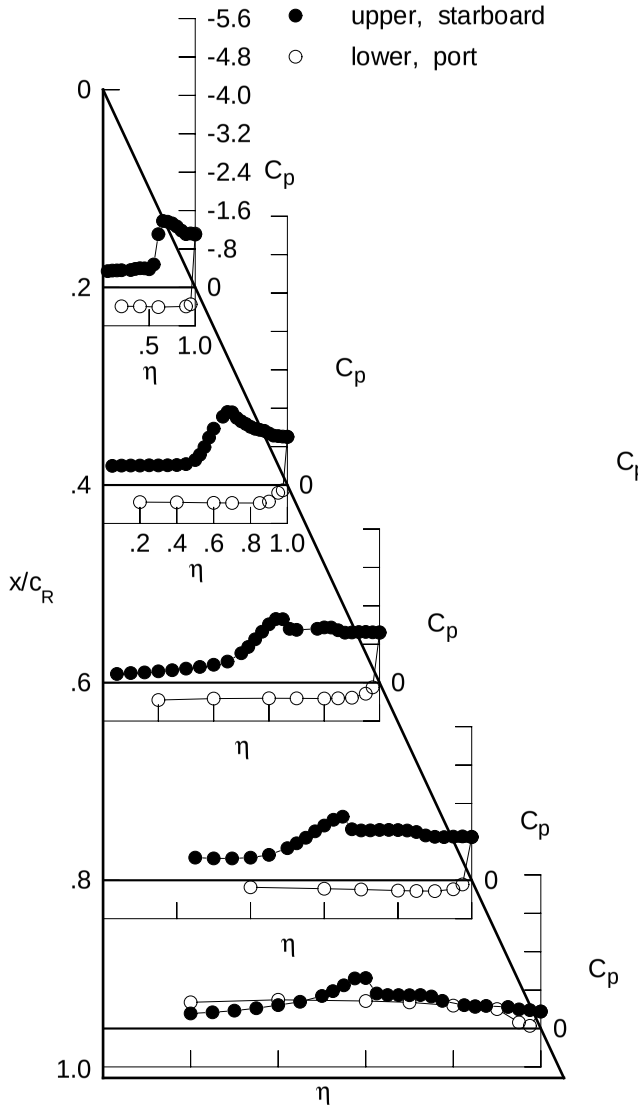



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.9665 | ******* |
| 0.20 | -1.0824 | -1.0983 |
| 0.30 | -1.0281 | ******* |
| 0.40 | -0.9787 | -0.9698 |
| 0.50 | -0.9823 | ******* |
| 0.60 | -0.9573 | -0.9645 |
| 0.70 | -0.8017 | ******* |
| 0.80 | -0.8800 | -0.8721 |
| 0.90 | -0.5471 | ******* |
| 0.95 | -0.3261 | -0.3269 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3383 | -0.3995 | -0.1805 | ******* | ******* |
| 0.100 | -0.3502 | -0.4051 | -0.2002 | ******* | ******* |
| 0.150 | -0.3540 | -0.4067 | -0.2131 | ******* | ******* |
| 0.200 | -0.3576 | -0.4058 | -0.2363 | ******* | -0.3138 |
| 0.250 | ******* | -0.4112 | -0.2591 | -0.4722 | -0.3377 |
| 0.300 | -0.3620 | -0.4087 | -0.2923 | -0.4564 | -0.3716 |
| 0.350 | -0.3846 | -0.4118 | -0.3274 | -0.4550 | -0.4223 |
| 0.400 | -0.3991 | -0.4166 | -0.3732 | -0.4715 | -0.4870 |
| 0.450 | -0.3965 | -0.4357 | -0.4393 | -0.5295 | -0.5566 |
| 0.500 | -0.3786 | -0.5211 | -0.6128 | -0.6692 | -0.6778 |
| 0.525 | ******* | -0.6300 | -0.7433 | -0.7703 | -0.7780 |
| 0.550 | -0.4774 | -0.7903 | -0.9028 | -0.8867 | -0.9003 |
| 0.575 | ******* | -0.9895 | -1.0605 | -1.0197 | -1.0432 |
| 0.600 | -1.1089 | -1.1744 | -1.2150 | -1.1397 | -1.0516 |
| 0.625 | ******* | ******* | -1.3256 | -1.2610 | -0.7300 |
| 0.650 | -1.3839 | -1.4238 | -1.3216 | -1.3247 | -0.6968 |
| 0.675 | ******* | -1.5218 | -1.1210 | -1.0629 | -0.6957 |
| 0.700 | -1.3678 | -1.5154 | -1.0999 | -1.0388 | -0.6934 |
| 0.725 | ******* | -1.3996 | ******* | -1.0399 | -0.6971 |
| 0.750 | -1.3325 | -1.3270 | ******* | -1.0486 | -0.6675 |
| 0.775 | ******* | -1.2721 | -1.1213 | -1.0496 | -0.5763 |
| 0.800 | -1.2688 | -1.2126 | -1.1506 | -1.0467 | ******* |
| 0.825 | ******* | -1.1722 | -1.1478 | -1.0364 | -0.4865 |
| 0.850 | -1.1835 | -1.1496 | -1.0920 | -1.0053 | -0.4645 |
| 0.875 | ******* | -1.1287 | -1.0409 | -0.9337 | -0.4705 |
| 0.900 | -1.1096 | -1.0744 | -1.0460 | -0.9055 | ******* |
| 0.925 | ******* | -1.0293 | -1.0547 | -0.8993 | -0.4489 |
| 0.950 | -1.1242 | -1.0201 | -1.0567 | -0.9096 | -0.3984 |
| 0.975 | ******* | -1.0100 | -1.0487 | -0.9144 | -0.3829 |
| 1.000 | -1.1008 | -1.0070 | -1.0493 | -0.9064 | -0.3533 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3948 | 0.3562 | 0.3624 | ******* | -0.5459 |
| -0.400 | 0.3948 | 0.3605 | 0.3323 | 0.1458 | -0.5981 |
| -0.600 | 0.4106 | 0.3714 | 0.3253 | 0.1757 | -0.5728 |
| -0.700 | ******* | 0.3737 | 0.3272 | 0.1921 | -0.5450 |
| -0.800 | ******* | ******* | 0.3311 | 0.2140 | -0.4767 |
| -0.850 | ******* | 0.3749 | 0.3263 | 0.2230 | -0.4502 |
| -0.900 | 0.3962 | 0.3446 | 0.3134 | 0.2254 | -0.4049 |
| -0.950 | 0.3518 | 0.1615 | 0.2306 | 0.1874 | -0.1269 |
| -0.975 | ******* | 0.1094 | 0.0974 | 0.0865 | -0.0552 |
| -1.000 | -1.1192 | -0.9998 | -1.0377 | -0.8973 | -0.3545 |

Surface Pressures




Small Radius L.E.

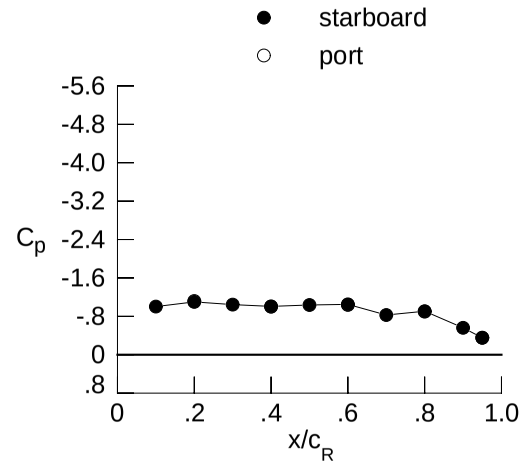
Run No. = 42 , Point No. = 884

$C_N$ = 0.884, $C_m$ = -0.1639

$\alpha$ = 17.6 °, $M_\infty$ = 0.869

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

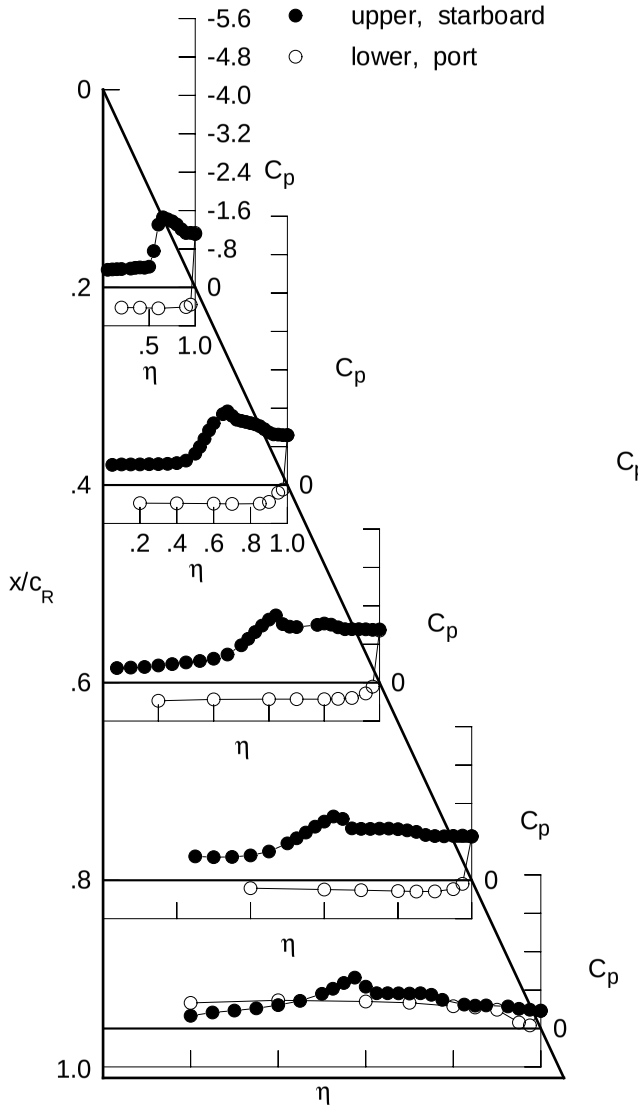



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0030 | ******* |
| 0.20 | -1.1008 | -1.1192 |
| 0.30 | -1.0442 | ******* |
| 0.40 | -1.0070 | -0.9998 |
| 0.50 | -1.0363 | ******* |
| 0.60 | -1.0493 | -1.0377 |
| 0.70 | -0.8273 | ******* |
| 0.80 | -0.9064 | -0.8973 |
| 0.90 | -0.5608 | ******* |
| 0.95 | -0.3533 | -0.3545 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3664 | -0.4197 | -0.3042 | ******* | ******* |
| 0.100 | -0.3747 | -0.4286 | -0.3140 | ******* | ******* |
| 0.150 | -0.3794 | -0.4291 | -0.3263 | ******* | ******* |
| 0.200 | -0.3828 | -0.4292 | -0.3574 | ******* | -0.2647 |
| 0.250 | ******* | -0.4347 | -0.3865 | -0.4974 | -0.3339 |
| 0.300 | -0.3908 | -0.4361 | -0.4209 | -0.4818 | -0.3732 |
| 0.350 | -0.4076 | -0.4419 | -0.4514 | -0.4860 | -0.4201 |
| 0.400 | -0.4155 | -0.4571 | -0.4982 | -0.5172 | -0.4875 |
| 0.450 | -0.4100 | -0.5089 | -0.5856 | -0.5991 | -0.5759 |
| 0.500 | -0.4313 | -0.6532 | -0.7788 | -0.7692 | -0.7226 |
| 0.525 | ******* | -0.7947 | -0.9125 | -0.8754 | -0.8276 |
| 0.550 | -0.7575 | -0.9601 | -1.0533 | -0.9945 | -0.9487 |
| 0.575 | ******* | -1.1386 | -1.1881 | -1.1166 | -1.0599 |
| 0.600 | -1.3077 | -1.2867 | -1.3130 | -1.2227 | -0.8712 |
| 0.625 | ******* | ******* | -1.4008 | -1.3290 | -0.7350 |
| 0.650 | -1.4599 | -1.4767 | -1.2195 | -1.2786 | -0.7355 |
| 0.675 | ******* | -1.5344 | -1.1652 | -1.0813 | -0.7330 |
| 0.700 | -1.4185 | -1.4420 | -1.1575 | -1.0715 | -0.7278 |
| 0.725 | ******* | -1.3612 | ******* | -1.0706 | -0.7346 |
| 0.750 | -1.3762 | -1.3363 | ******* | -1.0761 | -0.7020 |
| 0.775 | ******* | -1.3144 | -1.2029 | -1.0770 | -0.5972 |
| 0.800 | -1.3098 | -1.2892 | -1.2309 | -1.0650 | ******* |
| 0.825 | ******* | -1.2657 | -1.2083 | -1.0397 | -0.4983 |
| 0.850 | -1.2101 | -1.2258 | -1.1525 | -1.0083 | -0.4760 |
| 0.875 | ******* | -1.1635 | -1.1134 | -0.9439 | -0.4807 |
| 0.900 | -1.1329 | -1.0943 | -1.1146 | -0.9219 | ******* |
| 0.925 | ******* | -1.0564 | -1.1137 | -0.9164 | -0.4598 |
| 0.950 | -1.1359 | -1.0502 | -1.1113 | -0.9249 | -0.4107 |
| 0.975 | ******* | -1.0400 | -1.1000 | -0.9310 | -0.3910 |
| 1.000 | -1.1120 | -1.0408 | -1.1083 | -0.9210 | -0.3654 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4207 | 0.3777 | 0.3779 | ******* | -0.5333 |
| -0.400 | 0.4223 | 0.3816 | 0.3495 | 0.1647 | -0.5878 |
| -0.600 | 0.4363 | 0.3872 | 0.3442 | 0.1929 | -0.5628 |
| -0.700 | ******* | 0.3936 | 0.3437 | 0.2068 | -0.5358 |
| -0.800 | ******* | ******* | 0.3452 | 0.2239 | -0.4640 |
| -0.850 | ******* | 0.3879 | 0.3374 | 0.2342 | -0.4380 |
| -0.900 | 0.4097 | 0.3516 | 0.3192 | 0.2317 | -0.3909 |
| -0.950 | 0.3591 | 0.1593 | 0.2250 | 0.1844 | -0.1255 |
| -0.975 | ******* | 0.0949 | 0.0826 | 0.0745 | -0.0644 |
| -1.000 | -1.1343 | -1.0358 | -1.0837 | -0.9082 | -0.3740 |

Surface Pressures




Small Radius L.E.

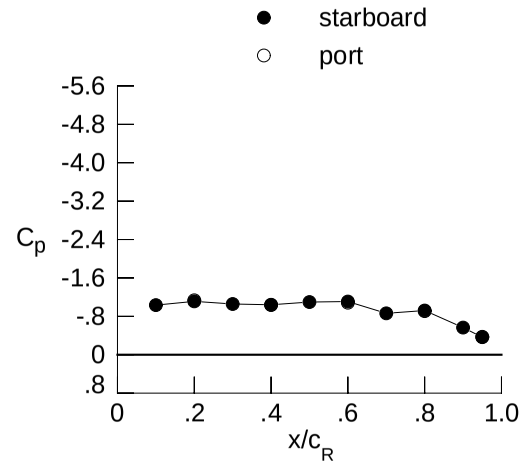
Run No. = 42 , Point No. = 885

$C_N$ = 0.946, $C_m$ = -0.1777

$\alpha$ = 18.6 °, $M_\infty$ = 0.870

$R_{mac}$ = $6.0 \times 10^6$

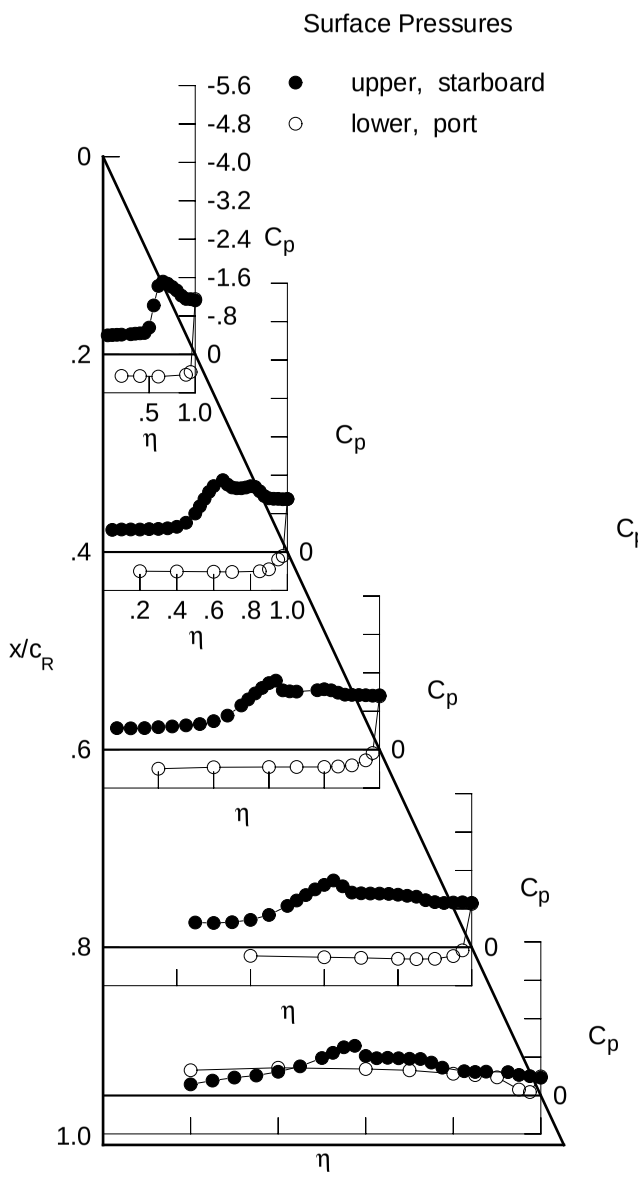
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0335 | ******* |
| 0.20 | -1.1120 | -1.1343 |
| 0.30 | -1.0570 | ******* |
| 0.40 | -1.0408 | -1.0358 |
| 0.50 | -1.0976 | ******* |
| 0.60 | -1.1083 | -1.0837 |
| 0.70 | -0.8625 | ******* |
| 0.80 | -0.9210 | -0.9082 |
| 0.90 | -0.5655 | ******* |
| 0.95 | -0.3654 | -0.3740 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3970 | -0.4620 | -0.4482 | ******* | ******* |
| 0.100 | -0.4031 | -0.4695 | -0.4436 | ******* | ******* |
| 0.150 | -0.4077 | -0.4704 | -0.4487 | ******* | ******* |
| 0.200 | -0.4112 | -0.4689 | -0.4681 | ******* | -0.2324 |
| 0.250 | ******* | -0.4780 | -0.4829 | -0.5158 | -0.3105 |
| 0.300 | -0.4200 | -0.4819 | -0.5059 | -0.5061 | -0.3736 |
| 0.350 | -0.4310 | -0.4945 | -0.5325 | -0.5221 | -0.4163 |
| 0.400 | -0.4382 | -0.5258 | -0.5938 | -0.5707 | -0.4944 |
| 0.450 | -0.4464 | -0.6104 | -0.7091 | -0.6737 | -0.6069 |
| 0.500 | -0.5581 | -0.8026 | -0.9202 | -0.8618 | -0.7805 |
| 0.525 | ******* | -0.9521 | -1.0463 | -0.9746 | -0.8889 |
| 0.550 | -1.0199 | -1.1044 | -1.1703 | -1.0883 | -1.0052 |
| 0.575 | ******* | -1.2525 | -1.2850 | -1.2062 | -1.0355 |
| 0.600 | -1.4259 | -1.3739 | -1.3866 | -1.2998 | -0.8239 |
| 0.625 | ******* | ******* | -1.4376 | -1.3924 | -0.7765 |
| 0.650 | -1.5158 | -1.4972 | -1.2355 | -1.2704 | -0.7858 |
| 0.675 | ******* | -1.4063 | -1.2146 | -1.1396 | -0.7762 |
| 0.700 | -1.4725 | -1.3455 | -1.2091 | -1.1248 | -0.7653 |
| 0.725 | ******* | -1.3287 | ******* | -1.1196 | -0.7608 |
| 0.750 | -1.4049 | -1.3286 | ******* | -1.1187 | -0.6858 |
| 0.775 | ******* | -1.3446 | -1.2373 | -1.1118 | -0.5798 |
| 0.800 | -1.3310 | -1.3708 | -1.2583 | -1.0950 | ******* |
| 0.825 | ******* | -1.3558 | -1.2361 | -1.0729 | -0.5063 |
| 0.850 | -1.2237 | -1.2656 | -1.1867 | -1.0532 | -0.4905 |
| 0.875 | ******* | -1.1663 | -1.1447 | -0.9814 | -0.4971 |
| 0.900 | -1.1559 | -1.1188 | -1.1410 | -0.9412 | ******* |
| 0.925 | ******* | -1.1093 | -1.1376 | -0.9223 | -0.4869 |
| 0.950 | -1.1503 | -1.1077 | -1.1334 | -0.9323 | -0.4288 |
| 0.975 | ******* | -1.1000 | -1.1243 | -0.9364 | -0.4034 |
| 1.000 | -1.1260 | -1.1032 | -1.1322 | -0.9255 | -0.3716 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4489 | 0.3996 | 0.3975 | ******* | -0.5266 |
| -0.400 | 0.4511 | 0.4050 | 0.3675 | 0.1787 | -0.5780 |
| -0.600 | 0.4628 | 0.4106 | 0.3623 | 0.2075 | -0.5520 |
| -0.700 | ******* | 0.4148 | 0.3615 | 0.2201 | -0.5250 |
| -0.800 | ******* | ******* | 0.3611 | 0.2399 | -0.4539 |
| -0.850 | ******* | 0.4011 | 0.3509 | 0.2467 | -0.4251 |
| -0.900 | 0.4249 | 0.3589 | 0.3274 | 0.2407 | -0.3784 |
| -0.950 | 0.3669 | 0.1542 | 0.2226 | 0.1832 | -0.1237 |
| -0.975 | ******* | 0.0822 | 0.0704 | 0.0641 | -0.0720 |
| -1.000 | -1.1520 | -1.1044 | -1.1097 | -0.9041 | -0.3967 |



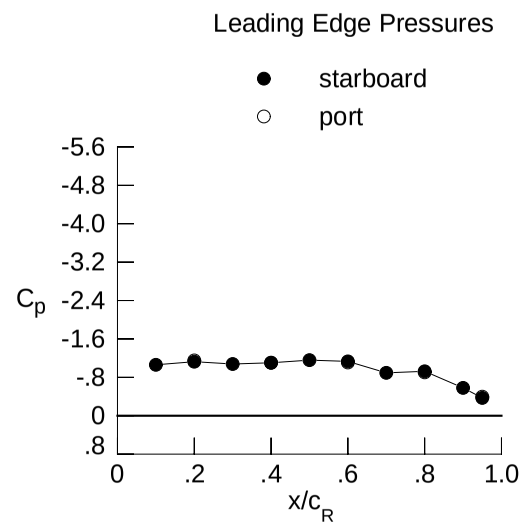

Small Radius L.E.

Run No. = 42 , Point No. = 886

$C_N$ = 1.001, $C_m$ = -0.1882

$\alpha$ = 19.6 °, $M_\infty$ = 0.869

$R_{mac}$ = $6.0 \times 10^6$

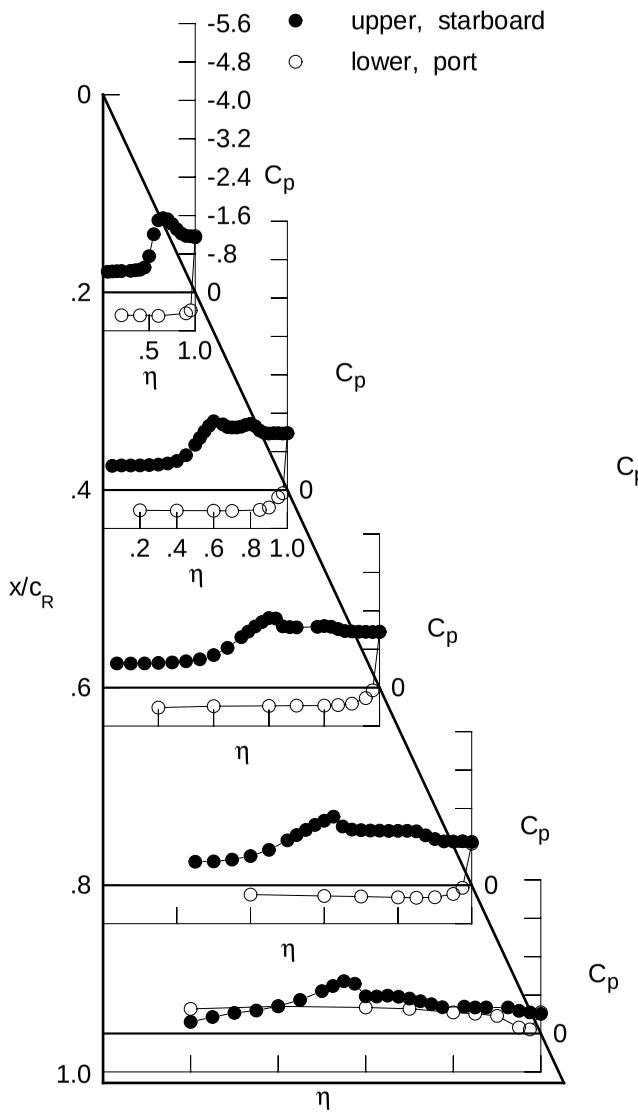



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0611 | ******* |
| 0.20 | -1.1260 | -1.1520 |
| 0.30 | -1.0775 | ******* |
| 0.40 | -1.1032 | -1.1044 |
| 0.50 | -1.1583 | ******* |
| 0.60 | -1.1322 | -1.1097 |
| 0.70 | -0.8932 | ******* |
| 0.80 | -0.9255 | -0.9041 |
| 0.90 | -0.5802 | ******* |
| 0.95 | -0.3716 | -0.3967 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4295 | -0.5040 | -0.5042 | ******* | ******* |
| 0.100 | -0.4362 | -0.5123 | -0.5024 | ******* | ******* |
| 0.150 | -0.4405 | -0.5115 | -0.5051 | ******* | ******* |
| 0.200 | -0.4446 | -0.5129 | -0.5149 | ******* | -0.2415 |
| 0.250 | ******* | -0.5206 | -0.5248 | -0.4902 | -0.3437 |
| 0.300 | -0.4492 | -0.5293 | -0.5491 | -0.4971 | -0.4285 |
| 0.350 | -0.4605 | -0.5526 | -0.5904 | -0.5351 | -0.4784 |
| 0.400 | -0.4721 | -0.6049 | -0.6783 | -0.6085 | -0.5705 |
| 0.450 | -0.5190 | -0.7252 | -0.8286 | -0.7385 | -0.6996 |
| 0.500 | -0.7544 | -0.9433 | -1.0503 | -0.9362 | -0.8835 |
| 0.525 | ******* | -1.0850 | -1.1672 | -1.0464 | -0.9898 |
| 0.550 | -1.2109 | -1.2180 | -1.2744 | -1.1533 | -1.0904 |
| 0.575 | ******* | -1.3387 | -1.3675 | -1.2580 | -1.0368 |
| 0.600 | -1.5027 | -1.4322 | -1.4505 | -1.3450 | -0.7744 |
| 0.625 | ******* | ******* | -1.4401 | -1.4292 | -0.7702 |
| 0.650 | -1.5461 | -1.3678 | -1.2769 | -1.2250 | -0.7885 |
| 0.675 | ******* | -1.3130 | -1.2604 | -1.1603 | -0.7665 |
| 0.700 | -1.5225 | -1.3040 | -1.2550 | -1.1481 | -0.7278 |
| 0.725 | ******* | -1.3034 | ******* | -1.1410 | -0.6732 |
| 0.750 | -1.4239 | -1.3204 | ******* | -1.1381 | -0.6104 |
| 0.775 | ******* | -1.3575 | -1.2671 | -1.1331 | -0.5469 |
| 0.800 | -1.3163 | -1.3802 | -1.2839 | -1.1343 | ******* |
| 0.825 | ******* | -1.3291 | -1.2679 | -1.1341 | -0.5599 |
| 0.850 | -1.2253 | -1.2385 | -1.2211 | -1.1240 | -0.5427 |
| 0.875 | ******* | -1.1906 | -1.1784 | -1.0398 | -0.5421 |
| 0.900 | -1.1770 | -1.1768 | -1.1701 | -0.9636 | ******* |
| 0.925 | ******* | -1.1837 | -1.1658 | -0.9142 | -0.5427 |
| 0.950 | -1.1698 | -1.1840 | -1.1628 | -0.9119 | -0.4731 |
| 0.975 | ******* | -1.1772 | -1.1585 | -0.9172 | -0.4398 |
| 1.000 | -1.1480 | -1.1808 | -1.1660 | -0.9026 | -0.4091 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4772 | 0.4225 | 0.4163 | ******* | -0.5127 |
| -0.400 | 0.4784 | 0.4283 | 0.3864 | 0.1934 | -0.5655 |
| -0.600 | 0.4894 | 0.4304 | 0.3806 | 0.2231 | -0.5422 |
| -0.700 | ******* | 0.4351 | 0.3745 | 0.2348 | -0.5144 |
| -0.800 | ******* | ******* | 0.3745 | 0.2530 | -0.4394 |
| -0.850 | ******* | 0.4132 | 0.3629 | 0.2601 | -0.4138 |
| -0.900 | 0.4363 | 0.3638 | 0.3334 | 0.2493 | -0.3671 |
| -0.950 | 0.3733 | 0.1515 | 0.2188 | 0.1808 | -0.1246 |
| -0.975 | ******* | 0.0657 | 0.0559 | 0.0525 | -0.0847 |
| -1.000 | -1.1730 | -1.1872 | -1.1575 | -0.8683 | -0.4417 |

Surface Pressures




Small Radius L.E.

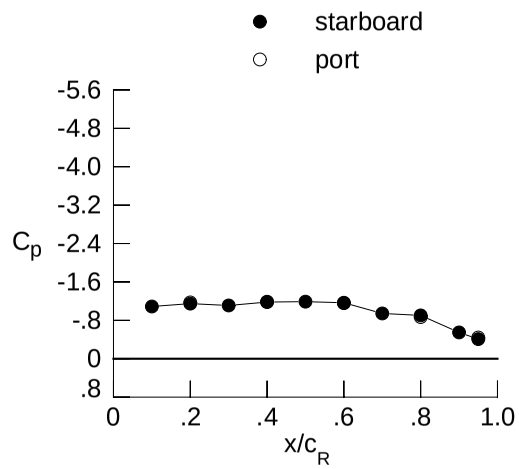
Run No. = 42 , Point No. = 887

$C_N$ = 1.050, $C_m$ = -0.1950

$\alpha$ = 20.6 °, $M_\infty$ = 0.870

$R_{mac}$ = $6.0 \times 10^6$

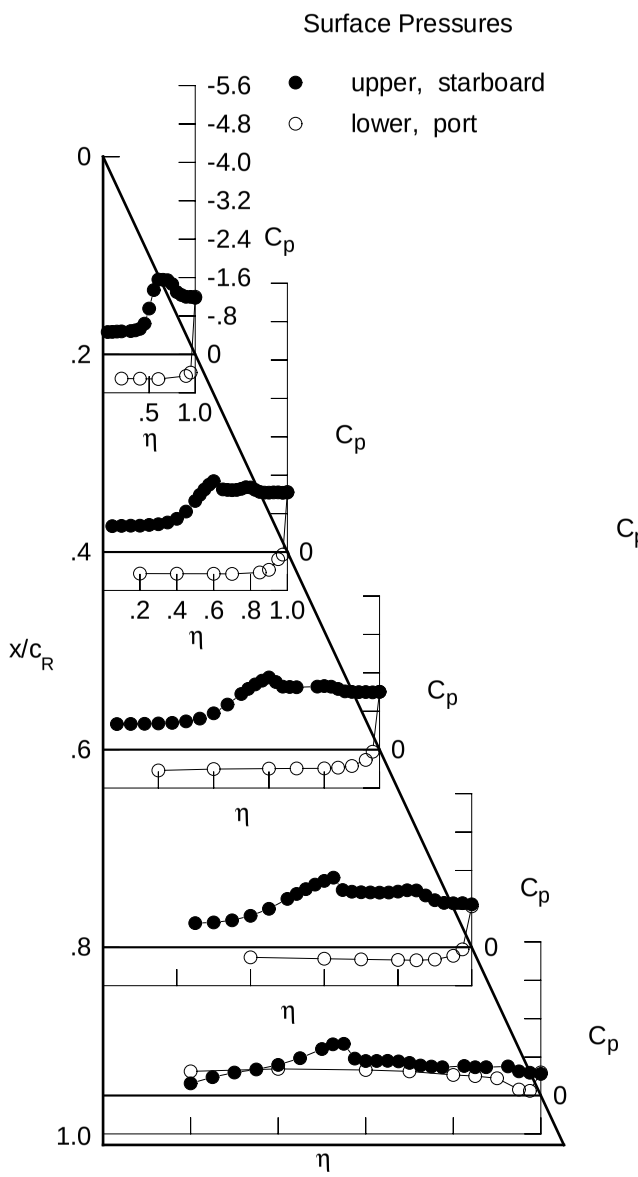
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0884 | ******* |
| 0.20 | -1.1480 | -1.1730 |
| 0.30 | -1.1092 | ******* |
| 0.40 | -1.1808 | -1.1872 |
| 0.50 | -1.1891 | ******* |
| 0.60 | -1.1660 | -1.1575 |
| 0.70 | -0.9432 | ******* |
| 0.80 | -0.9026 | -0.8683 |
| 0.90 | -0.5478 | ******* |
| 0.95 | -0.4091 | -0.4417 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4655 | -0.5390 | -0.5330 | ******* | ******* |
| 0.100 | -0.4692 | -0.5448 | -0.5356 | ******* | ******* |
| 0.150 | -0.4752 | -0.5490 | -0.5382 | ******* | ******* |
| 0.200 | -0.4789 | -0.5490 | -0.5457 | ******* | -0.2527 |
| 0.250 | ******* | -0.5650 | -0.5576 | -0.5030 | -0.3817 |
| 0.300 | -0.4856 | -0.5793 | -0.5887 | -0.5175 | -0.4785 |
| 0.350 | -0.5009 | -0.6156 | -0.6464 | -0.5617 | -0.5423 |
| 0.400 | -0.5320 | -0.6924 | -0.7564 | -0.6551 | -0.6378 |
| 0.450 | -0.6399 | -0.8431 | -0.9391 | -0.8012 | -0.7774 |
| 0.500 | -0.9549 | -1.0644 | -1.1594 | -1.0079 | -0.9682 |
| 0.525 | ******* | -1.1910 | -1.2655 | -1.1113 | -1.0666 |
| 0.550 | -1.3397 | -1.3026 | -1.3586 | -1.2110 | -1.0769 |
| 0.575 | ******* | -1.4023 | -1.4370 | -1.3059 | -0.7689 |
| 0.600 | -1.5588 | -1.4768 | -1.5042 | -1.3834 | -0.7185 |
| 0.625 | ******* | ******* | -1.4091 | -1.4504 | -0.7203 |
| 0.650 | -1.5543 | -1.3052 | -1.3124 | -1.1927 | -0.7226 |
| 0.675 | ******* | -1.2944 | -1.3057 | -1.1577 | -0.7103 |
| 0.700 | -1.5455 | -1.2887 | -1.2998 | -1.1467 | -0.6796 |
| 0.725 | ******* | -1.2941 | ******* | -1.1425 | -0.6248 |
| 0.750 | -1.4642 | -1.3168 | ******* | -1.1383 | -0.6034 |
| 0.775 | ******* | -1.3502 | -1.3131 | -1.1409 | -0.5888 |
| 0.800 | -1.2982 | -1.3449 | -1.3246 | -1.1598 | ******* |
| 0.825 | ******* | -1.2959 | -1.3110 | -1.1879 | -0.6155 |
| 0.850 | -1.2375 | -1.2531 | -1.2648 | -1.1842 | -0.5888 |
| 0.875 | ******* | -1.2379 | -1.2136 | -1.0790 | -0.5894 |
| 0.900 | -1.1997 | -1.2367 | -1.2031 | -0.9812 | ******* |
| 0.925 | ******* | -1.2428 | -1.1986 | -0.9250 | -0.6062 |
| 0.950 | -1.1987 | -1.2430 | -1.1999 | -0.9165 | -0.5028 |
| 0.975 | ******* | -1.2336 | -1.1936 | -0.9188 | -0.4741 |
| 1.000 | -1.1789 | -1.2391 | -1.2047 | -0.8948 | -0.4493 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5039 | 0.4485 | 0.4336 | ******* | -0.5029 |
| -0.400 | 0.5065 | 0.4514 | 0.4050 | 0.2095 | -0.5542 |
| -0.600 | 0.5139 | 0.4525 | 0.3951 | 0.2387 | -0.5316 |
| -0.700 | ******* | 0.4561 | 0.3916 | 0.2516 | -0.5022 |
| -0.800 | ******* | ******* | 0.3901 | 0.2642 | -0.4284 |
| -0.850 | ******* | 0.4260 | 0.3751 | 0.2705 | -0.4051 |
| -0.900 | 0.4493 | 0.3707 | 0.3408 | 0.2559 | -0.3592 |
| -0.950 | 0.3793 | 0.1484 | 0.2141 | 0.1780 | -0.1243 |
| -0.975 | ******* | 0.0529 | 0.0430 | 0.0432 | -0.0966 |
| -1.000 | -1.2009 | -1.2508 | -1.2047 | -0.8528 | -0.4805 |



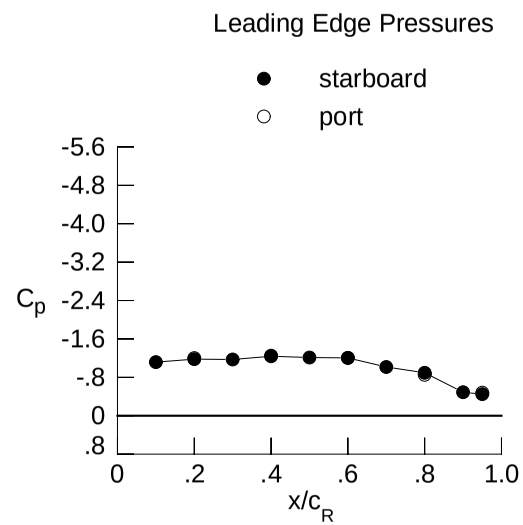

Small Radius L.E.

Run No. = 42 , Point No. = 888

$C_N$ = 1.100, $C_m$ = -0.2025

$\alpha$ = 21.6 °, $M_\infty$ = 0.869

$R_{mac}$ = $6.0 \times 10^6$

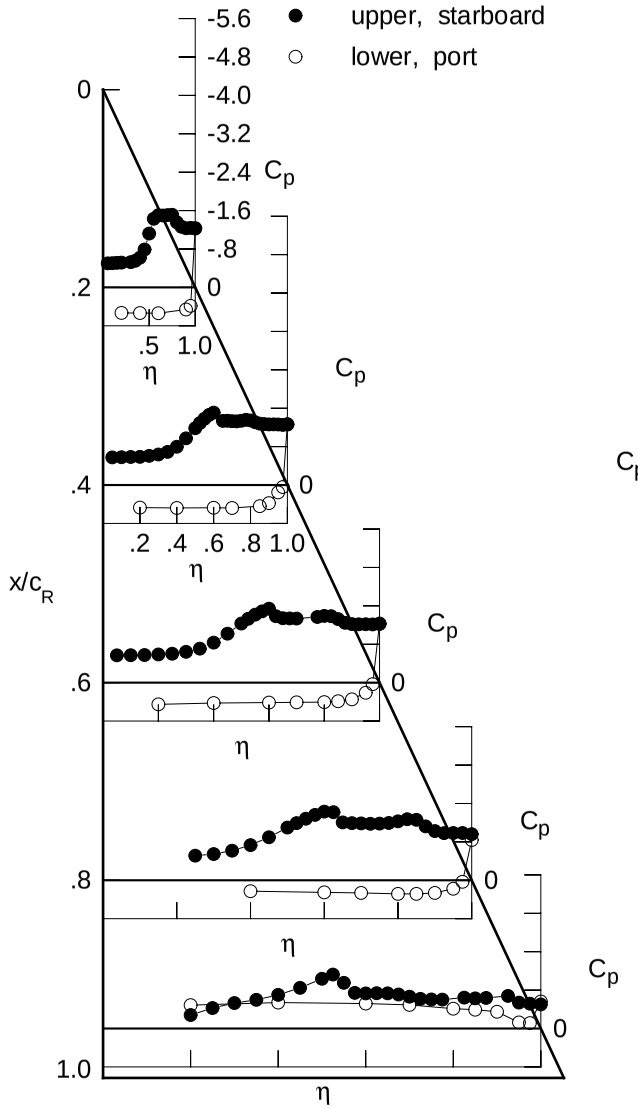



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1166 | ******* |
| 0.20 | -1.1789 | -1.2009 |
| 0.30 | -1.1720 | ******* |
| 0.40 | -1.2391 | -1.2508 |
| 0.50 | -1.2126 | ******* |
| 0.60 | -1.2047 | -1.2047 |
| 0.70 | -1.0154 | ******* |
| 0.80 | -0.8948 | -0.8528 |
| 0.90 | -0.4895 | ******* |
| 0.95 | -0.4493 | -0.4805 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5011 | -0.5763 | -0.5686 | ******* | ******* |
| 0.100 | -0.5038 | -0.5789 | -0.5714 | ******* | ******* |
| 0.150 | -0.5118 | -0.5848 | -0.5752 | ******* | ******* |
| 0.200 | -0.5160 | -0.5874 | -0.5873 | ******* | -0.2806 |
| 0.250 | ******* | -0.6077 | -0.6027 | -0.5128 | -0.4268 |
| 0.300 | -0.5256 | -0.6359 | -0.6427 | -0.5461 | -0.5303 |
| 0.350 | -0.5545 | -0.6906 | -0.7082 | -0.6172 | -0.5978 |
| 0.400 | -0.6185 | -0.7976 | -0.8338 | -0.7332 | -0.7011 |
| 0.450 | -0.7898 | -0.9728 | -1.0202 | -0.8962 | -0.8470 |
| 0.500 | -1.1218 | -1.1831 | -1.2309 | -1.0985 | -1.0363 |
| 0.525 | ******* | -1.2898 | -1.3302 | -1.1914 | -1.1237 |
| 0.550 | -1.4296 | -1.3801 | -1.4159 | -1.2823 | -0.9518 |
| 0.575 | ******* | -1.4606 | -1.4848 | -1.3627 | -0.7421 |
| 0.600 | -1.5052 | -1.5087 | -1.5409 | -1.4307 | -0.7314 |
| 0.625 | ******* | ******* | -1.3840 | -1.4185 | -0.7353 |
| 0.650 | -1.4973 | -1.3360 | -1.3423 | -1.2053 | -0.7331 |
| 0.675 | ******* | -1.3395 | -1.3373 | -1.1907 | -0.7091 |
| 0.700 | -1.5065 | -1.3302 | -1.3352 | -1.1847 | -0.6634 |
| 0.725 | ******* | -1.3267 | ******* | -1.1770 | -0.6177 |
| 0.750 | -1.5129 | -1.3394 | ******* | -1.1811 | -0.6053 |
| 0.775 | ******* | -1.3593 | -1.3676 | -1.1945 | -0.6027 |
| 0.800 | -1.3570 | -1.3463 | -1.3905 | -1.2282 | ******* |
| 0.825 | ******* | -1.3091 | -1.3842 | -1.2724 | -0.6434 |
| 0.850 | -1.2633 | -1.2792 | -1.3239 | -1.2599 | -0.6276 |
| 0.875 | ******* | -1.2694 | -1.2462 | -1.1230 | -0.6364 |
| 0.900 | -1.2320 | -1.2626 | -1.2190 | -1.0253 | ******* |
| 0.925 | ******* | -1.2640 | -1.2154 | -0.9822 | -0.6790 |
| 0.950 | -1.2398 | -1.2619 | -1.2165 | -0.9849 | -0.5397 |
| 0.975 | ******* | -1.2529 | -1.2126 | -0.9850 | -0.5173 |
| 1.000 | -1.2252 | -1.2596 | -1.2218 | -0.9605 | -0.5013 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5321 | 0.4703 | 0.4524 | ******* | -0.4869 |
| -0.400 | 0.5342 | 0.4772 | 0.4250 | 0.2272 | -0.5406 |
| -0.600 | 0.5385 | 0.4738 | 0.4149 | 0.2522 | -0.5198 |
| -0.700 | ******* | 0.4782 | 0.4105 | 0.2631 | -0.4920 |
| -0.800 | ******* | ******* | 0.4055 | 0.2833 | -0.4131 |
| -0.850 | ******* | 0.4402 | 0.3868 | 0.2832 | -0.3923 |
| -0.900 | 0.4603 | 0.3770 | 0.3479 | 0.2635 | -0.3484 |
| -0.950 | 0.3852 | 0.1527 | 0.2108 | 0.1764 | -0.1261 |
| -0.975 | ******* | 0.0413 | 0.0319 | 0.0315 | -0.1124 |
| -1.000 | -1.2342 | -1.2686 | -1.2318 | -0.8395 | -0.5626 |

Surface Pressures




Small Radius L.E.

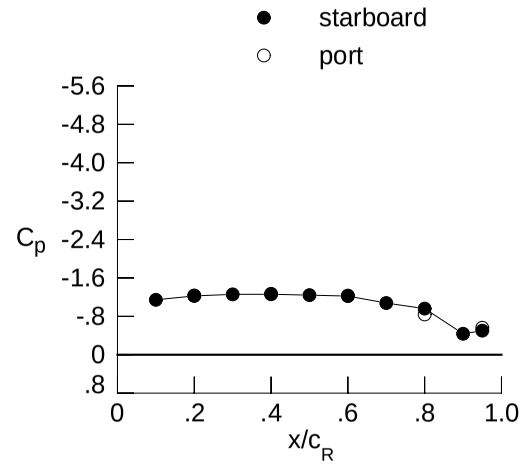
Run No. = 42 , Point No. = 889

$C_N$ = 1.147, $C_m$ = -0.2076

$\alpha$ = 22.6 °, $M_\infty$ = 0.869

$R_{mac}$ = $6.0 \times 10^6$

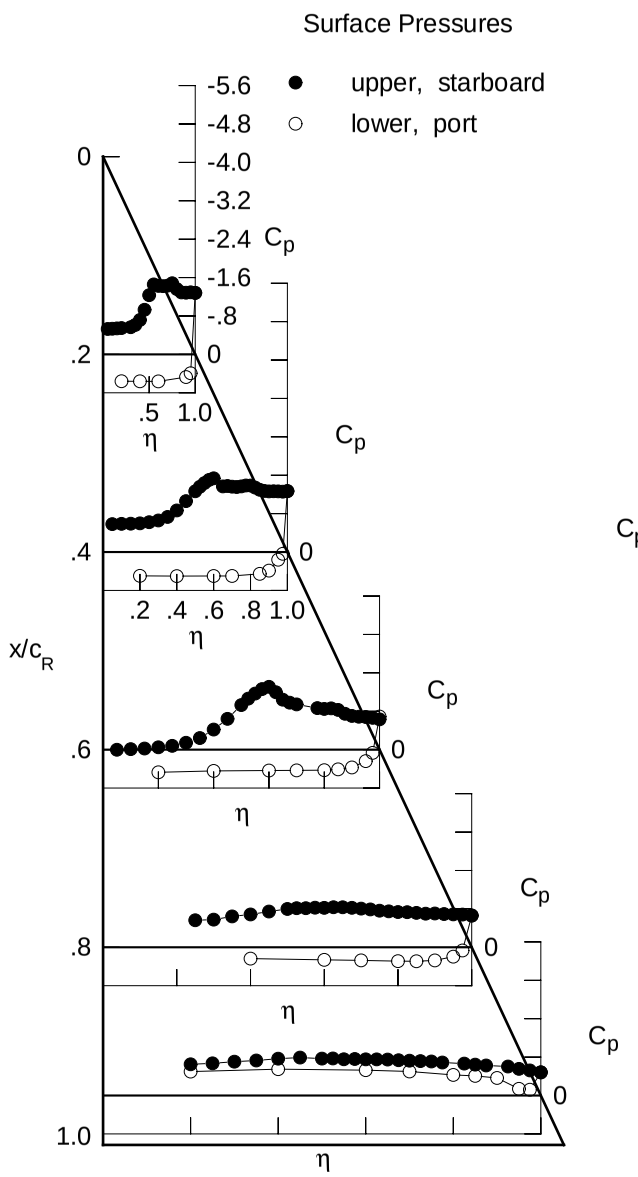
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1438 | ******* |
| 0.20 | -1.2252 | -1.2342 |
| 0.30 | -1.2580 | ******* |
| 0.40 | -1.2596 | -1.2686 |
| 0.50 | -1.2416 | ******* |
| 0.60 | -1.2218 | -1.2318 |
| 0.70 | -1.0767 | ******* |
| 0.80 | -0.9605 | -0.8395 |
| 0.90 | -0.4368 | ******* |
| 0.95 | -0.5013 | -0.5626 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5295 | -0.5817 | 0.0025 | ******* | ******* |
| 0.100 | -0.5344 | -0.5873 | -0.0106 | ******* | ******* |
| 0.150 | -0.5414 | -0.5904 | -0.0232 | ******* | ******* |
| 0.200 | -0.5488 | -0.5972 | -0.0488 | ******* | -0.6504 |
| 0.250 | ******* | -0.6216 | -0.0791 | -0.5633 | -0.6706 |
| 0.300 | -0.5662 | -0.6579 | -0.1429 | -0.5759 | -0.7045 |
| 0.350 | -0.6132 | -0.7311 | -0.2419 | -0.6433 | -0.7293 |
| 0.400 | -0.7179 | -0.8662 | -0.4183 | -0.6842 | -0.7672 |
| 0.450 | -0.9295 | -1.0607 | -0.6416 | -0.7449 | -0.7905 |
| 0.500 | -1.2336 | -1.2654 | -0.9291 | -0.7985 | -0.7687 |
| 0.525 | ******* | -1.3592 | -1.0626 | -0.8141 | -0.7723 |
| 0.550 | -1.4575 | -1.4371 | -1.1681 | -0.8147 | -0.7549 |
| 0.575 | ******* | -1.5024 | -1.2614 | -0.8250 | -0.7607 |
| 0.600 | -1.4272 | -1.5364 | -1.3088 | -0.8220 | -0.7539 |
| 0.625 | ******* | ******* | -1.1961 | -0.8347 | -0.7532 |
| 0.650 | -1.4214 | -1.3669 | -1.0408 | -0.8333 | -0.7491 |
| 0.675 | ******* | -1.3760 | -0.9781 | -0.8225 | -0.7354 |
| 0.700 | -1.4324 | -1.3616 | -0.9420 | -0.8054 | -0.7260 |
| 0.725 | ******* | -1.3543 | ******* | -0.7890 | -0.7170 |
| 0.750 | -1.4824 | -1.3668 | ******* | -0.7625 | -0.7086 |
| 0.775 | ******* | -1.3867 | -0.8655 | -0.7491 | -0.6875 |
| 0.800 | -1.3606 | -1.3853 | -0.8480 | -0.7348 | ******* |
| 0.825 | ******* | -1.3430 | -0.8596 | -0.7310 | -0.6644 |
| 0.850 | -1.2914 | -1.2969 | -0.8282 | -0.7167 | -0.6433 |
| 0.875 | ******* | -1.2725 | -0.7474 | -0.7003 | -0.6259 |
| 0.900 | -1.2846 | -1.2630 | -0.7020 | -0.7039 | ******* |
| 0.925 | ******* | -1.2661 | -0.6858 | -0.6927 | -0.6039 |
| 0.950 | -1.2938 | -1.2640 | -0.6797 | -0.6853 | -0.5554 |
| 0.975 | ******* | -1.2577 | -0.6621 | -0.6819 | -0.5225 |
| 1.000 | -1.2823 | -1.2663 | -0.6315 | -0.6630 | -0.4845 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5594 | 0.4964 | 0.4720 | ******* | -0.4984 |
| -0.400 | 0.5609 | 0.5012 | 0.4432 | 0.2358 | -0.5488 |
| -0.600 | 0.5627 | 0.4988 | 0.4348 | 0.2615 | -0.5279 |
| -0.700 | ******* | 0.4987 | 0.4319 | 0.2731 | -0.5005 |
| -0.800 | ******* | ******* | 0.4276 | 0.2889 | -0.4286 |
| -0.850 | ******* | 0.4545 | 0.4105 | 0.2911 | -0.4089 |
| -0.900 | 0.4724 | 0.3868 | 0.3716 | 0.2736 | -0.3653 |
| -0.950 | 0.3925 | 0.1603 | 0.2389 | 0.1951 | -0.1388 |
| -0.975 | ******* | 0.0367 | 0.0672 | 0.0662 | -0.1206 |
| -1.000 | -1.2797 | -1.2721 | -0.6895 | -0.6590 | -0.4802 |



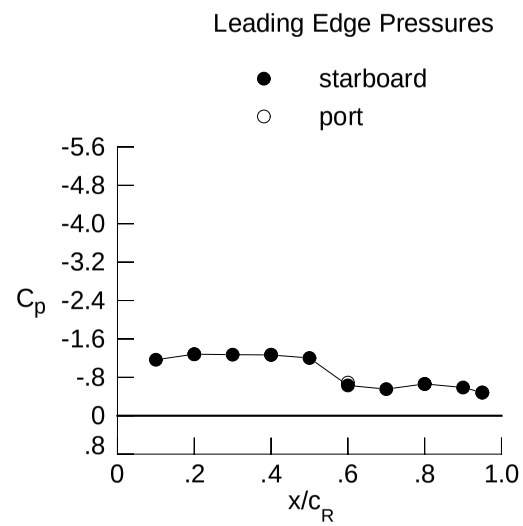

Small Radius L.E.

Run No. = 42 , Point No. = 890

$C_N$ = 1.053, $C_m$ = -0.1794

$\alpha$ = 23.6 °, $M_\infty$ = 0.872

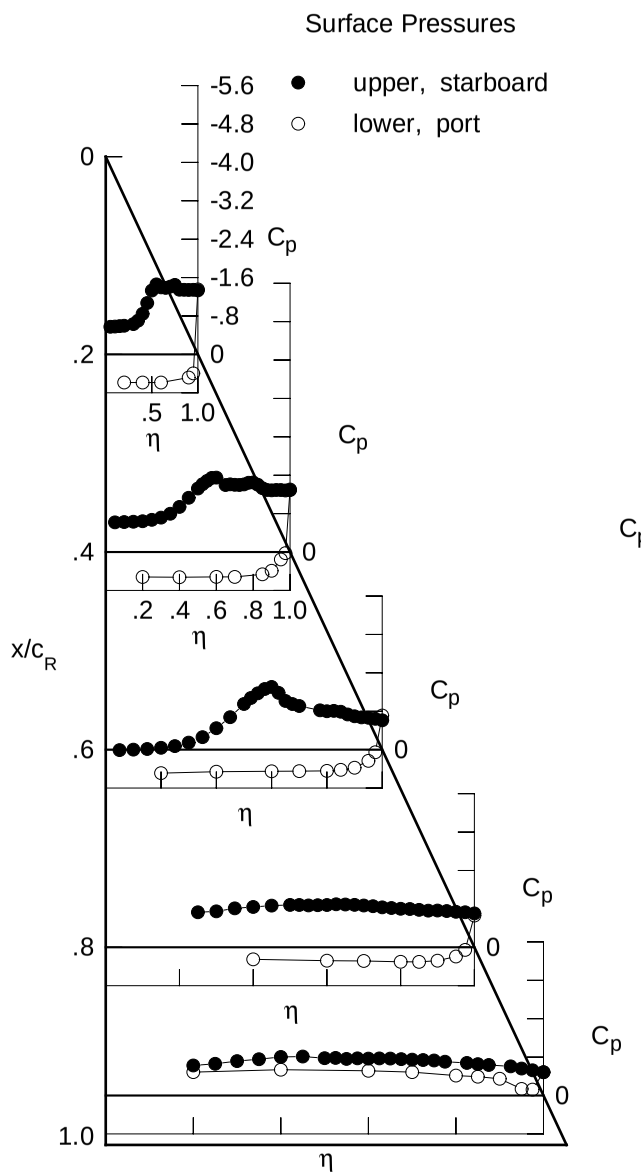
$R_{mac}$ = $6.0 \times 10^6$




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1662 | ******* |
| 0.20 | -1.2823 | -1.2797 |
| 0.30 | -1.2719 | ******* |
| 0.40 | -1.2663 | -1.2721 |
| 0.50 | -1.2026 | ******* |
| 0.60 | -0.6315 | -0.6895 |
| 0.70 | -0.5542 | ******* |
| 0.80 | -0.6630 | -0.6590 |
| 0.90 | -0.5882 | ******* |
| 0.95 | -0.4845 | -0.4802 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5748 | -0.6185 | 0.0100 | ******* | ******* |
| 0.100 | -0.5801 | -0.6244 | -0.0004 | ******* | ******* |
| 0.150 | -0.5891 | -0.6309 | -0.0134 | ******* | ******* |
| 0.200 | -0.5970 | -0.6419 | -0.0385 | ******* | -0.6258 |
| 0.250 | ******* | -0.6711 | -0.0735 | -0.7293 | -0.6610 |
| 0.300 | -0.6316 | -0.7170 | -0.1464 | -0.7486 | -0.7168 |
| 0.350 | -0.7022 | -0.7979 | -0.2599 | -0.8113 | -0.7561 |
| 0.400 | -0.8454 | -0.9403 | -0.4466 | -0.8402 | -0.8033 |
| 0.450 | -1.0702 | -1.1304 | -0.6760 | -0.8680 | -0.8117 |
| 0.500 | -1.3307 | -1.3231 | -0.9509 | -0.8821 | -0.7774 |
| 0.525 | ******* | -1.4131 | -1.0756 | -0.8818 | -0.7832 |
| 0.550 | -1.4586 | -1.4827 | -1.1738 | -0.8717 | -0.7623 |
| 0.575 | ******* | -1.5437 | -1.2631 | -0.8765 | -0.7746 |
| 0.600 | -1.3962 | -1.5502 | -1.3062 | -0.8810 | -0.7689 |
| 0.625 | ******* | ******* | -1.1829 | -0.8959 | -0.7729 |
| 0.650 | -1.3856 | -1.3959 | -1.0141 | -0.8915 | -0.7697 |
| 0.675 | ******* | -1.4107 | -0.9501 | -0.8837 | -0.7579 |
| 0.700 | -1.4113 | -1.4010 | -0.9089 | -0.8700 | -0.7475 |
| 0.725 | ******* | -1.3972 | ******* | -0.8561 | -0.7395 |
| 0.750 | -1.4480 | -1.4086 | ******* | -0.8323 | -0.7297 |
| 0.775 | ******* | -1.4434 | -0.8192 | -0.8182 | -0.7042 |
| 0.800 | -1.3470 | -1.4498 | -0.8003 | -0.8021 | ******* |
| 0.825 | ******* | -1.4021 | -0.8084 | -0.7977 | -0.6783 |
| 0.850 | -1.3459 | -1.3303 | -0.7894 | -0.7799 | -0.6536 |
| 0.875 | ******* | -1.2931 | -0.7330 | -0.7633 | -0.6357 |
| 0.900 | -1.3422 | -1.2854 | -0.6951 | -0.7654 | ******* |
| 0.925 | ******* | -1.2929 | -0.6718 | -0.7548 | -0.6069 |
| 0.950 | -1.3457 | -1.2917 | -0.6638 | -0.7392 | -0.5614 |
| 0.975 | ******* | -1.2826 | -0.6425 | -0.7294 | -0.5258 |
| 1.000 | -1.3334 | -1.2902 | -0.6113 | -0.7058 | -0.4865 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5858 | 0.5198 | 0.4895 | ******* | -0.4869 |
| -0.400 | 0.5867 | 0.5251 | 0.4597 | 0.2510 | -0.5378 |
| -0.600 | 0.5866 | 0.5179 | 0.4509 | 0.2792 | -0.5150 |
| -0.700 | ******* | 0.5180 | 0.4482 | 0.2852 | -0.4871 |
| -0.800 | ******* | ******* | 0.4422 | 0.3025 | -0.4151 |
| -0.850 | ******* | 0.4642 | 0.4210 | 0.3036 | -0.3924 |
| -0.900 | 0.4823 | 0.3903 | 0.3766 | 0.2794 | -0.3484 |
| -0.950 | 0.3953 | 0.1543 | 0.2336 | 0.1921 | -0.1371 |
| -0.975 | ******* | 0.0230 | 0.0541 | 0.0544 | -0.1232 |
| -1.000 | -1.3538 | -1.3025 | -0.7107 | -0.6606 | -0.4838 |



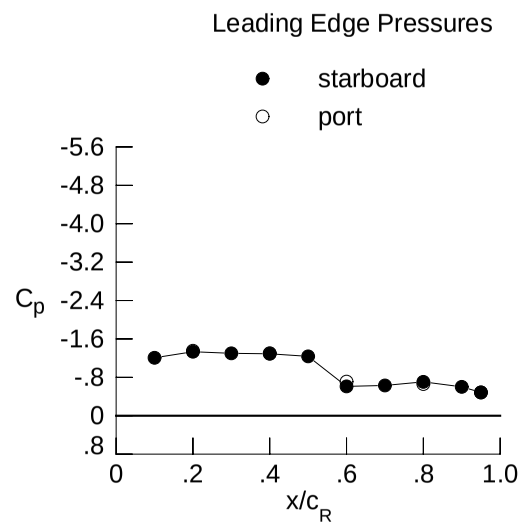

Small Radius L.E.

Run No. = 42 , Point No. = 891

$C_N$ = 1.087, $C_m$ = -0.1766

$\alpha$ = 24.6 °, $M_\infty$ = 0.869

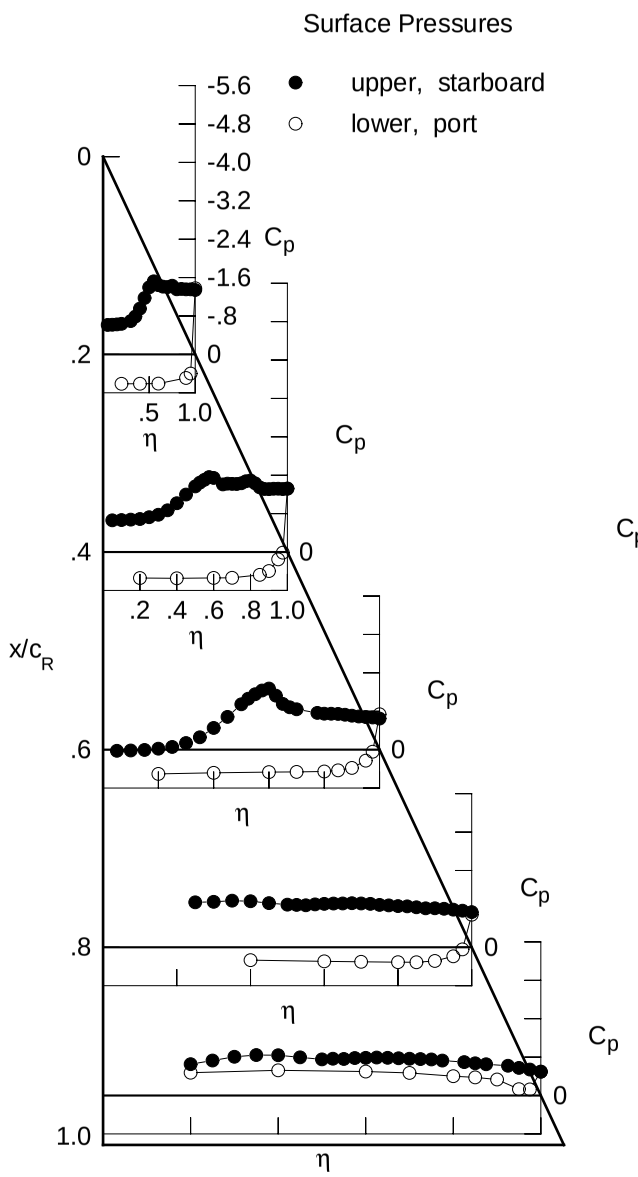
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.2075 | ******* |
| 0.20 | -1.3334 | -1.3538 |
| 0.30 | -1.3002 | ******* |
| 0.40 | -1.2902 | -1.3025 |
| 0.50 | -1.2372 | ******* |
| 0.60 | -0.6113 | -0.7107 |
| 0.70 | -0.6308 | ******* |
| 0.80 | -0.7058 | -0.6606 |
| 0.90 | -0.6019 | ******* |
| 0.95 | -0.4865 | -0.4838 |

# Table D5. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6134 | -0.6610 | 0.0239 | ******* | ******* |
| 0.100 | -0.6177 | -0.6662 | 0.0174 | ******* | ******* |
| 0.150 | -0.6247 | -0.6750 | 0.0061 | ******* | ******* |
| 0.200 | -0.6369 | -0.6882 | -0.0197 | ******* | -0.6526 |
| 0.250 | ******* | -0.7252 | -0.0563 | -0.9366 | -0.7285 |
| 0.300 | -0.6943 | -0.7765 | -0.1378 | -0.9469 | -0.8069 |
| 0.350 | -0.7883 | -0.8698 | -0.2577 | -0.9710 | -0.8431 |
| 0.400 | -0.9543 | -1.0166 | -0.4518 | -0.9589 | -0.8394 |
| 0.450 | -1.1742 | -1.1978 | -0.6828 | -0.9203 | -0.7950 |
| 0.500 | -1.3959 | -1.3674 | -0.9451 | -0.8882 | -0.7525 |
| 0.525 | ******* | -1.4457 | -1.0605 | -0.8835 | -0.7668 |
| 0.550 | -1.5225 | -1.5050 | -1.1545 | -0.8750 | -0.7617 |
| 0.575 | ******* | -1.5613 | -1.2324 | -0.8939 | -0.7811 |
| 0.600 | -1.4421 | -1.5443 | -1.2725 | -0.9048 | -0.7847 |
| 0.625 | ******* | ******* | -1.1246 | -0.9114 | -0.7914 |
| 0.650 | -1.4115 | -1.4085 | -0.9525 | -0.9127 | -0.7856 |
| 0.675 | ******* | -1.4246 | -0.8825 | -0.9188 | -0.7763 |
| 0.700 | -1.4028 | -1.4202 | -0.8408 | -0.9128 | -0.7667 |
| 0.725 | ******* | -1.4178 | ******* | -0.9052 | -0.7594 |
| 0.750 | -1.4304 | -1.4328 | ******* | -0.8830 | -0.7511 |
| 0.775 | ******* | -1.4743 | -0.7653 | -0.8728 | -0.7279 |
| 0.800 | -1.3557 | -1.4903 | -0.7486 | -0.8581 | ******* |
| 0.825 | ******* | -1.4309 | -0.7484 | -0.8527 | -0.6962 |
| 0.850 | -1.3640 | -1.3474 | -0.7437 | -0.8336 | -0.6713 |
| 0.875 | ******* | -1.3132 | -0.7269 | -0.8121 | -0.6509 |
| 0.900 | -1.3552 | -1.3107 | -0.7075 | -0.8129 | ******* |
| 0.925 | ******* | -1.3187 | -0.6908 | -0.8025 | -0.6198 |
| 0.950 | -1.3551 | -1.3188 | -0.6792 | -0.7843 | -0.5750 |
| 0.975 | ******* | -1.3121 | -0.6693 | -0.7628 | -0.5412 |
| 1.000 | -1.3416 | -1.3201 | -0.6469 | -0.7327 | -0.4975 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.6132 | 0.5413 | 0.5054 | ******* | -0.4752 |
| -0.400 | 0.6113 | 0.5475 | 0.4828 | 0.2679 | -0.5248 |
| -0.600 | 0.6089 | 0.5395 | 0.4680 | 0.2931 | -0.4993 |
| -0.700 | ******* | 0.5369 | 0.4638 | 0.3022 | -0.4703 |
| -0.800 | ******* | ******* | 0.4550 | 0.3107 | -0.4022 |
| -0.850 | ******* | 0.4752 | 0.4309 | 0.3116 | -0.3778 |
| -0.900 | 0.4908 | 0.3957 | 0.3807 | 0.2852 | -0.3334 |
| -0.950 | 0.3991 | 0.1525 | 0.2300 | 0.1883 | -0.1322 |
| -0.975 | ******* | 0.0130 | 0.0432 | 0.0430 | -0.1274 |
| -1.000 | -1.3774 | -1.3224 | -0.7367 | -0.6784 | -0.4955 |



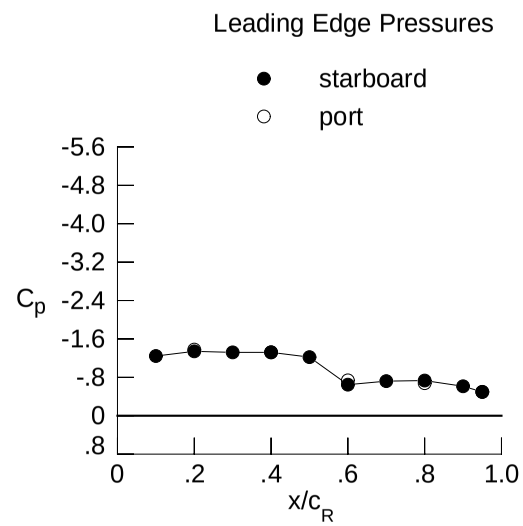

Small Radius L.E.

Run No. = 42 , Point No. = 892

$C_N$ = 1.124, $C_m$ = -0.1770

$\alpha$ = 25.7 °, $M_\infty$ = 0.870

$R_{mac}$ = $6.0 \times 10^6$

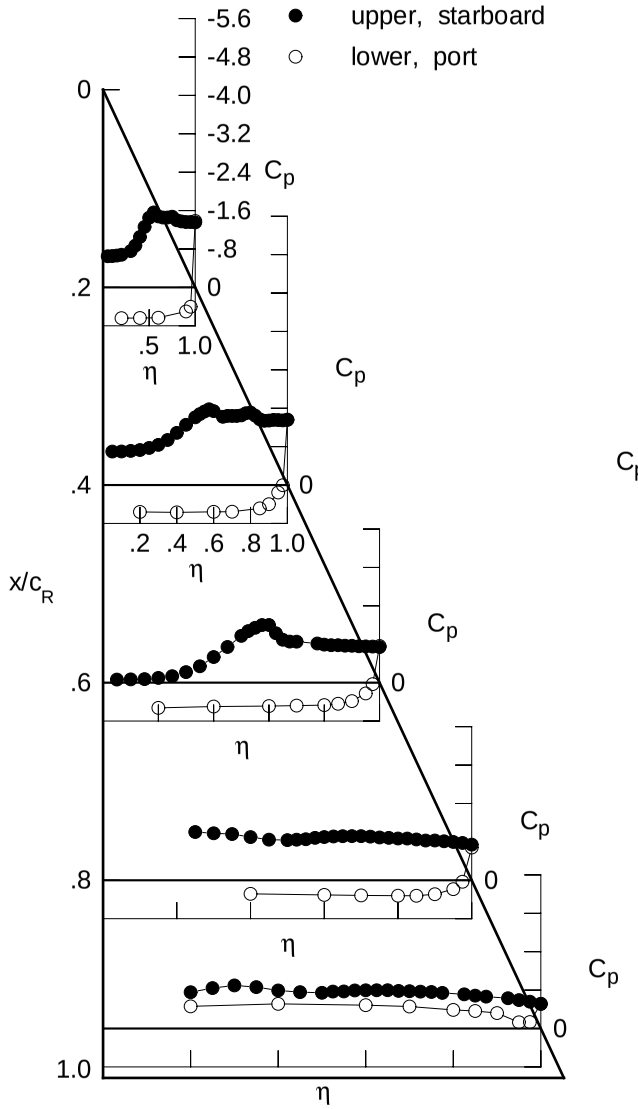



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.2437 | ******* |
| 0.20 | -1.3416 | -1.3774 |
| 0.30 | -1.3197 | ******* |
| 0.40 | -1.3201 | -1.3224 |
| 0.50 | -1.2210 | ******* |
| 0.60 | -0.6469 | -0.7367 |
| 0.70 | -0.7206 | ******* |
| 0.80 | -0.7327 | -0.6784 |
| 0.90 | -0.6136 | ******* |
| 0.95 | -0.4975 | -0.4955 |

# Table D5. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6488 | -0.6975 | -0.0643 | ******* | ******* |
| 0.100 | -0.6524 | -0.6995 | -0.0677 | ******* | ******* |
| 0.150 | -0.6629 | -0.7114 | -0.0732 | ******* | ******* |
| 0.200 | -0.6802 | -0.7299 | -0.0988 | ******* | -0.7564 |
| 0.250 | ******* | -0.7728 | -0.1343 | -1.0055 | -0.8424 |
| 0.300 | -0.7571 | -0.8366 | -0.2194 | -0.9791 | -0.8975 |
| 0.350 | -0.8709 | -0.9383 | -0.3407 | -0.9629 | -0.8624 |
| 0.400 | -1.0514 | -1.0874 | -0.5337 | -0.9002 | -0.7930 |
| 0.450 | -1.2603 | -1.2551 | -0.7435 | -0.8465 | -0.7579 |
| 0.500 | -1.4511 | -1.4105 | -0.9745 | -0.8371 | -0.7444 |
| 0.525 | ******* | -1.4774 | -1.0739 | -0.8454 | -0.7697 |
| 0.550 | -1.5612 | -1.5308 | -1.1427 | -0.8553 | -0.7723 |
| 0.575 | ******* | -1.5783 | -1.1998 | -0.8843 | -0.7927 |
| 0.600 | -1.4783 | -1.5398 | -1.2012 | -0.9010 | -0.7964 |
| 0.625 | ******* | ******* | -1.0298 | -0.9129 | -0.7966 |
| 0.650 | -1.4552 | -1.4216 | -0.8938 | -0.9185 | -0.7977 |
| 0.675 | ******* | -1.4406 | -0.8553 | -0.9199 | -0.7836 |
| 0.700 | -1.4557 | -1.4390 | -0.8538 | -0.9195 | -0.7775 |
| 0.725 | ******* | -1.4392 | ******* | -0.9100 | -0.7678 |
| 0.750 | -1.4727 | -1.4510 | ******* | -0.8918 | -0.7612 |
| 0.775 | ******* | -1.4958 | -0.8152 | -0.8838 | -0.7418 |
| 0.800 | -1.3981 | -1.5104 | -0.7918 | -0.8700 | ******* |
| 0.825 | ******* | -1.4465 | -0.7803 | -0.8696 | -0.7123 |
| 0.850 | -1.3748 | -1.3699 | -0.7797 | -0.8504 | -0.6849 |
| 0.875 | ******* | -1.3383 | -0.7693 | -0.8276 | -0.6640 |
| 0.900 | -1.3613 | -1.3428 | -0.7679 | -0.8290 | ******* |
| 0.925 | ******* | -1.3573 | -0.7575 | -0.8130 | -0.6315 |
| 0.950 | -1.3620 | -1.3539 | -0.7552 | -0.7986 | -0.5918 |
| 0.975 | ******* | -1.3468 | -0.7513 | -0.7777 | -0.5586 |
| 1.000 | -1.3534 | -1.3621 | -0.7408 | -0.7428 | -0.5150 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.6407 | 0.5606 | 0.5255 | ******* | -0.4619 |
| -0.400 | 0.6378 | 0.5697 | 0.4980 | 0.2825 | -0.5133 |
| -0.600 | 0.6321 | 0.5582 | 0.4881 | 0.3048 | -0.4861 |
| -0.700 | ******* | 0.5563 | 0.4787 | 0.3154 | -0.4582 |
| -0.800 | ******* | ******* | 0.4682 | 0.3210 | -0.3871 |
| -0.850 | ******* | 0.4864 | 0.4397 | 0.3220 | -0.3651 |
| -0.900 | 0.5013 | 0.3993 | 0.3849 | 0.2907 | -0.3216 |
| -0.950 | 0.4033 | 0.1554 | 0.2245 | 0.1848 | -0.1295 |
| -0.975 | ******* | 0.0041 | 0.0315 | 0.0301 | -0.1343 |
| -1.000 | -1.3828 | -1.3564 | -0.7641 | -0.6828 | -0.5124 |

Surface Pressures




Small Radius L.E.

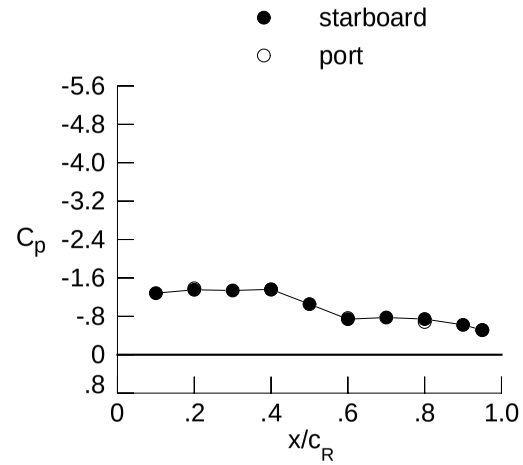
Run No. = 42 , Point No. = 893

$C_N$ = 1.156, $C_m$ = -0.1793

$\alpha$ = 26.7 °, $M_\infty$ = 0.871

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

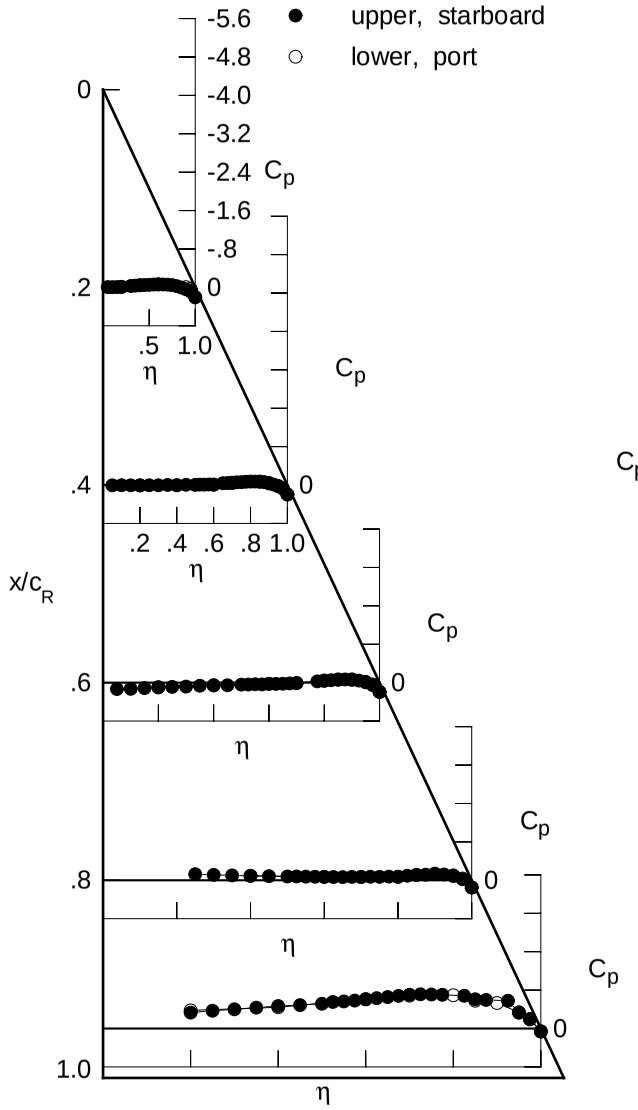



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.2823 | ******* |
| 0.20 | -1.3534 | -1.3828 |
| 0.30 | -1.3382 | ******* |
| 0.40 | -1.3621 | -1.3564 |
| 0.50 | -1.0542 | ******* |
| 0.60 | -0.7408 | -0.7641 |
| 0.70 | -0.7752 | ******* |
| 0.80 | -0.7428 | -0.6828 |
| 0.90 | -0.6227 | ******* |
| 0.95 | -0.5150 | -0.5124 |

# Table D5. Concluded.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0066 | 0.0067 | 0.1333 | ******* | ******* |
| 0.100 | -0.0050 | 0.0036 | 0.1285 | ******* | ******* |
| 0.150 | -0.0062 | 0.0055 | 0.1133 | ******* | ******* |
| 0.200 | -0.0130 | 0.0062 | 0.1004 | ******* | -0.3310 |
| 0.250 | ******* | 0.0045 | 0.0877 | -0.1273 | -0.3706 |
| 0.300 | -0.0287 | 0.0053 | 0.0825 | -0.1130 | -0.3998 |
| 0.350 | -0.0370 | -0.0022 | 0.0637 | -0.1016 | -0.4342 |
| 0.400 | -0.0429 | 0.0033 | 0.0592 | -0.0920 | -0.4683 |
| 0.450 | -0.0500 | -0.0059 | 0.0552 | -0.0861 | -0.4873 |
| 0.500 | -0.0524 | -0.0030 | 0.0413 | -0.0795 | -0.5164 |
| 0.525 | ******* | -0.0088 | 0.0390 | -0.0804 | -0.5534 |
| 0.550 | -0.0592 | -0.0079 | 0.0337 | -0.0758 | -0.5639 |
| 0.575 | ******* | -0.0120 | 0.0366 | -0.0734 | -0.5817 |
| 0.600 | -0.0619 | -0.0087 | 0.0261 | -0.0712 | -0.6061 |
| 0.625 | ******* | ******* | 0.0267 | -0.0679 | -0.6321 |
| 0.650 | -0.0609 | -0.0371 | 0.0224 | -0.0657 | -0.6552 |
| 0.675 | ******* | -0.0419 | 0.0160 | -0.0702 | -0.6802 |
| 0.700 | -0.0570 | -0.0495 | 0.0090 | -0.0672 | -0.7030 |
| 0.725 | ******* | -0.0569 | ******* | -0.0737 | -0.7131 |
| 0.750 | -0.0461 | -0.0602 | ******* | -0.0719 | -0.7084 |
| 0.775 | ******* | -0.0690 | -0.0266 | -0.0770 | -0.7028 |
| 0.800 | -0.0256 | -0.0722 | -0.0365 | -0.0719 | ******* |
| 0.825 | ******* | -0.0721 | -0.0508 | -0.0950 | -0.6825 |
| 0.850 | 0.0029 | -0.0689 | -0.0602 | -0.1087 | -0.6096 |
| 0.875 | ******* | -0.0603 | -0.0663 | -0.1165 | -0.5958 |
| 0.900 | 0.0401 | -0.0346 | -0.0586 | -0.1280 | ******* |
| 0.925 | ******* | -0.0107 | -0.0432 | -0.1213 | -0.5793 |
| 0.950 | 0.0838 | 0.0232 | -0.0072 | -0.0891 | -0.3289 |
| 0.975 | ******* | 0.0716 | 0.0506 | -0.0234 | -0.1908 |
| 1.000 | 0.2049 | 0.1980 | 0.1941 | 0.1475 | 0.0559 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0098 | 0.0089 | 0.0932 | ******* | -0.3775 |
| -0.400 | -0.0459 | 0.0043 | 0.0529 | -0.0936 | -0.4421 |
| -0.600 | -0.0651 | -0.0068 | 0.0222 | -0.0718 | -0.6131 |
| -0.700 | ******* | -0.0419 | 0.0090 | -0.0711 | -0.6849 |
| -0.800 | ******* | ******* | -0.0468 | -0.0754 | -0.6927 |
| -0.850 | ******* | -0.0722 | -0.0674 | -0.1148 | -0.5795 |
| -0.900 | -0.0052 | -0.0422 | -0.0686 | -0.1392 | -0.5309 |
| -0.950 | 0.0287 | 0.0212 | -0.0162 | -0.1029 | -0.3386 |
| -0.975 | ******* | 0.0691 | 0.0379 | -0.0371 | -0.2003 |
| -1.000 | 0.2046 | 0.1951 | 0.1929 | 0.1526 | 0.0661 |

Surface Pressures




Small Radius L.E.

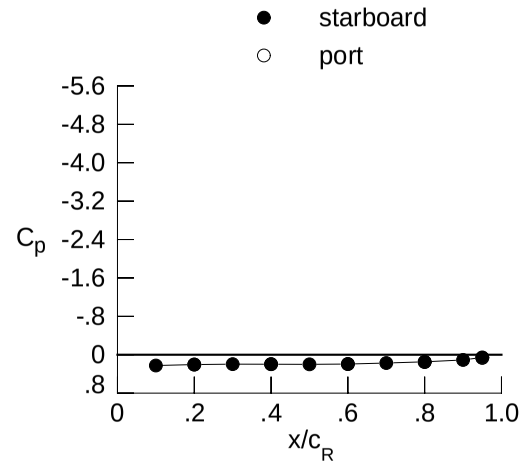
Run No. = 42 , Point No. = 894

$C_N$ = -0.014, $C_m$ = 0.0052

$\alpha$ = 0.1 °, $M_\infty$ = 0.868

$R_{mac}$ = $6.0 \times 10^6$

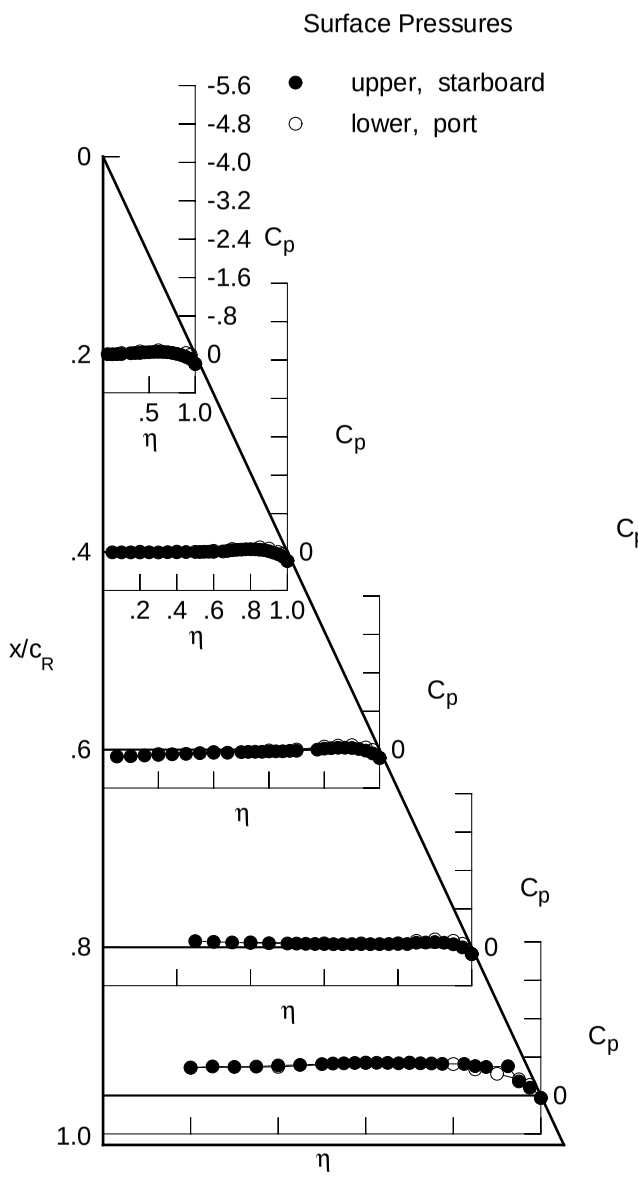
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2251 | ******* |
| 0.20 | 0.2049 | 0.2046 |
| 0.30 | 0.1962 | ******* |
| 0.40 | 0.1980 | 0.1951 |
| 0.50 | 0.2003 | ******* |
| 0.60 | 0.1941 | 0.1929 |
| 0.70 | 0.1729 | ******* |
| 0.80 | 0.1475 | 0.1526 |
| 0.90 | 0.1089 | ******* |
| 0.95 | 0.0559 | 0.0661 |

# Table D6. Tabulations and Plots of Surface Pressure Coefficients.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0038 | 0.0067 | 0.1440 | ******* | ******* |
| 0.100 | -0.0021 | 0.0068 | 0.1364 | ******* | ******* |
| 0.150 | -0.0055 | 0.0069 | 0.1215 | ******* | ******* |
| 0.200 | -0.0078 | 0.0079 | 0.1092 | ******* | -0.5782 |
| 0.250 | ******* | 0.0063 | 0.0966 | -0.1281 | -0.6047 |
| 0.300 | -0.0240 | 0.0088 | 0.0875 | -0.1132 | -0.5963 |
| 0.350 | -0.0297 | 0.0029 | 0.0726 | -0.1009 | -0.6023 |
| 0.400 | -0.0304 | 0.0050 | 0.0650 | -0.0916 | -0.6261 |
| 0.450 | -0.0423 | -0.0001 | 0.0637 | -0.0845 | -0.6372 |
| 0.500 | -0.0458 | -0.0025 | 0.0514 | -0.0790 | -0.6544 |
| 0.525 | ******* | -0.0013 | 0.0467 | -0.0770 | -0.6662 |
| 0.550 | -0.0521 | -0.0053 | 0.0440 | -0.0731 | -0.6704 |
| 0.575 | ******* | -0.0069 | 0.0447 | -0.0690 | -0.6784 |
| 0.600 | -0.0540 | -0.0051 | 0.0377 | -0.0685 | -0.6796 |
| 0.625 | ******* | ******* | 0.0354 | -0.0651 | -0.6813 |
| 0.650 | -0.0511 | -0.0118 | 0.0342 | -0.0642 | -0.6801 |
| 0.675 | ******* | -0.0232 | 0.0253 | -0.0653 | -0.6715 |
| 0.700 | -0.0458 | -0.0373 | 0.0232 | -0.0661 | -0.6787 |
| 0.725 | ******* | -0.0464 | ******* | -0.0650 | -0.6711 |
| 0.750 | -0.0316 | -0.0503 | ******* | -0.0659 | -0.6679 |
| 0.775 | ******* | -0.0575 | 0.0000 | -0.0675 | -0.6596 |
| 0.800 | -0.0110 | -0.0580 | -0.0206 | -0.0702 | ******* |
| 0.825 | ******* | -0.0563 | -0.0292 | -0.0677 | -0.6575 |
| 0.850 | 0.0153 | -0.0483 | -0.0399 | -0.0955 | -0.6131 |
| 0.875 | ******* | -0.0397 | -0.0401 | -0.0995 | -0.5941 |
| 0.900 | 0.0530 | -0.0160 | -0.0344 | -0.1077 | ******* |
| 0.925 | ******* | 0.0126 | -0.0133 | -0.0954 | -0.6093 |
| 0.950 | 0.0961 | 0.0460 | 0.0207 | -0.0626 | -0.2937 |
| 0.975 | ******* | 0.0955 | 0.0790 | 0.0027 | -0.1624 |
| 1.000 | 0.2021 | 0.1890 | 0.1768 | 0.1455 | 0.0493 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0270 | -0.0063 | 0.0931 | ******* | -0.5821 |
| -0.400 | -0.0615 | -0.0081 | 0.0494 | -0.1023 | -0.5968 |
| -0.600 | -0.0848 | -0.0253 | 0.0165 | -0.0813 | -0.6852 |
| -0.700 | ******* | -0.0631 | -0.0015 | -0.0809 | -0.6859 |
| -0.800 | ******* | ******* | -0.0630 | -0.0840 | -0.6550 |
| -0.850 | ******* | -0.0975 | -0.0840 | -0.1332 | -0.5448 |
| -0.900 | -0.0285 | -0.0713 | -0.0926 | -0.1635 | -0.4531 |
| -0.950 | 0.0057 | -0.0012 | -0.0451 | -0.1341 | -0.3370 |
| -0.975 | ******* | 0.0381 | 0.0076 | -0.0717 | -0.2200 |
| -1.000 | 0.1951 | 0.1804 | 0.1685 | 0.1350 | 0.0518 |



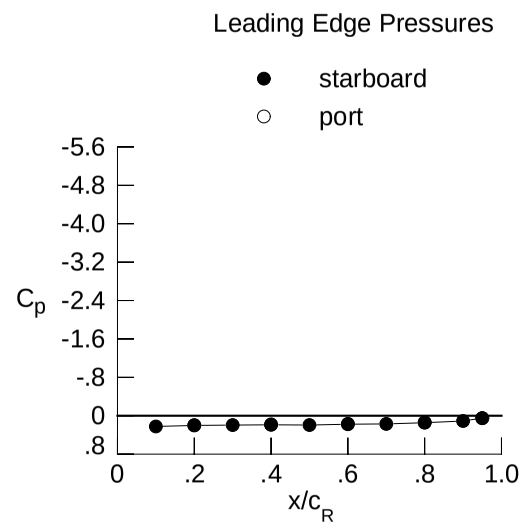

Small Radius L.E.

Run No. = 43 , Point No. = 895

$C_N$ = -0.033, $C_m$ = 0.0088

$\alpha$ = -0.4 °, $M_\infty$ = 0.900

$R_{mac}$ = $6.0 \times 10^6$

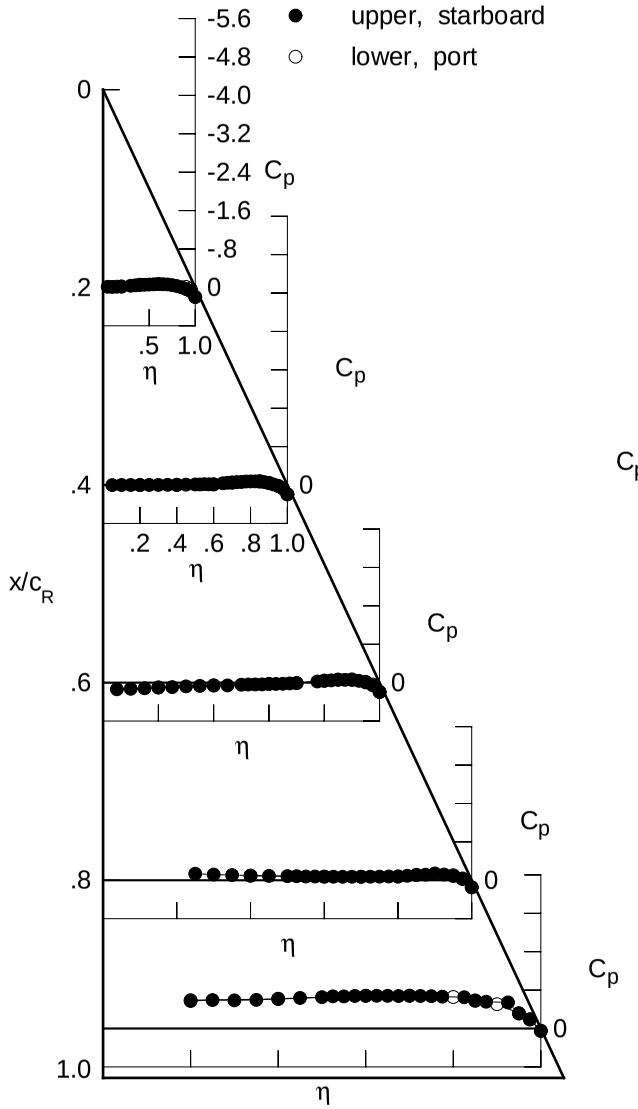



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2238 | ******* |
| 0.20 | 0.2021 | 0.1951 |
| 0.30 | 0.1948 | ******* |
| 0.40 | 0.1890 | 0.1804 |
| 0.50 | 0.1939 | ******* |
| 0.60 | 0.1768 | 0.1685 |
| 0.70 | 0.1706 | ******* |
| 0.80 | 0.1455 | 0.1350 |
| 0.90 | 0.1099 | ******* |
| 0.95 | 0.0493 | 0.0518 |

# Table D6. Continued.

| η | x/c_R .2 Cp,u | x/c_R .4 Cp,u | x/c_R .6 Cp,u | x/c_R .8 Cp,u | x/c_R .95 Cp,u |
|---|---|---|---|---|---|
| 0.050 | -0.0125 | 0.0006 | 0.1384 | ******* | ******* |
| 0.100 | -0.0096 | -0.0005 | 0.1284 | ******* | ******* |
| 0.150 | -0.0152 | -0.0007 | 0.1171 | ******* | ******* |
| 0.200 | -0.0180 | -0.0009 | 0.1025 | ******* | -0.5727 |
| 0.250 | ******* | -0.0014 | 0.0924 | -0.1369 | -0.5925 |
| 0.300 | -0.0345 | -0.0023 | 0.0782 | -0.1189 | -0.5867 |
| 0.350 | -0.0421 | -0.0051 | 0.0677 | -0.1089 | -0.5965 |
| 0.400 | -0.0568 | -0.0080 | 0.0598 | -0.0972 | -0.6209 |
| 0.450 | -0.0540 | -0.0091 | 0.0581 | -0.0909 | -0.6364 |
| 0.500 | -0.0589 | -0.0116 | 0.0431 | -0.0860 | -0.6530 |
| 0.525 | ******* | -0.0119 | 0.0389 | -0.0844 | -0.6701 |
| 0.550 | -0.0641 | -0.0173 | 0.0376 | -0.0781 | -0.6684 |
| 0.575 | ******* | -0.0149 | 0.0369 | -0.0782 | -0.6786 |
| 0.600 | -0.0676 | -0.0151 | 0.0295 | -0.0750 | -0.6804 |
| 0.625 | ******* | ******* | 0.0273 | -0.0747 | -0.6827 |
| 0.650 | -0.0654 | -0.0361 | 0.0234 | -0.0726 | -0.6805 |
| 0.675 | ******* | -0.0475 | 0.0156 | -0.0737 | -0.6768 |
| 0.700 | -0.0614 | -0.0551 | 0.0108 | -0.0744 | -0.6835 |
| 0.725 | ******* | -0.0606 | ******* | -0.0749 | -0.6777 |
| 0.750 | -0.0466 | -0.0630 | ******* | -0.0762 | -0.6727 |
| 0.775 | ******* | -0.0734 | -0.0239 | -0.0789 | -0.6642 |
| 0.800 | -0.0283 | -0.0754 | -0.0356 | -0.0773 | ******* |
| 0.825 | ******* | -0.0760 | -0.0470 | -0.0947 | -0.6515 |
| 0.850 | -0.0028 | -0.0699 | -0.0581 | -0.1085 | -0.5866 |
| 0.875 | ******* | -0.0618 | -0.0583 | -0.1173 | -0.5582 |
| 0.900 | 0.0351 | -0.0373 | -0.0569 | -0.1293 | ******* |
| 0.925 | ******* | -0.0120 | -0.0387 | -0.1199 | -0.5430 |
| 0.950 | 0.0786 | 0.0207 | -0.0051 | -0.0890 | -0.3103 |
| 0.975 | ******* | 0.0702 | 0.0537 | -0.0267 | -0.1860 |
| 1.000 | 0.2003 | 0.1957 | 0.1955 | 0.1465 | 0.0448 |
| | Cp,l | Cp,l | Cp,l | Cp,l | Cp,l |
| -0.200 | -0.0165 | 0.0013 | 0.0992 | ******* | -0.5907 |
| -0.400 | -0.0512 | 0.0006 | 0.0558 | -0.0948 | -0.6138 |
| -0.600 | -0.0713 | -0.0128 | 0.0246 | -0.0758 | -0.6831 |
| -0.700 | ******* | -0.0472 | 0.0089 | -0.0720 | -0.6828 |
| -0.800 | ******* | ******* | -0.0442 | -0.0805 | -0.6561 |
| -0.850 | ******* | -0.0824 | -0.0655 | -0.1152 | -0.5760 |
| -0.900 | -0.0094 | -0.0474 | -0.0685 | -0.1420 | -0.5062 |
| -0.950 | 0.0241 | 0.0161 | -0.0166 | -0.1057 | -0.3203 |
| -0.975 | ******* | 0.0661 | 0.0384 | -0.0388 | -0.1958 |
| -1.000 | 0.2012 | 0.1923 | 0.1923 | 0.1469 | 0.0526 |

Surface Pressures




Small Radius L.E.

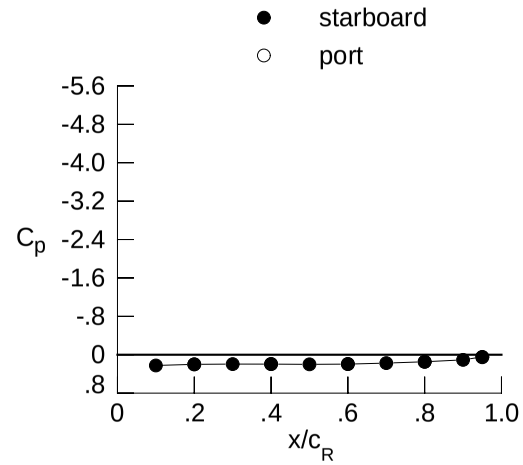
Run No. = 43 , Point No. = 896

$C_N$ = -0.013, $C_m$ = 0.0047

$\alpha$ = 0.1 °, $M_\infty$ = 0.900

$R_{mac}$ = $6.0 \times 10^6$

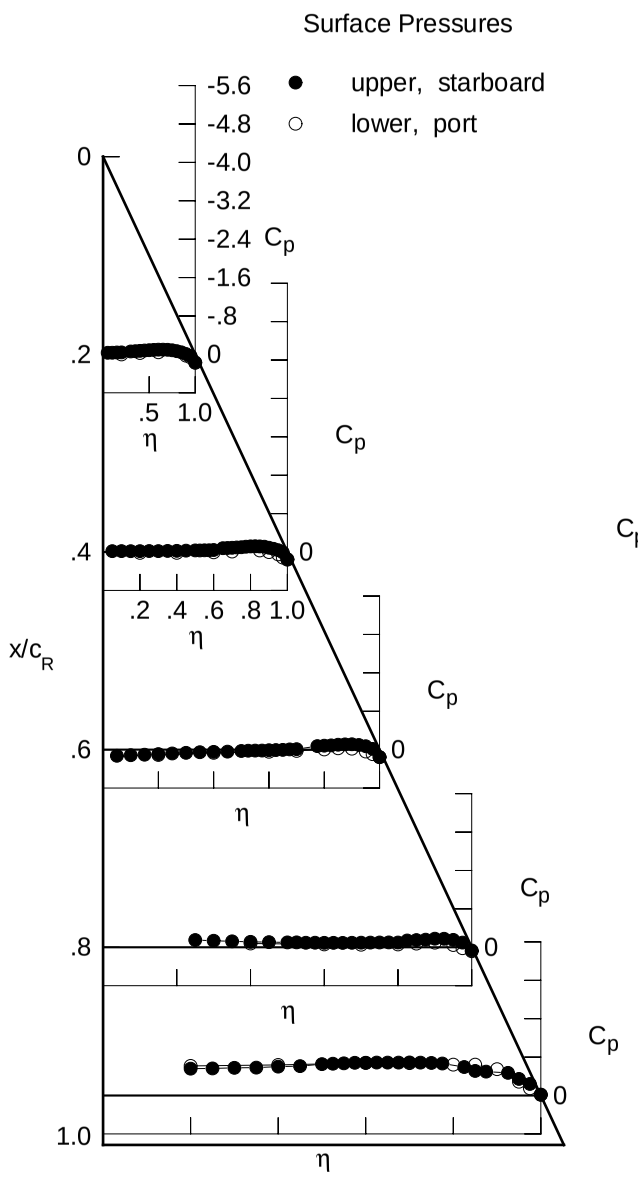
Leading Edge Pressures




| x/c_R | starb'd Cp | port Cp |
|---|---|---|
| 0.10 | 0.2237 | ******* |
| 0.20 | 0.2003 | 0.2012 |
| 0.30 | 0.1949 | ******* |
| 0.40 | 0.1957 | 0.1923 |
| 0.50 | 0.2004 | ******* |
| 0.60 | 0.1955 | 0.1923 |
| 0.70 | 0.1743 | ******* |
| 0.80 | 0.1465 | 0.1469 |
| 0.90 | 0.1069 | ******* |
| 0.95 | 0.0448 | 0.0526 |

# Table D6. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0336 | -0.0185 | 0.1278 | ******* | ******* |
| 0.100 | -0.0346 | -0.0193 | 0.1161 | ******* | ******* |
| 0.150 | -0.0402 | -0.0175 | 0.1056 | ******* | ******* |
| 0.200 | -0.0413 | -0.0187 | 0.0930 | ******* | -0.5594 |
| 0.250 | ******* | -0.0208 | 0.0798 | -0.1510 | -0.5637 |
| 0.300 | -0.0610 | -0.0196 | 0.0668 | -0.1360 | -0.5766 |
| 0.350 | -0.0664 | -0.0230 | 0.0538 | -0.1242 | -0.5810 |
| 0.400 | -0.0734 | -0.0246 | 0.0462 | -0.1134 | -0.6019 |
| 0.450 | -0.0806 | -0.0289 | 0.0419 | -0.1075 | -0.6119 |
| 0.500 | -0.0868 | -0.0332 | 0.0279 | -0.1018 | -0.6533 |
| 0.525 | ******* | -0.0331 | 0.0220 | -0.1022 | -0.6627 |
| 0.550 | -0.0933 | -0.0356 | 0.0197 | -0.0947 | -0.6707 |
| 0.575 | ******* | -0.0364 | 0.0191 | -0.0950 | -0.6816 |
| 0.600 | -0.0985 | -0.0424 | 0.0119 | -0.0927 | -0.6826 |
| 0.625 | ******* | ******* | 0.0088 | -0.0929 | -0.6861 |
| 0.650 | -0.0983 | -0.0799 | 0.0045 | -0.0915 | -0.6858 |
| 0.675 | ******* | -0.0836 | -0.0045 | -0.0935 | -0.6857 |
| 0.700 | -0.0958 | -0.0890 | -0.0097 | -0.0958 | -0.6885 |
| 0.725 | ******* | -0.0951 | ******* | -0.0973 | -0.6846 |
| 0.750 | -0.0856 | -0.1000 | ******* | -0.0998 | -0.6785 |
| 0.775 | ******* | -0.1114 | -0.0733 | -0.1012 | -0.6667 |
| 0.800 | -0.0674 | -0.1184 | -0.0822 | -0.0991 | ******* |
| 0.825 | ******* | -0.1212 | -0.0888 | -0.1412 | -0.5934 |
| 0.850 | -0.0431 | -0.1178 | -0.1021 | -0.1501 | -0.5122 |
| 0.875 | ******* | -0.1114 | -0.1092 | -0.1585 | -0.4975 |
| 0.900 | -0.0079 | -0.0900 | -0.1123 | -0.1796 | ******* |
| 0.925 | ******* | -0.0675 | -0.0966 | -0.1775 | -0.4718 |
| 0.950 | 0.0331 | -0.0382 | -0.0715 | -0.1546 | -0.3457 |
| 0.975 | ******* | 0.0067 | -0.0159 | -0.0979 | -0.2408 |
| 1.000 | 0.1661 | 0.1492 | 0.1547 | 0.0660 | -0.0184 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0010 | 0.0179 | 0.1114 | ******* | -0.6164 |
| -0.400 | -0.0290 | 0.0171 | 0.0668 | -0.0791 | -0.6370 |
| -0.600 | -0.0443 | 0.0057 | 0.0438 | -0.0599 | -0.6783 |
| -0.700 | ******* | -0.0106 | 0.0265 | -0.0539 | -0.6742 |
| -0.800 | ******* | ******* | -0.0042 | -0.0589 | -0.6429 |
| -0.850 | ******* | -0.0327 | -0.0277 | -0.0772 | -0.6434 |
| -0.900 | 0.0260 | 0.0016 | -0.0199 | -0.0963 | -0.5486 |
| -0.950 | 0.0631 | 0.0490 | 0.0396 | -0.0472 | -0.2872 |
| -0.975 | ******* | 0.1160 | 0.0946 | 0.0190 | -0.1498 |
| -1.000 | 0.1764 | 0.1590 | 0.1578 | 0.0822 | -0.0150 |



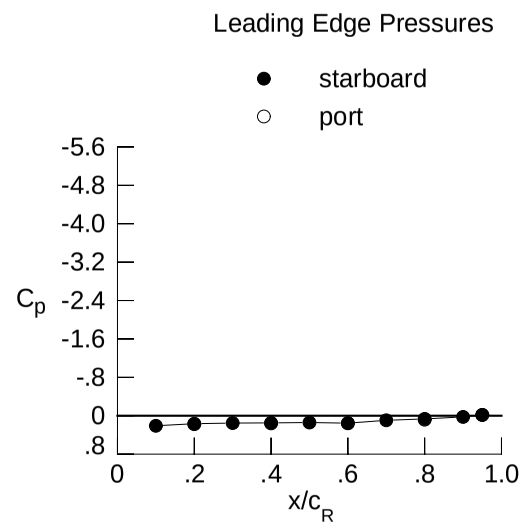

Small Radius L.E.

Run No. = 43 , Point No. = 897

$C_N$ = 0.030, $C_m$ = -0.0030

$\alpha$ = 1.1 °, $M_\infty$ = 0.902

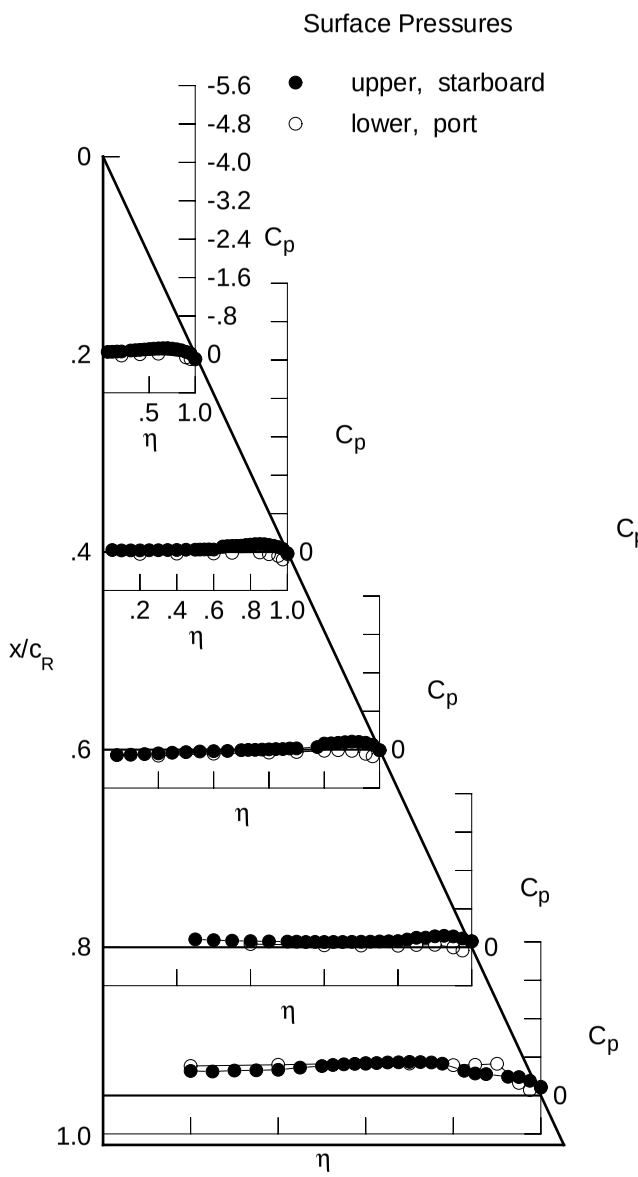
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2092 | ******* |
| 0.20 | 0.1661 | 0.1764 |
| 0.30 | 0.1527 | ******* |
| 0.40 | 0.1492 | 0.1590 |
| 0.50 | 0.1414 | ******* |
| 0.60 | 0.1547 | 0.1578 |
| 0.70 | 0.0955 | ******* |
| 0.80 | 0.0660 | 0.0822 |
| 0.90 | 0.0245 | ******* |
| 0.95 | -0.0184 | -0.0150 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0512 | -0.0418 | 0.1142 | ******* | ******* |
| 0.100 | -0.0545 | -0.0337 | 0.1064 | ******* | ******* |
| 0.150 | -0.0591 | -0.0343 | 0.0925 | ******* | ******* |
| 0.200 | -0.0601 | -0.0341 | 0.0780 | ******* | -0.5111 |
| 0.250 | ******* | -0.0377 | 0.0647 | -0.1650 | -0.5002 |
| 0.300 | -0.0811 | -0.0376 | 0.0522 | -0.1487 | -0.5200 |
| 0.350 | -0.0874 | -0.0416 | 0.0386 | -0.1372 | -0.5250 |
| 0.400 | -0.0938 | -0.0435 | 0.0313 | -0.1290 | -0.5359 |
| 0.450 | -0.1015 | -0.0480 | 0.0274 | -0.1221 | -0.5806 |
| 0.500 | -0.1099 | -0.0488 | 0.0108 | -0.1182 | -0.6140 |
| 0.525 | ******* | -0.0513 | 0.0054 | -0.1166 | -0.6364 |
| 0.550 | -0.1188 | -0.0539 | 0.0047 | -0.1102 | -0.6492 |
| 0.575 | ******* | -0.0553 | -0.0007 | -0.1120 | -0.6595 |
| 0.600 | -0.1260 | -0.0513 | -0.0053 | -0.1100 | -0.6624 |
| 0.625 | ******* | ******* | -0.0109 | -0.1112 | -0.6758 |
| 0.650 | -0.1291 | -0.1150 | -0.0118 | -0.1101 | -0.6878 |
| 0.675 | ******* | -0.1234 | -0.0240 | -0.1137 | -0.6916 |
| 0.700 | -0.1305 | -0.1274 | -0.0265 | -0.1156 | -0.6997 |
| 0.725 | ******* | -0.1291 | ******* | -0.1180 | -0.6963 |
| 0.750 | -0.1198 | -0.1324 | ******* | -0.1223 | -0.6883 |
| 0.775 | ******* | -0.1452 | -0.0538 | -0.1253 | -0.6636 |
| 0.800 | -0.1066 | -0.1547 | -0.1261 | -0.1295 | ******* |
| 0.825 | ******* | -0.1636 | -0.1316 | -0.1615 | -0.5152 |
| 0.850 | -0.0853 | -0.1660 | -0.1415 | -0.1984 | -0.4587 |
| 0.875 | ******* | -0.1635 | -0.1556 | -0.2005 | -0.4455 |
| 0.900 | -0.0530 | -0.1474 | -0.1675 | -0.2285 | ******* |
| 0.925 | ******* | -0.1296 | -0.1610 | -0.2389 | -0.3908 |
| 0.950 | -0.0162 | -0.1029 | -0.1433 | -0.2266 | -0.3838 |
| 0.975 | ******* | -0.0657 | -0.1007 | -0.1844 | -0.3071 |
| 1.000 | 0.0913 | 0.0220 | 0.0111 | -0.1271 | -0.1637 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0235 | 0.0386 | 0.1250 | ******* | -0.6151 |
| -0.400 | -0.0037 | 0.0322 | 0.0836 | -0.0669 | -0.6404 |
| -0.600 | -0.0153 | 0.0284 | 0.0605 | -0.0417 | -0.6750 |
| -0.700 | ******* | 0.0160 | 0.0488 | -0.0372 | -0.6664 |
| -0.800 | ******* | ******* | 0.0233 | -0.0325 | -0.6329 |
| -0.850 | ******* | 0.0082 | 0.0107 | -0.0480 | -0.6387 |
| -0.900 | 0.0626 | 0.0451 | 0.0249 | -0.0522 | -0.6610 |
| -0.950 | 0.0987 | 0.0798 | 0.0868 | 0.0026 | -0.2624 |
| -0.975 | ******* | 0.1548 | 0.1394 | 0.0676 | -0.1148 |
| -1.000 | 0.1040 | 0.0415 | 0.0131 | -0.1197 | -0.1823 |



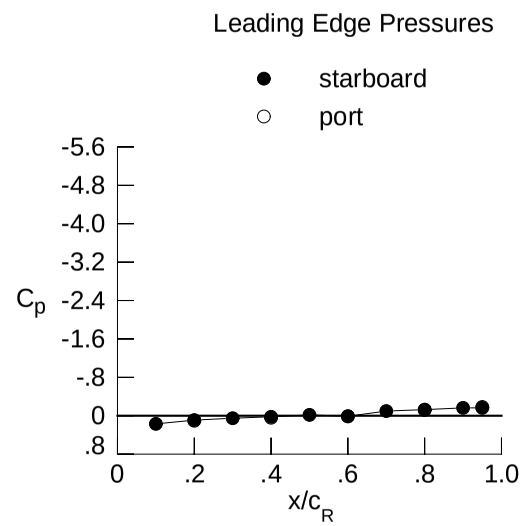

Small Radius L.E.

Run No. = 43 , Point No. = 898

$C_N$ = 0.073, $C_m$ = -0.0108

$\alpha$ = 2.2 °, $M_\infty$ = 0.900

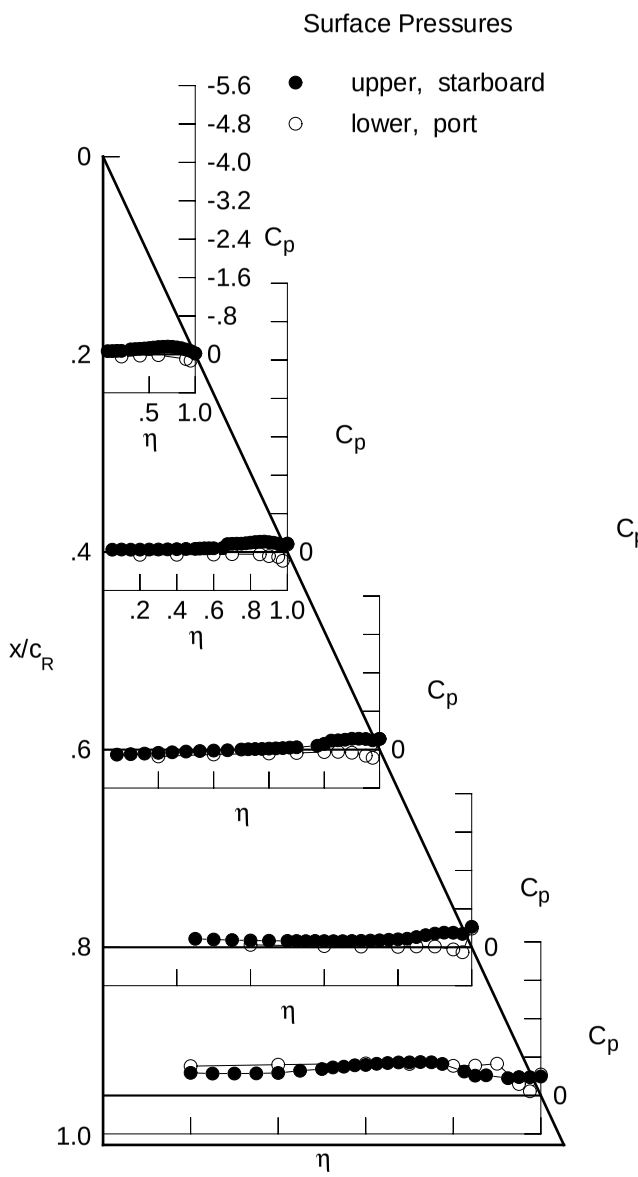
$R_{mac}$ = $6.0 \times 10^6$




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.1699 | ******* |
| 0.20 | 0.0913 | 0.1040 |
| 0.30 | 0.0516 | ******* |
| 0.40 | 0.0220 | 0.0415 |
| 0.50 | -0.0176 | ******* |
| 0.60 | 0.0111 | 0.0131 |
| 0.70 | -0.0970 | ******* |
| 0.80 | -0.1271 | -0.1197 |
| 0.90 | -0.1637 | ******* |
| 0.95 | -0.1637 | -0.1823 |

# Table D6. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0673 | -0.0486 | 0.1036 | ******* | ******* |
| 0.100 | -0.0685 | -0.0517 | 0.0944 | ******* | ******* |
| 0.150 | -0.0735 | -0.0484 | 0.0822 | ******* | ******* |
| 0.200 | -0.0735 | -0.0501 | 0.0666 | ******* | -0.4723 |
| 0.250 | ******* | -0.0524 | 0.0553 | -0.1768 | -0.4571 |
| 0.300 | -0.1050 | -0.0530 | 0.0399 | -0.1613 | -0.4572 |
| 0.350 | -0.1107 | -0.0562 | 0.0291 | -0.1505 | -0.4607 |
| 0.400 | -0.1164 | -0.0602 | 0.0191 | -0.1413 | -0.4697 |
| 0.450 | -0.1235 | -0.0649 | 0.0129 | -0.1359 | -0.5162 |
| 0.500 | -0.1311 | -0.0667 | -0.0026 | -0.1324 | -0.5509 |
| 0.525 | ******* | -0.0719 | -0.0079 | -0.1315 | -0.5844 |
| 0.550 | -0.1424 | -0.0774 | -0.0127 | -0.1281 | -0.6006 |
| 0.575 | ******* | -0.0787 | -0.0144 | -0.1323 | -0.6292 |
| 0.600 | -0.1530 | -0.0787 | -0.0217 | -0.1285 | -0.6372 |
| 0.625 | ******* | ******* | -0.0268 | -0.1268 | -0.6611 |
| 0.650 | -0.1585 | -0.0858 | -0.0322 | -0.1271 | -0.6767 |
| 0.675 | ******* | -0.1652 | -0.0420 | -0.1315 | -0.6889 |
| 0.700 | -0.1628 | -0.1713 | -0.0496 | -0.1341 | -0.6902 |
| 0.725 | ******* | -0.1734 | ******* | -0.1403 | -0.6970 |
| 0.750 | -0.1572 | -0.1736 | ******* | -0.1456 | -0.6918 |
| 0.775 | ******* | -0.1831 | -0.0818 | -0.1571 | -0.6574 |
| 0.800 | -0.1457 | -0.1950 | -0.1212 | -0.1657 | ******* |
| 0.825 | ******* | -0.2073 | -0.1892 | -0.1784 | -0.4990 |
| 0.850 | -0.1287 | -0.2140 | -0.1946 | -0.2127 | -0.4138 |
| 0.875 | ******* | -0.2177 | -0.2066 | -0.2525 | -0.4206 |
| 0.900 | -0.1006 | -0.2059 | -0.2269 | -0.2846 | ******* |
| 0.925 | ******* | -0.1934 | -0.2274 | -0.3051 | -0.3611 |
| 0.950 | -0.0708 | -0.1755 | -0.2226 | -0.3033 | -0.3841 |
| 0.975 | ******* | -0.1481 | -0.1946 | -0.2790 | -0.3811 |
| 1.000 | -0.0231 | -0.1769 | -0.2245 | -0.4271 | -0.3953 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0447 | 0.0572 | 0.1418 | ******* | -0.6119 |
| -0.400 | 0.0248 | 0.0559 | 0.1004 | -0.0504 | -0.6423 |
| -0.600 | 0.0152 | 0.0517 | 0.0796 | -0.0247 | -0.6684 |
| -0.700 | ******* | 0.0436 | 0.0693 | -0.0154 | -0.6567 |
| -0.800 | ******* | ******* | 0.0502 | -0.0100 | -0.6182 |
| -0.850 | ******* | 0.0474 | 0.0468 | -0.0187 | -0.6228 |
| -0.900 | 0.0965 | 0.0846 | 0.0642 | -0.0166 | -0.6627 |
| -0.950 | 0.1307 | 0.1023 | 0.1257 | 0.0448 | -0.2392 |
| -0.975 | ******* | 0.1827 | 0.1707 | 0.1035 | -0.0884 |
| -1.000 | -0.0172 | -0.1565 | -0.2242 | -0.3900 | -0.4376 |



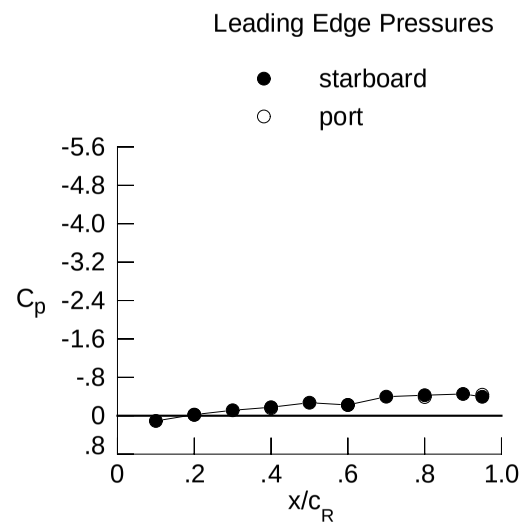

Small Radius L.E.

Run No. = 43 , Point No. = 899

$C_N$ = 0.121, $C_m$ = -0.0230

$\alpha$ = 3.2 °, $M_\infty$ = 0.899

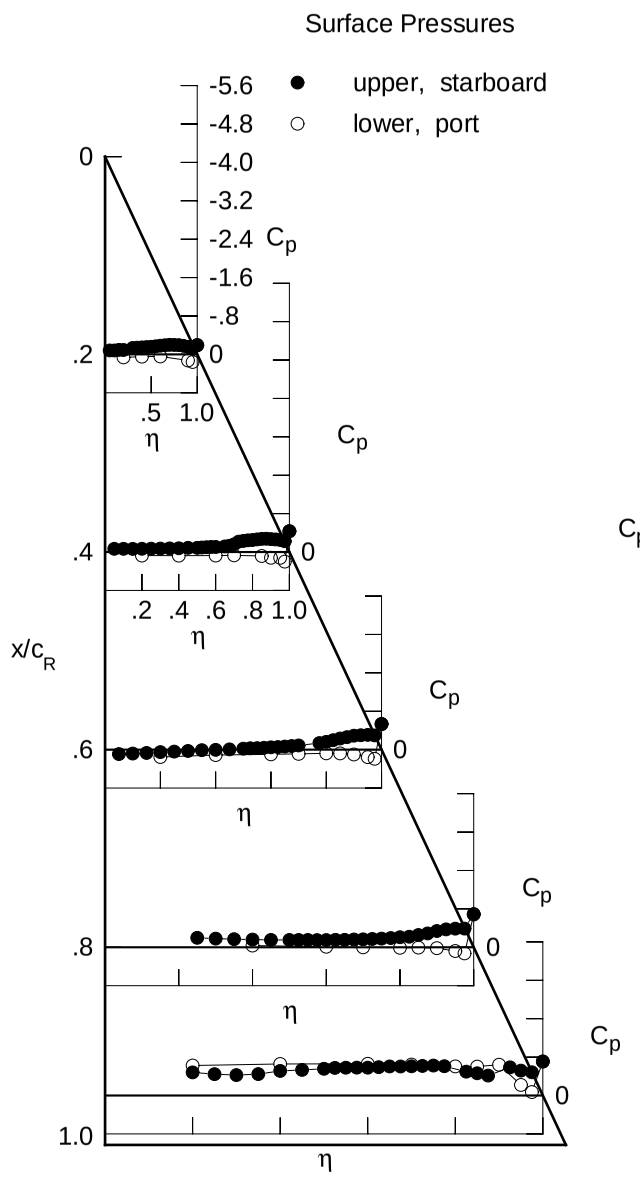
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.1085 | ******* |
| 0.20 | -0.0231 | -0.0172 |
| 0.30 | -0.1136 | ******* |
| 0.40 | -0.1769 | -0.1565 |
| 0.50 | -0.2714 | ******* |
| 0.60 | -0.2245 | -0.2242 |
| 0.70 | -0.3968 | ******* |
| 0.80 | -0.4271 | -0.3900 |
| 0.90 | -0.4534 | ******* |
| 0.95 | -0.3953 | -0.4376 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0827 | -0.0668 | 0.0917 | ******* | ******* |
| 0.100 | -0.0817 | -0.0669 | 0.0813 | ******* | ******* |
| 0.150 | -0.0938 | -0.0659 | 0.0691 | ******* | ******* |
| 0.200 | -0.0918 | -0.0677 | 0.0511 | ******* | -0.4816 |
| 0.250 | ******* | -0.0706 | 0.0412 | -0.1972 | -0.4448 |
| 0.300 | -0.1338 | -0.0723 | 0.0271 | -0.1807 | -0.4256 |
| 0.350 | -0.1397 | -0.0763 | 0.0114 | -0.1689 | -0.4463 |
| 0.400 | -0.1456 | -0.0781 | 0.0040 | -0.1608 | -0.5120 |
| 0.450 | -0.1516 | -0.0880 | -0.0055 | -0.1535 | -0.5333 |
| 0.500 | -0.1580 | -0.0876 | -0.0201 | -0.1526 | -0.5566 |
| 0.525 | ******* | -0.0945 | -0.0286 | -0.1526 | -0.5749 |
| 0.550 | -0.1690 | -0.1002 | -0.0314 | -0.1530 | -0.5796 |
| 0.575 | ******* | -0.1052 | -0.0383 | -0.1500 | -0.5809 |
| 0.600 | -0.1807 | -0.1058 | -0.0484 | -0.1506 | -0.5802 |
| 0.625 | ******* | ******* | -0.0534 | -0.1548 | -0.5903 |
| 0.650 | -0.1907 | -0.1172 | -0.0644 | -0.1551 | -0.6055 |
| 0.675 | ******* | -0.1304 | -0.0753 | -0.1627 | -0.6047 |
| 0.700 | -0.1990 | -0.1601 | -0.0872 | -0.1659 | -0.6090 |
| 0.725 | ******* | -0.2166 | ******* | -0.1733 | -0.6159 |
| 0.750 | -0.1968 | -0.2313 | ******* | -0.1810 | -0.6239 |
| 0.775 | ******* | -0.2439 | -0.1371 | -0.1924 | -0.6105 |
| 0.800 | -0.1928 | -0.2504 | -0.1628 | -0.2099 | ******* |
| 0.825 | ******* | -0.2636 | -0.1965 | -0.2201 | -0.4969 |
| 0.850 | -0.1783 | -0.2740 | -0.2321 | -0.2563 | -0.4632 |
| 0.875 | ******* | -0.2770 | -0.2602 | -0.2886 | -0.4149 |
| 0.900 | -0.1568 | -0.2700 | -0.2905 | -0.3392 | ******* |
| 0.925 | ******* | -0.2623 | -0.2998 | -0.3729 | -0.5869 |
| 0.950 | -0.1359 | -0.2513 | -0.3074 | -0.3880 | -0.5185 |
| 0.975 | ******* | -0.2247 | -0.2971 | -0.3897 | -0.4837 |
| 1.000 | -0.1875 | -0.4323 | -0.5376 | -0.6929 | -0.7068 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0625 | 0.0736 | 0.1533 | ******* | -0.6251 |
| -0.400 | 0.0467 | 0.0753 | 0.1126 | -0.0362 | -0.6570 |
| -0.600 | 0.0424 | 0.0737 | 0.0976 | -0.0108 | -0.6608 |
| -0.700 | ******* | 0.0688 | 0.0880 | 0.0007 | -0.6449 |
| -0.800 | ******* | ******* | 0.0765 | 0.0103 | -0.6064 |
| -0.850 | ******* | 0.0823 | 0.0781 | 0.0067 | -0.6026 |
| -0.900 | 0.1271 | 0.1189 | 0.1008 | 0.0181 | -0.6419 |
| -0.950 | 0.1582 | 0.1211 | 0.1561 | 0.0779 | -0.2202 |
| -0.975 | ******* | 0.1988 | 0.1905 | 0.1276 | -0.0722 |
| -1.000 | -0.1968 | -0.4362 | -0.5287 | -0.6825 | -0.7095 |



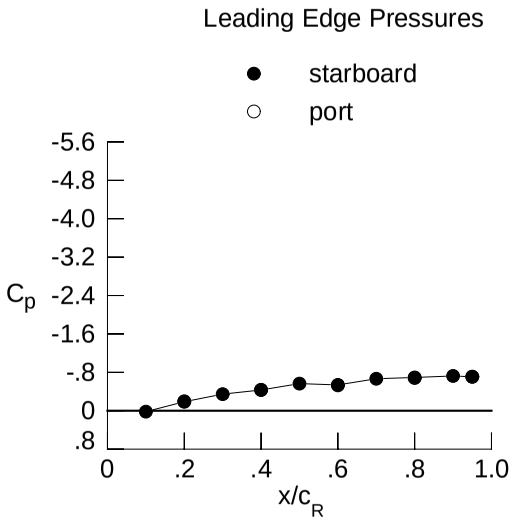

Small Radius L.E.

Run No. = 43 , Point No. = 900

$C_N$ = 0.169, $C_m$ = -0.0335

$\alpha$ = 4.2 °, $M_\infty$ = 0.901

$R_{mac}$ = $6.0 \times 10^6$

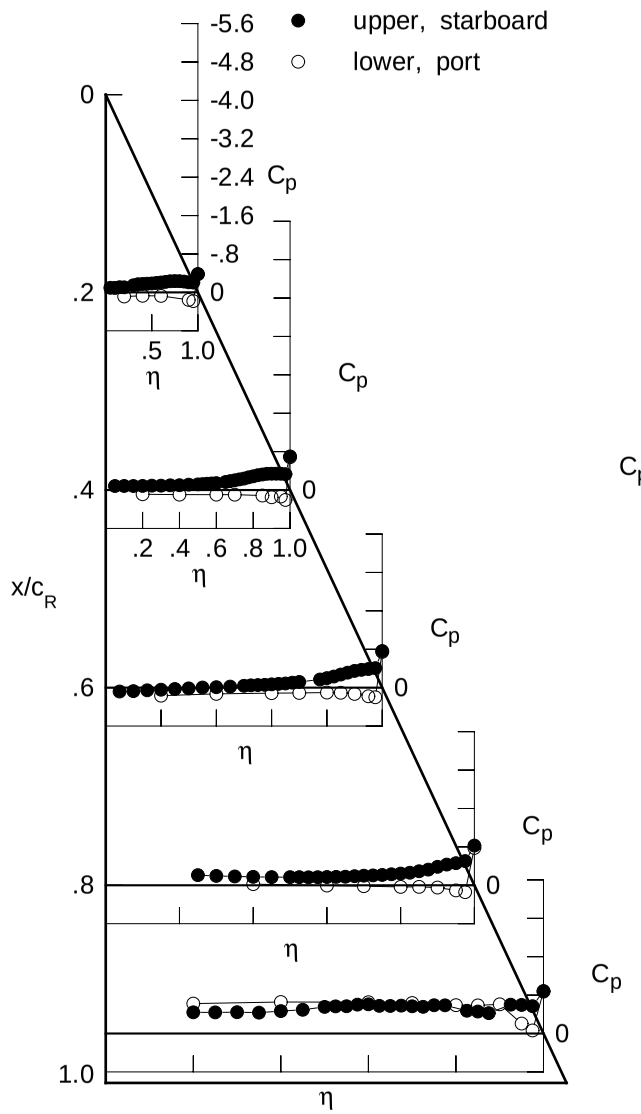



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.0188 | ******* |
| 0.20 | -0.1875 | -0.1968 |
| 0.30 | -0.3459 | ******* |
| 0.40 | -0.4323 | -0.4362 |
| 0.50 | -0.5651 | ******* |
| 0.60 | -0.5376 | -0.5287 |
| 0.70 | -0.6666 | ******* |
| 0.80 | -0.6929 | -0.6825 |
| 0.90 | -0.7246 | ******* |
| 0.95 | -0.7068 | -0.7095 |

# Table D6. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0963 | -0.0842 | 0.0805 | ******* | ******* |
| 0.100 | -0.0932 | -0.0847 | 0.0725 | ******* | ******* |
| 0.150 | -0.1078 | -0.0843 | 0.0552 | ******* | ******* |
| 0.200 | -0.1059 | -0.0856 | 0.0435 | ******* | -0.4412 |
| 0.250 | ******* | -0.0909 | 0.0278 | -0.2109 | -0.4396 |
| 0.300 | -0.1480 | -0.0916 | 0.0153 | -0.1949 | -0.4442 |
| 0.350 | -0.1703 | -0.0981 | -0.0023 | -0.1839 | -0.4347 |
| 0.400 | -0.1754 | -0.1007 | -0.0096 | -0.1758 | -0.4673 |
| 0.450 | -0.1811 | -0.1117 | -0.0220 | -0.1702 | -0.4945 |
| 0.500 | -0.1863 | -0.1177 | -0.0386 | -0.1695 | -0.5545 |
| 0.525 | ******* | -0.1229 | -0.0476 | -0.1699 | -0.5654 |
| 0.550 | -0.1958 | -0.1313 | -0.0535 | -0.1663 | -0.5683 |
| 0.575 | ******* | -0.1379 | -0.0586 | -0.1688 | -0.6012 |
| 0.600 | -0.2067 | -0.1437 | -0.0685 | -0.1726 | -0.6092 |
| 0.625 | ******* | ******* | -0.0787 | -0.1749 | -0.5756 |
| 0.650 | -0.2196 | -0.1671 | -0.0865 | -0.1788 | -0.5736 |
| 0.675 | ******* | -0.1858 | -0.1031 | -0.1899 | -0.5812 |
| 0.700 | -0.2318 | -0.2027 | -0.1187 | -0.1999 | -0.5673 |
| 0.725 | ******* | -0.2219 | ******* | -0.2058 | -0.5560 |
| 0.750 | -0.2349 | -0.2386 | ******* | -0.2150 | -0.5892 |
| 0.775 | ******* | -0.2650 | -0.1698 | -0.2294 | -0.5875 |
| 0.800 | -0.2335 | -0.2856 | -0.1987 | -0.2441 | ******* |
| 0.825 | ******* | -0.3092 | -0.2312 | -0.2618 | -0.4747 |
| 0.850 | -0.2254 | -0.3243 | -0.2725 | -0.2930 | -0.4578 |
| 0.875 | ******* | -0.3383 | -0.3116 | -0.3266 | -0.4242 |
| 0.900 | -0.2093 | -0.3397 | -0.3485 | -0.3849 | ******* |
| 0.925 | ******* | -0.3403 | -0.3715 | -0.4313 | -0.6011 |
| 0.950 | -0.2040 | -0.3389 | -0.3877 | -0.4605 | -0.5951 |
| 0.975 | ******* | -0.3309 | -0.4067 | -0.5050 | -0.5696 |
| 1.000 | -0.3812 | -0.7008 | -0.7633 | -0.8268 | -0.8855 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.0858 | 0.0884 | 0.1674 | ******* | -0.6231 |
| -0.400 | 0.0705 | 0.0956 | 0.1296 | -0.0240 | -0.6562 |
| -0.600 | 0.0724 | 0.0964 | 0.1152 | 0.0058 | -0.6520 |
| -0.700 | ******* | 0.0965 | 0.1104 | 0.0185 | -0.6351 |
| -0.800 | ******* | ******* | 0.1023 | 0.0338 | -0.5903 |
| -0.850 | ******* | 0.1145 | 0.1064 | 0.0326 | -0.5860 |
| -0.900 | 0.1560 | 0.1505 | 0.1305 | 0.0475 | -0.6083 |
| -0.950 | 0.1820 | 0.1351 | 0.1796 | 0.1062 | -0.2068 |
| -0.975 | ******* | 0.2066 | 0.2000 | 0.1424 | -0.0644 |
| -1.000 | -0.3797 | -0.6836 | -0.7442 | -0.7772 | -0.8721 |

Surface Pressures




Small Radius L.E.

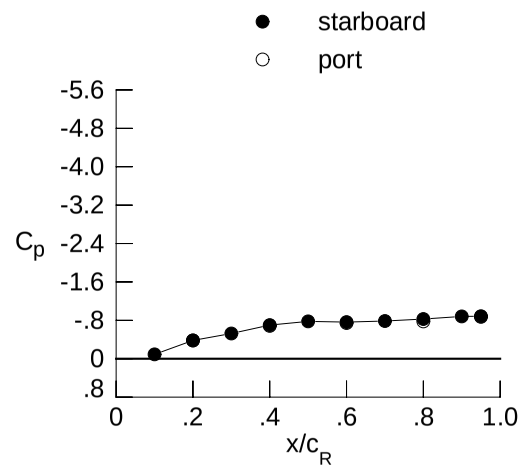
Run No. = 43 , Point No. = 901

$C_N$ = 0.212, $C_m$ = -0.0399

$\alpha$ = 5.3 °, $M_\infty$ = 0.901

$R_{mac}$ = $6.0 \times 10^6$

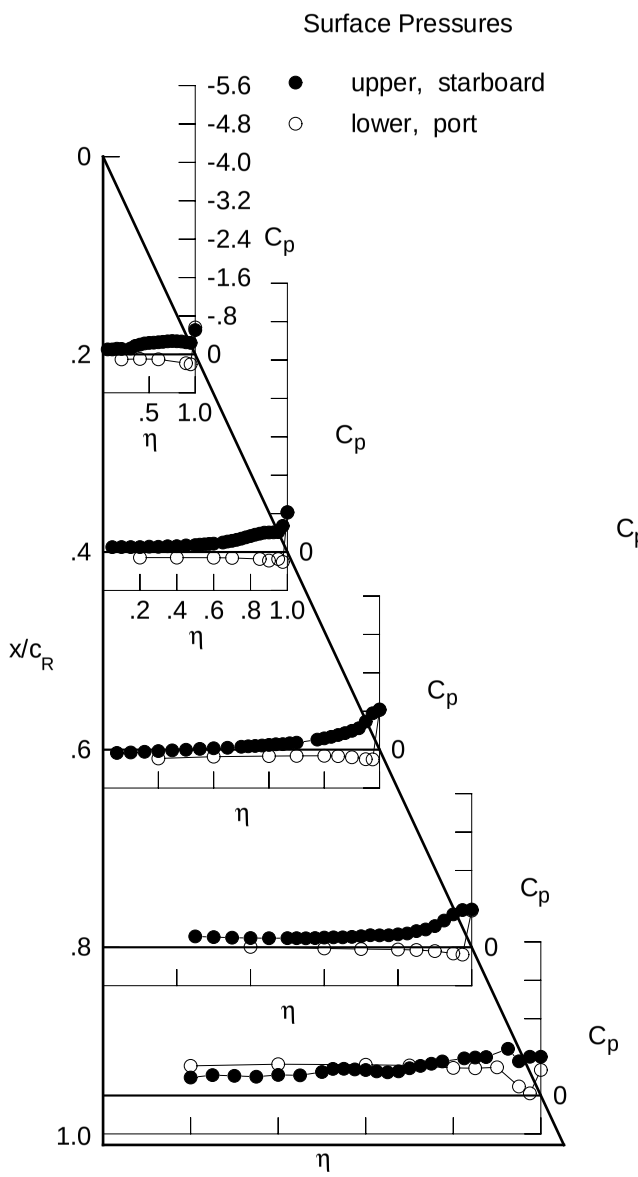
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.0909 | ******* |
| 0.20 | -0.3812 | -0.3797 |
| 0.30 | -0.5256 | ******* |
| 0.40 | -0.7008 | -0.6836 |
| 0.50 | -0.7781 | ******* |
| 0.60 | -0.7633 | -0.7442 |
| 0.70 | -0.7855 | ******* |
| 0.80 | -0.8268 | -0.7772 |
| 0.90 | -0.8813 | ******* |
| 0.95 | -0.8855 | -0.8721 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1043 | -0.1023 | 0.0685 | ******* | ******* |
| 0.100 | -0.1030 | -0.1036 | 0.0593 | ******* | ******* |
| 0.150 | -0.1183 | -0.1035 | 0.0450 | ******* | ******* |
| 0.200 | -0.1144 | -0.1033 | 0.0298 | ******* | -0.3743 |
| 0.250 | ******* | -0.1120 | 0.0152 | -0.2264 | -0.4246 |
| 0.300 | -0.1250 | -0.1099 | 0.0027 | -0.2121 | -0.4092 |
| 0.350 | -0.1770 | -0.1207 | -0.0162 | -0.1997 | -0.3910 |
| 0.400 | -0.2029 | -0.1223 | -0.0287 | -0.1930 | -0.4291 |
| 0.450 | -0.2278 | -0.1378 | -0.0388 | -0.1886 | -0.4198 |
| 0.500 | -0.2391 | -0.1440 | -0.0599 | -0.1904 | -0.4898 |
| 0.525 | ******* | -0.1533 | -0.0692 | -0.1893 | -0.5541 |
| 0.550 | -0.2437 | -0.1601 | -0.0769 | -0.1870 | -0.5567 |
| 0.575 | ******* | -0.1685 | -0.0859 | -0.1923 | -0.5432 |
| 0.600 | -0.2525 | -0.1740 | -0.0986 | -0.2025 | -0.5313 |
| 0.625 | ******* | ******* | -0.1118 | -0.2070 | -0.5026 |
| 0.650 | -0.2620 | -0.1976 | -0.1141 | -0.2069 | -0.4836 |
| 0.675 | ******* | -0.2186 | -0.1328 | -0.2164 | -0.5033 |
| 0.700 | -0.2718 | -0.2340 | -0.1448 | -0.2302 | -0.5684 |
| 0.725 | ******* | -0.2544 | ******* | -0.2512 | -0.6169 |
| 0.750 | -0.2783 | -0.2784 | ******* | -0.2489 | -0.6614 |
| 0.775 | ******* | -0.3067 | -0.2084 | -0.2508 | -0.7097 |
| 0.800 | -0.2735 | -0.3327 | -0.2353 | -0.2700 | ******* |
| 0.825 | ******* | -0.3608 | -0.2660 | -0.2871 | -0.7733 |
| 0.850 | -0.2691 | -0.3827 | -0.3048 | -0.3371 | -0.7914 |
| 0.875 | ******* | -0.4037 | -0.3443 | -0.3713 | -0.8012 |
| 0.900 | -0.2519 | -0.4072 | -0.3922 | -0.4413 | ******* |
| 0.925 | ******* | -0.4101 | -0.4453 | -0.5570 | -0.9726 |
| 0.950 | -0.2398 | -0.4148 | -0.5850 | -0.6857 | -0.7127 |
| 0.975 | ******* | -0.5451 | -0.7578 | -0.7758 | -0.8070 |
| 1.000 | -0.5060 | -0.8320 | -0.8378 | -0.7864 | -0.8075 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1038 | 0.1157 | 0.1840 | ******* | -0.6178 |
| -0.400 | 0.0954 | 0.1164 | 0.1467 | -0.0078 | -0.6519 |
| -0.600 | 0.1023 | 0.1181 | 0.1346 | 0.0242 | -0.6407 |
| -0.700 | ******* | 0.1226 | 0.1301 | 0.0368 | -0.6259 |
| -0.800 | ******* | ******* | 0.1277 | 0.0464 | -0.5753 |
| -0.850 | ******* | 0.1450 | 0.1348 | 0.0565 | -0.5682 |
| -0.900 | 0.1837 | 0.1784 | 0.1593 | 0.0795 | -0.5872 |
| -0.950 | 0.2060 | 0.1453 | 0.1988 | 0.1287 | -0.1883 |
| -0.975 | ******* | 0.2067 | 0.2032 | 0.1519 | -0.0451 |
| -1.000 | -0.5605 | -0.8193 | -0.8250 | -0.7643 | -0.5330 |



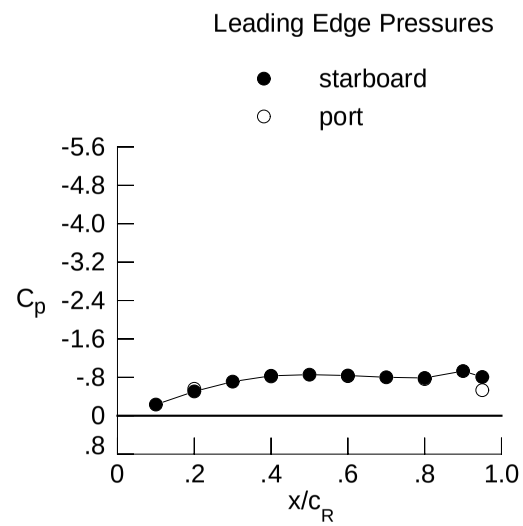

Small Radius L.E.

Run No. = 43 , Point No. = 902

$C_N$ = 0.263, $C_m$ = -0.0505

$\alpha$ = 6.3 °, $M_\infty$ = 0.900

$R_{mac}$ = $6.0 \times 10^6$

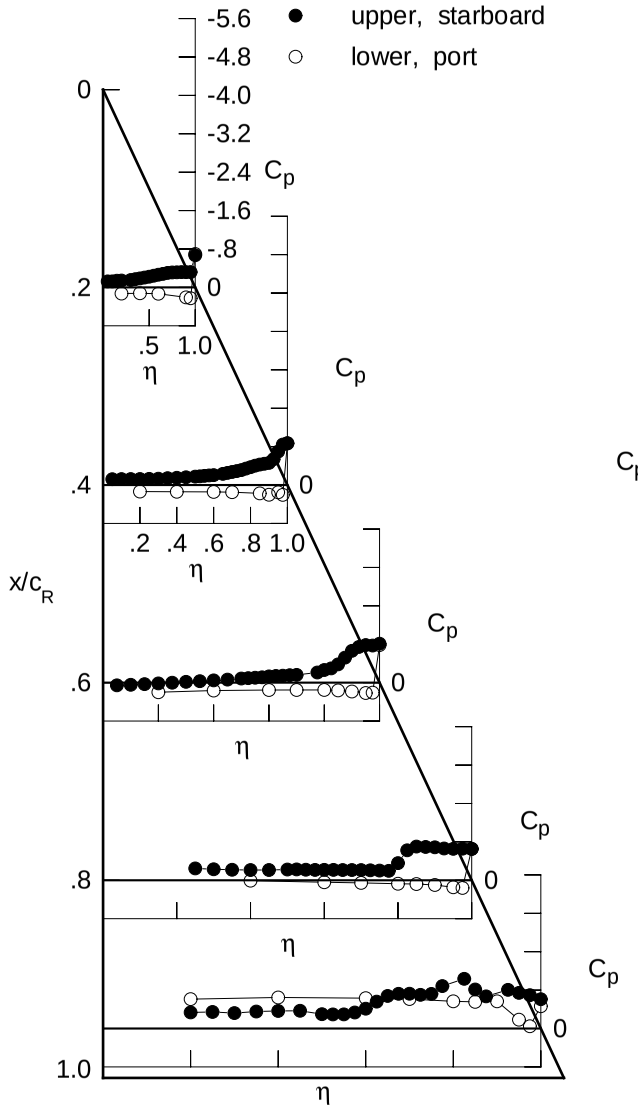



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.2326 | ******* |
| 0.20 | -0.5060 | -0.5605 |
| 0.30 | -0.7107 | ******* |
| 0.40 | -0.8320 | -0.8193 |
| 0.50 | -0.8556 | ******* |
| 0.60 | -0.8378 | -0.8250 |
| 0.70 | -0.8009 | ******* |
| 0.80 | -0.7864 | -0.7643 |
| 0.90 | -0.9304 | ******* |
| 0.95 | -0.8075 | -0.5330 |

# Table D6. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1257 | -0.1212 | 0.0556 | ******* | ******* |
| 0.100 | -0.1258 | -0.1240 | 0.0449 | ******* | ******* |
| 0.150 | -0.1391 | -0.1244 | 0.0311 | ******* | ******* |
| 0.200 | -0.1429 | -0.1252 | 0.0158 | ******* | -0.3350 |
| 0.250 | ******* | -0.1290 | 0.0014 | -0.2470 | -0.3448 |
| 0.300 | -0.1536 | -0.1317 | -0.0168 | -0.2298 | -0.3213 |
| 0.350 | -0.1711 | -0.1433 | -0.0303 | -0.2195 | -0.3539 |
| 0.400 | -0.1875 | -0.1511 | -0.0475 | -0.2135 | -0.3658 |
| 0.450 | -0.2048 | -0.1619 | -0.0628 | -0.2145 | -0.3695 |
| 0.500 | -0.2227 | -0.1753 | -0.0855 | -0.2238 | -0.2983 |
| 0.525 | ******* | -0.1818 | -0.0937 | -0.2262 | -0.2939 |
| 0.550 | -0.2435 | -0.1911 | -0.1023 | -0.2199 | -0.2941 |
| 0.575 | ******* | -0.2003 | -0.1114 | -0.2159 | -0.3338 |
| 0.600 | -0.2638 | -0.2063 | -0.1304 | -0.2180 | -0.4128 |
| 0.625 | ******* | ******* | -0.1392 | -0.2172 | -0.5603 |
| 0.650 | -0.2814 | -0.2331 | -0.1447 | -0.2136 | -0.6786 |
| 0.675 | ******* | -0.2527 | -0.1552 | -0.2137 | -0.7235 |
| 0.700 | -0.3013 | -0.2720 | -0.1616 | -0.2127 | -0.7248 |
| 0.725 | ******* | -0.2905 | ******* | -0.2077 | -0.7019 |
| 0.750 | -0.3115 | -0.3113 | ******* | -0.2023 | -0.7210 |
| 0.775 | ******* | -0.3421 | -0.2110 | -0.1969 | -0.8840 |
| 0.800 | -0.3141 | -0.3719 | -0.2635 | -0.3577 | ******* |
| 0.825 | ******* | -0.4029 | -0.2967 | -0.6251 | -1.0353 |
| 0.850 | -0.3186 | -0.4263 | -0.3809 | -0.7022 | -0.8126 |
| 0.875 | ******* | -0.4428 | -0.5211 | -0.6945 | -0.6694 |
| 0.900 | -0.3178 | -0.4607 | -0.6628 | -0.6872 | ******* |
| 0.925 | ******* | -0.5381 | -0.7432 | -0.6625 | -0.8053 |
| 0.950 | -0.3193 | -0.6979 | -0.7829 | -0.6556 | -0.7427 |
| 0.975 | ******* | -0.8430 | -0.7727 | -0.6585 | -0.6941 |
| 1.000 | -0.6694 | -0.8728 | -0.8114 | -0.6548 | -0.6102 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1285 | 0.1360 | 0.1996 | ******* | -0.6117 |
| -0.400 | 0.1228 | 0.1399 | 0.1645 | 0.0083 | -0.6468 |
| -0.600 | 0.1320 | 0.1431 | 0.1538 | 0.0406 | -0.6323 |
| -0.700 | ******* | 0.1489 | 0.1527 | 0.0543 | -0.6147 |
| -0.800 | ******* | ******* | 0.1521 | 0.0720 | -0.5660 |
| -0.850 | ******* | 0.1734 | 0.1616 | 0.0781 | -0.5554 |
| -0.900 | 0.2078 | 0.2025 | 0.1846 | 0.0975 | -0.5663 |
| -0.950 | 0.2267 | 0.1512 | 0.2162 | 0.1459 | -0.1838 |
| -0.975 | ******* | 0.2050 | 0.2077 | 0.1596 | -0.0469 |
| -1.000 | -0.6961 | -0.8653 | -0.7825 | -0.6536 | -0.4639 |

Surface Pressures




Small Radius L.E.

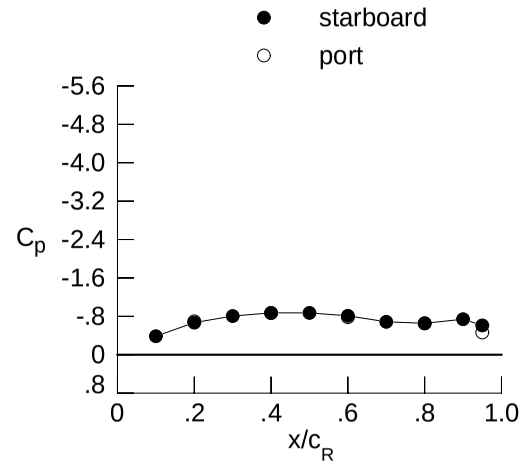
Run No. = 43 , Point No. = 903

$C_N$ = 0.323, $C_m$ = -0.0652

$\alpha$ = 7.3 °, $M_\infty$ = 0.900

$R_{mac}$ = $6.0 \times 10^6$

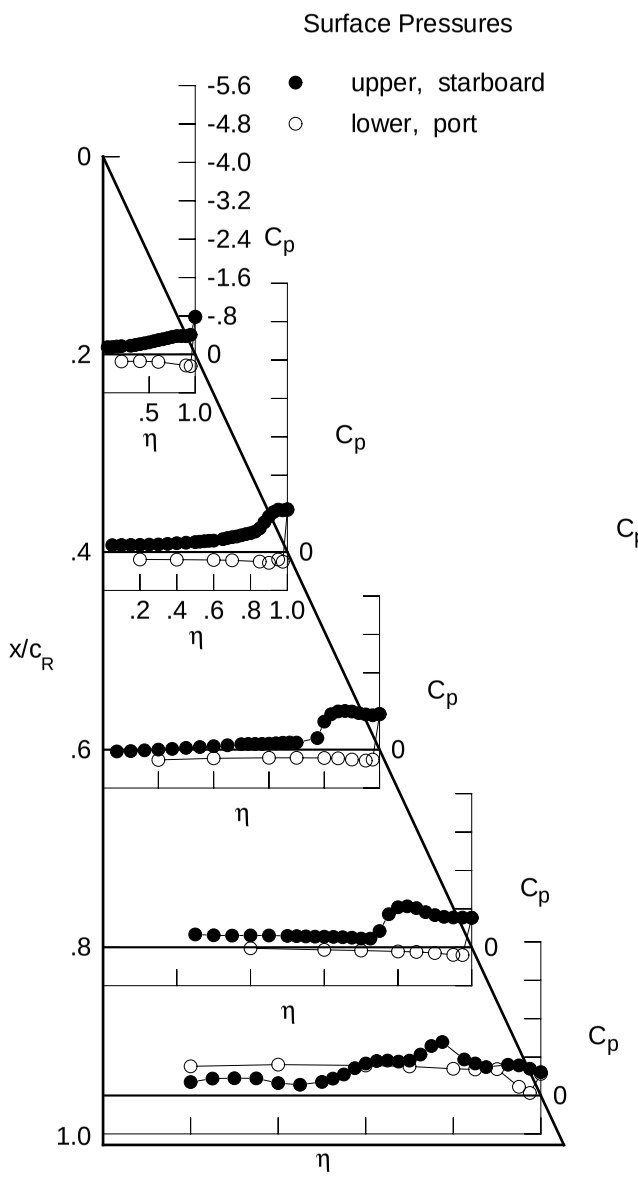
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.3860 | ******* |
| 0.20 | -0.6694 | -0.6961 |
| 0.30 | -0.8054 | ******* |
| 0.40 | -0.8728 | -0.8653 |
| 0.50 | -0.8713 | ******* |
| 0.60 | -0.8114 | -0.7825 |
| 0.70 | -0.6859 | ******* |
| 0.80 | -0.6548 | -0.6536 |
| 0.90 | -0.7398 | ******* |
| 0.95 | -0.6102 | -0.4639 |

# Table D6. Continued.

| η | x/c_R .2 Cp,u | x/c_R .4 Cp,u | x/c_R .6 Cp,u | x/c_R .8 Cp,u | x/c_R .95 Cp,u |
|---|---|---|---|---|---|
| 0.050 | -0.1508 | -0.1428 | 0.0380 | ******* | ******* |
| 0.100 | -0.1523 | -0.1463 | 0.0306 | ******* | ******* |
| 0.150 | -0.1643 | -0.1471 | 0.0147 | ******* | ******* |
| 0.200 | -0.1710 | -0.1489 | -0.0009 | ******* | -0.2798 |
| 0.250 | ******* | -0.1544 | -0.0154 | -0.2671 | -0.3532 |
| 0.300 | -0.1798 | -0.1579 | -0.0365 | -0.2502 | -0.3604 |
| 0.350 | -0.1953 | -0.1698 | -0.0542 | -0.2429 | -0.3568 |
| 0.400 | -0.2133 | -0.1841 | -0.0720 | -0.2474 | -0.2582 |
| 0.450 | -0.2320 | -0.1948 | -0.0912 | -0.2456 | -0.2238 |
| 0.500 | -0.2507 | -0.2070 | -0.1138 | -0.2369 | -0.2829 |
| 0.525 | ******* | -0.2155 | -0.1183 | -0.2325 | -0.3517 |
| 0.550 | -0.2744 | -0.2253 | -0.1183 | -0.2264 | -0.4374 |
| 0.575 | ******* | -0.2336 | -0.1191 | -0.2216 | -0.5693 |
| 0.600 | -0.2976 | -0.2378 | -0.1238 | -0.2206 | -0.6662 |
| 0.625 | ******* | ******* | -0.1329 | -0.2171 | -0.7195 |
| 0.650 | -0.3158 | -0.2670 | -0.1435 | -0.2094 | -0.7279 |
| 0.675 | ******* | -0.2922 | -0.1487 | -0.2004 | -0.7066 |
| 0.700 | -0.3386 | -0.3094 | -0.1469 | -0.1819 | -0.7273 |
| 0.725 | ******* | -0.3239 | ******* | -0.1800 | -0.8527 |
| 0.750 | -0.3633 | -0.3486 | ******* | -0.3385 | -1.0310 |
| 0.775 | ******* | -0.3728 | -0.2408 | -0.6886 | -1.1148 |
| 0.800 | -0.3812 | -0.3926 | -0.5839 | -0.8336 | ******* |
| 0.825 | ******* | -0.4246 | -0.7381 | -0.8529 | -0.7514 |
| 0.850 | -0.3820 | -0.4930 | -0.7963 | -0.8159 | -0.6670 |
| 0.875 | ******* | -0.6194 | -0.8052 | -0.7316 | -0.5924 |
| 0.900 | -0.3793 | -0.7417 | -0.7934 | -0.6706 | ******* |
| 0.925 | ******* | -0.8321 | -0.7606 | -0.6342 | -0.6410 |
| 0.950 | -0.4090 | -0.8836 | -0.7335 | -0.6206 | -0.6271 |
| 0.975 | ******* | -0.8681 | -0.7157 | -0.6186 | -0.5574 |
| 1.000 | -0.7853 | -0.8934 | -0.7463 | -0.6163 | -0.4863 |
| | Cp,l | Cp,l | Cp,l | Cp,l | Cp,l |
| -0.200 | 0.1475 | 0.1553 | 0.2142 | ******* | -0.6079 |
| -0.400 | 0.1416 | 0.1583 | 0.1810 | 0.0210 | -0.6435 |
| -0.600 | 0.1557 | 0.1656 | 0.1700 | 0.0536 | -0.6255 |
| -0.700 | ******* | 0.1729 | 0.1705 | 0.0676 | -0.6055 |
| -0.800 | ******* | ******* | 0.1734 | 0.0869 | -0.5565 |
| -0.850 | ******* | 0.1989 | 0.1812 | 0.0967 | -0.5431 |
| -0.900 | 0.2307 | 0.2245 | 0.2064 | 0.1198 | -0.5493 |
| -0.950 | 0.2439 | 0.1557 | 0.2279 | 0.1572 | -0.1816 |
| -0.975 | ******* | 0.2014 | 0.2069 | 0.1610 | -0.0526 |
| -1.000 | -0.7760 | -0.8762 | -0.7333 | -0.6128 | -0.4504 |



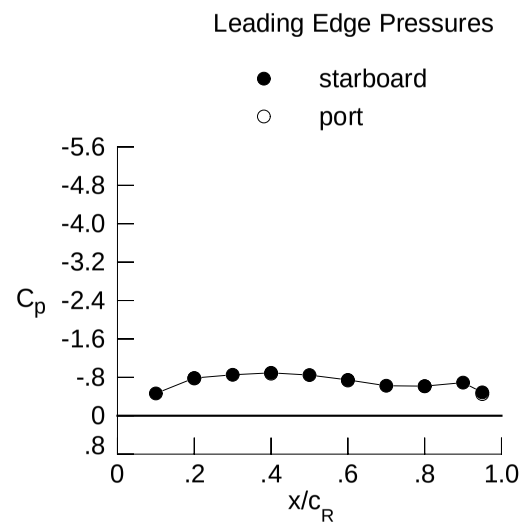

Small Radius L.E.

Run No. = 43 , Point No. = 904

$C_N$ = 0.376, $C_m$ = -0.0751

$\alpha$ = 8.3 °, $M_\infty$ = 0.901

$R_{mac}$ = $6.0 \times 10^6$

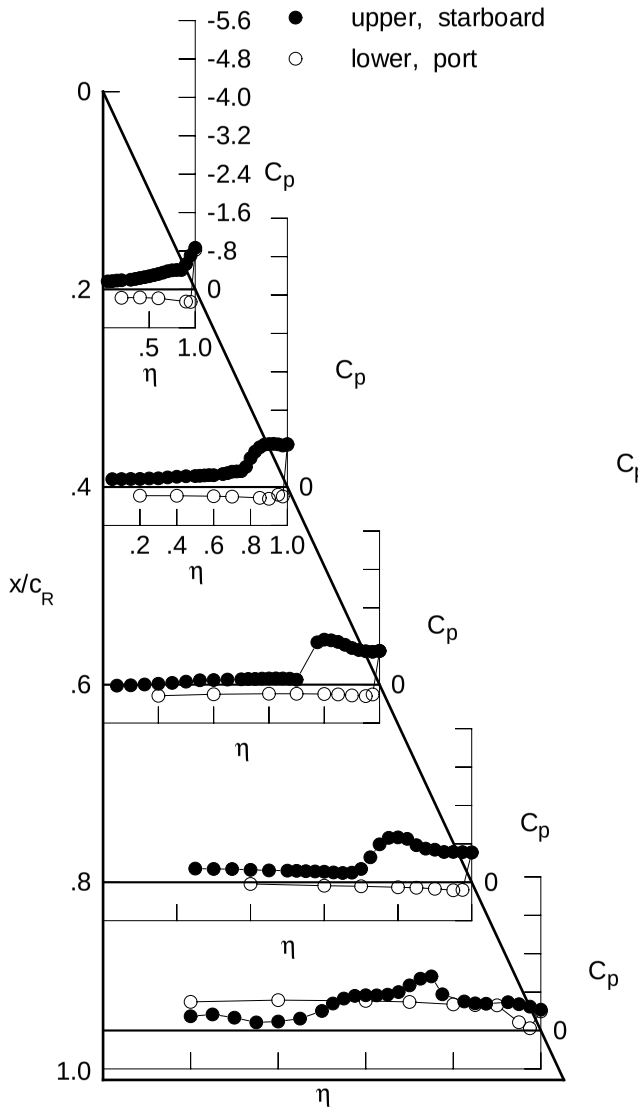



| x/c_R | starb'd Cp | port Cp |
|---|---|---|
| 0.10 | -0.4641 | ******* |
| 0.20 | -0.7853 | -0.7760 |
| 0.30 | -0.8530 | ******* |
| 0.40 | -0.8934 | -0.8762 |
| 0.50 | -0.8470 | ******* |
| 0.60 | -0.7463 | -0.7333 |
| 0.70 | -0.6244 | ******* |
| 0.80 | -0.6163 | -0.6128 |
| 0.90 | -0.6899 | ******* |
| 0.95 | -0.4863 | -0.4504 |

# Table D6. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.1673 | -0.1637 | 0.0212 | ******* | ******* |
| 0.100 | -0.1724 | -0.1655 | 0.0133 | ******* | ******* |
| 0.150 | -0.1841 | -0.1684 | -0.0033 | ******* | ******* |
| 0.200 | -0.1904 | -0.1691 | -0.0187 | ******* | -0.2965 |
| 0.250 | ******* | -0.1780 | -0.0358 | -0.2859 | -0.3347 |
| 0.300 | -0.2007 | -0.1818 | -0.0622 | -0.2773 | -0.2674 |
| 0.350 | -0.2179 | -0.2004 | -0.0913 | -0.2761 | -0.1691 |
| 0.400 | -0.2371 | -0.2145 | -0.0960 | -0.2593 | -0.1869 |
| 0.450 | -0.2542 | -0.2248 | -0.1059 | -0.2471 | -0.2480 |
| 0.500 | -0.2733 | -0.2289 | -0.1114 | -0.2420 | -0.4075 |
| 0.525 | ******* | -0.2347 | -0.1181 | -0.2381 | -0.5625 |
| 0.550 | -0.2969 | -0.2417 | -0.1190 | -0.2309 | -0.6659 |
| 0.575 | ******* | -0.2478 | -0.1253 | -0.2258 | -0.7218 |
| 0.600 | -0.3210 | -0.2464 | -0.1291 | -0.2199 | -0.7344 |
| 0.625 | ******* | ******* | -0.1300 | -0.2050 | -0.7319 |
| 0.650 | -0.3491 | -0.2706 | -0.1287 | -0.1932 | -0.7461 |
| 0.675 | ******* | -0.2899 | -0.1237 | -0.2010 | -0.8006 |
| 0.700 | -0.3785 | -0.3192 | -0.1023 | -0.2772 | -0.9403 |
| 0.725 | ******* | -0.3249 | ******* | -0.5207 | -1.0796 |
| 0.750 | -0.3977 | -0.3311 | ******* | -0.7903 | -1.1275 |
| 0.775 | ******* | -0.4197 | -0.8814 | -0.9265 | -0.7543 |
| 0.800 | -0.4037 | -0.6007 | -0.9375 | -0.9354 | ******* |
| 0.825 | ******* | -0.7377 | -0.9232 | -0.9051 | -0.6046 |
| 0.850 | -0.4038 | -0.8277 | -0.8908 | -0.7731 | -0.5659 |
| 0.875 | ******* | -0.8830 | -0.8308 | -0.7008 | -0.5574 |
| 0.900 | -0.5285 | -0.8953 | -0.7643 | -0.6787 | ******* |
| 0.925 | ******* | -0.9000 | -0.7217 | -0.6316 | -0.5895 |
| 0.950 | -0.7074 | -0.8895 | -0.6959 | -0.6331 | -0.5484 |
| 0.975 | ******* | -0.8652 | -0.6834 | -0.6281 | -0.4973 |
| 1.000 | -0.8663 | -0.8953 | -0.7056 | -0.6188 | -0.4333 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.1753 | 0.1798 | 0.2316 | ******* | -0.5967 |
| -0.400 | 0.1686 | 0.1816 | 0.2006 | 0.0351 | -0.6331 |
| -0.600 | 0.1849 | 0.1914 | 0.1896 | 0.0713 | -0.6169 |
| -0.700 | ******* | 0.2002 | 0.1901 | 0.0836 | -0.5947 |
| -0.800 | ******* | ******* | 0.1956 | 0.1043 | -0.5441 |
| -0.850 | ******* | 0.2253 | 0.2043 | 0.1139 | -0.5299 |
| -0.900 | 0.2534 | 0.2448 | 0.2250 | 0.1350 | -0.5248 |
| -0.950 | 0.2606 | 0.1599 | 0.2383 | 0.1660 | -0.1719 |
| -0.975 | ******* | 0.1969 | 0.2042 | 0.1587 | -0.0473 |
| -1.000 | -0.8230 | -0.8791 | -0.6985 | -0.6222 | -0.3975 |

Surface Pressures




Small Radius L.E.

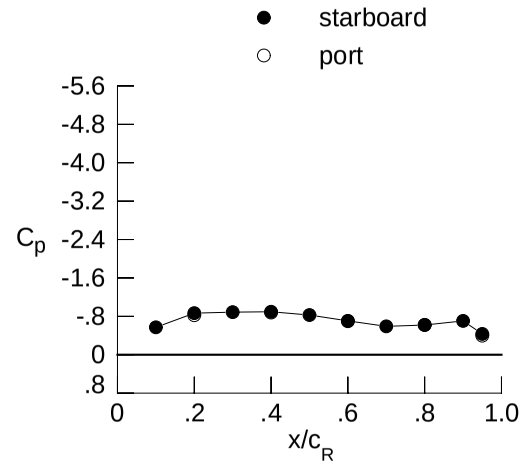
Run No. = 43 , Point No. = 905

$C_N$ = 0.435, $C_m$ = -0.0871

$\alpha$ = 9.4 °, $M_\infty$ = 0.902

$R_{mac}$ = $6.0 \times 10^6$

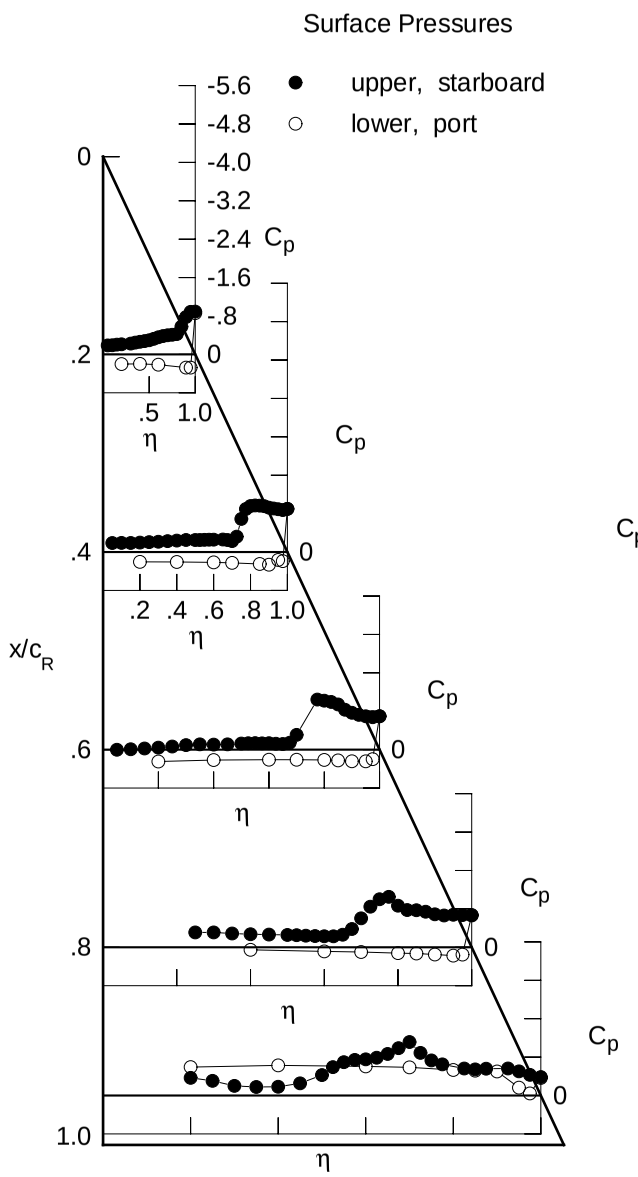
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.5711 | ******* |
| 0.20 | -0.8663 | -0.8230 |
| 0.30 | -0.8871 | ******* |
| 0.40 | -0.8953 | -0.8791 |
| 0.50 | -0.8270 | ******* |
| 0.60 | -0.7056 | -0.6985 |
| 0.70 | -0.5911 | ******* |
| 0.80 | -0.6188 | -0.6222 |
| 0.90 | -0.7046 | ******* |
| 0.95 | -0.4333 | -0.3975 |

# Table D6. Continued.

| η | x/c_R .2 Cp,u | x/c_R .4 Cp,u | x/c_R .6 Cp,u | x/c_R .8 Cp,u | x/c_R .95 Cp,u |
|---|---|---|---|---|---|
| 0.050 | -0.1870 | -0.1884 | 0.0026 | ******* | ******* |
| 0.100 | -0.1906 | -0.1906 | -0.0083 | ******* | ******* |
| 0.150 | -0.2035 | -0.1889 | -0.0239 | ******* | ******* |
| 0.200 | -0.2103 | -0.1971 | -0.0415 | ******* | -0.3684 |
| 0.250 | ******* | -0.2064 | -0.0644 | -0.3099 | -0.3057 |
| 0.300 | -0.2244 | -0.2144 | -0.0941 | -0.3094 | -0.2004 |
| 0.350 | -0.2460 | -0.2275 | -0.1105 | -0.2868 | -0.1778 |
| 0.400 | -0.2623 | -0.2386 | -0.1049 | -0.2722 | -0.1822 |
| 0.450 | -0.2765 | -0.2510 | -0.1104 | -0.2645 | -0.2537 |
| 0.500 | -0.2947 | -0.2505 | -0.1268 | -0.2572 | -0.4259 |
| 0.525 | ******* | -0.2505 | -0.1338 | -0.2517 | -0.5914 |
| 0.550 | -0.3244 | -0.2544 | -0.1361 | -0.2413 | -0.6946 |
| 0.575 | ******* | -0.2567 | -0.1311 | -0.2341 | -0.7415 |
| 0.600 | -0.3571 | -0.2577 | -0.1348 | -0.2296 | -0.7533 |
| 0.625 | ******* | ******* | -0.1233 | -0.2286 | -0.7871 |
| 0.650 | -0.3813 | -0.2606 | -0.1178 | -0.2618 | -0.8654 |
| 0.675 | ******* | -0.2504 | -0.1441 | -0.3807 | -0.9866 |
| 0.700 | -0.3983 | -0.2282 | -0.3079 | -0.6032 | -1.1142 |
| 0.725 | ******* | -0.3207 | ******* | -0.8456 | -0.8877 |
| 0.750 | -0.4092 | -0.6892 | ******* | -1.0009 | -0.7314 |
| 0.775 | ******* | -0.8970 | -1.0430 | -1.0510 | -0.6488 |
| 0.800 | -0.4231 | -0.9588 | -1.0200 | -0.8661 | ******* |
| 0.825 | ******* | -0.9706 | -0.9938 | -0.7759 | -0.5621 |
| 0.850 | -0.5778 | -0.9667 | -0.9415 | -0.7718 | -0.5437 |
| 0.875 | ******* | -0.9553 | -0.8315 | -0.7409 | -0.5580 |
| 0.900 | -0.7777 | -0.9241 | -0.7681 | -0.6869 | ******* |
| 0.925 | ******* | -0.9070 | -0.7251 | -0.6623 | -0.5630 |
| 0.950 | -0.8864 | -0.8919 | -0.6953 | -0.6779 | -0.5031 |
| 0.975 | ******* | -0.8741 | -0.6749 | -0.6709 | -0.4307 |
| 1.000 | -0.8914 | -0.8981 | -0.6969 | -0.6632 | -0.3848 |
| | Cp,l | Cp,l | Cp,l | Cp,l | Cp,l |
| -0.200 | 0.2019 | 0.2045 | 0.2474 | ******* | -0.5921 |
| -0.400 | 0.1973 | 0.2070 | 0.2169 | 0.0527 | -0.6277 |
| -0.600 | 0.2143 | 0.2155 | 0.2096 | 0.0856 | -0.6065 |
| -0.700 | ******* | 0.2257 | 0.2100 | 0.0986 | -0.5866 |
| -0.800 | ******* | ******* | 0.2148 | 0.1220 | -0.5320 |
| -0.850 | ******* | 0.2492 | 0.2241 | 0.1299 | -0.5179 |
| -0.900 | 0.2750 | 0.2641 | 0.2426 | 0.1506 | -0.5009 |
| -0.950 | 0.2755 | 0.1651 | 0.2431 | 0.1735 | -0.1641 |
| -0.975 | ******* | 0.1898 | 0.1985 | 0.1517 | -0.0430 |
| -1.000 | -0.8594 | -0.8990 | -0.6943 | -0.6730 | -0.3654 |



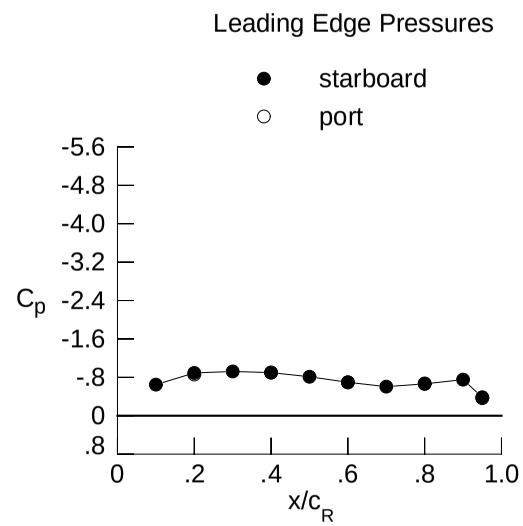

Small Radius L.E.

Run No. = 43 , Point No. = 906

$C_N$ = 0.495, $C_m$ = -0.0995

$\alpha$ = 10.4 °, $M_\infty$ = 0.900

$R_{mac}$ = $6.0 \times 10^6$

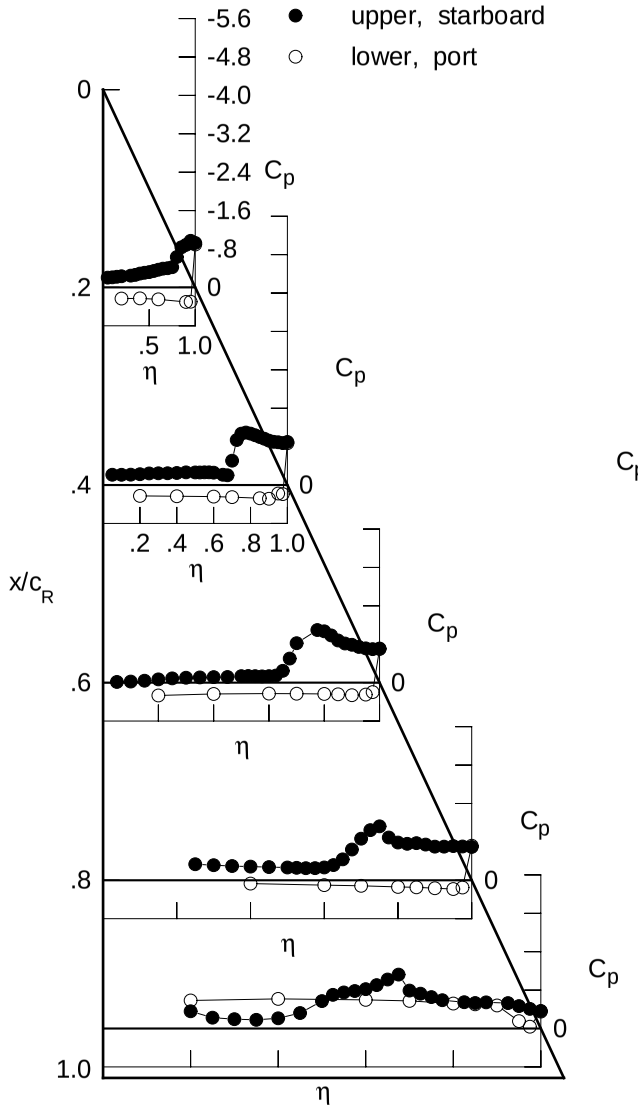



| x/c_R | starb'd Cp | port Cp |
|---|---|---|
| 0.10 | -0.6477 | ******* |
| 0.20 | -0.8914 | -0.8594 |
| 0.30 | -0.9222 | ******* |
| 0.40 | -0.8981 | -0.8990 |
| 0.50 | -0.8124 | ******* |
| 0.60 | -0.6969 | -0.6943 |
| 0.70 | -0.6062 | ******* |
| 0.80 | -0.6632 | -0.6730 |
| 0.90 | -0.7523 | ******* |
| 0.95 | -0.3848 | -0.3654 |

# Table D6. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2028 | -0.2147 | -0.0142 | ******* | ******* |
| 0.100 | -0.2099 | -0.2136 | -0.0224 | ******* | ******* |
| 0.150 | -0.2214 | -0.2159 | -0.0403 | ******* | ******* |
| 0.200 | -0.2319 | -0.2254 | -0.0681 | ******* | -0.3591 |
| 0.250 | ******* | -0.2414 | -0.0892 | -0.3342 | -0.2258 |
| 0.300 | -0.2449 | -0.2448 | -0.1025 | -0.3143 | -0.1943 |
| 0.350 | -0.2604 | -0.2458 | -0.1085 | -0.2967 | -0.1812 |
| 0.400 | -0.2877 | -0.2514 | -0.1152 | -0.2845 | -0.2130 |
| 0.450 | -0.3049 | -0.2641 | -0.1179 | -0.2749 | -0.3221 |
| 0.500 | -0.3180 | -0.2623 | -0.1356 | -0.2660 | -0.5713 |
| 0.525 | ******* | -0.2617 | -0.1385 | -0.2601 | -0.7013 |
| 0.550 | -0.3413 | -0.2648 | -0.1353 | -0.2521 | -0.7515 |
| 0.575 | ******* | -0.2651 | -0.1301 | -0.2532 | -0.7812 |
| 0.600 | -0.3678 | -0.2579 | -0.1352 | -0.2672 | -0.8199 |
| 0.625 | ******* | ******* | -0.1476 | -0.3172 | -0.9038 |
| 0.650 | -0.3908 | -0.2144 | -0.2467 | -0.4358 | -1.0204 |
| 0.675 | ******* | -0.2029 | -0.5016 | -0.6406 | -1.1234 |
| 0.700 | -0.3989 | -0.5075 | -0.8214 | -0.8665 | -0.7906 |
| 0.725 | ******* | -0.9378 | ******* | -1.0446 | -0.7259 |
| 0.750 | -0.4212 | -1.0707 | ******* | -1.1242 | -0.6541 |
| 0.775 | ******* | -1.0938 | -1.0956 | -0.8913 | -0.5892 |
| 0.800 | -0.6326 | -1.0710 | -1.0698 | -0.7864 | ******* |
| 0.825 | ******* | -1.0377 | -0.9841 | -0.7604 | -0.5480 |
| 0.850 | -0.8355 | -1.0009 | -0.8780 | -0.7738 | -0.5313 |
| 0.875 | ******* | -0.9651 | -0.8155 | -0.7438 | -0.5451 |
| 0.900 | -0.8854 | -0.9245 | -0.7891 | -0.7007 | ******* |
| 0.925 | ******* | -0.9009 | -0.7438 | -0.7007 | -0.5299 |
| 0.950 | -0.9703 | -0.8911 | -0.7147 | -0.7130 | -0.4668 |
| 0.975 | ******* | -0.8733 | -0.6975 | -0.7043 | -0.4087 |
| 1.000 | -0.9267 | -0.8972 | -0.7106 | -0.6947 | -0.3664 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2325 | 0.2265 | 0.2673 | ******* | -0.5840 |
| -0.400 | 0.2291 | 0.2334 | 0.2356 | 0.0687 | -0.6172 |
| -0.600 | 0.2488 | 0.2410 | 0.2277 | 0.1011 | -0.5964 |
| -0.700 | ******* | 0.2520 | 0.2303 | 0.1149 | -0.5751 |
| -0.800 | ******* | ******* | 0.2355 | 0.1385 | -0.5204 |
| -0.850 | ******* | 0.2751 | 0.2430 | 0.1465 | -0.5043 |
| -0.900 | 0.3035 | 0.2861 | 0.2619 | 0.1654 | -0.4803 |
| -0.950 | 0.2983 | 0.1768 | 0.2485 | 0.1820 | -0.1535 |
| -0.975 | ******* | 0.1891 | 0.1964 | 0.1506 | -0.0377 |
| -1.000 | -0.8936 | -0.8712 | -0.7004 | -0.7199 | -0.3517 |

Surface Pressures




Small Radius L.E.

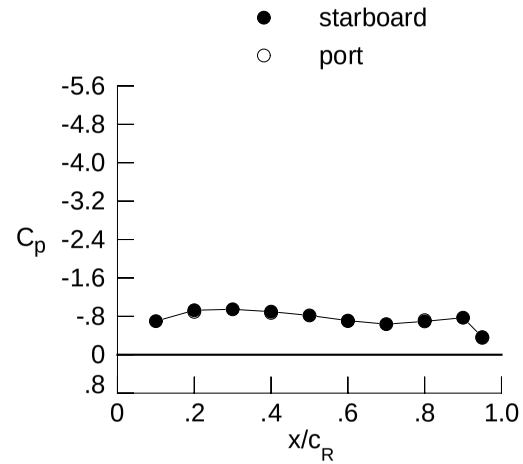
Run No. = 43 , Point No. = 907

$C_N$ = 0.548, $C_m$ = -0.1063

$\alpha$ = 11.4 °, $M_\infty$ = 0.900

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

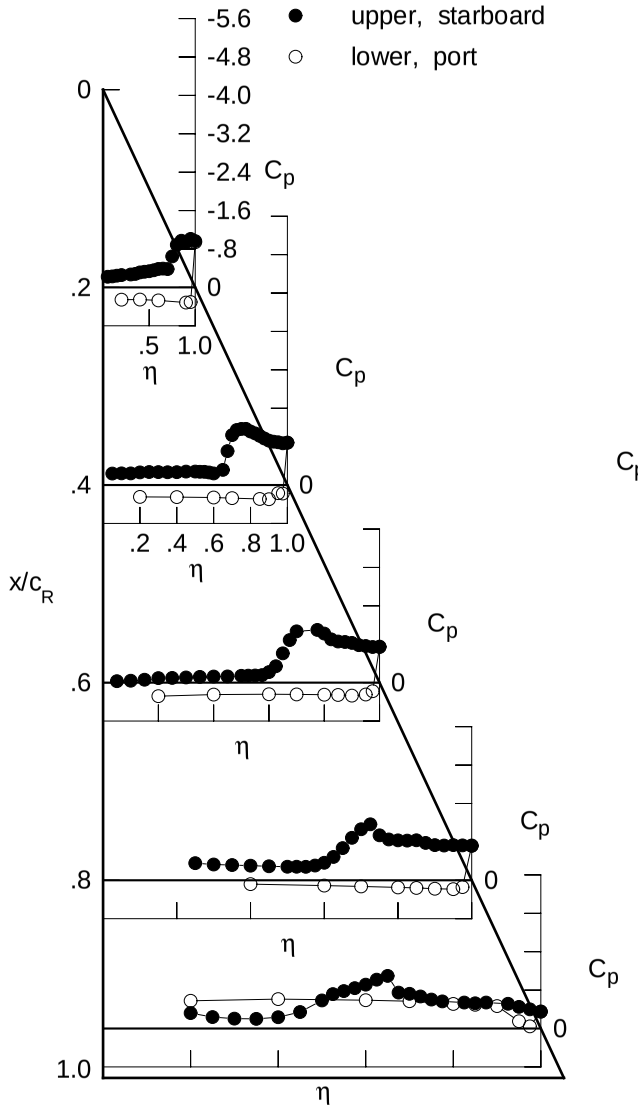



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.6990 | ******* |
| 0.20 | -0.9267 | -0.8936 |
| 0.30 | -0.9467 | ******* |
| 0.40 | -0.8972 | -0.8712 |
| 0.50 | -0.8183 | ******* |
| 0.60 | -0.7106 | -0.7004 |
| 0.70 | -0.6369 | ******* |
| 0.80 | -0.6947 | -0.7199 |
| 0.90 | -0.7716 | ******* |
| 0.95 | -0.3664 | -0.3517 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2214 | -0.2393 | -0.0302 | ******* | ******* |
| 0.100 | -0.2291 | -0.2435 | -0.0403 | ******* | ******* |
| 0.150 | -0.2443 | -0.2423 | -0.0607 | ******* | ******* |
| 0.200 | -0.2571 | -0.2633 | -0.0945 | ******* | -0.3214 |
| 0.250 | ******* | -0.2708 | -0.0981 | -0.3568 | -0.2381 |
| 0.300 | -0.2686 | -0.2699 | -0.1082 | -0.3286 | -0.2058 |
| 0.350 | -0.2807 | -0.2662 | -0.1198 | -0.3177 | -0.2009 |
| 0.400 | -0.3117 | -0.2678 | -0.1272 | -0.3042 | -0.2352 |
| 0.450 | -0.3258 | -0.2800 | -0.1296 | -0.2921 | -0.3433 |
| 0.500 | -0.3367 | -0.2807 | -0.1424 | -0.2821 | -0.5846 |
| 0.525 | ******* | -0.2763 | -0.1454 | -0.2820 | -0.7171 |
| 0.550 | -0.3569 | -0.2754 | -0.1484 | -0.2806 | -0.7798 |
| 0.575 | ******* | -0.2620 | -0.1569 | -0.3076 | -0.8407 |
| 0.600 | -0.3836 | -0.2418 | -0.2198 | -0.3644 | -0.9138 |
| 0.625 | ******* | ******* | -0.3416 | -0.4864 | -1.0180 |
| 0.650 | -0.3914 | -0.3159 | -0.6108 | -0.6701 | -1.0956 |
| 0.675 | ******* | -0.7073 | -0.8871 | -0.8845 | -0.7478 |
| 0.700 | -0.3817 | -1.0402 | -1.0689 | -1.0628 | -0.7231 |
| 0.725 | ******* | -1.1463 | ******* | -1.1662 | -0.6673 |
| 0.750 | -0.6454 | -1.1689 | ******* | -0.9371 | -0.6034 |
| 0.775 | ******* | -1.1707 | -1.0985 | -0.8507 | -0.5649 |
| 0.800 | -0.8874 | -1.1154 | -1.0227 | -0.8320 | ******* |
| 0.825 | ******* | -1.0763 | -0.9026 | -0.8266 | -0.5411 |
| 0.850 | -0.9721 | -1.0251 | -0.8568 | -0.8332 | -0.5255 |
| 0.875 | ******* | -0.9708 | -0.8470 | -0.7783 | -0.5406 |
| 0.900 | -0.9393 | -0.9252 | -0.8280 | -0.7328 | ******* |
| 0.925 | ******* | -0.9030 | -0.7811 | -0.7236 | -0.5151 |
| 0.950 | -1.0100 | -0.8909 | -0.7636 | -0.7332 | -0.4515 |
| 0.975 | ******* | -0.8698 | -0.7427 | -0.7270 | -0.3990 |
| 1.000 | -0.9647 | -0.8824 | -0.7501 | -0.7170 | -0.3554 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2561 | 0.2470 | 0.2819 | ******* | -0.5774 |
| -0.400 | 0.2534 | 0.2514 | 0.2485 | 0.0801 | -0.6124 |
| -0.600 | 0.2711 | 0.2600 | 0.2415 | 0.1104 | -0.5898 |
| -0.700 | ******* | 0.2731 | 0.2452 | 0.1281 | -0.5684 |
| -0.800 | ******* | ******* | 0.2508 | 0.1485 | -0.5117 |
| -0.850 | ******* | 0.2901 | 0.2566 | 0.1589 | -0.4945 |
| -0.900 | 0.3161 | 0.2952 | 0.2702 | 0.1760 | -0.4673 |
| -0.950 | 0.3050 | 0.1695 | 0.2473 | 0.1849 | -0.1510 |
| -0.975 | ******* | 0.1769 | 0.1785 | 0.1420 | -0.0451 |
| -1.000 | -0.9414 | -0.8824 | -0.7414 | -0.7248 | -0.3492 |

Surface Pressures




Small Radius L.E.

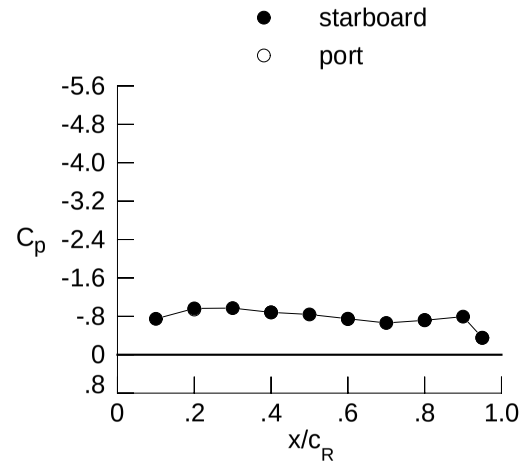
Run No. = 43 , Point No. = 908

$C_N$ = 0.606, $C_m$ = -0.1188

$\alpha$ = 12.4 °, $M_\infty$ = 0.900

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

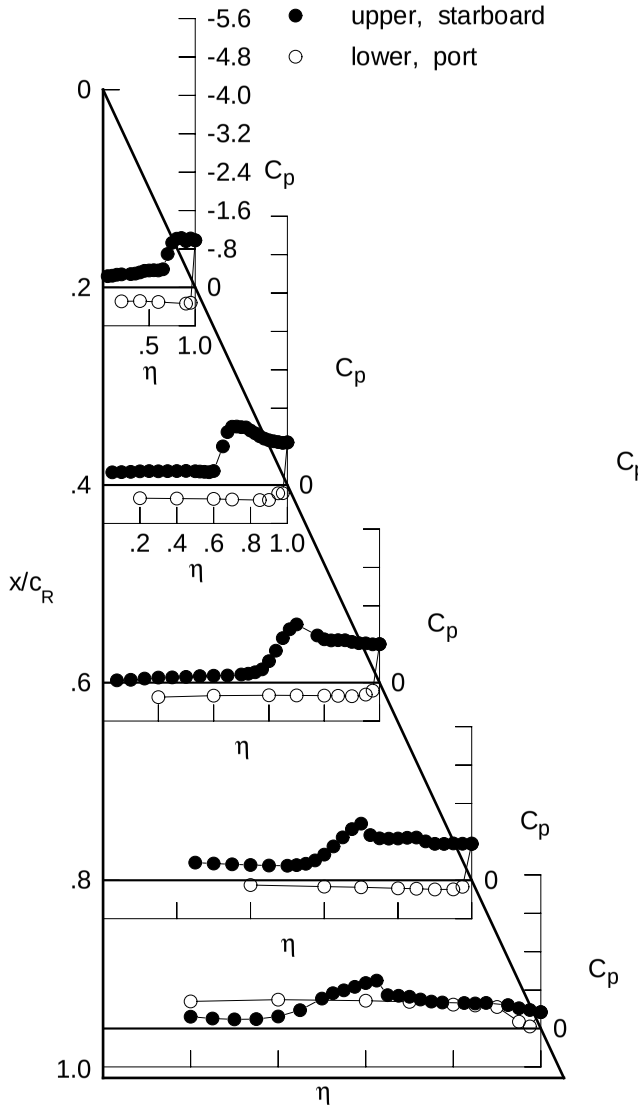



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.7476 | ******* |
| 0.20 | -0.9647 | -0.9414 |
| 0.30 | -0.9713 | ******* |
| 0.40 | -0.8824 | -0.8824 |
| 0.50 | -0.8389 | ******* |
| 0.60 | -0.7501 | -0.7414 |
| 0.70 | -0.6616 | ******* |
| 0.80 | -0.7170 | -0.7248 |
| 0.90 | -0.7936 | ******* |
| 0.95 | -0.3554 | -0.3492 |

# Table D6. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2332 | -0.2649 | -0.0476 | ******* | ******* |
| 0.100 | -0.2430 | -0.2686 | -0.0591 | ******* | ******* |
| 0.150 | -0.2636 | -0.2746 | -0.0850 | ******* | ******* |
| 0.200 | -0.2714 | -0.2859 | -0.1055 | ******* | -0.2459 |
| 0.250 | ******* | -0.2905 | -0.1094 | -0.3684 | -0.2077 |
| 0.300 | -0.2768 | -0.2862 | -0.1198 | -0.3488 | -0.1903 |
| 0.350 | -0.2868 | -0.2894 | -0.1364 | -0.3330 | -0.1958 |
| 0.400 | -0.3119 | -0.2909 | -0.1439 | -0.3185 | -0.2505 |
| 0.450 | -0.3452 | -0.2940 | -0.1484 | -0.3074 | -0.3818 |
| 0.500 | -0.3521 | -0.2869 | -0.1699 | -0.3029 | -0.6233 |
| 0.525 | ******* | -0.2808 | -0.1859 | -0.3160 | -0.7351 |
| 0.550 | -0.3576 | -0.2749 | -0.2160 | -0.3441 | -0.7954 |
| 0.575 | ******* | -0.2672 | -0.2767 | -0.4137 | -0.8684 |
| 0.600 | -0.3524 | -0.2919 | -0.4473 | -0.5346 | -0.9471 |
| 0.625 | ******* | ******* | -0.6655 | -0.7057 | -0.9973 |
| 0.650 | -0.3773 | -0.8050 | -0.9269 | -0.8936 | -0.6943 |
| 0.675 | ******* | -1.1029 | -1.1123 | -1.0659 | -0.6826 |
| 0.700 | -0.6959 | -1.2147 | -1.2129 | -1.1803 | -0.6615 |
| 0.725 | ******* | -1.2188 | ******* | -0.9414 | -0.6040 |
| 0.750 | -0.9299 | -1.2058 | ******* | -0.8733 | -0.5612 |
| 0.775 | ******* | -1.2002 | -0.9826 | -0.8671 | -0.5418 |
| 0.800 | -1.0144 | -1.1355 | -0.9034 | -0.8702 | ******* |
| 0.825 | ******* | -1.0773 | -0.8800 | -0.8853 | -0.5313 |
| 0.850 | -1.0285 | -1.0164 | -0.8850 | -0.8908 | -0.5220 |
| 0.875 | ******* | -0.9666 | -0.8832 | -0.8101 | -0.5329 |
| 0.900 | -0.9632 | -0.9329 | -0.8487 | -0.7596 | ******* |
| 0.925 | ******* | -0.9117 | -0.8222 | -0.7575 | -0.4882 |
| 0.950 | -1.0196 | -0.8954 | -0.8186 | -0.7677 | -0.4226 |
| 0.975 | ******* | -0.8778 | -0.7981 | -0.7612 | -0.3855 |
| 1.000 | -0.9818 | -0.8894 | -0.7999 | -0.7549 | -0.3412 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.2909 | 0.2741 | 0.3022 | ******* | -0.5643 |
| -0.400 | 0.2850 | 0.2819 | 0.2710 | 0.0992 | -0.6007 |
| -0.600 | 0.3042 | 0.2890 | 0.2632 | 0.1317 | -0.5792 |
| -0.700 | ******* | 0.3014 | 0.2664 | 0.1457 | -0.5555 |
| -0.800 | ******* | ******* | 0.2705 | 0.1677 | -0.4977 |
| -0.850 | ******* | 0.3134 | 0.2755 | 0.1762 | -0.4803 |
| -0.900 | 0.3376 | 0.3111 | 0.2826 | 0.1908 | -0.4483 |
| -0.950 | 0.3201 | 0.1720 | 0.2486 | 0.1894 | -0.1417 |
| -0.975 | ******* | 0.1698 | 0.1665 | 0.1354 | -0.0420 |
| -1.000 | -0.9790 | -0.8855 | -0.8033 | -0.7662 | -0.3412 |

Surface Pressures




Small Radius L.E.

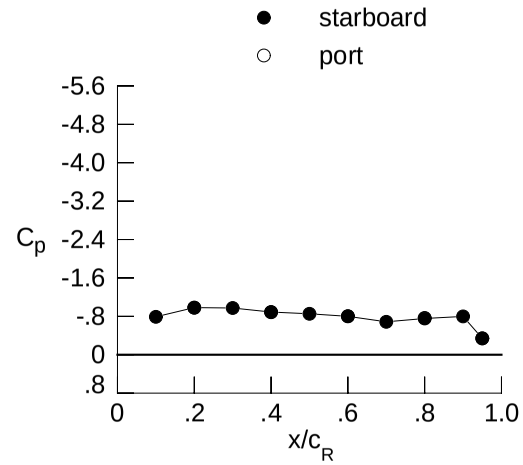
Run No. = 43 , Point No. = 909

$C_N$ = 0.662, $C_m$ = -0.1264

$\alpha$ = 13.5 °, $M_\infty$ = 0.899

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

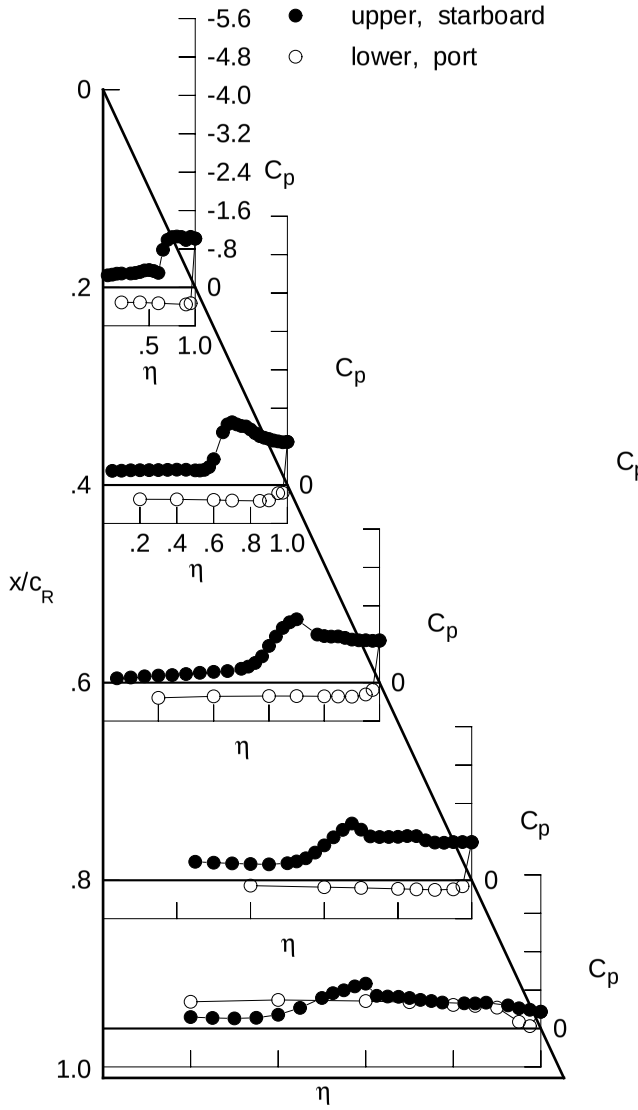



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.7900 | ******* |
| 0.20 | -0.9818 | -0.9790 |
| 0.30 | -0.9734 | ******* |
| 0.40 | -0.8894 | -0.8855 |
| 0.50 | -0.8530 | ******* |
| 0.60 | -0.7999 | -0.8033 |
| 0.70 | -0.6858 | ******* |
| 0.80 | -0.7549 | -0.7662 |
| 0.90 | -0.7980 | ******* |
| 0.95 | -0.3412 | -0.3412 |

# Table D6. Continued.

| η | x/c_R .2 Cp,u | x/c_R .4 Cp,u | x/c_R .6 Cp,u | x/c_R .8 Cp,u | x/c_R .95 Cp,u |
|---|---|---|---|---|---|
| 0.050 | -0.2513 | -0.2950 | -0.0904 | ******* | ******* |
| 0.100 | -0.2654 | -0.2981 | -0.1072 | ******* | ******* |
| 0.150 | -0.2854 | -0.3069 | -0.1321 | ******* | ******* |
| 0.200 | -0.2890 | -0.3091 | -0.1468 | ******* | -0.2381 |
| 0.250 | ******* | -0.3106 | -0.1574 | -0.3858 | -0.2196 |
| 0.300 | -0.2892 | -0.3121 | -0.1794 | -0.3664 | -0.2103 |
| 0.350 | -0.2997 | -0.3164 | -0.2050 | -0.3516 | -0.2228 |
| 0.400 | -0.3205 | -0.3201 | -0.2245 | -0.3388 | -0.2867 |
| 0.450 | -0.3532 | -0.3181 | -0.2416 | -0.3317 | -0.4295 |
| 0.500 | -0.3615 | -0.3055 | -0.2884 | -0.3551 | -0.6362 |
| 0.525 | ******* | -0.3024 | -0.3338 | -0.3927 | -0.7361 |
| 0.550 | -0.3408 | -0.3167 | -0.4107 | -0.4586 | -0.7958 |
| 0.575 | ******* | -0.3746 | -0.5476 | -0.5766 | -0.8775 |
| 0.600 | -0.3025 | -0.5387 | -0.7648 | -0.7269 | -0.9344 |
| 0.625 | ******* | ******* | -0.9603 | -0.8948 | -0.6819 |
| 0.650 | -0.7841 | -1.0988 | -1.1397 | -1.0501 | -0.6662 |
| 0.675 | ******* | -1.2639 | -1.2573 | -1.1821 | -0.6608 |
| 0.700 | -0.9904 | -1.3080 | -1.3198 | -1.0544 | -0.6363 |
| 0.725 | ******* | -1.2630 | ******* | -0.9144 | -0.5960 |
| 0.750 | -1.0481 | -1.2307 | ******* | -0.9014 | -0.5725 |
| 0.775 | ******* | -1.2198 | -1.0013 | -0.9026 | -0.5409 |
| 0.800 | -1.0603 | -1.1565 | -0.9706 | -0.9055 | ******* |
| 0.825 | ******* | -1.0807 | -0.9588 | -0.9219 | -0.5245 |
| 0.850 | -1.0506 | -1.0188 | -0.9622 | -0.9203 | -0.5221 |
| 0.875 | ******* | -0.9847 | -0.9330 | -0.8331 | -0.5387 |
| 0.900 | -0.9875 | -0.9583 | -0.8971 | -0.7856 | ******* |
| 0.925 | ******* | -0.9289 | -0.8818 | -0.7818 | -0.4815 |
| 0.950 | -1.0524 | -0.9095 | -0.8830 | -0.7961 | -0.4216 |
| 0.975 | ******* | -0.8915 | -0.8716 | -0.7967 | -0.3905 |
| 1.000 | -1.0146 | -0.9003 | -0.8713 | -0.7876 | -0.3484 |
| | Cp,l | Cp,l | Cp,l | Cp,l | Cp,l |
| -0.200 | 0.3133 | 0.2968 | 0.3165 | ******* | -0.5566 |
| -0.400 | 0.3125 | 0.2989 | 0.2859 | 0.1116 | -0.5950 |
| -0.600 | 0.3307 | 0.3105 | 0.2790 | 0.1432 | -0.5723 |
| -0.700 | ******* | 0.3229 | 0.2798 | 0.1584 | -0.5487 |
| -0.800 | ******* | ******* | 0.2848 | 0.1780 | -0.4912 |
| -0.850 | ******* | 0.3303 | 0.2877 | 0.1886 | -0.4713 |
| -0.900 | 0.3550 | 0.3195 | 0.2918 | 0.1998 | -0.4355 |
| -0.950 | 0.3293 | 0.1699 | 0.2464 | 0.1887 | -0.1393 |
| -0.975 | ******* | 0.1601 | 0.1510 | 0.1243 | -0.0494 |
| -1.000 | -1.0195 | -0.8975 | -0.8834 | -0.7984 | -0.3502 |

Surface Pressures




Small Radius L.E.

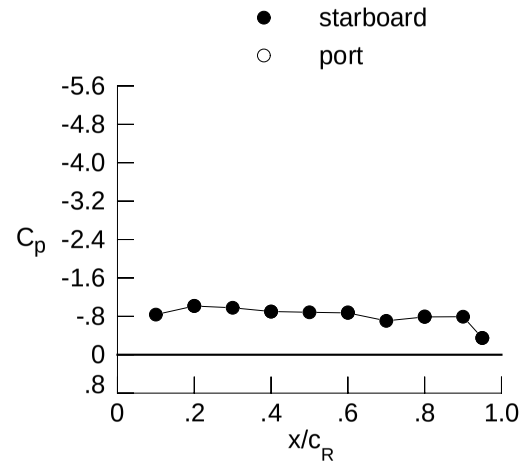
Run No. = 43 , Point No. = 910

$C_N$ = 0.719, $C_m$ = -0.1376

$\alpha$ = 14.5 °, $M_\infty$ = 0.899

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

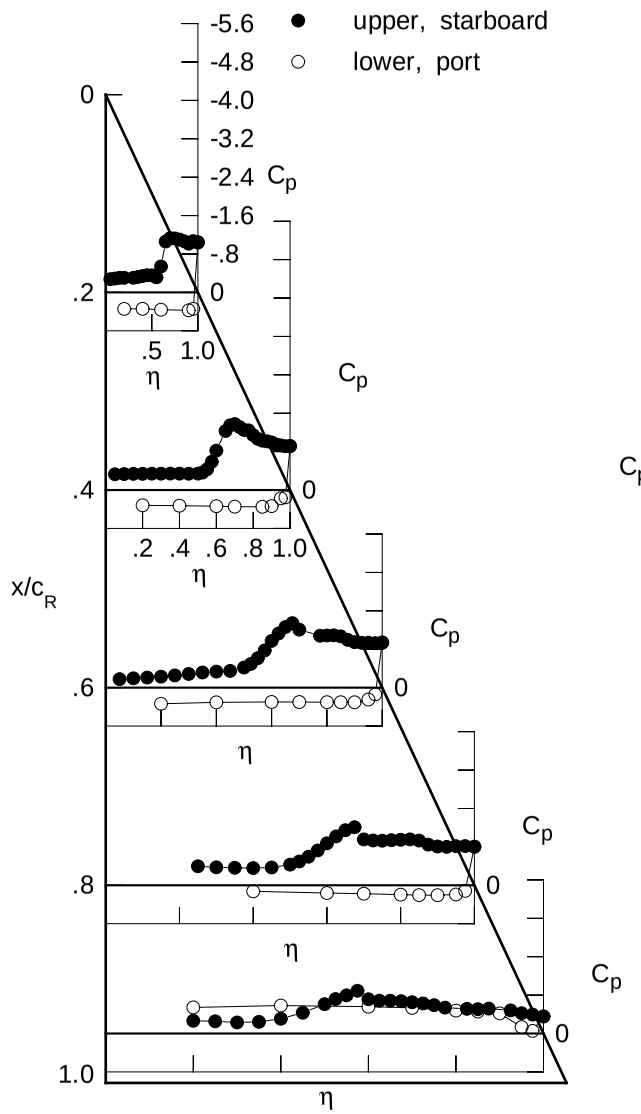



| x/c_R | starb'd Cp | port Cp |
|---|---|---|
| 0.10 | -0.8363 | ******* |
| 0.20 | -1.0146 | -1.0195 |
| 0.30 | -0.9781 | ******* |
| 0.40 | -0.9003 | -0.8975 |
| 0.50 | -0.8843 | ******* |
| 0.60 | -0.8713 | -0.8834 |
| 0.70 | -0.7060 | ******* |
| 0.80 | -0.7876 | -0.7984 |
| 0.90 | -0.7920 | ******* |
| 0.95 | -0.3484 | -0.3502 |

# Table D6. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.2751 | -0.3286 | -0.1779 | ******* | ******* |
| 0.100 | -0.2890 | -0.3330 | -0.1946 | ******* | ******* |
| 0.150 | -0.3032 | -0.3378 | -0.2103 | ******* | ******* |
| 0.200 | -0.3040 | -0.3374 | -0.2288 | ******* | -0.2654 |
| 0.250 | ******* | -0.3411 | -0.2545 | -0.3957 | -0.2541 |
| 0.300 | -0.3041 | -0.3405 | -0.2844 | -0.3747 | -0.2303 |
| 0.350 | -0.3209 | -0.3434 | -0.3149 | -0.3649 | -0.2432 |
| 0.400 | -0.3409 | -0.3419 | -0.3344 | -0.3582 | -0.3075 |
| 0.450 | -0.3575 | -0.3398 | -0.3489 | -0.3705 | -0.4329 |
| 0.500 | -0.3559 | -0.3422 | -0.4183 | -0.4307 | -0.6110 |
| 0.525 | ******* | -0.3652 | -0.4940 | -0.4961 | -0.7177 |
| 0.550 | -0.3138 | -0.4323 | -0.6133 | -0.5949 | -0.7954 |
| 0.575 | ******* | -0.5881 | -0.7757 | -0.7254 | -0.8903 |
| 0.600 | -0.5411 | -0.8221 | -0.9735 | -0.8745 | -0.7139 |
| 0.625 | ******* | ******* | -1.1290 | -1.0185 | -0.6841 |
| 0.650 | -1.0589 | -1.2301 | -1.2634 | -1.1472 | -0.6834 |
| 0.675 | ******* | -1.3479 | -1.3437 | -1.2098 | -0.6740 |
| 0.700 | -1.1306 | -1.3750 | -1.2084 | -0.9559 | -0.6508 |
| 0.725 | ******* | -1.3147 | ******* | -0.9340 | -0.6261 |
| 0.750 | -1.1237 | -1.2520 | ******* | -0.9291 | -0.5901 |
| 0.775 | ******* | -1.2429 | -1.0819 | -0.9389 | -0.5391 |
| 0.800 | -1.1005 | -1.1444 | -1.0861 | -0.9484 | ******* |
| 0.825 | ******* | -1.0664 | -1.0903 | -0.9561 | -0.5142 |
| 0.850 | -1.0667 | -1.0281 | -1.0684 | -0.9320 | -0.5063 |
| 0.875 | ******* | -1.0151 | -0.9958 | -0.8472 | -0.5191 |
| 0.900 | -1.0147 | -0.9919 | -0.9468 | -0.8077 | ******* |
| 0.925 | ******* | -0.9486 | -0.9345 | -0.8010 | -0.4816 |
| 0.950 | -1.0690 | -0.9303 | -0.9371 | -0.8150 | -0.4221 |
| 0.975 | ******* | -0.9117 | -0.9266 | -0.8165 | -0.3944 |
| 1.000 | -1.0366 | -0.9212 | -0.9356 | -0.8060 | -0.3562 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3437 | 0.3188 | 0.3360 | ******* | -0.5432 |
| -0.400 | 0.3422 | 0.3264 | 0.3062 | 0.1261 | -0.5823 |
| -0.600 | 0.3609 | 0.3364 | 0.2983 | 0.1611 | -0.5588 |
| -0.700 | ******* | 0.3469 | 0.3000 | 0.1753 | -0.5346 |
| -0.800 | ******* | ******* | 0.3035 | 0.1951 | -0.4775 |
| -0.850 | ******* | 0.3491 | 0.3042 | 0.2047 | -0.4573 |
| -0.900 | 0.3736 | 0.3349 | 0.3049 | 0.2064 | -0.4190 |
| -0.950 | 0.3432 | 0.1728 | 0.2471 | 0.1920 | -0.1338 |
| -0.975 | ******* | 0.1509 | 0.1401 | 0.1170 | -0.0543 |
| -1.000 | -1.0463 | -0.9121 | -0.9436 | -0.8009 | -0.3557 |

Surface Pressures




Small Radius L.E.

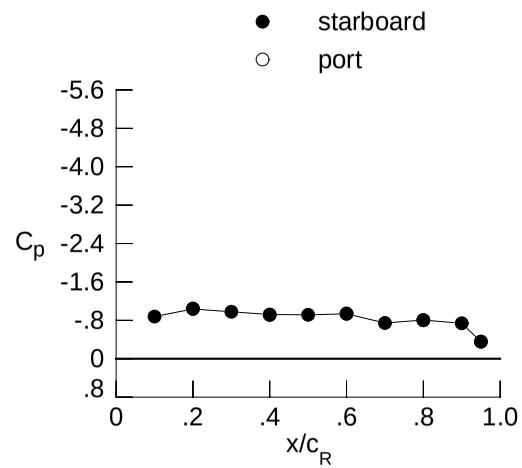
Run No. = 43 , Point No. = 911

$C_N$ = 0.775, $C_m$ = -0.1481

$\alpha$ = 15.5 °, $M_\infty$ = 0.900

$R_{mac}$ = $6.0 \times 10^6$

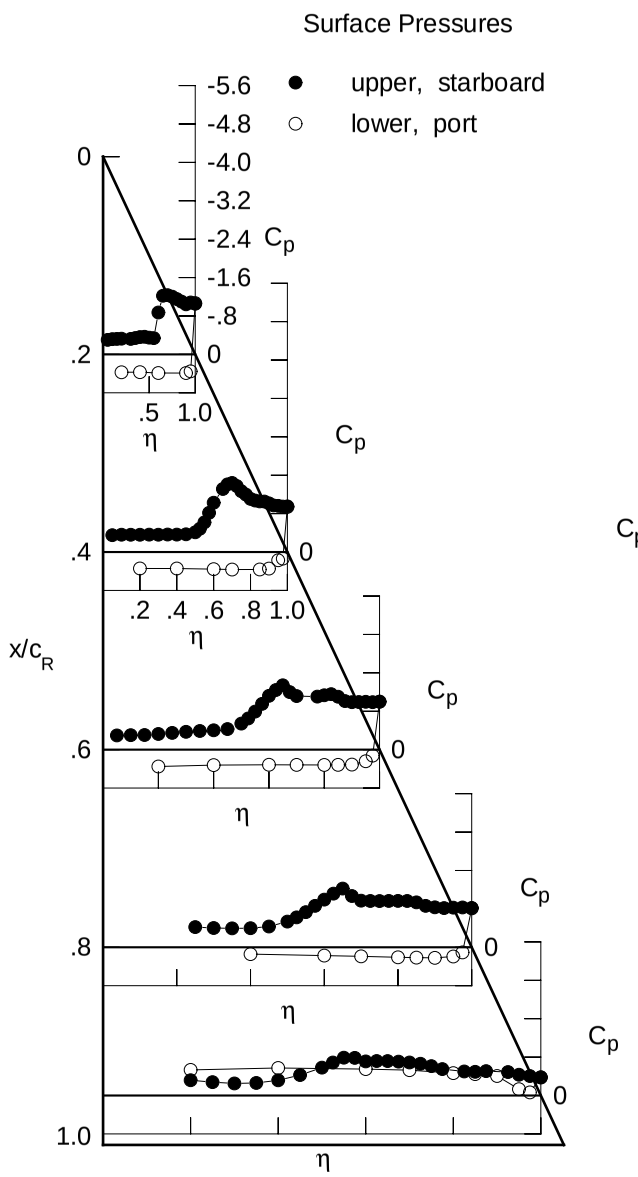
Leading Edge Pressures




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.8788 | ******* |
| 0.20 | -1.0366 | -1.0463 |
| 0.30 | -0.9780 | ******* |
| 0.40 | -0.9212 | -0.9121 |
| 0.50 | -0.9148 | ******* |
| 0.60 | -0.9356 | -0.9436 |
| 0.70 | -0.7444 | ******* |
| 0.80 | -0.8060 | -0.8009 |
| 0.90 | -0.7384 | ******* |
| 0.95 | -0.3562 | -0.3557 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3024 | -0.3510 | -0.2963 | ******* | ******* |
| 0.100 | -0.3177 | -0.3609 | -0.3014 | ******* | ******* |
| 0.150 | -0.3227 | -0.3603 | -0.3047 | ******* | ******* |
| 0.200 | -0.3270 | -0.3601 | -0.3261 | ******* | -0.3181 |
| 0.250 | ******* | -0.3626 | -0.3488 | -0.4207 | -0.2784 |
| 0.300 | -0.3224 | -0.3608 | -0.3710 | -0.4015 | -0.2512 |
| 0.350 | -0.3410 | -0.3650 | -0.3886 | -0.3945 | -0.2616 |
| 0.400 | -0.3608 | -0.3635 | -0.4031 | -0.3973 | -0.3170 |
| 0.450 | -0.3671 | -0.3700 | -0.4292 | -0.4330 | -0.4261 |
| 0.500 | -0.3488 | -0.4111 | -0.5420 | -0.5353 | -0.5804 |
| 0.525 | ******* | -0.4850 | -0.6498 | -0.6228 | -0.6875 |
| 0.550 | -0.3388 | -0.6183 | -0.7924 | -0.7320 | -0.7879 |
| 0.575 | ******* | -0.8171 | -0.9534 | -0.8632 | -0.7836 |
| 0.600 | -0.8725 | -1.0273 | -1.1205 | -0.9932 | -0.7106 |
| 0.625 | ******* | ******* | -1.2413 | -1.1173 | -0.7185 |
| 0.650 | -1.2216 | -1.3134 | -1.3408 | -1.2229 | -0.7176 |
| 0.675 | ******* | -1.4098 | -1.1990 | -1.0682 | -0.7054 |
| 0.700 | -1.2334 | -1.4389 | -1.1159 | -0.9710 | -0.6877 |
| 0.725 | ******* | -1.3763 | ******* | -0.9649 | -0.6617 |
| 0.750 | -1.2026 | -1.2670 | ******* | -0.9633 | -0.6122 |
| 0.775 | ******* | -1.1966 | -1.1046 | -0.9657 | -0.5503 |
| 0.800 | -1.1524 | -1.1074 | -1.1324 | -0.9662 | ******* |
| 0.825 | ******* | -1.0725 | -1.1560 | -0.9650 | -0.5006 |
| 0.850 | -1.1009 | -1.0544 | -1.1021 | -0.9362 | -0.4937 |
| 0.875 | ******* | -1.0522 | -1.0119 | -0.8630 | -0.5083 |
| 0.900 | -1.0429 | -1.0142 | -0.9887 | -0.8331 | ******* |
| 0.925 | ******* | -0.9700 | -0.9924 | -0.8168 | -0.4890 |
| 0.950 | -1.0814 | -0.9622 | -0.9970 | -0.8260 | -0.4328 |
| 0.975 | ******* | -0.9473 | -0.9884 | -0.8294 | -0.4056 |
| 1.000 | -1.0547 | -0.9509 | -1.0011 | -0.8202 | -0.3741 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.3725 | 0.3425 | 0.3512 | ******* | -0.5332 |
| -0.400 | 0.3702 | 0.3433 | 0.3222 | 0.1421 | -0.5734 |
| -0.600 | 0.3881 | 0.3565 | 0.3153 | 0.1731 | -0.5500 |
| -0.700 | ******* | 0.3646 | 0.3175 | 0.1887 | -0.5281 |
| -0.800 | ******* | ******* | 0.3191 | 0.2084 | -0.4665 |
| -0.850 | ******* | 0.3636 | 0.3170 | 0.2156 | -0.4455 |
| -0.900 | 0.3890 | 0.3444 | 0.3109 | 0.2204 | -0.4063 |
| -0.950 | 0.3528 | 0.1714 | 0.2419 | 0.1921 | -0.1324 |
| -0.975 | ******* | 0.1377 | 0.1250 | 0.1064 | -0.0645 |
| -1.000 | -1.0684 | -0.9394 | -0.9974 | -0.8101 | -0.3820 |



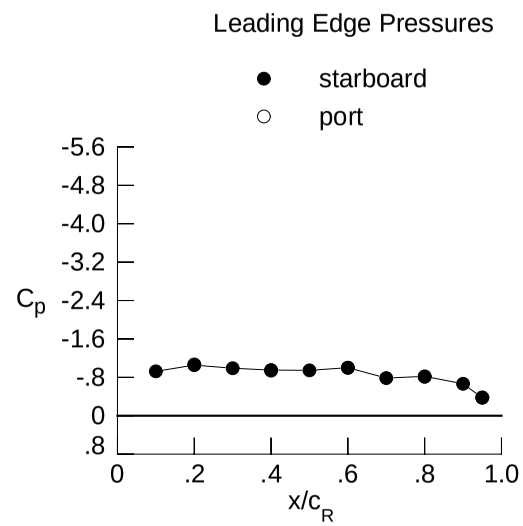

Small Radius L.E.

Run No. = 43 , Point No. = 912

$C_N$ = 0.831, $C_m$ = -0.1582

$\alpha$ = 16.6 °, $M_\infty$ = 0.899

$R_{mac}$ = $6.0 \times 10^6$

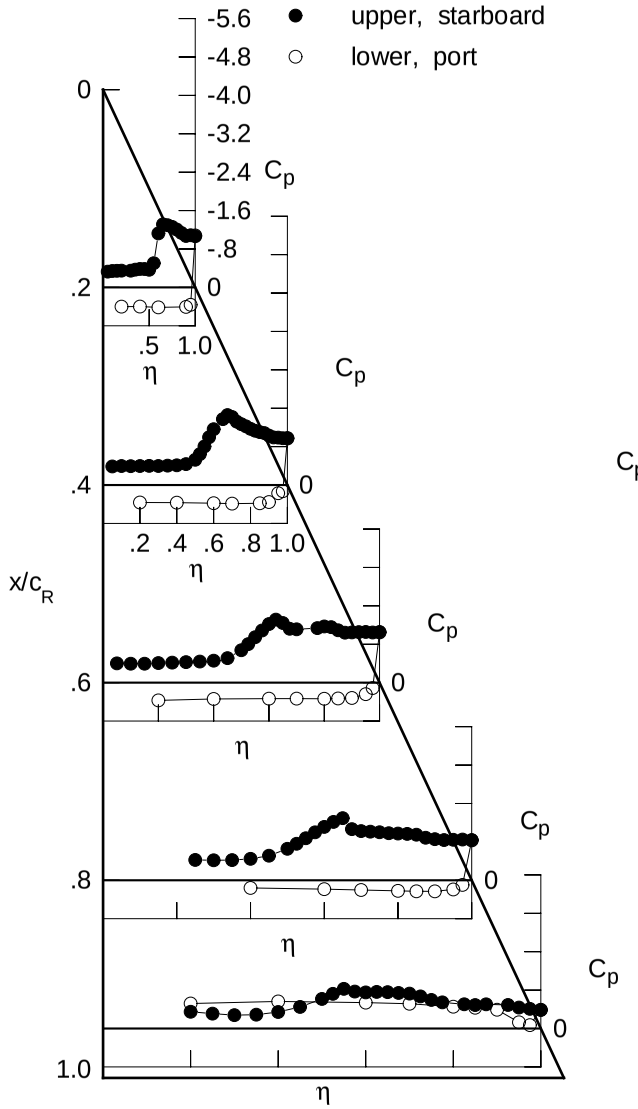



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.9250 | ******* |
| 0.20 | -1.0547 | -1.0684 |
| 0.30 | -0.9894 | ******* |
| 0.40 | -0.9509 | -0.9394 |
| 0.50 | -0.9457 | ******* |
| 0.60 | -1.0011 | -0.9974 |
| 0.70 | -0.7843 | ******* |
| 0.80 | -0.8202 | -0.8101 |
| 0.90 | -0.6655 | ******* |
| 0.95 | -0.3741 | -0.3820 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3282 | -0.3870 | -0.4017 | ******* | ******* |
| 0.100 | -0.3419 | -0.3957 | -0.3944 | ******* | ******* |
| 0.150 | -0.3456 | -0.3927 | -0.3947 | ******* | ******* |
| 0.200 | -0.3486 | -0.3957 | -0.4080 | ******* | -0.3490 |
| 0.250 | ******* | -0.3991 | -0.4168 | -0.4243 | -0.3100 |
| 0.300 | -0.3477 | -0.3967 | -0.4276 | -0.4169 | -0.2786 |
| 0.350 | -0.3692 | -0.4039 | -0.4394 | -0.4209 | -0.2876 |
| 0.400 | -0.3837 | -0.4109 | -0.4579 | -0.4468 | -0.3436 |
| 0.450 | -0.3835 | -0.4362 | -0.5106 | -0.5120 | -0.4497 |
| 0.500 | -0.3674 | -0.5267 | -0.6748 | -0.6556 | -0.6157 |
| 0.525 | ******* | -0.6434 | -0.8021 | -0.7606 | -0.7222 |
| 0.550 | -0.5041 | -0.8038 | -0.9465 | -0.8762 | -0.8265 |
| 0.575 | ******* | -0.9951 | -1.0861 | -0.9994 | -0.7698 |
| 0.600 | -1.1247 | -1.1630 | -1.2206 | -1.1119 | -0.7518 |
| 0.625 | ******* | ******* | -1.3126 | -1.2158 | -0.7624 |
| 0.650 | -1.3135 | -1.3729 | -1.2425 | -1.2947 | -0.7580 |
| 0.675 | ******* | -1.4574 | -1.1223 | -1.0653 | -0.7406 |
| 0.700 | -1.2953 | -1.4179 | -1.1114 | -1.0250 | -0.7272 |
| 0.725 | ******* | -1.3207 | ******* | -1.0124 | -0.6689 |
| 0.750 | -1.2601 | -1.2682 | ******* | -1.0011 | -0.5950 |
| 0.775 | ******* | -1.2232 | -1.1362 | -0.9812 | -0.5449 |
| 0.800 | -1.2048 | -1.1714 | -1.1704 | -0.9740 | ******* |
| 0.825 | ******* | -1.1314 | -1.1562 | -0.9666 | -0.5047 |
| 0.850 | -1.1346 | -1.1034 | -1.0915 | -0.9496 | -0.4885 |
| 0.875 | ******* | -1.0826 | -1.0407 | -0.8868 | -0.5043 |
| 0.900 | -1.0714 | -1.0295 | -1.0463 | -0.8569 | ******* |
| 0.925 | ******* | -0.9923 | -1.0530 | -0.8386 | -0.4902 |
| 0.950 | -1.0863 | -0.9878 | -1.0557 | -0.8443 | -0.4370 |
| 0.975 | ******* | -0.9754 | -1.0446 | -0.8487 | -0.4097 |
| 1.000 | -1.0655 | -0.9791 | -1.0553 | -0.8386 | -0.3864 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4007 | 0.3637 | 0.3699 | ******* | -0.5204 |
| -0.400 | 0.3993 | 0.3669 | 0.3401 | 0.1596 | -0.5639 |
| -0.600 | 0.4163 | 0.3786 | 0.3333 | 0.1845 | -0.5392 |
| -0.700 | ******* | 0.3875 | 0.3329 | 0.2026 | -0.5158 |
| -0.800 | ******* | ******* | 0.3360 | 0.2201 | -0.4542 |
| -0.850 | ******* | 0.3802 | 0.3294 | 0.2295 | -0.4324 |
| -0.900 | 0.4061 | 0.3546 | 0.3190 | 0.2300 | -0.3913 |
| -0.950 | 0.3628 | 0.1705 | 0.2402 | 0.1908 | -0.1296 |
| -0.975 | ******* | 0.1288 | 0.1126 | 0.0963 | -0.0701 |
| -1.000 | -1.0822 | -0.9688 | -1.0453 | -0.8312 | -0.3904 |

Surface Pressures




Small Radius L.E.

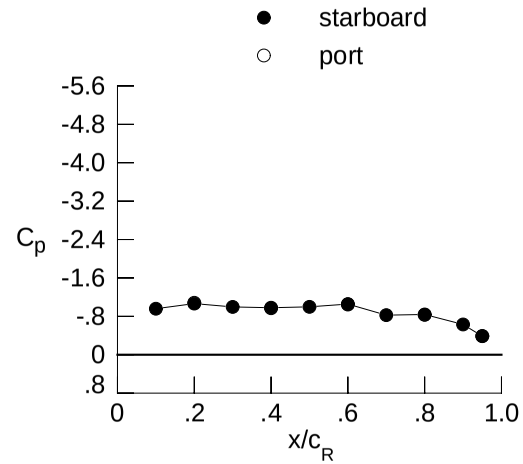
Run No. = 43 , Point No. = 913

$C_N$ = 0.887, $C_m$ = -0.1686

$\alpha$ = 17.6 °, $M_\infty$ = 0.900

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

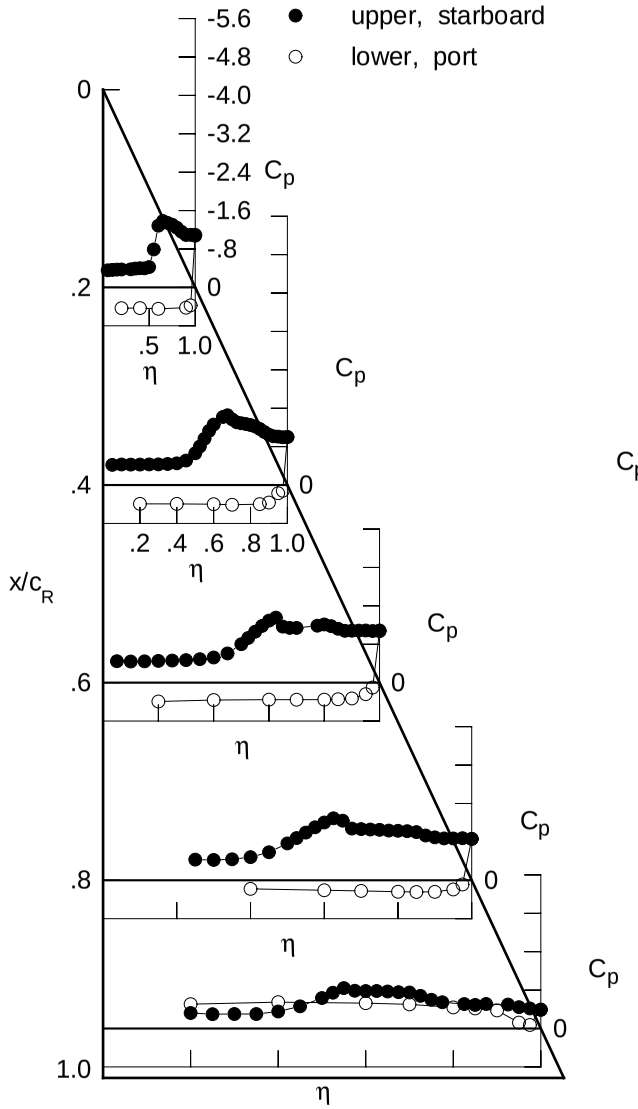



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.9587 | ******* |
| 0.20 | -1.0655 | -1.0822 |
| 0.30 | -0.9959 | ******* |
| 0.40 | -0.9791 | -0.9688 |
| 0.50 | -0.9978 | ******* |
| 0.60 | -1.0553 | -1.0453 |
| 0.70 | -0.8245 | ******* |
| 0.80 | -0.8386 | -0.8312 |
| 0.90 | -0.6308 | ******* |
| 0.95 | -0.3864 | -0.3904 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3556 | -0.4202 | -0.4462 | ******* | ******* |
| 0.100 | -0.3639 | -0.4278 | -0.4402 | ******* | ******* |
| 0.150 | -0.3703 | -0.4258 | -0.4442 | ******* | ******* |
| 0.200 | -0.3739 | -0.4261 | -0.4530 | ******* | -0.3233 |
| 0.250 | ******* | -0.4300 | -0.4604 | -0.4307 | -0.2985 |
| 0.300 | -0.3767 | -0.4302 | -0.4687 | -0.4237 | -0.3027 |
| 0.350 | -0.3918 | -0.4388 | -0.4886 | -0.4376 | -0.3014 |
| 0.400 | -0.3992 | -0.4524 | -0.5236 | -0.4822 | -0.3542 |
| 0.450 | -0.3964 | -0.5100 | -0.6080 | -0.5841 | -0.4617 |
| 0.500 | -0.4228 | -0.6610 | -0.8005 | -0.7683 | -0.6351 |
| 0.525 | ******* | -0.8021 | -0.9303 | -0.8800 | -0.7460 |
| 0.550 | -0.7913 | -0.9631 | -1.0606 | -0.9937 | -0.8420 |
| 0.575 | ******* | -1.1277 | -1.1819 | -1.1041 | -0.7863 |
| 0.600 | -1.2853 | -1.2589 | -1.2923 | -1.2043 | -0.7807 |
| 0.625 | ******* | ******* | -1.3551 | -1.2913 | -0.7819 |
| 0.650 | -1.3824 | -1.4177 | -1.1672 | -1.2417 | -0.7710 |
| 0.675 | ******* | -1.4540 | -1.1411 | -1.0778 | -0.7565 |
| 0.700 | -1.3428 | -1.3686 | -1.1398 | -1.0667 | -0.7506 |
| 0.725 | ******* | -1.3071 | ******* | -1.0576 | -0.6810 |
| 0.750 | -1.3055 | -1.2874 | ******* | -1.0513 | -0.5996 |
| 0.775 | ******* | -1.2716 | -1.1868 | -1.0359 | -0.5469 |
| 0.800 | -1.2434 | -1.2496 | -1.2121 | -1.0315 | ******* |
| 0.825 | ******* | -1.2210 | -1.1767 | -1.0229 | -0.5095 |
| 0.850 | -1.1598 | -1.1688 | -1.1227 | -1.0039 | -0.4911 |
| 0.875 | ******* | -1.1050 | -1.0797 | -0.9331 | -0.5110 |
| 0.900 | -1.0918 | -1.0484 | -1.0822 | -0.8941 | ******* |
| 0.925 | ******* | -1.0151 | -1.0843 | -0.8723 | -0.4993 |
| 0.950 | -1.0951 | -1.0085 | -1.0865 | -0.8709 | -0.4445 |
| 0.975 | ******* | -0.9951 | -1.0755 | -0.8767 | -0.4174 |
| 1.000 | -1.0768 | -1.0013 | -1.0870 | -0.8640 | -0.3877 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4329 | 0.3922 | 0.3926 | ******* | -0.5068 |
| -0.400 | 0.4310 | 0.3931 | 0.3624 | 0.1788 | -0.5490 |
| -0.600 | 0.4462 | 0.3995 | 0.3546 | 0.2078 | -0.5284 |
| -0.700 | ******* | 0.4112 | 0.3551 | 0.2216 | -0.5031 |
| -0.800 | ******* | ******* | 0.3541 | 0.2384 | -0.4401 |
| -0.850 | ******* | 0.3978 | 0.3459 | 0.2436 | -0.4182 |
| -0.900 | 0.4233 | 0.3650 | 0.3297 | 0.2404 | -0.3758 |
| -0.950 | 0.3740 | 0.1715 | 0.2401 | 0.1912 | -0.1232 |
| -0.975 | ******* | 0.1193 | 0.1014 | 0.0861 | -0.0733 |
| -1.000 | -1.0960 | -0.9991 | -1.0715 | -0.8609 | -0.3953 |

Surface Pressures




Small Radius L.E.

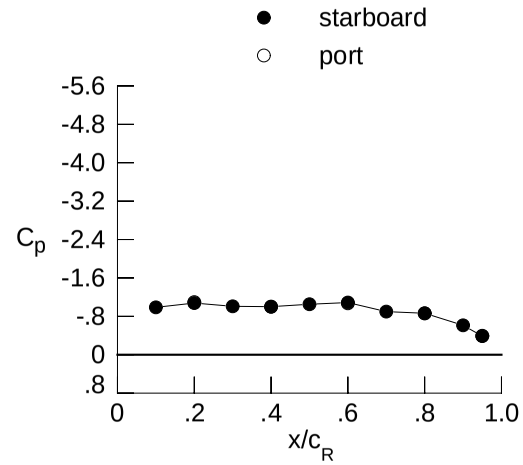
Run No. = 43 , Point No. = 914

$C_N$ = 0.944, $C_m$ = -0.1785

$\alpha$ = 18.6 °, $M_\infty$ = 0.899

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

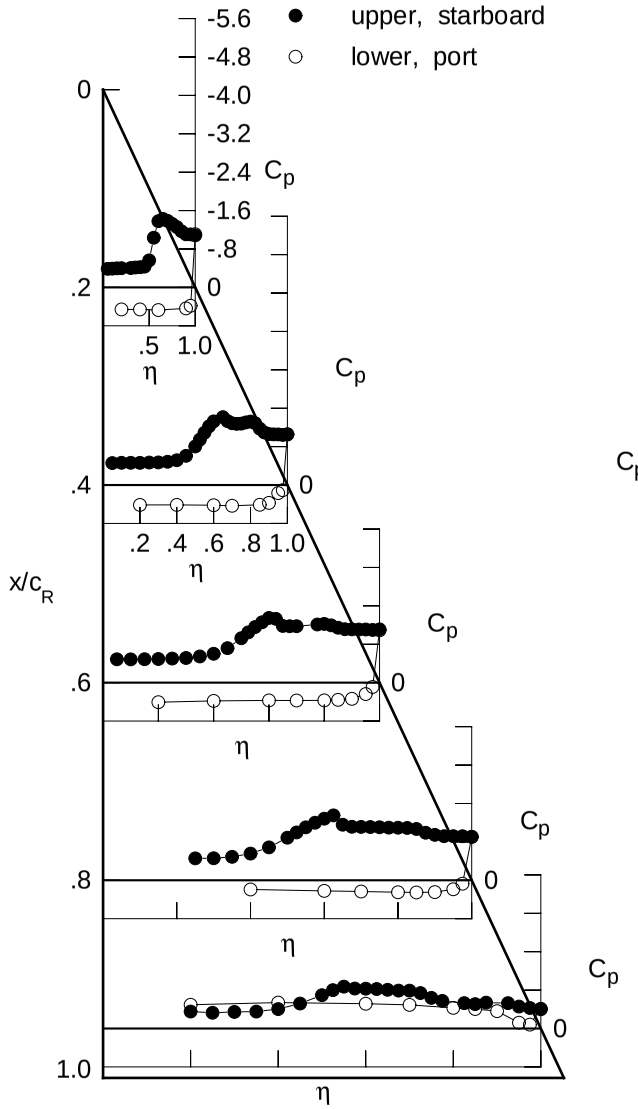



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -0.9871 | ******* |
| 0.20 | -1.0768 | -1.0960 |
| 0.30 | -1.0085 | ******* |
| 0.40 | -1.0013 | -0.9991 |
| 0.50 | -1.0517 | ******* |
| 0.60 | -1.0870 | -1.0715 |
| 0.70 | -0.8981 | ******* |
| 0.80 | -0.8640 | -0.8609 |
| 0.90 | -0.6130 | ******* |
| 0.95 | -0.3877 | -0.3953 |

# Table D6. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.3861 | -0.4578 | -0.4861 | ******* | ******* |
| 0.100 | -0.3906 | -0.4634 | -0.4851 | ******* | ******* |
| 0.150 | -0.3973 | -0.4630 | -0.4877 | ******* | ******* |
| 0.200 | -0.4002 | -0.4626 | -0.4932 | ******* | -0.3536 |
| 0.250 | ******* | -0.4687 | -0.5015 | -0.4571 | -0.3281 |
| 0.300 | -0.4035 | -0.4712 | -0.5137 | -0.4589 | -0.3455 |
| 0.350 | -0.4142 | -0.4846 | -0.5452 | -0.4887 | -0.3529 |
| 0.400 | -0.4203 | -0.5162 | -0.6015 | -0.5562 | -0.4052 |
| 0.450 | -0.4322 | -0.6088 | -0.7183 | -0.6855 | -0.5202 |
| 0.500 | -0.5630 | -0.8030 | -0.9257 | -0.8875 | -0.6945 |
| 0.525 | ******* | -0.9453 | -1.0467 | -0.9966 | -0.7988 |
| 0.550 | -1.0344 | -1.0890 | -1.1582 | -1.1030 | -0.8721 |
| 0.575 | ******* | -1.2232 | -1.2576 | -1.1992 | -0.8325 |
| 0.600 | -1.3790 | -1.3260 | -1.3479 | -1.2828 | -0.8294 |
| 0.625 | ******* | ******* | -1.3299 | -1.3523 | -0.8228 |
| 0.650 | -1.4257 | -1.4146 | -1.1819 | -1.1579 | -0.8068 |
| 0.675 | ******* | -1.3317 | -1.1753 | -1.1147 | -0.7895 |
| 0.700 | -1.3859 | -1.2874 | -1.1754 | -1.1122 | -0.7886 |
| 0.725 | ******* | -1.2753 | ******* | -1.1095 | -0.7382 |
| 0.750 | -1.3222 | -1.2795 | ******* | -1.1048 | -0.6380 |
| 0.775 | ******* | -1.3048 | -1.2110 | -1.0970 | -0.5756 |
| 0.800 | -1.2577 | -1.3223 | -1.2238 | -1.0951 | ******* |
| 0.825 | ******* | -1.2889 | -1.1933 | -1.0903 | -0.5290 |
| 0.850 | -1.1695 | -1.1740 | -1.1441 | -1.0687 | -0.5082 |
| 0.875 | ******* | -1.0951 | -1.1124 | -0.9907 | -0.5388 |
| 0.900 | -1.1052 | -1.0627 | -1.1104 | -0.9462 | ******* |
| 0.925 | ******* | -1.0558 | -1.1066 | -0.9194 | -0.5288 |
| 0.950 | -1.1039 | -1.0545 | -1.1068 | -0.9193 | -0.4577 |
| 0.975 | ******* | -1.0441 | -1.0976 | -0.9173 | -0.4270 |
| 1.000 | -1.0840 | -1.0532 | -1.1093 | -0.9061 | -0.4012 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4593 | 0.4145 | 0.4073 | ******* | -0.4946 |
| -0.400 | 0.4590 | 0.4134 | 0.3806 | 0.1913 | -0.5403 |
| -0.600 | 0.4716 | 0.4207 | 0.3702 | 0.2212 | -0.5162 |
| -0.700 | ******* | 0.4319 | 0.3724 | 0.2337 | -0.4920 |
| -0.800 | ******* | ******* | 0.3696 | 0.2493 | -0.4301 |
| -0.850 | ******* | 0.4115 | 0.3581 | 0.2534 | -0.4057 |
| -0.900 | 0.4376 | 0.3718 | 0.3376 | 0.2467 | -0.3619 |
| -0.950 | 0.3828 | 0.1678 | 0.2373 | 0.1872 | -0.1204 |
| -0.975 | ******* | 0.1077 | 0.0898 | 0.0712 | -0.0808 |
| -1.000 | -1.1082 | -1.0592 | -1.0907 | -0.9040 | -0.4124 |

Surface Pressures




Small Radius L.E.

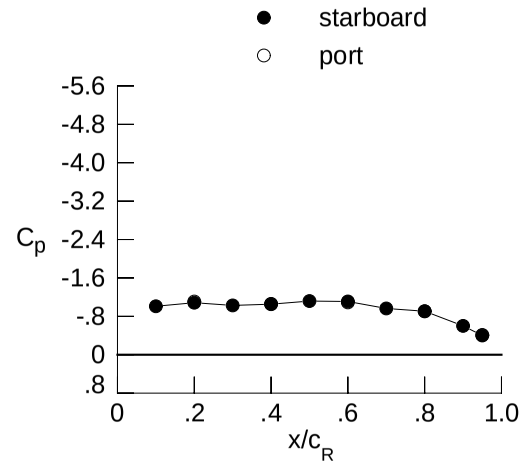
Run No. = 43 , Point No. = 915

$C_N$ = 1.009, $C_m$ = -0.1951

$\alpha$ = 19.6 °, $M_\infty$ = 0.900

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

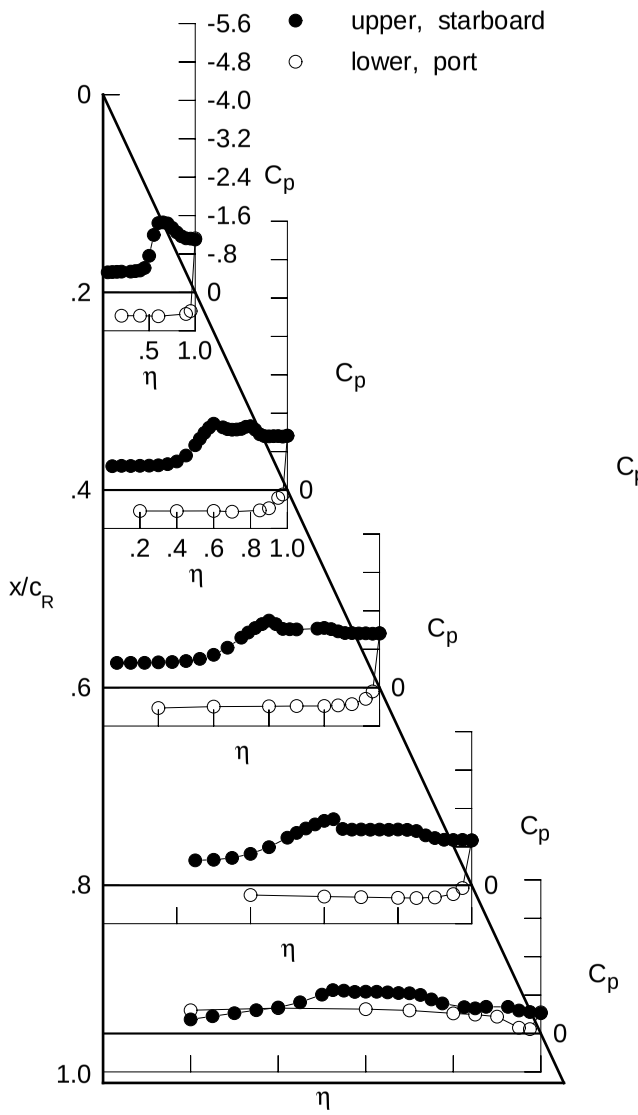



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0099 | ******* |
| 0.20 | -1.0840 | -1.1082 |
| 0.30 | -1.0272 | ******* |
| 0.40 | -1.0532 | -1.0592 |
| 0.50 | -1.1180 | ******* |
| 0.60 | -1.1093 | -1.0907 |
| 0.70 | -0.9639 | ******* |
| 0.80 | -0.9061 | -0.9040 |
| 0.90 | -0.6011 | ******* |
| 0.95 | -0.4012 | -0.4124 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4184 | -0.4971 | -0.5153 | ******* | ******* |
| 0.100 | -0.4241 | -0.5040 | -0.5163 | ******* | ******* |
| 0.150 | -0.4277 | -0.5006 | -0.5172 | ******* | ******* |
| 0.200 | -0.4323 | -0.5049 | -0.5273 | ******* | -0.2938 |
| 0.250 | ******* | -0.5078 | -0.5334 | -0.5195 | -0.3599 |
| 0.300 | -0.4327 | -0.5156 | -0.5544 | -0.5315 | -0.4231 |
| 0.350 | -0.4433 | -0.5395 | -0.5993 | -0.5704 | -0.4859 |
| 0.400 | -0.4563 | -0.5955 | -0.6843 | -0.6544 | -0.5412 |
| 0.450 | -0.5087 | -0.7191 | -0.8317 | -0.7934 | -0.6501 |
| 0.500 | -0.7626 | -0.9338 | -1.0411 | -0.9912 | -0.8097 |
| 0.525 | ******* | -1.0670 | -1.1478 | -1.0911 | -0.9044 |
| 0.550 | -1.1964 | -1.1906 | -1.2413 | -1.1834 | -0.8927 |
| 0.575 | ******* | -1.2976 | -1.3238 | -1.2677 | -0.8667 |
| 0.600 | -1.4437 | -1.3817 | -1.3964 | -1.3423 | -0.8713 |
| 0.625 | ******* | ******* | -1.3235 | -1.3770 | -0.8699 |
| 0.650 | -1.4581 | -1.3066 | -1.2230 | -1.1739 | -0.8569 |
| 0.675 | ******* | -1.2684 | -1.2165 | -1.1596 | -0.8432 |
| 0.700 | -1.4371 | -1.2571 | -1.2127 | -1.1623 | -0.8387 |
| 0.725 | ******* | -1.2607 | ******* | -1.1578 | -0.8029 |
| 0.750 | -1.3449 | -1.2738 | ******* | -1.1598 | -0.7101 |
| 0.775 | ******* | -1.3174 | -1.2293 | -1.1560 | -0.6261 |
| 0.800 | -1.2506 | -1.3303 | -1.2442 | -1.1616 | ******* |
| 0.825 | ******* | -1.2584 | -1.2192 | -1.1543 | -0.5486 |
| 0.850 | -1.1695 | -1.1613 | -1.1724 | -1.1305 | -0.5242 |
| 0.875 | ******* | -1.1243 | -1.1379 | -1.0402 | -0.5560 |
| 0.900 | -1.1262 | -1.1184 | -1.1366 | -0.9839 | ******* |
| 0.925 | ******* | -1.1221 | -1.1287 | -0.9480 | -0.5551 |
| 0.950 | -1.1202 | -1.1237 | -1.1320 | -0.9443 | -0.4791 |
| 0.975 | ******* | -1.1132 | -1.1231 | -0.9454 | -0.4477 |
| 1.000 | -1.1013 | -1.1281 | -1.1363 | -0.9334 | -0.4225 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.4868 | 0.4368 | 0.4245 | ******* | -0.4843 |
| -0.400 | 0.4854 | 0.4372 | 0.3954 | 0.2029 | -0.5288 |
| -0.600 | 0.4971 | 0.4350 | 0.3891 | 0.2350 | -0.5075 |
| -0.700 | ******* | 0.4521 | 0.3829 | 0.2471 | -0.4804 |
| -0.800 | ******* | ******* | 0.3822 | 0.2617 | -0.4193 |
| -0.850 | ******* | 0.4238 | 0.3699 | 0.2653 | -0.3946 |
| -0.900 | 0.4497 | 0.3790 | 0.3443 | 0.2525 | -0.3509 |
| -0.950 | 0.3889 | 0.1639 | 0.2339 | 0.1839 | -0.1202 |
| -0.975 | ******* | 0.0930 | 0.0783 | 0.0574 | -0.0914 |
| -1.000 | -1.1260 | -1.1344 | -1.1247 | -0.9364 | -0.4404 |

Surface Pressures




Small Radius L.E.

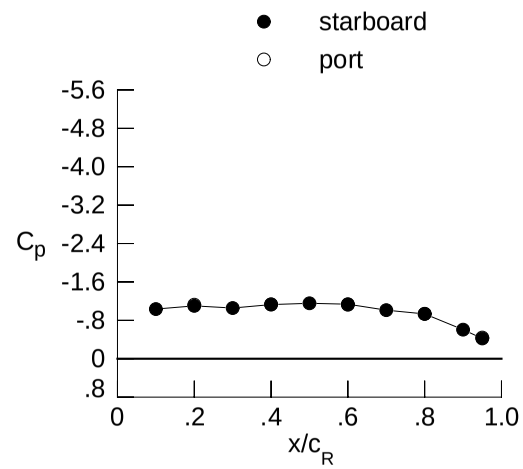
Run No. = 43 , Point No. = 916

$C_N$ = 1.061, $C_m$ = -0.2015

$\alpha$ = 20.6 °, $M_\infty$ = 0.900

$R_{mac}$ = $6.0 \times 10^6$

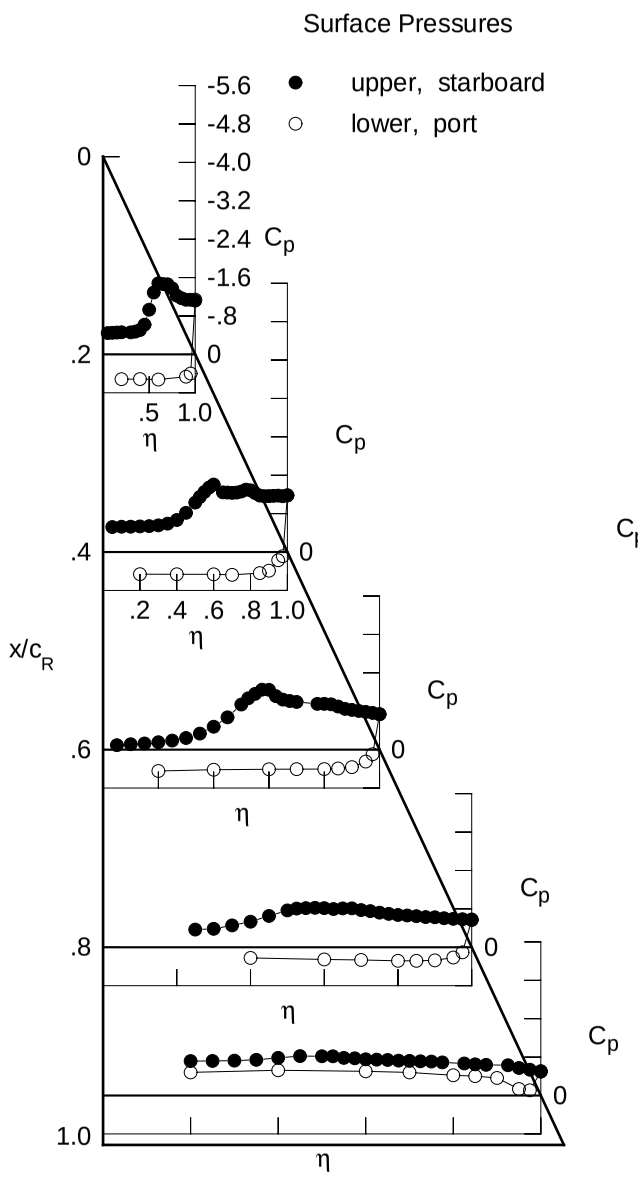
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0348 | ******* |
| 0.20 | -1.1013 | -1.1260 |
| 0.30 | -1.0562 | ******* |
| 0.40 | -1.1281 | -1.1344 |
| 0.50 | -1.1548 | ******* |
| 0.60 | -1.1363 | -1.1247 |
| 0.70 | -1.0118 | ******* |
| 0.80 | -0.9334 | -0.9364 |
| 0.90 | -0.6054 | ******* |
| 0.95 | -0.4225 | -0.4404 |

# Table D6. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4437 | -0.5208 | -0.0926 | ******* | ******* |
| 0.100 | -0.4493 | -0.5273 | -0.1131 | ******* | ******* |
| 0.150 | -0.4555 | -0.5283 | -0.1292 | ******* | ******* |
| 0.200 | -0.4605 | -0.5334 | -0.1545 | ******* | -0.7176 |
| 0.250 | ******* | -0.5403 | -0.1887 | -0.3686 | -0.7198 |
| 0.300 | -0.4589 | -0.5561 | -0.2423 | -0.3849 | -0.7268 |
| 0.350 | -0.4745 | -0.5908 | -0.3346 | -0.4556 | -0.7435 |
| 0.400 | -0.5073 | -0.6670 | -0.4774 | -0.5327 | -0.7851 |
| 0.450 | -0.6188 | -0.8171 | -0.6728 | -0.6530 | -0.8211 |
| 0.500 | -0.9313 | -1.0295 | -0.9397 | -0.7678 | -0.8179 |
| 0.525 | ******* | -1.1475 | -1.0696 | -0.8061 | -0.8168 |
| 0.550 | -1.2891 | -1.2509 | -1.1623 | -0.8157 | -0.7841 |
| 0.575 | ******* | -1.3433 | -1.2494 | -0.8224 | -0.7755 |
| 0.600 | -1.4810 | -1.4064 | -1.2466 | -0.8157 | -0.7546 |
| 0.625 | ******* | ******* | -1.1146 | -0.7968 | -0.7472 |
| 0.650 | -1.4652 | -1.2432 | -1.0422 | -0.8093 | -0.7411 |
| 0.675 | ******* | -1.2392 | -1.0139 | -0.8114 | -0.7261 |
| 0.700 | -1.4606 | -1.2331 | -0.9937 | -0.7751 | -0.7219 |
| 0.725 | ******* | -1.2396 | ******* | -0.7538 | -0.7128 |
| 0.750 | -1.3754 | -1.2604 | ******* | -0.7215 | -0.7071 |
| 0.775 | ******* | -1.3001 | -0.9535 | -0.6959 | -0.6894 |
| 0.800 | -1.2237 | -1.2868 | -0.9548 | -0.6738 | ******* |
| 0.825 | ******* | -1.2283 | -0.9444 | -0.6625 | -0.6671 |
| 0.850 | -1.1713 | -1.1760 | -0.8984 | -0.6480 | -0.6498 |
| 0.875 | ******* | -1.1638 | -0.8493 | -0.6297 | -0.6391 |
| 0.900 | -1.1387 | -1.1654 | -0.8277 | -0.6255 | ******* |
| 0.925 | ******* | -1.1715 | -0.8065 | -0.6055 | -0.6304 |
| 0.950 | -1.1374 | -1.1753 | -0.7864 | -0.5926 | -0.5736 |
| 0.975 | ******* | -1.1627 | -0.7650 | -0.5850 | -0.5372 |
| 1.000 | -1.1203 | -1.1768 | -0.7385 | -0.5802 | -0.5084 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5165 | 0.4615 | 0.4448 | ******* | -0.4819 |
| -0.400 | 0.5144 | 0.4633 | 0.4184 | 0.2215 | -0.5259 |
| -0.600 | 0.5240 | 0.4645 | 0.4087 | 0.2534 | -0.5038 |
| -0.700 | ******* | 0.4750 | 0.4061 | 0.2643 | -0.4806 |
| -0.800 | ******* | ******* | 0.4048 | 0.2814 | -0.4212 |
| -0.850 | ******* | 0.4392 | 0.3924 | 0.2823 | -0.4036 |
| -0.900 | 0.4642 | 0.3890 | 0.3651 | 0.2727 | -0.3653 |
| -0.950 | 0.3992 | 0.1710 | 0.2480 | 0.2134 | -0.1350 |
| -0.975 | ******* | 0.0868 | 0.0950 | 0.1046 | -0.1090 |
| -1.000 | -1.1420 | -1.1841 | -0.7379 | -0.5674 | -0.4955 |



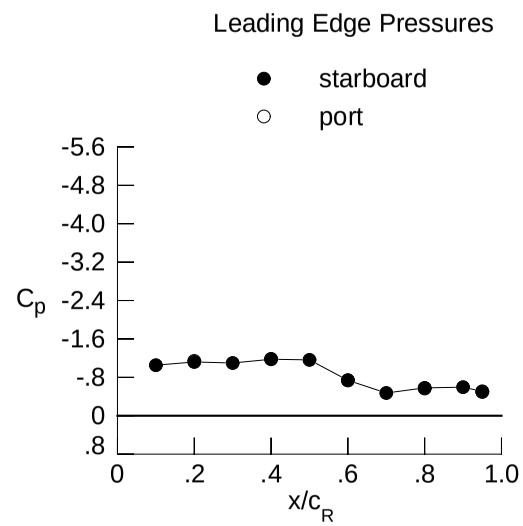

Small Radius L.E.

Run No. = 43 , Point No. = 917

$C_N$ = 0.963, $C_m$ = -0.1621

$\alpha$ = 21.6 °, $M_\infty$ = 0.901

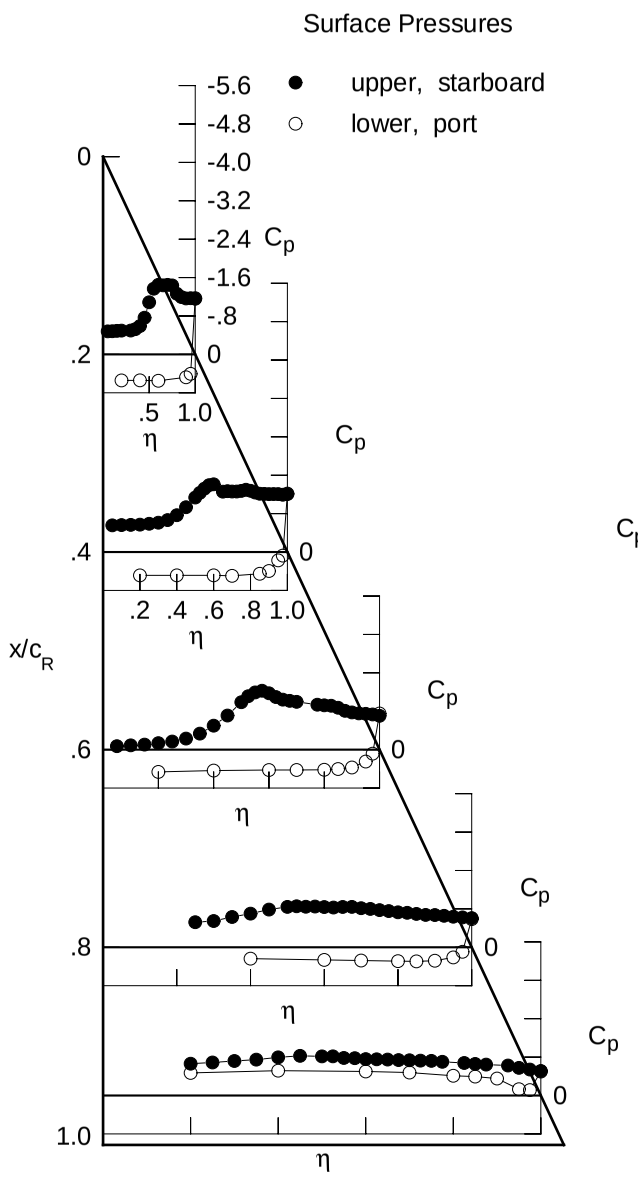
$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0530 | ******* |
| 0.20 | -1.1203 | -1.1420 |
| 0.30 | -1.0984 | ******* |
| 0.40 | -1.1768 | -1.1841 |
| 0.50 | -1.1636 | ******* |
| 0.60 | -0.7385 | -0.7379 |
| 0.70 | -0.4734 | ******* |
| 0.80 | -0.5802 | -0.5674 |
| 0.90 | -0.5949 | ******* |
| 0.95 | -0.5084 | -0.4955 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.4803 | -0.5561 | -0.0720 | ******* | ******* |
| 0.100 | -0.4824 | -0.5613 | -0.0896 | ******* | ******* |
| 0.150 | -0.4903 | -0.5659 | -0.1052 | ******* | ******* |
| 0.200 | -0.4953 | -0.5705 | -0.1355 | ******* | -0.6626 |
| 0.250 | ******* | -0.5887 | -0.1687 | -0.5220 | -0.6882 |
| 0.300 | -0.4966 | -0.6113 | -0.2301 | -0.5475 | -0.7194 |
| 0.350 | -0.5256 | -0.6658 | -0.3333 | -0.6316 | -0.7473 |
| 0.400 | -0.5903 | -0.7668 | -0.4995 | -0.7010 | -0.7953 |
| 0.450 | -0.7642 | -0.9336 | -0.7108 | -0.7860 | -0.8267 |
| 0.500 | -1.0854 | -1.1348 | -0.9881 | -0.8418 | -0.8153 |
| 0.525 | ******* | -1.2329 | -1.1129 | -0.8541 | -0.8164 |
| 0.550 | -1.3678 | -1.3208 | -1.1919 | -0.8449 | -0.7821 |
| 0.575 | ******* | -1.3925 | -1.2276 | -0.8491 | -0.7775 |
| 0.600 | -1.4497 | -1.4114 | -1.1748 | -0.8385 | -0.7583 |
| 0.625 | ******* | ******* | -1.0964 | -0.8281 | -0.7542 |
| 0.650 | -1.4386 | -1.2579 | -1.0412 | -0.8398 | -0.7488 |
| 0.675 | ******* | -1.2676 | -1.0168 | -0.8420 | -0.7386 |
| 0.700 | -1.4491 | -1.2608 | -0.9957 | -0.8145 | -0.7345 |
| 0.725 | ******* | -1.2611 | ******* | -0.7991 | -0.7261 |
| 0.750 | -1.4365 | -1.2737 | ******* | -0.7745 | -0.7219 |
| 0.775 | ******* | -1.2977 | -0.9360 | -0.7541 | -0.7020 |
| 0.800 | -1.2639 | -1.2757 | -0.9230 | -0.7288 | ******* |
| 0.825 | ******* | -1.2398 | -0.9145 | -0.7182 | -0.6776 |
| 0.850 | -1.1941 | -1.2141 | -0.8727 | -0.6949 | -0.6579 |
| 0.875 | ******* | -1.2113 | -0.8091 | -0.6744 | -0.6439 |
| 0.900 | -1.1654 | -1.2065 | -0.7750 | -0.6722 | ******* |
| 0.925 | ******* | -1.2082 | -0.7552 | -0.6559 | -0.6252 |
| 0.950 | -1.1702 | -1.2074 | -0.7462 | -0.6371 | -0.5760 |
| 0.975 | ******* | -1.1934 | -0.7332 | -0.6225 | -0.5407 |
| 1.000 | -1.1584 | -1.2074 | -0.7050 | -0.6077 | -0.5108 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5427 | 0.4860 | 0.4637 | ******* | -0.4707 |
| -0.400 | 0.5410 | 0.4855 | 0.4359 | 0.2367 | -0.5175 |
| -0.600 | 0.5495 | 0.4853 | 0.4244 | 0.2630 | -0.5009 |
| -0.700 | ******* | 0.4957 | 0.4239 | 0.2756 | -0.4782 |
| -0.800 | ******* | ******* | 0.4195 | 0.2889 | -0.4112 |
| -0.850 | ******* | 0.4528 | 0.4041 | 0.2933 | -0.3943 |
| -0.900 | 0.4770 | 0.3952 | 0.3723 | 0.2801 | -0.3535 |
| -0.950 | 0.4048 | 0.1734 | 0.2480 | 0.2108 | -0.1314 |
| -0.975 | ******* | 0.0748 | 0.0836 | 0.0933 | -0.1127 |
| -1.000 | -1.1715 | -1.2180 | -0.7530 | -0.5864 | -0.4982 |



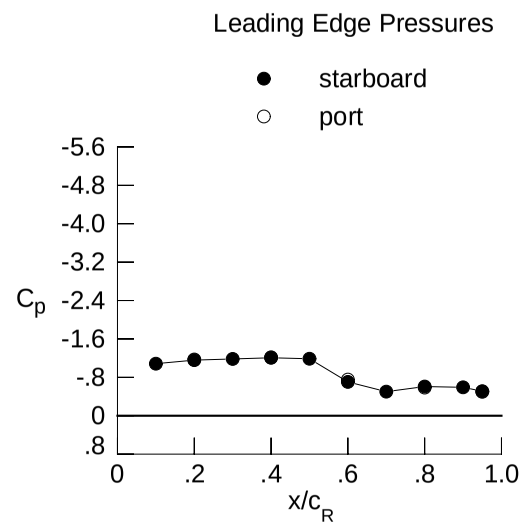

Small Radius L.E.

Run No. = 43 , Point No. = 918

$C_N$ = 1.013, $C_m$ = -0.1736

$\alpha$ = 22.6 °, $M_\infty$ = 0.899

$R_{mac}$ = $6.0 \times 10^6$

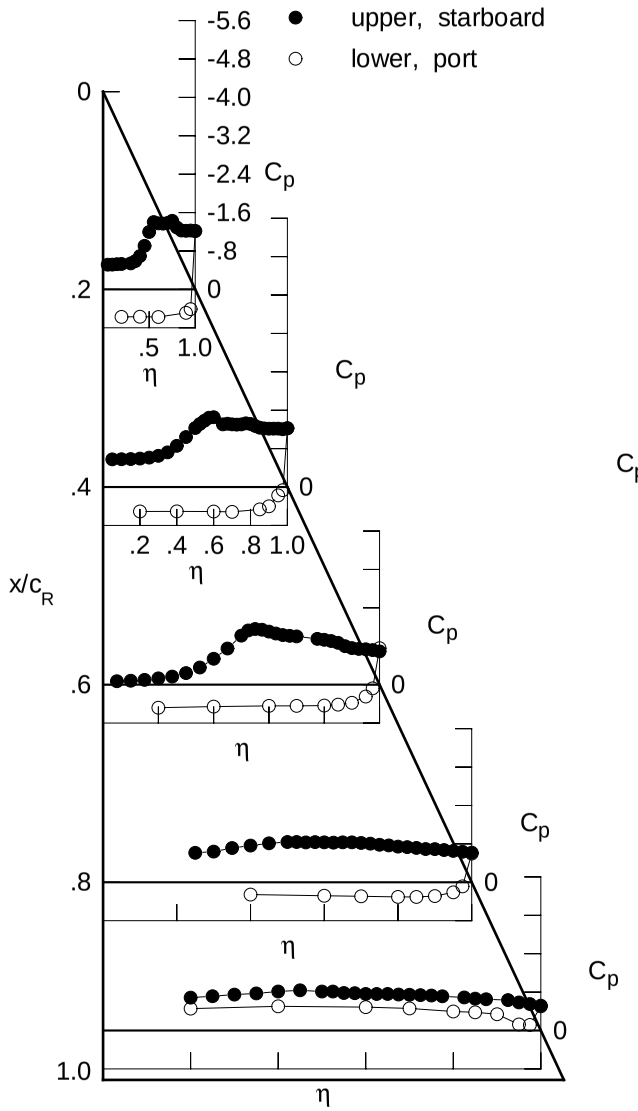



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.0843 | ******* |
| 0.20 | -1.1584 | -1.1715 |
| 0.30 | -1.1828 | ******* |
| 0.40 | -1.2074 | -1.2180 |
| 0.50 | -1.1869 | ******* |
| 0.60 | -0.7050 | -0.7530 |
| 0.70 | -0.5016 | ******* |
| 0.80 | -0.6077 | -0.5864 |
| 0.90 | -0.5920 | ******* |
| 0.95 | -0.5108 | -0.4982 |

# Table D6. Continued.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5145 | -0.5766 | -0.0710 | ******* | ******* |
| 0.100 | -0.5164 | -0.5789 | -0.0816 | ******* | ******* |
| 0.150 | -0.5248 | -0.5834 | -0.0995 | ******* | ******* |
| 0.200 | -0.5295 | -0.5930 | -0.1310 | ******* | -0.6850 |
| 0.250 | ******* | -0.6128 | -0.1679 | -0.6139 | -0.7146 |
| 0.300 | -0.5415 | -0.6507 | -0.2409 | -0.6392 | -0.7483 |
| 0.350 | -0.5886 | -0.7226 | -0.3565 | -0.7137 | -0.7724 |
| 0.400 | -0.6945 | -0.8583 | -0.5393 | -0.7648 | -0.8127 |
| 0.450 | -0.9076 | -1.0413 | -0.7529 | -0.8116 | -0.8379 |
| 0.500 | -1.1963 | -1.2300 | -1.0208 | -0.8396 | -0.8119 |
| 0.525 | ******* | -1.3126 | -1.1291 | -0.8395 | -0.8119 |
| 0.550 | -1.4025 | -1.3811 | -1.1593 | -0.8307 | -0.7817 |
| 0.575 | ******* | -1.4440 | -1.1441 | -0.8364 | -0.7780 |
| 0.600 | -1.3755 | -1.4540 | -1.1047 | -0.8321 | -0.7616 |
| 0.625 | ******* | ******* | -1.0644 | -0.8259 | -0.7611 |
| 0.650 | -1.3699 | -1.3059 | -1.0325 | -0.8321 | -0.7613 |
| 0.675 | ******* | -1.3193 | -1.0169 | -0.8319 | -0.7500 |
| 0.700 | -1.3842 | -1.3055 | -1.0049 | -0.8194 | -0.7447 |
| 0.725 | ******* | -1.2996 | ******* | -0.8051 | -0.7372 |
| 0.750 | -1.4287 | -1.3047 | ******* | -0.7815 | -0.7291 |
| 0.775 | ******* | -1.3270 | -0.9536 | -0.7683 | -0.7124 |
| 0.800 | -1.2901 | -1.3124 | -0.9344 | -0.7434 | ******* |
| 0.825 | ******* | -1.2727 | -0.9091 | -0.7330 | -0.6886 |
| 0.850 | -1.2264 | -1.2362 | -0.8711 | -0.7163 | -0.6638 |
| 0.875 | ******* | -1.2210 | -0.8016 | -0.6931 | -0.6511 |
| 0.900 | -1.2206 | -1.2151 | -0.7619 | -0.6911 | ******* |
| 0.925 | ******* | -1.2161 | -0.7439 | -0.6720 | -0.6333 |
| 0.950 | -1.2262 | -1.2169 | -0.7365 | -0.6539 | -0.5850 |
| 0.975 | ******* | -1.2037 | -0.7203 | -0.6362 | -0.5514 |
| 1.000 | -1.2184 | -1.2217 | -0.6930 | -0.6176 | -0.5177 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5729 | 0.5091 | 0.4804 | ******* | -0.4556 |
| -0.400 | 0.5697 | 0.5074 | 0.4573 | 0.2556 | -0.5039 |
| -0.600 | 0.5751 | 0.5106 | 0.4424 | 0.2806 | -0.4872 |
| -0.700 | ******* | 0.5175 | 0.4422 | 0.2917 | -0.4598 |
| -0.800 | ******* | ******* | 0.4361 | 0.3045 | -0.3964 |
| -0.850 | ******* | 0.4658 | 0.4165 | 0.3053 | -0.3795 |
| -0.900 | 0.4887 | 0.4016 | 0.3782 | 0.2868 | -0.3395 |
| -0.950 | 0.4114 | 0.1740 | 0.2480 | 0.2092 | -0.1264 |
| -0.975 | ******* | 0.0658 | 0.0768 | 0.0848 | -0.1157 |
| -1.000 | -1.2133 | -1.2273 | -0.7593 | -0.5982 | -0.5040 |

Surface Pressures




Small Radius L.E.

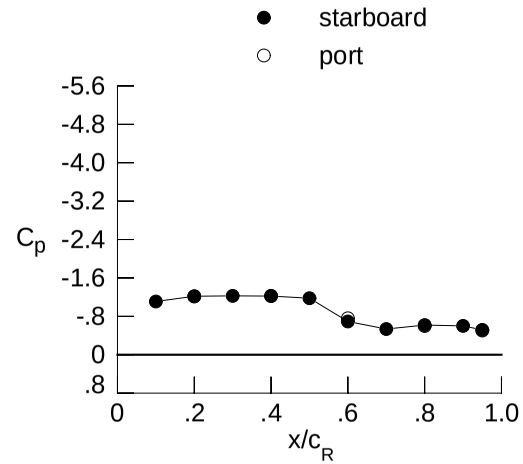
Run No. = 43 , Point No. = 919

$C_N$ = 1.053, $C_m$ = -0.1802

$\alpha$ = 23.6 °, $M_\infty$ = 0.899

$R_{mac}$ = $6.0 \times 10^6$

Leading Edge Pressures

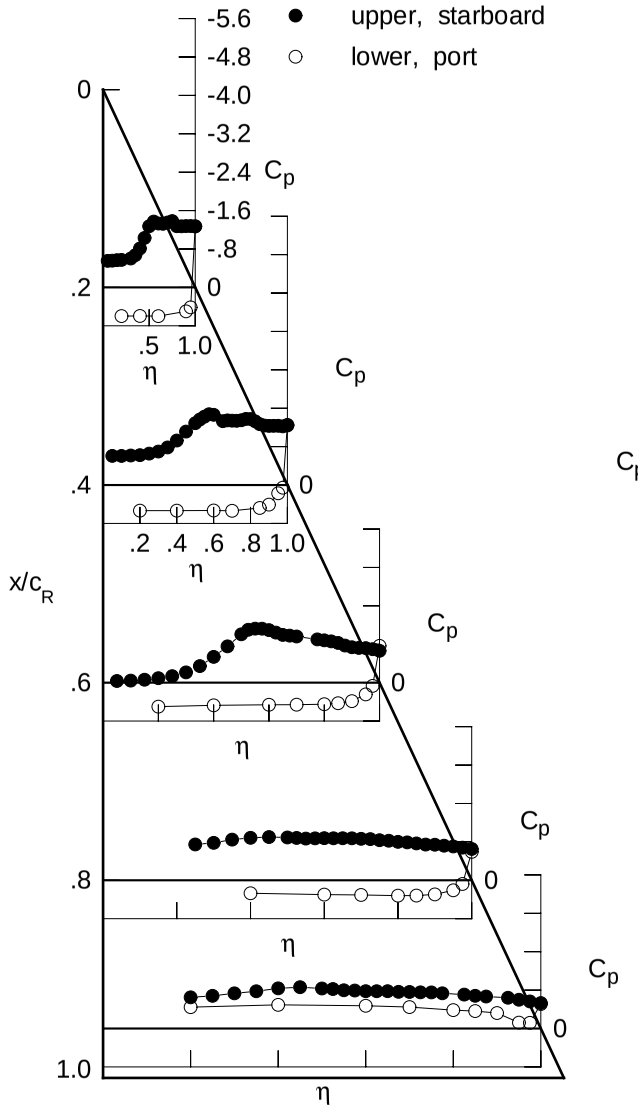



| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1092 | ******* |
| 0.20 | -1.2184 | -1.2133 |
| 0.30 | -1.2265 | ******* |
| 0.40 | -1.2217 | -1.2273 |
| 0.50 | -1.1777 | ******* |
| 0.60 | -0.6930 | -0.7593 |
| 0.70 | -0.5356 | ******* |
| 0.80 | -0.6176 | -0.5982 |
| 0.90 | -0.6011 | ******* |
| 0.95 | -0.5177 | -0.5040 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5526 | -0.6069 | -0.0342 | ******* | ******* |
| 0.100 | -0.5568 | -0.6065 | -0.0426 | ******* | ******* |
| 0.150 | -0.5669 | -0.6152 | -0.0609 | ******* | ******* |
| 0.200 | -0.5732 | -0.6227 | -0.0929 | ******* | -0.6495 |
| 0.250 | ******* | -0.6543 | -0.1348 | -0.7463 | -0.6806 |
| 0.300 | -0.6014 | -0.6973 | -0.2136 | -0.7801 | -0.7331 |
| 0.350 | -0.6710 | -0.7832 | -0.3448 | -0.8468 | -0.7757 |
| 0.400 | -0.8109 | -0.9270 | -0.5367 | -0.8844 | -0.8366 |
| 0.450 | -1.0306 | -1.1135 | -0.7564 | -0.9008 | -0.8604 |
| 0.500 | -1.2739 | -1.2878 | -1.0070 | -0.8923 | -0.8335 |
| 0.525 | ******* | -1.3646 | -1.1016 | -0.8823 | -0.8223 |
| 0.550 | -1.3712 | -1.4249 | -1.1248 | -0.8689 | -0.7966 |
| 0.575 | ******* | -1.4755 | -1.1240 | -0.8738 | -0.7910 |
| 0.600 | -1.3307 | -1.4633 | -1.0943 | -0.8775 | -0.7773 |
| 0.625 | ******* | ******* | -1.0422 | -0.8750 | -0.7767 |
| 0.650 | -1.3245 | -1.3307 | -0.9942 | -0.8762 | -0.7776 |
| 0.675 | ******* | -1.3473 | -0.9789 | -0.8743 | -0.7637 |
| 0.700 | -1.3518 | -1.3409 | -0.9613 | -0.8644 | -0.7618 |
| 0.725 | ******* | -1.3382 | ******* | -0.8578 | -0.7538 |
| 0.750 | -1.3817 | -1.3494 | ******* | -0.8355 | -0.7521 |
| 0.775 | ******* | -1.3774 | -0.9011 | -0.8238 | -0.7334 |
| 0.800 | -1.2744 | -1.3754 | -0.8817 | -0.8010 | ******* |
| 0.825 | ******* | -1.3280 | -0.8598 | -0.7898 | -0.7061 |
| 0.850 | -1.2732 | -1.2681 | -0.8268 | -0.7677 | -0.6814 |
| 0.875 | ******* | -1.2390 | -0.7726 | -0.7438 | -0.6661 |
| 0.900 | -1.2780 | -1.2323 | -0.7375 | -0.7412 | ******* |
| 0.925 | ******* | -1.2333 | -0.7228 | -0.7211 | -0.6406 |
| 0.950 | -1.2786 | -1.2348 | -0.7195 | -0.7048 | -0.5990 |
| 0.975 | ******* | -1.2223 | -0.6969 | -0.6799 | -0.5636 |
| 1.000 | -1.2700 | -1.2412 | -0.6635 | -0.6532 | -0.5307 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.5979 | 0.5334 | 0.4996 | ******* | -0.4451 |
| -0.400 | 0.5952 | 0.5333 | 0.4726 | 0.2703 | -0.4932 |
| -0.600 | 0.5985 | 0.5305 | 0.4610 | 0.2982 | -0.4739 |
| -0.700 | ******* | 0.5367 | 0.4594 | 0.3054 | -0.4468 |
| -0.800 | ******* | ******* | 0.4496 | 0.3201 | -0.3830 |
| -0.850 | ******* | 0.4778 | 0.4290 | 0.3183 | -0.3628 |
| -0.900 | 0.4995 | 0.4081 | 0.3855 | 0.2940 | -0.3226 |
| -0.950 | 0.4162 | 0.1719 | 0.2448 | 0.2085 | -0.1221 |
| -0.975 | ******* | 0.0555 | 0.0675 | 0.0767 | -0.1183 |
| -1.000 | -1.2727 | -1.2538 | -0.7663 | -0.5919 | -0.5098 |

Surface Pressures




Small Radius L.E.

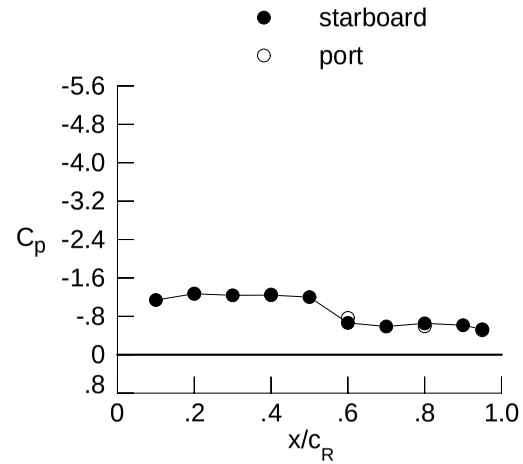
Run No. = 43 , Point No. = 920

$C_N$ = 1.086, $C_m$ = -0.1816

$\alpha$ = 24.6 °, $M_\infty$ = 0.899

$R_{mac}$ = $5.9 \times 10^6$

Leading Edge Pressures

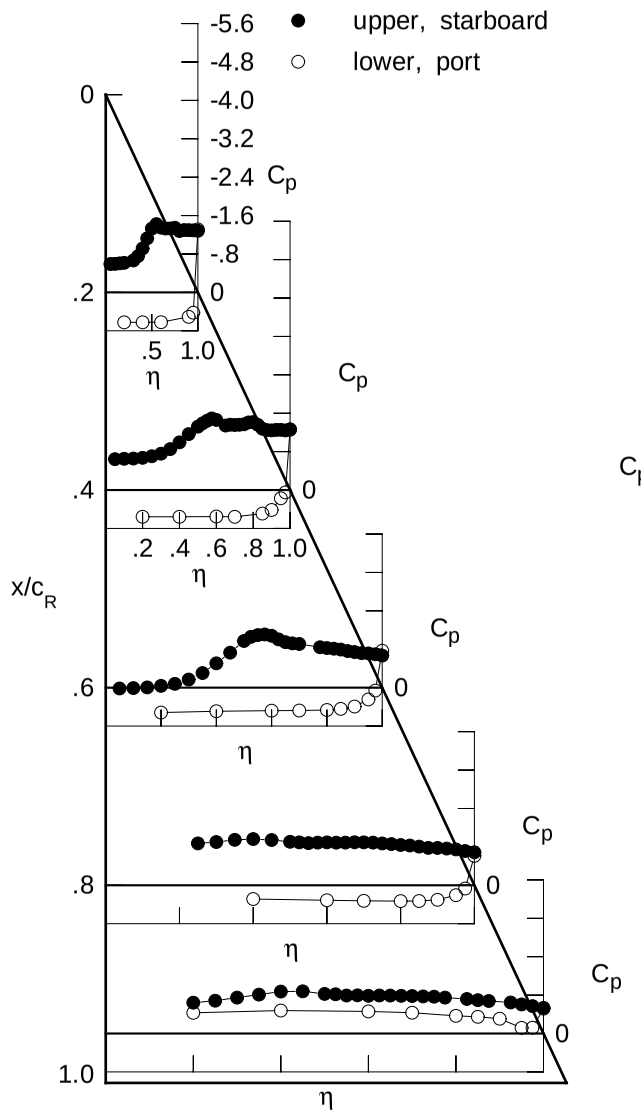



| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1402 | ******* |
| 0.20 | -1.2700 | -1.2727 |
| 0.30 | -1.2379 | ******* |
| 0.40 | -1.2412 | -1.2538 |
| 0.50 | -1.2008 | ******* |
| 0.60 | -0.6635 | -0.7663 |
| 0.70 | -0.5882 | ******* |
| 0.80 | -0.6532 | -0.5919 |
| 0.90 | -0.6147 | ******* |
| 0.95 | -0.5307 | -0.5098 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.5913 | -0.6433 | 0.0174 | ******* | ******* |
| 0.100 | -0.5942 | -0.6509 | 0.0086 | ******* | ******* |
| 0.150 | -0.6049 | -0.6562 | -0.0052 | ******* | ******* |
| 0.200 | -0.6151 | -0.6709 | -0.0365 | ******* | -0.6424 |
| 0.250 | ******* | -0.7038 | -0.0791 | -0.8731 | -0.6835 |
| 0.300 | -0.6645 | -0.7576 | -0.1688 | -0.9016 | -0.7484 |
| 0.350 | -0.7548 | -0.8528 | -0.3042 | -0.9472 | -0.8108 |
| 0.400 | -0.9150 | -0.9932 | -0.5067 | -0.9629 | -0.8739 |
| 0.450 | -1.1255 | -1.1655 | -0.7290 | -0.9432 | -0.8792 |
| 0.500 | -1.3298 | -1.3204 | -0.9717 | -0.9061 | -0.8249 |
| 0.525 | ******* | -1.3883 | -1.0577 | -0.8944 | -0.8176 |
| 0.550 | -1.4223 | -1.4430 | -1.0955 | -0.8786 | -0.7915 |
| 0.575 | ******* | -1.4913 | -1.1081 | -0.8890 | -0.7949 |
| 0.600 | -1.3489 | -1.4607 | -1.0804 | -0.8932 | -0.7856 |
| 0.625 | ******* | ******* | -1.0050 | -0.8883 | -0.7919 |
| 0.650 | -1.3304 | -1.3429 | -0.9473 | -0.8890 | -0.7901 |
| 0.675 | ******* | -1.3609 | -0.9223 | -0.8962 | -0.7848 |
| 0.700 | -1.3324 | -1.3551 | -0.9092 | -0.8943 | -0.7811 |
| 0.725 | ******* | -1.3597 | ******* | -0.8890 | -0.7732 |
| 0.750 | -1.3471 | -1.3693 | ******* | -0.8709 | -0.7671 |
| 0.775 | ******* | -1.4086 | -0.8414 | -0.8585 | -0.7478 |
| 0.800 | -1.2781 | -1.4156 | -0.8246 | -0.8395 | ******* |
| 0.825 | ******* | -1.3594 | -0.8113 | -0.8290 | -0.7194 |
| 0.850 | -1.2981 | -1.2768 | -0.7935 | -0.8059 | -0.6942 |
| 0.875 | ******* | -1.2477 | -0.7626 | -0.7789 | -0.6776 |
| 0.900 | -1.2964 | -1.2433 | -0.7414 | -0.7782 | ******* |
| 0.925 | ******* | -1.2528 | -0.7195 | -0.7649 | -0.6467 |
| 0.950 | -1.2921 | -1.2542 | -0.7135 | -0.7469 | -0.6053 |
| 0.975 | ******* | -1.2415 | -0.6953 | -0.7145 | -0.5703 |
| 1.000 | -1.2829 | -1.2572 | -0.6673 | -0.6872 | -0.5347 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.6242 | 0.5567 | 0.5189 | ******* | -0.4314 |
| -0.400 | 0.6231 | 0.5576 | 0.4922 | 0.2861 | -0.4785 |
| -0.600 | 0.6219 | 0.5523 | 0.4796 | 0.3120 | -0.4600 |
| -0.700 | ******* | 0.5584 | 0.4766 | 0.3242 | -0.4326 |
| -0.800 | ******* | ******* | 0.4655 | 0.3297 | -0.3680 |
| -0.850 | ******* | 0.4906 | 0.4424 | 0.3281 | -0.3481 |
| -0.900 | 0.5095 | 0.4149 | 0.3932 | 0.3022 | -0.3080 |
| -0.950 | 0.4229 | 0.1722 | 0.2459 | 0.2068 | -0.1177 |
| -0.975 | ******* | 0.0487 | 0.0619 | 0.0675 | -0.1213 |
| -1.000 | -1.3123 | -1.2652 | -0.7690 | -0.6128 | -0.5176 |

Surface Pressures




Small Radius L.E.

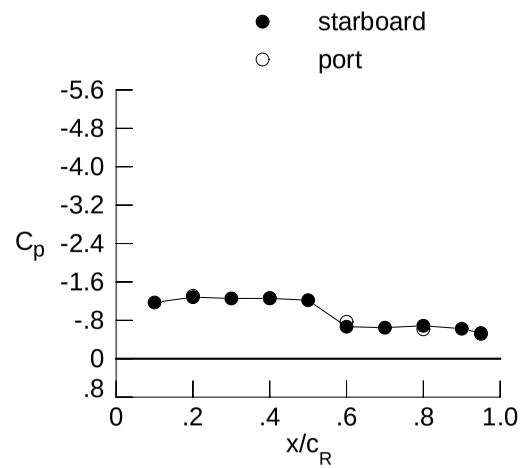
Run No. = 43 , Point No. = 921

$C_N$ = 1.115, $C_m$ = -0.1794

$\alpha$ = 25.7 °, $M_\infty$ = 0.900

$R_{mac}$ = $5.9 \times 10^6$

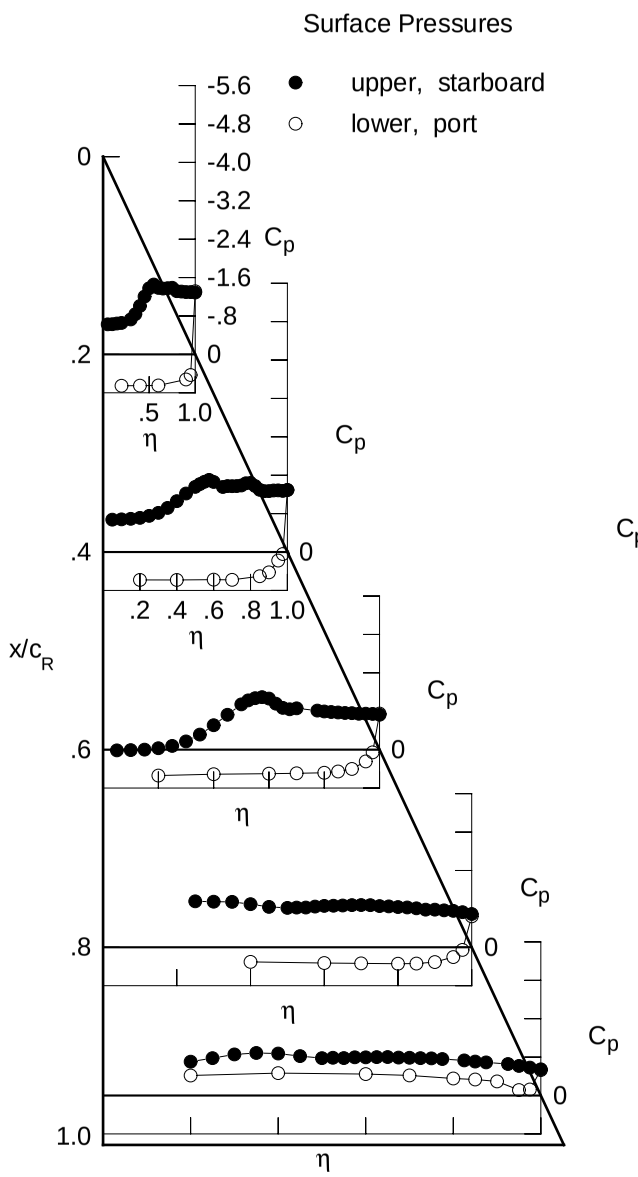
Leading Edge Pressures




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.1711 | ******* |
| 0.20 | -1.2829 | -1.3123 |
| 0.30 | -1.2559 | ******* |
| 0.40 | -1.2572 | -1.2652 |
| 0.50 | -1.2189 | ******* |
| 0.60 | -0.6673 | -0.7690 |
| 0.70 | -0.6475 | ******* |
| 0.80 | -0.6872 | -0.6128 |
| 0.90 | -0.6256 | ******* |
| 0.95 | -0.5347 | -0.5176 |

# Table D6. Continued.

| η | x/c_R .2 $C_{p,u}$ | x/c_R .4 $C_{p,u}$ | x/c_R .6 $C_{p,u}$ | x/c_R .8 $C_{p,u}$ | x/c_R .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.6261 | -0.6742 | 0.0153 | ******* | ******* |
| 0.100 | -0.6286 | -0.6811 | 0.0100 | ******* | ******* |
| 0.150 | -0.6428 | -0.6918 | 0.0000 | ******* | ******* |
| 0.200 | -0.6554 | -0.7122 | -0.0298 | ******* | -0.7051 |
| 0.250 | ******* | -0.7533 | -0.0778 | -0.9575 | -0.7784 |
| 0.300 | -0.7281 | -0.8157 | -0.1710 | -0.9494 | -0.8558 |
| 0.350 | -0.8386 | -0.9188 | -0.3133 | -0.9460 | -0.8861 |
| 0.400 | -1.0093 | -1.0598 | -0.5089 | -0.8984 | -0.8741 |
| 0.450 | -1.2045 | -1.2192 | -0.7263 | -0.8419 | -0.8206 |
| 0.500 | -1.3769 | -1.3576 | -0.9431 | -0.8208 | -0.7787 |
| 0.525 | ******* | -1.4153 | -1.0264 | -0.8273 | -0.7866 |
| 0.550 | -1.4552 | -1.4633 | -1.0720 | -0.8277 | -0.7800 |
| 0.575 | ******* | -1.5034 | -1.0935 | -0.8481 | -0.7958 |
| 0.600 | -1.3852 | -1.4602 | -1.0639 | -0.8622 | -0.7954 |
| 0.625 | ******* | ******* | -0.9577 | -0.8653 | -0.8003 |
| 0.650 | -1.3714 | -1.3549 | -0.8703 | -0.8701 | -0.8018 |
| 0.675 | ******* | -1.3743 | -0.8409 | -0.8784 | -0.7908 |
| 0.700 | -1.3792 | -1.3718 | -0.8608 | -0.8803 | -0.7864 |
| 0.725 | ******* | -1.3743 | ******* | -0.8775 | -0.7788 |
| 0.750 | -1.3880 | -1.3861 | ******* | -0.8584 | -0.7736 |
| 0.775 | ******* | -1.4328 | -0.8133 | -0.8518 | -0.7598 |
| 0.800 | -1.3164 | -1.4400 | -0.7950 | -0.8381 | ******* |
| 0.825 | ******* | -1.3753 | -0.7843 | -0.8298 | -0.7309 |
| 0.850 | -1.3086 | -1.2956 | -0.7746 | -0.8121 | -0.7069 |
| 0.875 | ******* | -1.2679 | -0.7644 | -0.7838 | -0.6898 |
| 0.900 | -1.2987 | -1.2694 | -0.7601 | -0.7840 | ******* |
| 0.925 | ******* | -1.2824 | -0.7475 | -0.7697 | -0.6558 |
| 0.950 | -1.2972 | -1.2846 | -0.7489 | -0.7593 | -0.6158 |
| 0.975 | ******* | -1.2734 | -0.7439 | -0.7311 | -0.5820 |
| 1.000 | -1.2885 | -1.2927 | -0.7268 | -0.6934 | -0.5456 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | 0.6532 | 0.5810 | 0.5398 | ******* | -0.4172 |
| -0.400 | 0.6514 | 0.5818 | 0.5122 | 0.3043 | -0.4665 |
| -0.600 | 0.6475 | 0.5754 | 0.5008 | 0.3281 | -0.4468 |
| -0.700 | ******* | 0.5794 | 0.4931 | 0.3354 | -0.4183 |
| -0.800 | ******* | ******* | 0.4818 | 0.3425 | -0.3547 |
| -0.850 | ******* | 0.5040 | 0.4550 | 0.3388 | -0.3333 |
| -0.900 | 0.5225 | 0.4229 | 0.4020 | 0.3082 | -0.2937 |
| -0.950 | 0.4300 | 0.1776 | 0.2454 | 0.2037 | -0.1139 |
| -0.975 | ******* | 0.0414 | 0.0560 | 0.0541 | -0.1255 |
| -1.000 | -1.3155 | -1.2921 | -0.7515 | -0.6450 | -0.5294 |



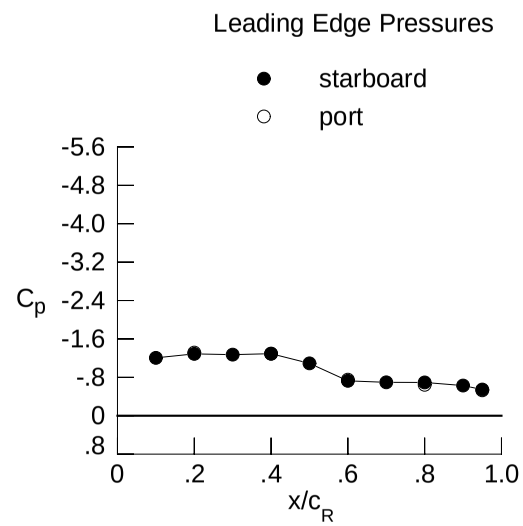

Small Radius L.E.

Run No. = 43 , Point No. = 922

$C_N$ = 1.144, $C_m$ = -0.1806

$\alpha$ = 26.7 °, $M_\infty$ = 0.900

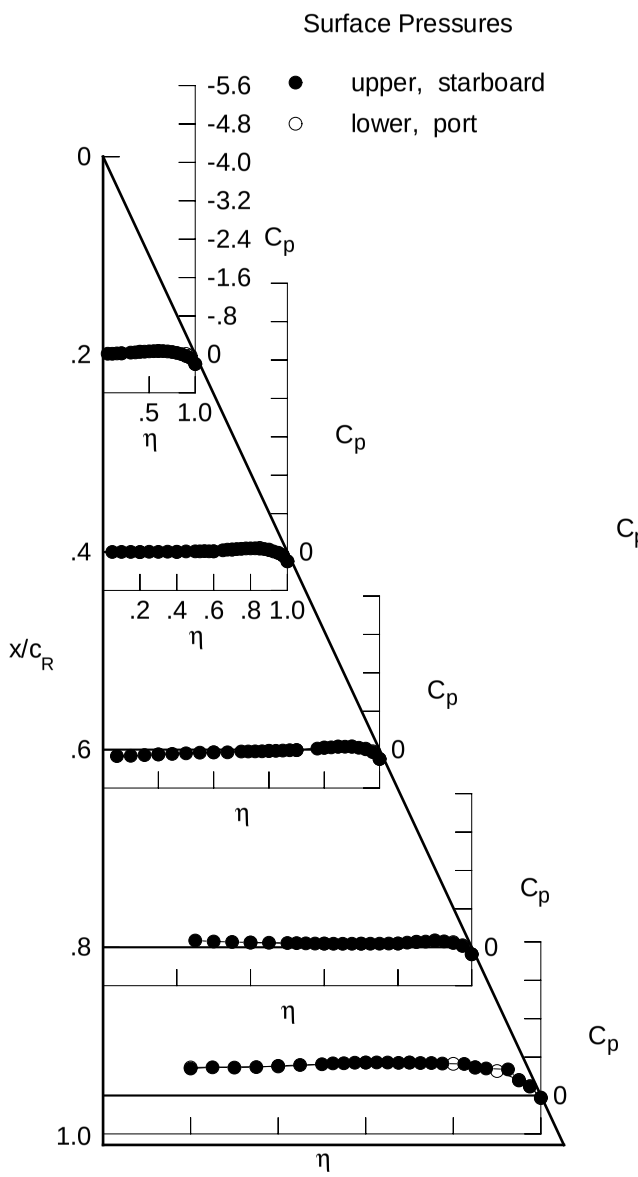
$R_{mac}$ = $5.9 \times 10^6$




| x/c_R | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | -1.2057 | ******* |
| 0.20 | -1.2885 | -1.3155 |
| 0.30 | -1.2725 | ******* |
| 0.40 | -1.2927 | -1.2921 |
| 0.50 | -1.0910 | ******* |
| 0.60 | -0.7268 | -0.7515 |
| 0.70 | -0.6958 | ******* |
| 0.80 | -0.6934 | -0.6450 |
| 0.90 | -0.6284 | ******* |
| 0.95 | -0.5456 | -0.5294 |

# Table D6. Concluded.

| η | $x/c_R$ .2 $C_{p,u}$ | $x/c_R$ .4 $C_{p,u}$ | $x/c_R$ .6 $C_{p,u}$ | $x/c_R$ .8 $C_{p,u}$ | $x/c_R$ .95 $C_{p,u}$ |
|---|---|---|---|---|---|
| 0.050 | -0.0133 | -0.0015 | 0.1345 | ******* | ******* |
| 0.100 | -0.0129 | -0.0020 | 0.1277 | ******* | ******* |
| 0.150 | -0.0199 | -0.0025 | 0.1138 | ******* | ******* |
| 0.200 | -0.0244 | -0.0002 | 0.1002 | ******* | -0.5627 |
| 0.250 | ******* | -0.0052 | 0.0890 | -0.1410 | -0.5871 |
| 0.300 | -0.0371 | -0.0031 | 0.0767 | -0.1198 | -0.5819 |
| 0.350 | -0.0416 | -0.0072 | 0.0631 | -0.1111 | -0.5917 |
| 0.400 | -0.0569 | -0.0068 | 0.0581 | -0.0992 | -0.6177 |
| 0.450 | -0.0561 | -0.0127 | 0.0558 | -0.0942 | -0.6361 |
| 0.500 | -0.0629 | -0.0141 | 0.0389 | -0.0890 | -0.6512 |
| 0.525 | ******* | -0.0142 | 0.0382 | -0.0865 | -0.6696 |
| 0.550 | -0.0669 | -0.0191 | 0.0362 | -0.0812 | -0.6722 |
| 0.575 | ******* | -0.0155 | 0.0342 | -0.0777 | -0.6832 |
| 0.600 | -0.0699 | -0.0154 | 0.0285 | -0.0782 | -0.6859 |
| 0.625 | ******* | ******* | 0.0249 | -0.0733 | -0.6890 |
| 0.650 | -0.0684 | -0.0361 | 0.0195 | -0.0730 | -0.6873 |
| 0.675 | ******* | -0.0493 | 0.0124 | -0.0737 | -0.6799 |
| 0.700 | -0.0613 | -0.0534 | 0.0101 | -0.0760 | -0.6873 |
| 0.725 | ******* | -0.0618 | ******* | -0.0745 | -0.6768 |
| 0.750 | -0.0500 | -0.0661 | ******* | -0.0755 | -0.6771 |
| 0.775 | ******* | -0.0750 | -0.0219 | -0.0778 | -0.6654 |
| 0.800 | -0.0300 | -0.0762 | -0.0364 | -0.0772 | ******* |
| 0.825 | ******* | -0.0779 | -0.0472 | -0.0967 | -0.6573 |
| 0.850 | -0.0056 | -0.0708 | -0.0588 | -0.1107 | -0.5913 |
| 0.875 | ******* | -0.0620 | -0.0611 | -0.1185 | -0.5629 |
| 0.900 | 0.0342 | -0.0406 | -0.0581 | -0.1332 | ******* |
| 0.925 | ******* | -0.0120 | -0.0391 | -0.1233 | -0.5443 |
| 0.950 | 0.0769 | 0.0193 | -0.0081 | -0.0900 | -0.3136 |
| 0.975 | ******* | 0.0713 | 0.0509 | -0.0280 | -0.1858 |
| 1.000 | 0.2001 | 0.1932 | 0.1954 | 0.1451 | 0.0425 |
| | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ | $C_{p,l}$ |
| -0.200 | -0.0197 | 0.0022 | 0.0993 | ******* | -0.5848 |
| -0.400 | -0.0527 | 0.0000 | 0.0541 | -0.0975 | -0.6055 |
| -0.600 | -0.0719 | -0.0146 | 0.0230 | -0.0749 | -0.6873 |
| -0.700 | ******* | -0.0498 | 0.0087 | -0.0746 | -0.6859 |
| -0.800 | ******* | ******* | -0.0456 | -0.0804 | -0.6603 |
| -0.850 | ******* | -0.0863 | -0.0665 | -0.1156 | -0.5782 |
| -0.900 | -0.0087 | -0.0508 | -0.0693 | -0.1448 | -0.5095 |
| -0.950 | 0.0227 | 0.0154 | -0.0203 | -0.1074 | -0.3245 |
| -0.975 | ******* | 0.0648 | 0.0337 | -0.0428 | -0.1957 |
| -1.000 | 0.2012 | 0.1917 | 0.1928 | 0.1467 | 0.0540 |



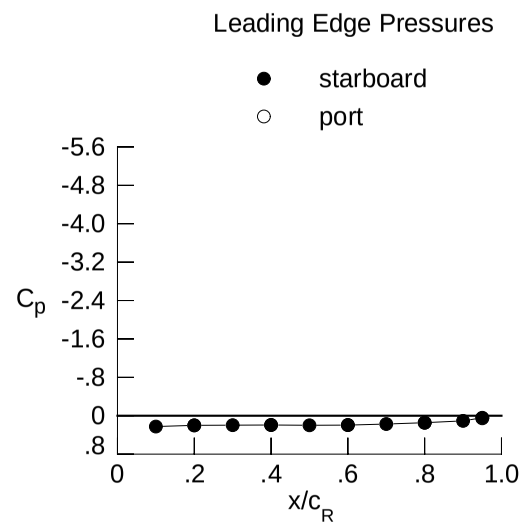

Small Radius L.E.

Run No. = 43 , Point No. = 924

$C_N$ = -0.014, $C_m$ = 0.0054

$\alpha$ = 0.1 °, $M_\infty$ = 0.898

$R_{mac}$ = $6.0 \times 10^6$




| $x/c_R$ | starb'd $C_p$ | port $C_p$ |
|---|---|---|
| 0.10 | 0.2254 | ******* |
| 0.20 | 0.2001 | 0.2012 |
| 0.30 | 0.1967 | ******* |
| 0.40 | 0.1932 | 0.1917 |
| 0.50 | 0.1989 | ******* |
| 0.60 | 0.1954 | 0.1928 |
| 0.70 | 0.1731 | ******* |
| 0.80 | 0.1451 | 0.1467 |
| 0.90 | 0.1069 | ******* |
| 0.95 | 0.0425 | 0.0540 |